

**FINAL GENERIC ENVIRONMENTAL IMPACT STATEMENT (FGEIS)  
DOLSONTOWN CORRIDOR  
Town of Wawayanda, Orange County, New York**

**Lead Agency:** Planning Board, Town of Wawayanda

**Lead Agency Contact:** John Razzano, Chairperson  
80 Ridgebury Hill Road  
Slate Hill, NY 10973  
(845) 355-5700

**APPENDIX A:  
DEWPOINT SOUTH, RDM #3**

**FINAL GENERIC ENVIRONMENTAL IMPACT STATEMENT (FGEIS)  
DOLSONTOWN CORRIDOR**

**APPENDIX A: DEWPOINT SOUTH, RDM #3**

**Table of Contents**

**Letter from NYS Parks, Recreation, and Historic Preservation Letter..... Section 1**

**Threatened and Endangered Species Habitat Suitability Assessment Report ..... Section 2**

**Stormwater Pollution Prevention Plan (SWPPP) ..... Section 3**

**Phase 1A/1B Archaeological Assessment..... Section 4**

**Noise Evaluation..... Section 5**

**Preliminary Site Plans ..... Section 6**

**Environmental Assessment Form Narrative..... Section 7**



## Section 1



**Parks, Recreation,  
and Historic Preservation**

**KATHY HOCHUL**  
Governor

**ERIK KULLESEID**  
Commissioner

December 30, 2021

Sean Brady  
Landscape Architect  
Colliers Engineering & Design  
555 Hudson Valley Avenue Suite 101  
New Windsor, NY 12553

Re: USACE  
Dewpoint South: Warehouse Construction  
Town of Wawayanda, Orange County, NY  
21PR03137

Dear Sean Brady:

Thank you for requesting the comments of the New York State Historic Preservation Office (SHPO). We have reviewed the provided documentation in accordance with Section 106 of the National Historic Preservation Act of 1966. These comments are those of the SHPO and relate only to Historic/Cultural resources. They do not include other environmental impacts to New York State Parkland that may be involved in or near your project. Such impacts must be considered as part of the environmental review of the project pursuant to the National Environmental Policy Act and/or the State Environmental Quality Review Act (New York Environmental Conservation Law Article 8).

SHPO has reviewed the Phase IA/IB Archaeological Survey report entitled "Phase IA Literature Search and Sensitivity Assessment, Phase IB Archaeological Field Reconnaissance Survey, Dewpoint South: Warehouse Construction Project, 1030 Dolsontown Road, Wawayanda, Orange County, New York" prepared by Hudson Valley Cultural Resource Consultants, Ltd. (November 2021; 21SR67692). No archaeological sites were identified by the survey. Therefore, it is the opinion of the New York SHPO that no historic properties, including archaeological and/or historic resources, will be affected by this undertaking.

If you have any questions, I can be reached at [Jessica.Schreyer@parks.ny.gov](mailto:Jessica.Schreyer@parks.ny.gov).

Sincerely,

Jessica Schreyer  
Scientist Archaeology

## Section 2

*Threatened and Endangered Species  
Habitat Suitability Assessment Report*

Dewpoint South Site  
Dolsontown Road  
Town of Wawayanda, New York

November 24, 2021

Prepared by:

Michael Nowicki  
Ecological Solutions, LLC  
121 Leon Stocker Drive  
Stratton, VT 05360  
(203) 910-4716

**1.0 INTRODUCTION ..... 3**  
    TABLE 1 COVER TYPES IDENTIFIED ON THE SITE ..... 3

**2.0 HABITAT SUITABILITY ASSESSMENT/CONCLUSION ..... 4**

**2.1 Small whorled pogonia ..... 4**

**2.2 Indiana and Northern long-eared bats ..... 4**

**2.3 Monarch butterfly ..... 5**

**3.0 PHOTOGRAPHS ..... 6**  
    Figure 1 Location Map ..... 8  
    Attachment 1 - NYSDEC Mapper ..... 9  
    Attachment 2 - USFWS List ..... 10

## 1.0 INTRODUCTION

Ecological Solutions, LLC completed a threatened and endangered species habitat suitability assessment on the Dewpoint South site (4-1-50.32) located on Dolsontown Road in the Town of Waywayanda, Orange County, New York (Figure 1). The site totals 11.66 acres of vacant wooded land. The Applicant is proposing to construct a 125,000 sq. ft. warehouse with associated improvements including access road, parking areas, and stormwater management.

The New York State Department of Environmental Conservation (NYSDEC) Environmental Assessment Form indicates that the Indiana bat (*Myotis sodalis*) may be located in the vicinity of the site. The US Fish and Wildlife Service (USFWS) also lists the Northern long-eared bat (*Myotis septentrionalis*) and small whorled pogonia (*Isotria medeoloides*) as threatened and endangered species potentially located on the site and monarch butterfly (*Danaus plexippus*) as a candidate species that also is potentially located on the site (Attachments 1 and 2). This assessment was completed to determine if suitable habitat exists on the site for these species and determine potential impacts to suitable habitat and recommends measures to mitigate the impacts that can not be avoided or minimized. Habitat was observed on the site on November 20, 2021 and is listed in Table 1.

**TABLE 1  
 COVER TYPES IDENTIFIED ON THE SITE**

<u>HABITAT COVER TYPES</u>			
NO.	DESCRIPTION	COVERAGE (ACRES)	DISTURBANCE (ACRES)
1	Wetlands	2.3	0.01
2	Upland Forest	9.2	8.7
3	Developed Area	0.2	0.2

Upland Hardwood Forest - The site contains upland hardwood forest which is a young forest type with soils that are well drained. The canopy is dominated by a mixture of oaks and maples. The oaks include one or more of the following: black oak (*Quercus velutina*), red oak (*Q. rubra*), and white oak (*Q. alba*), red maple (*Acer rubrum*), American beech (*Fagus grandifolia*), and black cherry (*Prunus serotina*) are common associates occurring at low densities. Sizes of the trees vary from saplings to mature trees with a wide range of dbh from 3--6 inches and tree conditions including dead wood, crevices, and holes.

Wetlands - Wetlands on the site are Federal regulated forested wetlands dominated by red maple swamp species.

## 2.0 HABITAT SUITABILITY ASSESSMENT/CONCLUSION

### 2.1 Small whorled pogonia

The small whorled pogonia is a member of the orchid family. It usually has a single grayish-green stem that grows about 10 inches tall when in flower and about 14 inches when bearing fruit. The plant is named for the whorl of five or six leaves near the top of the stem and beneath the flower. The leaves are grayish-green, somewhat oblong and 1 to 3.5 inches long. The single or paired greenish-yellow flowers are about 0.5 to 1 inch long and appear in May or June. The fruit, an upright ellipsoid capsule, appears later in the year. This orchid grows in older hardwood stands of beech, birch, maple, oak, and hickory that have an open understory. Sometimes it grows in stands of softwoods such as hemlock. It prefers acidic soils with a thick layer of dead leaves, often on slopes near small streams.

**Conclusion** - There is no potential habitat for this species since there is no older growth forest on the site but rather young woods with a thick dense understory.

### 2.2 Indiana and Northern long-eared bats

The Indiana bat typically hibernates in caves/mines in the winter and roosts under bark or in tree crevices in the spring, summer, and fall. Suitable potential summer roosting habitat is characterized by trees (dead, dying, or alive) or snags with exfoliating or defoliating bark, or containing cracks or crevices that could potentially be used by Indiana bats as a roost. The minimum diameter of roost trees observed to date is 2.5 inches for males and 4.3 inches for females. However, maternity colonies generally use trees greater than or equal to 9 inches dbh. Overall, roost tree structure appears to be more important to Indiana bats than a particular tree species or habitat type. Females appear to be more habitat specific than males presumably because of the warmer temperature requirements associated with gestation and rearing of young. As a result, they are generally found at lower elevations than males may be found. Roosts are warmed by direct exposure to solar radiation, thus trees exposed to extended periods of direct sunlight are preferred over those in shaded areas. However, shaded roosts may be preferred in very hot conditions. As larger trees afford a greater thermal mass for heat retention, they appear to be preferred over smaller trees.

Streams associated with floodplain forests, and impounded water bodies (ponds, wetlands, reservoirs, etc.) where abundant supplies of flying insects are likely found provide preferred foraging habitat for Indiana bats, some of which may fly up to 2-5 miles from upland roosts on a regular basis. Indiana bats also forage within the canopy of upland forests, over clearings with early successional vegetation (e.g., old fields), along the borders of croplands, along wooded fencerows, and over farm ponds in pastures. While Indiana bats appear to forage in a wide variety of habitats, they seem to tend to stay fairly close to tree cover.

The northern long eared bat requires/occupies practically the same habitat niche as the Indiana bat. Impacts to habitat and mitigation would be consistent with the recommendations for the Indiana bat.

**Conclusion** - This proposed project will require about 8.7 acres of tree clearing, grubbing, and earth moving in upland forest area. The disturbance activities will not result in adverse effects to this species since will be removed when bats are not on site between October 1 and March 31 or as approved by the

NYSDEC (Emergence survey/s) outside this clearing timeframe. Generation of dust and noise, potential for changes to surface water quality, and increased lighting on the site may cause an impact to foraging bats but can be mitigated as per below.

The site owner proposes to avoid, minimize, and mitigate for effects by:

- Site lighting will use approved light fixtures that have tops that direct light down to minimize light pollution and not interfere with potential bat foraging activities;
- Implementing soil conservation and dust control best management practices, such as watering dry disturbed soil areas to keep dust down, and using staked, recessed silt fence and anti tracking pads to prevent erosion and sedimentation in surface waters on the site, and;
- Stormwater pond/s will not be maintained with any chemicals that might adversely affect bats or insect populations on which they may feed.

These measures will result in avoiding adverse effects to Indiana and Northern long-eared bats.

### **2.3 Monarch butterfly**

Monarchs, like all other butterflies and moths, go through egg, larval (caterpillar), chrysalis (pupa), and adult stages. Monarch caterpillars ingest milkweed that contains a toxic compound. The presence of this toxin is used by the monarch butterfly as a defense against predators.

In late August, masses of monarch butterflies begin an epic migration stretching thousands of miles from areas across the United States and as far north as Canada (east of the Rocky Mountains) to overwinter in mountaintops of Central Mexico.

**Conclusion** – No milkweed plants occur on the site and the impacts from the project are minor and will not impact this species directly or through the loss of habitat (i.e milkweed plants).



### 3.0 PHOTOGRAPHS

Existing woods on site.

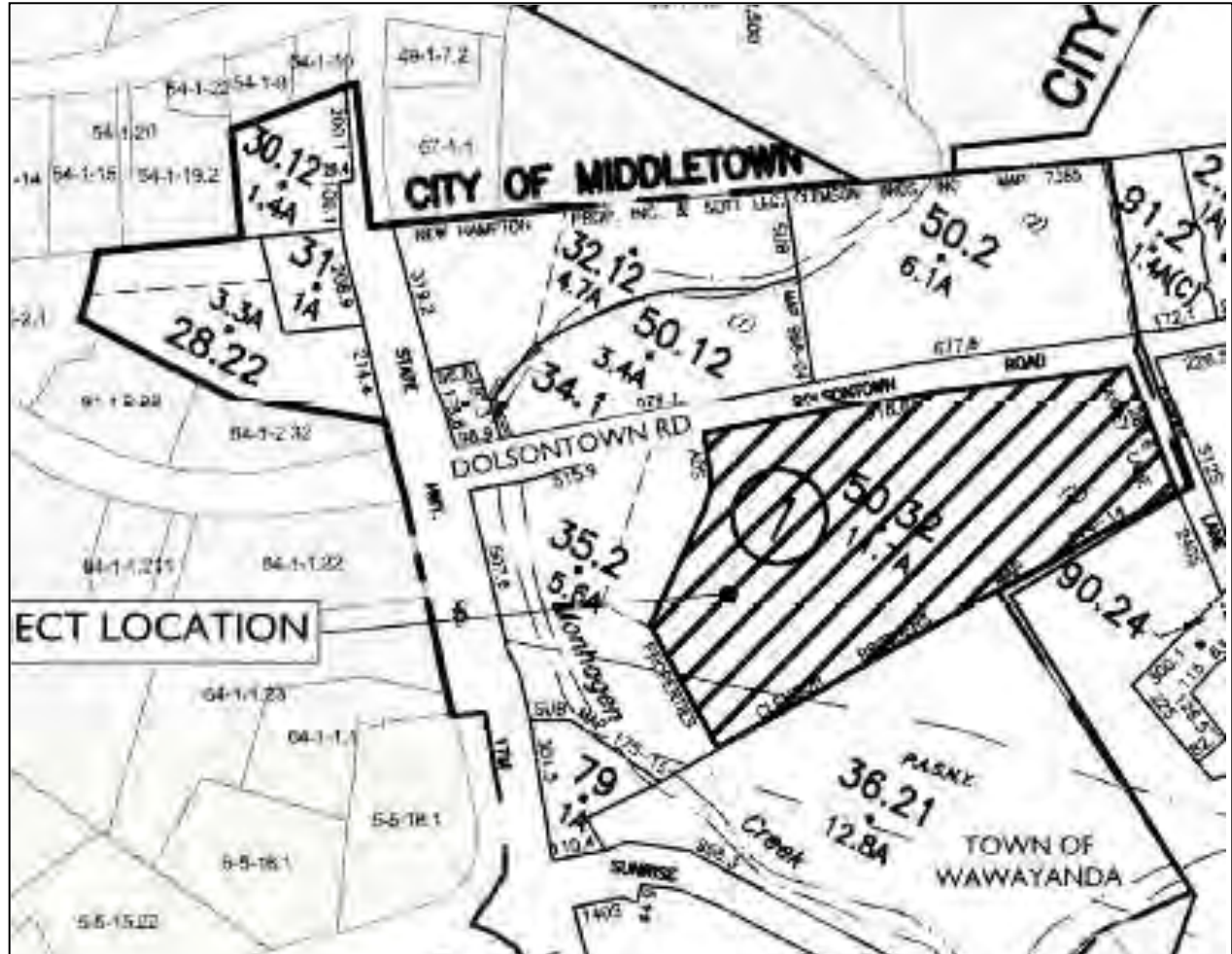


Existing woods on the site.

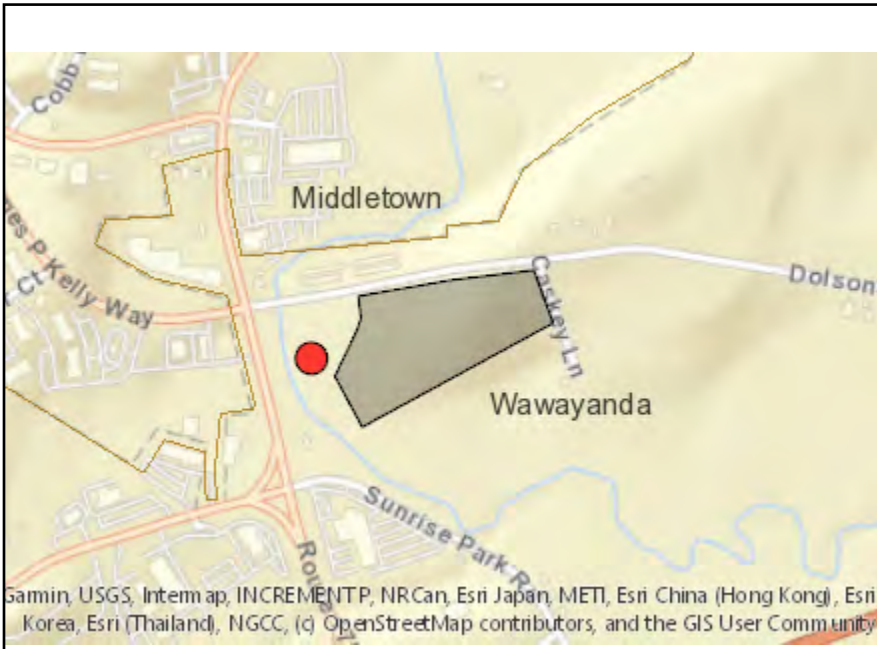




Figure 1 Location Map



## Attachment 1 - NYSDEC Mapper



**Disclaimer:** The EAF Mapper is a screening tool intended to assist project sponsors and reviewing agencies in preparing an environmental assessment form (EAF). Not all questions asked in the EAF are answered by the EAF Mapper. Additional information on any EAF question can be obtained by consulting the EAF Workbooks. Although the EAF Mapper provides the most up-to-date digital data available to DEC, you may also need to contact local or other data sources in order to obtain data not provided by the Mapper. Digital data is not a substitute for agency determinations.



B.i.i [Coastal or Waterfront Area]	No
B.i.ii [Local Waterfront Revitalization Area]	No
C.2.b. [Special Planning District]	Digital mapping data are not available or are incomplete. Refer to EAF Workbook.
E.1.h [DEC Spills or Remediation Site - Potential Contamination History]	Digital mapping data are not available or are incomplete. Refer to EAF Workbook.
E.1.h.i [DEC Spills or Remediation Site - Listed]	Digital mapping data are not available or are incomplete. Refer to EAF Workbook.
E.1.h.i [DEC Spills or Remediation Site - Environmental Site Remediation Database]	Digital mapping data are not available or are incomplete. Refer to EAF Workbook.
E.1.h.iii [Within 2,000' of DEC Remediation Site]	Yes
E.1.h.iii [Within 2,000' of DEC Remediation Site - DEC ID]	V00289, 336029
E.2.g [Unique Geologic Features]	No
E.2.h.i [Surface Water Features]	No
E.2.h.ii [Surface Water Features]	Yes
E.2.h.iii [Surface Water Features]	Yes - Digital mapping information on local and federal wetlands and waterbodies is known to be incomplete. Refer to EAF Workbook.
E.2.h.v [Impaired Water Bodies]	No
E.2.i. [Floodway]	No
E.2.j. [100 Year Floodplain]	No
E.2.k. [500 Year Floodplain]	No
E.2.l. [Aquifers]	No
E.2.n. [Natural Communities]	No
E.2.o. [Endangered or Threatened Species]	Yes

E.2.o. [Endangered or Threatened Species - Name]	Indiana Bat
E.2.p. [Rare Plants or Animals]	No
E.3.a. [Agricultural District]	Yes
E.3.a. [Agricultural District]	ORAN002
E.3.c. [National Natural Landmark]	No
E.3.d [Critical Environmental Area]	No
E.3.e. [National or State Register of Historic Places or State Eligible Sites]	Digital mapping data are not available or are incomplete. Refer to EAF Workbook.
E.3.f. [Archeological Sites]	Yes
E.3.i. [Designated River Corridor]	No

## Attachment 2 - USFWS List



## United States Department of the Interior



FISH AND WILDLIFE SERVICE  
New York Ecological Services Field Office  
3817 Luker Road  
Cortland, NY 13045-9385

Phone: (607) 753-9334 Fax: (607) 753-9699

<http://www.fws.gov/northeast/nyfo/es/section7.htm>

In Reply Refer To:

November 15, 2021

Consultation Code: 05E1NY00-2022-SLI-0455

Event Code: 05E1NY00-2022-E-01825

Project Name: Dewpoint South

Subject: List of threatened and endangered species that may occur in your proposed project location or may be affected by your proposed project

To Whom It May Concern:

The enclosed species list identifies threatened, endangered, proposed and candidate species, as well as proposed and final designated critical habitat, that may occur within the boundary of your proposed project and/or may be affected by your proposed project. The species list fulfills the requirements of the U.S. Fish and Wildlife Service (Service) under section 7(c) of the Endangered Species Act (ESA) of 1973, as amended (16 U.S.C. 1531 *et seq.*). This list can also be used to determine whether listed species may be present for projects without federal agency involvement. New information based on updated surveys, changes in the abundance and distribution of species, changed habitat conditions, or other factors could change this list.

Please feel free to contact us if you need more current information or assistance regarding the potential impacts to federally proposed, listed, and candidate species and federally designated and proposed critical habitat. Please note that under 50 CFR 402.12(e) of the regulations implementing section 7 of the ESA, the accuracy of this species list should be verified after 90 days. This verification can be completed formally or informally as desired. The Service recommends that verification be completed by visiting the ECOS-IPaC site at regular intervals during project planning and implementation for updates to species lists and information. An updated list may be requested through the ECOS-IPaC system by completing the same process used to receive the enclosed list. If listed, proposed, or candidate species were identified as potentially occurring in the project area, coordination with our office is encouraged. Information on the steps involved with assessing potential impacts from projects can be found at: <http://www.fws.gov/northeast/nyfo/es/section7.htm>

Please be aware that bald and golden eagles are protected under the Bald and Golden Eagle Protection Act (16 U.S.C. 668 *et seq.*), and projects affecting these species may require development of an eagle conservation plan ([http://www.fws.gov/windenergy/eagle\\_guidance.html](http://www.fws.gov/windenergy/eagle_guidance.html)). Additionally, wind energy projects should follow the Services wind



energy guidelines (<http://www.fws.gov/windenergy/>) for minimizing impacts to migratory birds and bats.

Guidance for minimizing impacts to migratory birds for projects including communications towers (e.g., cellular, digital television, radio, and emergency broadcast) can be found at: <http://www.fws.gov/migratorybirds/CurrentBirdIssues/Hazards/towers/towers.htm>; <http://www.towerkill.com>; and <http://www.fws.gov/migratorybirds/CurrentBirdIssues/Hazards/towers/comtow.html>.

We appreciate your concern for threatened and endangered species. The Service encourages Federal agencies to include conservation of threatened and endangered species into their project planning to further the purposes of the ESA. Please include the Consultation Tracking Number in the header of this letter with any request for consultation or correspondence about your project that you submit to our office.

Attachment(s):

- Official Species List

## Official Species List

This list is provided pursuant to Section 7 of the Endangered Species Act, and fulfills the requirement for Federal agencies to "request of the Secretary of the Interior information whether any species which is listed or proposed to be listed may be present in the area of a proposed action".

This species list is provided by:

**New York Ecological Services Field Office**

3817 Luker Road

Cortland, NY 13045-9385

(607) 753-9334

---

## Project Summary

Consultation Code: 05E1NY00-2022-SLI-0455

Event Code: Some(05E1NY00-2022-E-01825)

Project Name: Dewpoint South

Project Type: DEVELOPMENT

Project Description: Warehouse development

Project Location:

Approximate location of the project can be viewed in Google Maps: <https://www.google.com/maps/@41.422196,-74.42463578518186,14z>



Counties: Orange County, New York

---

## Endangered Species Act Species

There is a total of 4 threatened, endangered, or candidate species on this species list.

Species on this list should be considered in an effects analysis for your project and could include species that exist in another geographic area. For example, certain fish may appear on the species list because a project could affect downstream species.

IPaC does not display listed species or critical habitats under the sole jurisdiction of NOAA Fisheries<sup>1</sup>, as USFWS does not have the authority to speak on behalf of NOAA and the Department of Commerce.

See the "Critical habitats" section below for those critical habitats that lie wholly or partially within your project area under this office's jurisdiction. Please contact the designated FWS office if you have questions.

1. [NOAA Fisheries](#), also known as the National Marine Fisheries Service (NMFS), is an office of the National Oceanic and Atmospheric Administration within the Department of Commerce.

### Mammals

NAME	STATUS
Indiana Bat <i>Myotis sodalis</i> There is <b>final</b> critical habitat for this species. The location of the critical habitat is not available. Species profile: <a href="https://ecos.fws.gov/ecp/species/5949">https://ecos.fws.gov/ecp/species/5949</a>	Endangered
Northern Long-eared Bat <i>Myotis septentrionalis</i> No critical habitat has been designated for this species. Species profile: <a href="https://ecos.fws.gov/ecp/species/9045">https://ecos.fws.gov/ecp/species/9045</a>	Threatened

### Insects

NAME	STATUS
Monarch Butterfly <i>Danaus plexippus</i> No critical habitat has been designated for this species. Species profile: <a href="https://ecos.fws.gov/ecp/species/9743">https://ecos.fws.gov/ecp/species/9743</a>	Candidate

### Flowering Plants

NAME	STATUS
Small Whorled Pogonia <i>Isotria medeoloides</i> Population: No critical habitat has been designated for this species. Species profile: <a href="https://ecos.fws.gov/ecp/species/1890">https://ecos.fws.gov/ecp/species/1890</a>	Threatened

## **Critical habitats**

THERE ARE NO CRITICAL HABITATS WITHIN YOUR PROJECT AREA UNDER THIS OFFICE'S JURISDICTION.

---

## Section 3



Engineering  
& Design

# Storm Water Pollution Prevention Plan (SWPPP)

February 2022

Revised January 2023

Dewpoint South  
Town of Wawayanda  
SBL: 4-1-50.32  
Orange County, New York

Prepared for:

Dewpoint Development LLC  
1 International Boulevard, Suite 410  
Mahwah, NJ 07430

Prepared by:

**Cory D. Robinson, P.E.**  
New York Professional  
Licensed Professional Engineer  
License No. 103788

**Colliers Engineering & Design**  
555 Hudson Valley Avenue Suite 101  
New Windsor, New York 12553  
Main: 845.564.4495  
Colliersengineering.com

Project No. 20006912A

# Table of Contents

<i>List of Appendices</i> .....	0
<b>I. EXECUTIVE SUMMARY</b> .....	1
<i>Figure 1: Project Location (Source: Google Earth)</i> .....	1
<b>II. INTRODUCTION</b> .....	2
<b>III. STORMWATER MANAGEMENT GOALS</b> .....	3
<b>IV. METHODOLOGY</b> .....	4
<b>V. DISCUSSION</b> .....	5
<i>Discussion of Design Points</i> .....	5
<b>TABLE 1: WATERSHED CHARACTERISTICS</b> .....	5
<b>4.3.3 SOIL BORING AND INFILTRATION TESTING</b> .....	6
<b>ZERO-NET INCREASE:</b> .....	6
<b>TABLE 2: Existing and Proposed Peak Flow Summary to the Design Point</b> .....	7
<b>HOTSPOT RUNOFF</b> .....	7
<b>WATER QUALITY VOLUME (WQV):</b> .....	7
<b>TABLE 3: REQUIRED WATER QUALITY CALCULATION</b> .....	8
<b>RUNOFF REDUCTION VOLUME</b> .....	8
<b>TABLE 4 –RRv Volumes Provided</b> .....	9
<b>RUNOFF REDUCTION VOLUME (RRV) THROUGH SITE PLANNING:</b> .....	9
<b>TABLE 5: GREEN INFRASTRUCTURE SITE PLANNING</b> .....	10
<b>GREEN INFRASTRUCTURE TECHNIQUES (GITS):</b> .....	11
<b>TABLE 6: GREEN INFRASTRUCTURE FEASIBILITY</b> .....	11
<b>BIORETENTION BASINS WITH UNDERDRAIN (NO INFILTRATION):</b> .....	13
<b>SUBSURFACE CHAMBERS:</b> .....	15
<i>Jelly Fish Treatment Box:</i> .....	15
<i>Hydrodynamic Separator (Swirl Chamber):</i> .....	15



*Table 7: Swirl Chamber Sizing Calculations* ..... 17

**VI. EROSION & SEDIMENT CONTROL**..... 17

*303(d) Segments Impaired by Construction related pollutants*..... 18

*Construction Sequencing:* ..... 21

**VII. GOOD HOUSEKEEPING**..... 23

**VIII. RESPONSIBLE PARTIES**..... 25

**IX. END OF PROJECT – TERMINATION OF PERMIT** ..... 26

**X. SUMMARY OF PROPOSED STORMWATER IMPROVEMENTS** ..... 26

**XI. CONCLUSION**..... 26

## List of Appendices

Appendix 1	Watershed Maps
Appendix 2a	HydroCAD Data (Existing Conditions)
Appendix 2b	HydroCAD Data (Proposed Conditions)
Appendix 3	NYSDEC Green Infrastructure Worksheets
Appendix 4	SPDES GP-0-20-001
Appendix 5	Draft Notice of Intent (N.O.I.)
Appendix 6	Draft Notice of Termination (N.O.T.)
Appendix 7	Draft MS4 Acceptance Form
Appendix 8	NRCS Hydrologic Soil Mapping
Appendix 9	Construction Site Log Book (Bluebook Appendix H)
Appendix 10	NYSDEC Construction Stormwater Inspection Manual
Appendix 11	Blank Contractor Certification Form
Appendix 12	NYSDEC Deep-Ripping & Decompaction Manual
Appendix 13	NRCC Precipitation Tables
Appendix 14	Operation and Maintenance Plan
Appendix 15	ADS Stormtech Subsurface Chamber Information
Appendix 16	Hydro International First Defense Swirl Chamber Information
Appendix 17	Geotechnical Investigation Report & Infiltration Results by Kevin L. Patton, P.E.
Appendix 18	Erosion and Sediment Control Plan and Details

# I. EXECUTIVE SUMMARY

<b>Project Name:</b>	<b>Operator Name and Address:</b>
Dewpoint South Town of Wawayanda Orange County, NY	Dewpoint Development LLC 1 International Boulevard, Suite 410 Mahwah, NJ 07430 & GDBP 2171 LLC 2118 61st Street Brooklyn, New York 11204
<b>Project Engineer and Firm:</b>	<b>Contractor Name and Address:</b>
Cory D. Robinson, P.E. Colliers Engineering & Design CT, P.C. 555 Hudson Valley Avenue, Suite 101 New Windsor, NY 12553 (845) 564-4495	TBD
<b>Project Location:</b>	<b>MS4 Contact:</b>
Dolsontown Road & Caskey Lane SBL: 4-1-50.32 Town of Wawayanda, Orange County, NY	Town of Wawayanda (NYR20A279) 80 Ridgebury Hill Road Slate Hill, NY 10973



**Figure 1: Project Location** (Source: Google Earth)

## II. INTRODUCTION

The existing parcel is approximately 11.66 acres in size, has frontage along Dolsontown Road to the north and frontage along Caskey Lane to the east. The parcel is currently undeveloped with a mixture of woodlands and wetlands. The site contains approximately 2.24 acres of Federal Wetlands. As part of the project, a minor amount of wetland disturbance is proposed. The applicant will submit a Preconstruction Notification to the Army Corps of Engineers for confirmation on jurisdiction and permission of filling. The parcel is within the Town's Sanitary Sewer District #1 and Water District #1. The project is within the Town of Wawayanda MC-1 (Mixed Commercial) zoning district.

The proposed project will consist of construction of a 125,000 square foot warehouse/distribution facility. Other associated site improvements include 65 vehicle parking spaces & 37 loading docks. The lot has a proposed driveway entrance on Dolsontown Road for vehicular and truck access to the facility, and a proposed emergency access driveway to Caskey Lane. A lot line adjustment is also proposed as part of this project which will dedicate approx. 3,185 sq. ft. of the current parcel to the Dolsontown Road Right-of-Way (ROW) and create a minimum 66' wide ROW across the frontage.

Stormwater runoff currently sheet flows from east to the west & south, towards the southern property line and the wetland on site. The proposed condition will convey stormwater via sheet flow across the parking lots, into inlets and pipes, and into a variety of Green Infrastructure techniques, including bioretention ponds and subsurface storage chambers, where the runoff will be treated for Water Quality (WQ) and Runoff Reduction (RRv) before the excess runoff is discharged towards the wetland or the property line. Stormwater 'Hotspot' runoff from truck loading bays and trailer storage/parking areas has been pretreated using oil-water separating swirl chambers prior to any infiltration where applicable. Stormwater facilities on site have been designed in accordance with the 2015 New York State Stormwater Management Design Manual and local requirements.

The site has been analyzed as new development and stormwater practices sized to manage the increase in impervious area. The study area was generally limited to the project site, utilizing the southern property line and nearby wetland, tributary to the Monhagen Brook, as the design point. The proposed improvements will result in the addition of roughly 5.6 acres of impervious area.

Due to the size of the project, coverage under the State Pollutant Discharge Elimination System Permit (SPDES GP 0-20-001) administered by New York State Department of Environmental Conservation (NYSDEC) is required.

Due to the size of the proposed building and associated earthwork/site improvements, the project will disturb more than 5 acres of soil at one time, therefore the applicant will be seeking a waiver from the MS4 to create more than 5 acres of soil disturbance at one time. Phasing the project to limit the disturbance below 5 acres is not practical due to the size of the building and the existing topography. Enhanced erosion control measures have been included on the plans and later in this report to mitigate this additional soil disturbance and ensure compliance with the permit requirements.

## III. STORMWATER MANAGEMENT GOALS

### GOALS

This Stormwater Pollution Prevention Plan (SWPPP) has been prepared in compliance with the New York State Department of Environmental Conservation (NYSDEC) State Pollutant Discharge Elimination System (SPDES) General Permit for Stormwater Discharges from Construction Activity, Permit No. GP-0-20-001 (See Appendix 4). The SWPPP is a plan for controlling runoff and pollutants from a site during and after construction activities. The principle objective of this document is to comply with the SPDES Permit for construction activities by planning and implementing the following practices:

- Reduction or elimination of erosion and sediment loading to water bodies during and after construction.
- Control of the impact of stormwater runoff on the water quality of the receiving waters.
- Control of the peak rate of runoff during and after construction.
- Maintenance of stormwater controls during and after completion of construction.
- Minimize impacts to the Monhagen Brook, which is on the NYSDEC's 303(d) list as an impaired water.

### CLASSIFICATION & STANDARDS

The activities associated with this project are eligible for coverage under this permit. Using the General Permit guidelines for coverage, a summary of classification and requirements is provided below:

Project Type:

- Commercial development and redevelopment.
- Parking lot construction and reconstruction.
- All other construction activities that include the construction or reconstruction of impervious area or alter the hydrology from pre to post development conditions and are not listed in Table 1 of GP-0-20-001.

**Classification: GP-0-20-001 Appendix B, Table 2 - "Construction activities that require the preparation of a SWPPP that includes Post Construction Stormwater Practices".**

This project is located within the Town of Wawayanda regulated, traditional land use control Municipal Separate Stormwater Sewer System (MS4). The following guidance documents, in addition to various resources located on the NYS Department of Environmental Conservation website, were used in preparation of this SWPPP.

The New York State Stormwater Management Design Manual, by New York State Department of Environmental Conservation, August 2015 (NYSSMDM).

New York Standard Specifications for Erosion and Sediment Control, by New York State Department of Environmental Conservation, November 2016 ("Blue Book").

The SWPPP is intended to be a *living* document and should be revised and updated whenever site conditions dictate. Any proposed modifications shall be reviewed by the owner/operator prior to incorporation in the SWPPP and implementation at the project site. The certifying engineer of this SWPPP document shall be notified of any proposed modifications to this document. Any proposed modifications shall be in accordance with the NYSDEC technical standards.

## IV. METHODOLOGY

1. The watersheds are divided into subareas, by topography, soils, and land use. A summary of the watershed areas, composite curve numbers, and travel times are shown in Table 1 below.
2. Rainfall depths used for this analysis are those published by the Northeast Regional Climate Center for the project location for the 100, 10, and 1-year frequency storms as directed in the NYSSMDM.
3. Boundary & Topographical mapping is taken from a survey titled “Outbound & Topographic Survey Plan Prepared for Dolsontown Road Section 4 Block 1 Lot 50.32” prepared by John W. McCord, Sr. PLS (License #050904) revised 09/01/2021.
4. The required water quality volume (WQv) was calculated in accordance with the Section 4.2 of the NYSSMDM. This is also the required RRv as per Section 4.3 of the NYSSMDM.
5. The provided RRv was calculated through the use of the Green Infrastructure (GI) Worksheets, Version 1.6, provided by NYSDEC. The GI worksheets are included in Appendix 3.
6. The peak flows from the watersheds in the existing condition are computed using the runoff curve numbers taken from TR-55 to determine undeveloped peak runoff and runoff hydrographs at the design points. The existing condition peak flows are presented in the report.
7. In the post-development condition, the peak flows from the proposed development are computed using the runoff curve numbers taken from TR-55. The watersheds are adjusted for the proposed improvements and grading of the site. The runoff flows are hydraulically routed for updated travel times, diversions, and new storage structures, as necessary. The resulting proposed peak flows at the design point are presented in the report.
8. A full Erosion & Sediment Control Plan (plans, details and construction sequencing) was designed in accordance with the New York State Standards and Specifications for Erosion and Sediment Control (aka the “bluebook”) and has been included as an appendix of this report.
9. A long term Operation & Maintenance Plan was developed for the proposed post-construction stormwater control practices and is included as an appendix of this report.
10. Maps indicating the various drainage conditions are enclosed in the appendices of this report. Schematic diagrams of the flow models in the existing and proposed conditions are included in the HydroCAD output within the Appendix.
11. A draft MS4 SWPPP Acceptance form, Notice of Termination (NOT), and Notice of Intent (NOI) have been included in the Appendix of this report to be executed as part of the SPDES permit. The MS4 form is to be completed by the municipality at the time of SWPPP acceptance and replaced in this report with the executed version. The NOI shall be filed electronically with the NYSDEC at the time of permit activation and replaced in this report with the executed version. The NOT is to be completed and filed with the municipality and NYSDEC at the time of permit closure. .

## V. DISCUSSION

### Discussion of Design Points

The Project has one design point, the southern property line where the existing runoff sheet flows towards and the wetland also discharges towards. The drainage areas were limited, wherever possible to the area of proposed development.

The design points evaluated in this report is described as follows:

Design Point 1 is the southern property line of the parcel. The site runoff generally sheets from the east towards the southern property line or from east to west into the ACOE wetland which drains towards the southern property line.

The Design Point location, the pre- and post-development land use, travel times flow paths, and watersheds are clearly identified on the watershed maps found in the Appendix of this report. The pre-development (hereafter “existing”) and post-development (hereafter “proposed”) watershed characteristics can be found in Table 1 below.

**TABLE 1: WATERSHED CHARACTERISTICS**

<b>Existing Conditions</b>			
	<b>Area (acres)</b>	<b>CN</b>	<b>Tc (minutes)</b>
EW1	11.66	78	34.7
<b>Totals</b>	11.66	78	-
<b>Proposed Conditions</b>			
	<b>Area (acres)</b>	<b>CN</b>	<b>Tc</b>
PW1A	4.17	78	34.7
PW1BN	1.57	91	6.0
PW1BS	1.44	98	6.0
PW1C	0.61	96	6.0
PW1D	0.91	88	6.0
PW1E	0.84	92	6.0
PW1F	0.42	93	6.0
PW1G	1.16	97	6.0
PW1H	0.54	98	6.0



<b>Totals</b>	11.66	88	-
---------------	-------	----	---

The minimum Tc of 6 minutes, or 0.10 hours, is shown above for the catchment areas where the composite travel time did not meet this minimum. Watersheds with a Tc greater than the minimum have been identified with the travel path on the watershed maps in the Appendix.

**SOIL TYPES**

Soil data for this project was obtained from the USDA Natural Resources Conservation Service Web Soil Survey (NRCS WSS). A copy of the report generated for the site can be found in the Appendix of this report.

Several different soil designations are identified throughout the entire project. A further detailed description of the soil characteristics and properties can be found in the NRCS WSS included as an Appendix to this report.

**HYDROLOGIC SOIL GROUP (HSG)**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long duration storms. The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). Dual class soil groups are conservatively considered “D” soils.

All of the soils existing on site have been identified through the NRCS WSS as HSG ‘D’ Soils.

**4.3.3 SOIL BORING AND INFILTRATION TESTING**

Project specific geotechnical testing has been performed by others and the geotechnical report has been included as an appendix to this report. Site specific stormwater infiltration testing was also performed under this scope, by others, and a summary of the results has been included in the appendix with the geotechnical report. The presence of shallow groundwater around the site prohibits the use of infiltration practices.

**ZERO-NET INCREASE:**

The proposed storm water improvements for the site provide the required channel protection (CPv), overbank flood protection (Qp), and extreme flood protection (Qf). Peak flows have been reduced at the selected design point in the proposed condition for the 100, 10, and 1-year storms. These peak flow reductions can also be found in Table 2 below.

As is evident in the table below, attenuation of the peak flows by reduction of impervious areas in the redeveloped areas, utilization of SMP’s with RRv capacity, and site planning, have effectively reduced the peak discharge while providing the required runoff reduction; which will be further discussed below.



**TABLE 2: Existing and Proposed Peak Flow Summary to the Design Point**

<u>Design Point</u>	<u>Storm Events (yr)</u>	<u>Existing (cfs)</u>	<u>Proposed (cfs)</u>	<u>Diff. (cfs)</u>	<u>Percent</u>
DP1	1	6.03	4.45	-1.58	-26%
	10	17.57	15.77	-1.8	-10%
	100	40.06	39.68	-0.38	-1%

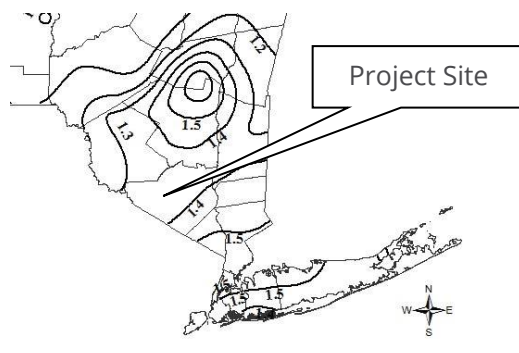
**HOTSPOT RUNOFF**

As defined in section 4.11 of the NYSSWDM, stormwater “hotspots” are land uses and activities that generate higher concentration of hydrocarbons, trace metals or toxicants that are found in typical stormwater runoff. The loading docks and trailer storage/parking areas would fall under the definition of a hotspot.

To meet the design criteria for hot spot runoff, the loading dock runoff pretreatment is provided using either swirl chambers or an ‘isolator row’ and hotspot runoff is then treated using a proprietary treatment device ‘Jelly Fish’ unit which essentially functions as a condensed bioretention area. The trailer storage runoff is pretreated with a swirl chamber and then treatment is provided with a conventional bioretention area.

**WATER QUALITY VOLUME (WQV):**

The Water Quality Volume (WQv) requirement is designed to improve water quality. The WQv is directly related to the impervious cover created at a site. The design captures and treats 90% of the average annual stormwater runoff volume. The 90% rainfall event value (P) used in the calculations (1.4”) is shown below in the portion of Figure 4.1 from Section 4.2, page 4-3 in the NYSSMDM (depicted below).



**90% Rule:**

$$WQ_v = [(P)(R_v)(A)] / 12$$

$$R_v = 0.05 + 0.009(I)$$

I = Impervious Cover (Percent)  
 Minimum R<sub>v</sub> = 0.2  
 P = 90% Rainfall Event Number (See Figure 4.1)  
 A = site area in acres

Using the total impervious area for the project site, both in the existing and proposed condition. The Runoff Coefficient “Rv” in the computation of Water Quality Volume WQv is dependent on the percent impervious cover. As per Section 4.2 of the NYSSMDM, 100% of the water quality volume shall be treated.

**TABLE 3: REQUIRED WATER QUALITY CALCULATION**

Catchment (GI Worksheet numbering)	Description (HydroCAD designation)	90% Rainfall Event Number (P) Inches	Total Area (acres)	Impervious Area (acres)	Percent Impervious (I) %	Runoff Coefficient Rv	Required WQv (cf)	Provided WQv (cf)
1	PW1BN	1.4	1.57	0.93	59%	0.58	4,649	4,649
2	PW1C, PW1D, & PW1H	1.4	2.06	1.48	72%	.70	7,293	7,293
3	PW1E	1.4	0.85	0.58	68%	.66	2,849	2,849
4	PW1F	1.4	0.42	0.29	70%	0.68	1,432	1,432
5	PW1G & PW1BS	1.4	2.60	2.51	97%	0.92	12,140	12,140
<b>TOTAL</b>	-	-	<b>7.49</b>	<b>5.79</b>	<b>77%</b>	<b>0.75</b>	<b>28,362</b>	<b>28,362</b>

The provided WQv for Catchment 5 is provided using a rate based treatment device “Jelly Fish Filter” unit JF-4 produced by Contech and sized appropriately for the WQv storm flow routed to the device.

The current design exceeds the requirement for treating the WQv for the impervious areas of new construction.

**RUNOFF REDUCTION VOLUME**

The runoff reduction volume (RRv) is designed to reduce the stormwater volume leaving the site by capturing an amount equal to the computed water quality volume and infiltrating it onsite. However, for sites that cannot reduce runoff in the amount equal to the water quality volume, a minimum RRv is allowed if the project demonstrates acceptable limitations. The minimum RRv requirement (in acre-feet) was calculated as follows:

$$RRv_{min} = [(P)(\bar{R}v)(S)(Aic)]/12 \text{ where,}$$

I = Percent Impervious Cover (must be 100%)  
P = 90% rainfall event = 1.4  
 $\bar{R}v = 0.05 + [(0.009)(I)] = 0.95$   
S = Hydrologic Soil Group Reduction Factor = 0.20 for HSG D  
Aic = Total Area of new impervious cover (acres) = **5.60**

$$RRv_{min} = \frac{[(P)(\bar{R}v)(S)(Aic)]}{12} = \frac{[(1.4)(0.95)(0.20)(5.60)]}{12} = 0.124 \text{ ac-ft} = \mathbf{5,407 \text{ cf}}$$

Runoff from the development has been treated using bioretention ponds & subsurface infiltration chambers. Within these proposed practices the entire WQv has not been reduced through the use of standard SMPs with RRv capacity. The RRv and for each proposed practice is included in Table 4 below.

**TABLE 4 –RRv Volumes Provided**

Catchment (GI Worksheet numbering)	Description (HydroCAD designation)	RRv Provided (cf)
1	PW1BN	1,891
2	PW1C, PW1D, & PW1H	2,925
3	PW1E	1,294
4	PW1F	593
5	PW1G & PW1BS	0
<b>TOTAL</b>	-	6,703

The proposed design exceeds the minimum requirement by providing an RRv in excess of the minimum amount required and provides >100% of the water quality volume set forth by the NYSDEC requirements. This aspect of the design has been met.

**RUNOFF REDUCTION VOLUME (RRV) THROUGH SITE PLANNING:**

The application of site planning and green infrastructure to reduce water quality volume with runoff reduction practices can either reduce the required water quality volume to be treated or can completely account for the required water quality volume, which is recommended; the summary of this analysis can be found below. The combination of practices provided on site exceeds the minimum required water quality and runoff reduction for the proposed development.

The basic premise of runoff reduction is to recognize the water quality benefits of certain practices by allowing for a reduction in the water quality treatment volume. Runoff reduction is first achieved through better site design during the planning stages and has been implemented in the planning and design of this project as described in this report.

In accordance with Section 5.2 "Planning for Green Infrastructure: Reduction of Impervious Cover" of the NYSDEC Stormwater Management Design Manual, the proposed site plan has been designed to meet the planning techniques as follows:

**TABLE 5: GREEN INFRASTRUCTURE SITE PLANNING**

Preservation of Undisturbed Areas	
Delineate and place into permanent conservation undisturbed forests, native vegetated areas, riparian corridors, wetlands, and natural terrain.	This practice has not been applied to this project.
Preservations of Buffers	
Define, delineate, and preserve naturally vegetated buffers along perennial streams, rivers, shorelines and wetlands.	Existing federally regulated wetland areas exist on site which have been primarily preserved with the exception of a minor disturbance as indicated on the site plans.
Reduction of Clearing & Grading	
Limit clearing and grading to the minimum amount needed for roads, driveways, foundations, utilities and stormwater management facilities.	The development has been limited as much as possible while still meeting the developer's requirements.
Locating Development in Less Sensitive Areas	
Avoid sensitive resource areas such as floodplains, steep slopes, erodible soils, wetlands, mature forests and critical habitats by locating development to fit the terrain in areas that will create the least impact.	Existing federally regulated wetland areas exist on site which have been primarily preserved with the exception of a minor disturbance as indicated on the site plans.
Open Space Design	
Use clustering, conservation design or open space design to reduce impervious cover, preserve more open space and protect water resources.	Not applicable to this project.
Soil Restoration	
Restore the original properties and porosity of the soil by deep till and amendment with compost to reduce the generation of runoff and enhance the runoff reduction performance of post construction practices.	Compacted soils located in open areas without shallow utilities will be tilled in order to restore the original properties of the soil prior to seeding.
Roadway Reduction	
Minimize roadway widths and lengths to reduce site impervious area	Roadway widths were reduced wherever possible while still maintaining the necessary access.
Sidewalk Reduction	
Minimize sidewalk lengths and widths to reduce site impervious area	Sidewalks added where needed to serve the pedestrian needs adequately and safely of the facility.

Driveway Reduction	
Minimize driveway lengths and widths to reduce site impervious area	The proposed driveways have been minimized wherever possible.
Cul-de-Sac Reduction	
Minimize the number of cul-de-sacs and incorporate landscaped areas to reduce their impervious cover.	Not applicable to this project.
Building Footprint Reduction	
Reduce the impervious footprint of residences and commercial buildings by using alternate or taller buildings while maintaining the same floor to area ratio.	The building footprints have been designed to meet the developer's needs.
Parking Reduction	
Reduce imperviousness on parking lots by eliminating unneeded spaces, providing compact car spaces and efficient parking lanes, minimizing stall dimensions, using porous pavement surfaces in overflow parking areas, and using multi-storied parking decks where appropriate.	The site has been developed to meet the developer's needs and the applicable requirements.

GREEN INFRASTRUCTURE TECHNIQUES (GITS):

After taking into account the reductions through Site Planning mentioned above, RRv remains to be treated through GITs and/or Standard SMPs. Chapter 5 of the NYSSMDM outlines the various Green Infrastructure Techniques which can be implemented on-site to achieve runoff reduction. The GI Worksheets included in the Appendix of this report provide the calculations for the green infrastructure techniques chosen to treat the Runoff Reduction Volume for this project. Below is a brief description of each Green Infrastructure Technique along with a discussion regarding the feasibility of each technique with respect to this project.

**TABLE 6: GREEN INFRASTRUCTURE FEASIBILITY**

Conservation of Natural Areas	
Retain the pre-development hydrologic and water quality characteristics of undisturbed natural areas, stream and wetland buffers by restoring and/or permanently conserving these areas on a site.	Existing federally regulated wetland areas exist on site which have been primarily preserved with the exception of a minor disturbance as indicated on the site plans.
Sheetflow to Riparian Buffers or Filter Strips	
Undisturbed natural areas such as forested conservation areas and stream buffers or vegetated	Wetlands remain on site, however these features have not been quantified as stormwater mitigation.

filter strips and riparian buffers can be used to treat and control stormwater runoff from some areas of a development project.	
Vegetated Open Swale	
The natural drainage paths, or properly designed vegetated channels, can be used instead of constructing underground storm sewers or concrete open channels to increase time of concentration, reduce the peak discharge, and provide infiltration.	Overland sheet flow and vegetated swales have been implemented as feasible, however these features have not been quantified as a stormwater mitigation.
Tree Planting/Tree Box	
Plant or conserve trees to reduce stormwater runoff, increase nutrient uptake, and provide bank stabilization. Trees can be used for applications such as landscaping, stormwater management practice areas, conservation areas and erosion and sediment control.	Tree planting has been proposed through the site but has not been quantified as a stormwater mitigation.
Disconnection of Rooftop Runoff	
Direct runoff from residential rooftop areas and upland overland runoff flow to designated pervious areas to reduce runoff volumes and rates.	Not applicable to this project.
Stream Daylighting for Redevelopment Projects	
Stream Daylight previously-culverted/piped streams to restore natural habitats, better attenuate runoff by increasing the storage size, promoting infiltration, and help reduce pollutant loads.	Not applicable to the project.
Rain Garden	
Manage and treat small volumes of stormwater runoff using a conditioned planting soil bed and planting materials to filter runoff stored within a shallow depression.	Rain gardens are not proposed as part of this project since the use of other GITs is more practicable.
Green Roof	
Capture runoff by a layer of vegetation and soil installed on top of a conventional flat or sloped roof. The rooftop vegetation allows evaporation and evapotranspiration processes to reduce volume and discharge rate of runoff entering conveyance system.	Not used.

Stormwater Planter	
Small landscaped stormwater treatment devices that can be designed as infiltration or filtering practices. Stormwater planters use soil infiltration and biogeochemical processes to decrease stormwater quantity and improve quality.	Landscaping in green areas and planted beds are proposed throughout the development, but planters have not been proposed for treatment. No credit has been taken in the SWPPP.
Rain Tank or Cistern	
Capture and store stormwater runoff to be used for irrigation systems or filtered and reused for non-contact activities.	Not used.
Porous Pavement	
Pervious types of pavements that provide an alternative to conventional paved surfaces, designed to infiltrate rainfall through the surface, thereby reducing stormwater runoff from a site and providing some pollutant uptake in the underlying soils.	Porous pavers have not been used in this design.

The bioretention practices & infiltration chambers account for the runoff reduction as required.

Refer to Tables 5 and 6 above for the decision-making matrices utilized herein. The design for the project utilized a standard SMPs with RRV capacity to attain the required runoff reduction volume and water quality for new construction. NYSDEC Green Infrastructure (GI) worksheets can be found in Appendix 3 summarizing the calculations.

**BIORETENTION BASINS WITH UNDERDRAIN (NO INFILTRATION):**

The proposed development implements the use of bioretention with a proposed underdrain (F-5). Runoff from the development is proposed to be routed to a bioretention basin to provide runoff reduction capacity as well as water quality treatment volume. The basins are proposed with a 3” mulch layer, 2.5 feet of soil media, and an 8-inch drainage stone layer with a 6-inch underdrain that connects to an outlet control structure and discharges downstream to attenuate peak flows. Bioretention soils shall meet the design criteria outlined in Appendix H of the NYSSMDM.

The sizing calculation for the bioretention system was completed in accordance with design requirements set forth in Section 6.4.4 of the NYSSMDM. An exception to the design is that grass filter strips have not been provided in all locations for pre-treatment of the sheet flow from the paved areas. Frequent observance of scour and destruction of existing bioretention areas have led the design to include properly sized riprap inlet protection at all curb cuts and proper scour protection for discharging pipes. Although the intent of the design requires grass filter strips, we believe the longevity of the system design and maintenance of the mulch layer and vegetation will adequately treat the runoff from the proposed development and this design alteration will meet the long-term goals of the permit. Hydrodynamic separator swirl chambers (proprietary devices

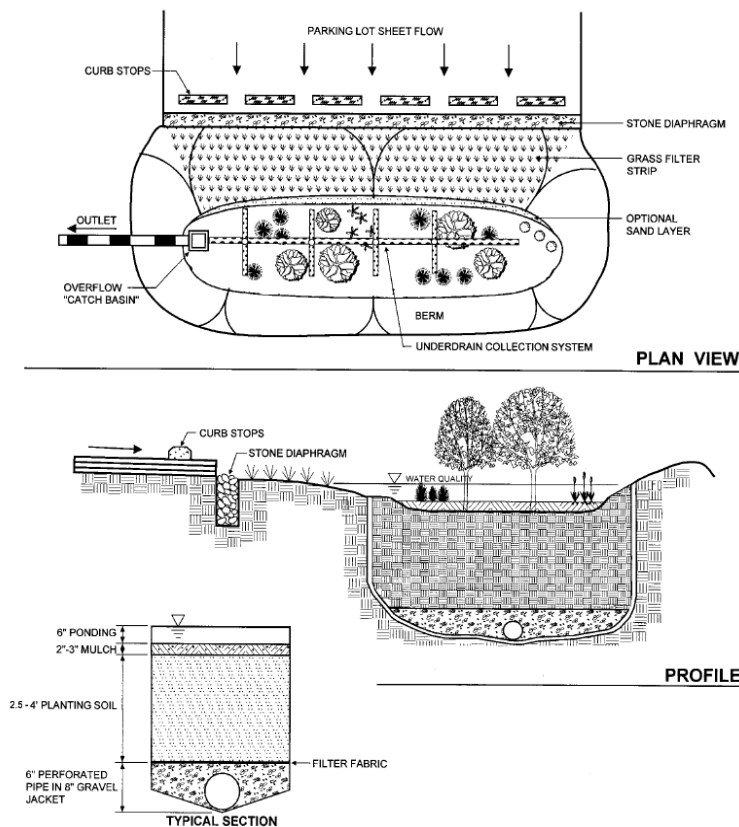
designed as flow-through structures with a settling or separation unit to remove sediment and other pollutants) have also been included as pretreatment and hotspot removal devices.

Bioretention facilities must be carefully constructed following the recommendations in Appendix C of the design manual and preserving the natural porosity of the installed planting soils. Bioretention planting soil must be pre-mixed, stockpiled, lab tested for the necessary parameters, and submitted as a shop drawing for approval prior to installation.

The stage/storage information of the bioretention areas can be found in the HydroCAD output within the Appendix of this report. The NYSDEC GI worksheet for runoff reduction and water quality treatment can be found in the Appendix for RRv capacity calculations (See NYSDEC GI worksheets). A summary of the water quality provided in these facilities can be found in the Tables above.

In addition to the swirl chambers that have been included as pretreatment and hotspot runoff removal devices where practical, bioretention areas accepting hotspot runoff (**BIO-1E**) will also have an impermeable liner to prevent hotspot runoff from infiltration and satisfy the requirements of the permit.

Figure 6.19 Bioretention (F-5)



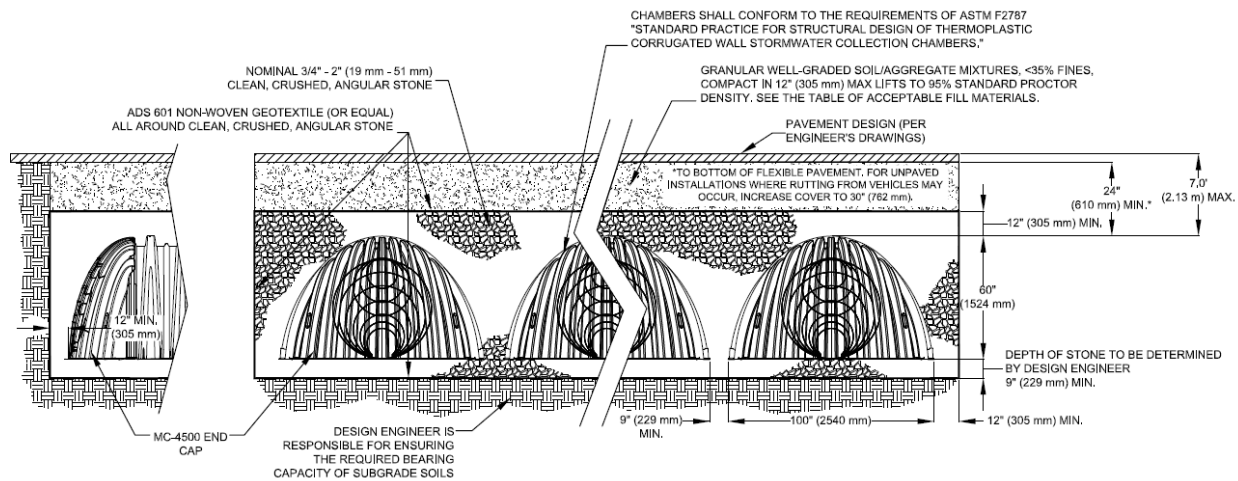


**SUBSURFACE CHAMBERS:**

The StormTech MC-4500 is a resin chamber that allows the storage of large volumes at reasonable subsurface depths. We have designed an underground system, as shown on the site plans. Sizing for the system includes storage capacity to provide storage for peak flow mitigation, and can be found in the HydroCAD output Appendix of this report. The calculations shown include the volume within the chambers and stone voids of 40% per the manufacturer’s recommendations.

**General Cross Section**

\*\*Contact your local StormTech representative or visit [www.stormtech.com](http://www.stormtech.com) for a copy of the latest installation instructions.



To provide pretreatment, an ‘isolator row’ is used as the row of chambers that the site storm drainage system discharges into. This isolator row provides a layer of filter fabric for water entering the system during the more frequent storm pass through prior to entering the stone beneath the chambers.

The chambers will be fitted with an underdrain, and no infiltration capacity has been claimed towards RRv or WQv.

**Jelly Fish Treatment Box:**

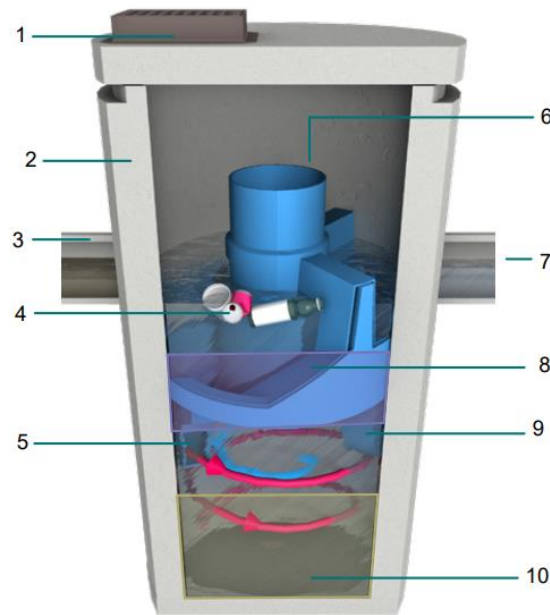
The subsurface storage system discharges to a Contech “Jelly Fish” system in a concrete vault, which provided the required water quality treatment. Sizing of the Jelly Fish system (an alternative stormwater practice) requires the application of a “rate-based” sizing approach for water quality treatment. In the “rate-based” approach, the device should be sized to treat the peak rate of runoff from the WQv storm; utilizing the WQv storm precipitation depth, the peak runoff for each tributary area can then be determined, and the associated devices sized appropriately. Details for the jelly fish system can be found on the site plans.

**Hydrodynamic Separator (Swirl Chamber):**

The applicant proposes to install a hydrodynamic separator to provide water quality pre-treatment and hotspot treatment as part of the “treatment train” upstream of the standard mitigation practices with Runoff reduction capacity. Hydrodynamic separators are devices that move water in a circular, centrifugal manner to accelerate the separation and deposition of primarily sediment from the

water. They are suitable for removal of coarse particles, oils, and fuels over small drainage areas. The NYSDEC refers to the New Jersey Department of Environmental Protection for a list of Stormwater Manufactured Treatment Devices which have received Interim Certification (included in the Appendix). One of the products on the list is the Hydro International First Defense unit.

Sizing of the First Defense system (an alternative stormwater practice), requires the application of a “rate-based” sizing approach for water quality treatment. In the “rate-based” approach, the device should be sized to treat the peak rate of runoff from the WQv storm; utilizing the WQv storm precipitation depth, the peak runoff for each tributary area can then be determined, and the associated devices sized appropriately. HydroCAD was used to determine the water quality flow rate for treatment sizing of the First Defense system. The table below lists the water quality storm event, its associated flowrate for the treatment structure, the tributary catchments, and the appropriately sized First Defense system capacity which provides in excess of the required flow, for the location shown on the plans



### Components

- |   |                               |
|---|-------------------------------|
| 1. Inlet Grate (optional)                     | 6. Internal Bypass            |
| 2. Precast chamber                            | 7. Outlet pipe                |
| 3. Inlet Pipe (optional)                      | 8. Oil and Floatables Storage |
| 4. Floatables Draw Off Slot<br>(not pictured) | 9. Outlet chute               |
| 5. Inlet Chute                                | 10. Sediment Storage Sump     |

**Table 1. First Defense® High Capacity Design Criteria.**

First Defense® High Capacity Model Number	Diameter	Typical TSS Treatment Flow Rates			Peak Online Flow Rate	Maximum Pipe Diameter <sup>1</sup>	Oil Storage Capacity	Typical Sediment Storage Capacity <sup>2</sup>	Minimum Distance from Outlet Invert to Top of Rim <sup>3</sup>	Standard Distance from Outlet Invert to Sump Floor
		NJDEP Certified	106µm	230µm						
	(ft / m)	(cfs / L/s)	(cfs / L/s)	(cfs / L/s)	(cfs / L/s)	(in / mm)	(gal / L)	(yd <sup>3</sup> / m <sup>3</sup> )	(ft / m)	(ft / m)
FD-3HC	3 / 0.9	0.84 / 23.7	0.3 / 8.77	0.53 / 15.0	15 / 424	18 / 457	125 / 473	0.4 / 0.3	2.0 - 3.5 / 0.6 - 1.0	3.71 / 1.13
FD-4HC	4 / 1.2	1.50 / 42.4	0.7 / 20	1.2 / 34	18 / 510	24 / 600	191 / 723	0.7 / 0.5	2.3 - 3.9 / 0.7 - 1.2	4.97 / 1.5
FD-5HC	5 / 1.5	2.34 / 66.2	1.3 / 37.9	2.2 / 62.2	20 / 566	24 / 609	300 / 1135	1.1 / .84	2.5 - 4.5 / 0.7 - 1.3	5.19 / 1.5
FD-6HC	6 / 1.8	3.38 / 95.7	2.2 / 63	3.8 / 108	32 / 906	30 / 750	496 / 1,878	1.6 / 1.2	3.0 - 5.1 / 0.9 - 1.6	5.97 / 1.8
FD-8HC	8 / 2.4	6.00 / 169.9	5.1 / 144	8.6 / 243	50 / 1,415	48 / 1219	1120 / 4239	2.8 / 2.1	3.0 - 6.0 / 0.9 - 1.8	7.40 / 2.2

Contact Hydro International when larger pipe sizes are required.  
<sup>1</sup>Contact Hydro International when custom sediment storage capacity is required.  
<sup>3</sup>Minimum distance for models depends on pipe diameter.

The First Defense treatment system has the capacity of bypassing high flow rates internally as well as controlling flow through the treatment chamber so as to avoid wash-out of previously captured pollutants. The HydroCAD output can be found in the Appendix of this report. Specifications for the First Defense Systems can also be found in the appendix of this report along with certification from NYSDEC that it is an accepted proprietary device. The NJCAT testing certification is also included within the Appendix.

**Table 7: Swirl Chamber Sizing Calculations**

Proposed First Defense System	90% Rainfall Event Number (P) Inches	Tributary Catchment Areas (WS-#)	Required Water Quality Flow, cfs	Hydro International First Defense Model	Treatment Capacity, cfs
H-1	1.40	PW1C, PW1D, PW1H	1.89	FD-5HC	2.34
H-2		PW1E	0.7	FD-3HC	0.84
H-3		PW1F	0.37	FD-3HC	0.84

## VI. EROSION & SEDIMENT CONTROL

Construction operations shall be carried out in such a manner that erosion will be controlled and sediment migration minimized. Federal, State, and Local laws concerning pollution reduction will be

followed. The control practices indicated on attached Erosion & Sediment Control Plans shall be installed and used on this project.

The list of measures and practices below are contained on the Erosion and Sediment Control Plans in the appendix of this report and shall be installed and maintained per the most current edition of the New York Standard Specifications for Erosion and Sediment Control Handbook ("Bluebook"). All erosion control measures implemented shall be in accordance with the construction sequence schedule as described in Section VIII of this narrative.

Infiltration areas must be protected from sedimentation at all times during construction until all tributary areas have met the criteria of final stabilization. Engineered bioretention soils cannot be installed in the ponds until tributary areas have been stabilized unless the soil media is otherwise protected runoff that could compromise the composition of the soil media.

### **303(d) Segments Impaired by Construction related pollutants**

As stated earlier in this report, the site design point discharges to a tributary of the Monhagen Brook, a waterbody listed on the 303(d) list within the general permit. As such, the following requirements will need to be met during construction.

- For construction sites that directly discharge to one of the 303(d) segments listed in Appendix E or is located in one of the watersheds listed in Appendix C of GP-0-20-001, the qualified inspector shall conduct at least two (2) site inspections every seven (7) calendar days. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
- For construction sites that directly discharge to one of the 303(d) segments listed in Appendix E or is located in one of the watersheds listed in Appendix C of GP-0-20-001, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days

### **Temporary Measures**

Silt Fence – Silt fence shall be placed along the toe of all fill areas or any location where surface sheet flow could be expected in accordance with temporary soil erosion and sediment control plans serving to reduce runoff velocity and effect deposition of transported sediment load. Where silt fence ends, the end shall turn and run perpendicular to contours for a length of ten (10) feet, or for a difference in elevation of two (2) feet, whichever comes first.

Mulching – Mulching of all disturbed surfaces will be mandatory. Hydroseeding with mulch only mixes will be the preferred method.

Stabilized Construction Access - A stabilized pad of aggregate underlain with geotextile located at any point where traffic will be entering or leaving a construction site to or from a public right-of-way, street, alley, sidewalk, or parking area. The purpose of stabilized construction access is to reduce or eliminate the tracking of sediment onto public rights-of-way or streets.

The access shall be maintained in a condition which will prevent tracking of sediment onto public rights-of-way or streets. This may require periodic top dressing with additional aggregate. All sediment spilled, dropped, or washed onto public rights-of-way must be removed immediately. When necessary, wheels must be cleaned to remove sediment prior to entrance onto public rights-of-way. When washing is required, it shall be done on an area stabilized with aggregate, which drains into an approved sediment trapping device. All sediment shall be prevented from entering storm drains, ditches, or watercourses.

Concrete Washout Station - A temporary concrete washout station is to be used near the entrance to the site. The station will have a depth of 24 inches and shall be a minimum of 10 feet by 10 feet. Station shall be lined with a 10mil waterproof plastic membrane. Any tools or equipment that were used for concrete work will be cleaned here before leaving the site.

#### Permanent Measures

Topsoil, Seed & Mulch – Final vegetative stabilization shall be used at all locations where the ground has been disturbed and impervious covers are not specified. Mulch shall be applied with, or immediately after seeding.

Rock outlet protection- Stone riprap is to be placed at the outlet end of the culverts beneath the flared end section to slow down the flow of the runoff and reduce erosion.

#### Maintenance and Inspection of Measures

All temporary and permanent soil erosion and sediment measures shall be maintained by the contractor during the life of the project. The contractor shall have a trained contractor, as defined in the GP-0-20-001 (See Appendix 4) on site at all times. The trained contractor shall be responsible for the day to day construction and maintenance of all erosion and sediment control measures.

All temporary measures (silt fence, inlet protection, silt sock, sediment basins, etc.) and permanent measures (landscaping) shall be inspected by the Qualified Inspector every seven calendar days. The Qualified Inspector role and inspection requirements are outlined in Part IV.C of the GP-0-20-001 (See Appendix 4). All inspections are required to be completed within one calendar day. Any comments, suggestions or corrective actions the Qualified Inspector notes shall be addressed by the contractor within 24 hours of the inspection.

#### General Enhanced Erosion and Sediment Control Plan:

- Enlarged sediment ponds or sediment storage traps utilizing the maximum practical area in excess of the minimum amount recommended in the Bluebook
- Apply slope protection measures within 3 days after earthmoving on a particular slope is complete.
- Install reinforced silt fences with hay bale or silt sock backing along wetlands or other sensitive areas.
- Install bonded fiber matrix hydraulically applied mulch as temporary stabilization (hay/straw mulch and unbonded hydraulically applied mulches are not acceptable)

- Install flexible growth medium with seed, soil amendment, and fertilizer to seek final stabilization
- Perform equipment (cat) tracking for bare slopes to be protected. (See page 4.56 of the Bluebook)
- Install slope crest protection (perimeter dike/swale) measures to divert flow from going down the newly graded slope. (See page 3.36 of the Bluebook)
- Install pipe slope drains. (See page 3.37 of the Bluebook) Install reverse slope bench on the long slopes to convey water to a stable outlet. (See page 4.24 of the Bluebook)
- Install Geosynthetic Turf Reinforcement Mats available from Profile Products or equal on the embankments of sediment basins; immediately following construction. (See pages 5.19 to 5.41 of the Bluebook)
- Install Geosynthetic Turf Reinforcement Mats available from Profile Products or equal in temporary diversion ditches within two days of construction to stabilize the ditch.
- Install floating water skimmers connected to the outlet riser pipe in sedimentation ponds (See attached diagrams)
- Install sediment filter bags on the downstream end of the outlet pipe. (See page 5.16 of the Bluebook)
- Design sedimentation pond to maximize the sediment residence time. (See pages 5.19 to 5.41 of the Bluebook)
- Address the disposal or storage of sediment cleaned from sediment control devices, sediment ponds, ditches, and drainage inlets.
- Stabilize construction access roads with crushed stone, item 4, etc.
- Assign a dedicated and trained crew to maintain and repair erosion and sediment control measures daily.
- Install hydroseed & erosion control matting on all disturbed slopes 3H:1V or steeper
- Follow NYSDEC guidelines which limit the maximum soil disturbance area to 18 acres at any given time (or 5 acres max for projects not seeking 5-acre disturbance waiver). Temporary stabilization must be utilized in inactive areas to manage the amount of active open soil disturbance.

#### Construction Sequence:

All work to be done in accordance with the New York Standards and Specifications for Erosion and Sediment Control. See the Erosion & Sediment Control Plan included in the appendix of this report which has general erosion and sediment control notes and a sequence of construction, which can also be found below.

The erosion control practices designed specifically for the site phasing are to be implemented during construction. These include sediment traps, inlet protection, a stabilized construction entrance, staging areas, silt fence, temporary swales, temporary stockpiles, temporary sediment ponds, silt socks, erosion control matting/blankets, and temporary/permanent stabilization. The E&SC Plan



and Details found in the appendix of this report depict the location and size of the proposed erosion control practices to be used during construction.

A sediment trap detail and sizing criteria have been provided on the plans. These sizes and volumes are required through the device can be relocated as practical by the Contractor (note: traps must be sized to provide 3,600 CF of storage per 1-acre of disturbance and tributary to each location). It is recommended to provide increased storage in excess of the required volume.

**Sediment Pond Restoration:** When temporary structures have served their intended purpose and the contributing drainage area has been properly stabilized, the embankment and resulting sediment deposits are to be leveled or otherwise disposed of. Sediment can be disposed of by exporting it off site for disposal or be used as fill in lawn areas. Sediment ponds in future open space or lawn areas may be pumped dry, graded, and backfilled. Sediment ponds in paved or structural areas must have the basin material and trapped sediments removed, safely disposed of, and backfilled with structural fill. Sediment ponds in locations of future stormwater ponds must have the trapped sediment removed leaving the basin area open for the development of the final stormwater pond.

The applicant and the applicant's contractor are required to attend a preconstruction meeting with representatives from the Town Building Departments, Highway Departments, Engineers and any other parties deemed necessary to review all protocols, bonding requirements, agreements and the sequence and scheduling of the work being undertaken, as applicable.

### **Construction Sequencing:**

Refer to the erosion & sediment controls plans included as an appendix to this report for construction limit of disturbance, recommended temporary sediment basin sizing, and other recommended erosion control measures.

1. The contractor must first delineate and protect the wetlands and associated buffer areas. Install construction entrances and all applicable erosion control measures as shown on the plan, including silt fencing and temporary swales. Establish staging areas.
2. Contractor shall install the temporary sediment basins as indicated on the site plan and/or as required to construct the project while maintaining functionality of the necessary storage. Contractor to construct additional temporary diversion swales and sediment traps as needed to direct and capture runoff from disturbed areas. Locations and size of the erosions and sediment control practices are noted on the plan. These may vary depending on the contractor's schedule and approach but 3,600 cf of storage must be provided at a minimum per acre of upstream disturbance. Sediment traps shall be installed in accordance with the plans and details. Sediment traps and basins shall be sized in accordance with the New York Standards and Specifications for Erosion and Sediment Control Manual. Sediment ponds should have non-erosive inlets and the embankments should be stabilized with vegetation or mechanical control measures to minimize turbidity of the stored water to the maximum extent practical.
3. Disturbed soils shall be temporarily stabilized as soon as practical. Materials stored in stockpiles shall be cordoned off with silt fence per the appropriate specifications and details. The operator

shall initiate stabilization measures as soon as practical in portions of the site where construction activities have temporarily or permanently ceased, but in no case more than (14) days after the construction activity in that portion of the site has temporarily or permanently ceased.

Temporary Stabilization - means that exposed soil has been covered with material(s) as set forth in the technical standard, New York Standards and Specifications for Erosion and Sediment Control, to prevent the exposed soil from eroding. The materials can include, but are not limited to, mulch, seed and mulch, and erosion control mats (e.g. jute twisted yarn, excelsior wood fiber mats). Stabilization shall be maintained per SPDES General Permit for stormwater runoff from construction activity, GP-0-20-001 or as amended.

4. The Contractor shall grade the site systematically, installed stone roadways in heavily trafficked areas and installing pavement subbase materials as soon as practical to minimize the amount of actively open soil area. Remove soil/rock/stockpile excess material as necessary. The contractor will then install the site utilities and remaining retaining walls. Temporary swales must be used throughout the grading process to ensure runoff is always directed towards a sediment pond prior to discharging the site.
5. The subbase and curbing shall be installed as soon as practicable to provide a stabilized surface.
6. Once the areas upland of the sediment traps/basins have been stabilized, the bioretention systems, underdrains, and soil media can be installed. All upstream structures must have adequate inlet protection prior to the system being place on-line.
7. Grade and spread topsoil on all lawn areas and seed, install sidewalks. Maintain all seeded and planted areas to insure a viable stabilized vegetative cover.
8. The project site must meet final stabilization criteria prior to removing all erosion and sediment control devices and closing out the project. Litter and construction debris shall be removed as practical throughout the life of the project.
  - Final Stabilization means that all soil disturbance activities have ceased and a uniform, perennial vegetative cover with a density of eighty (80) percent over the entire pervious surface has been established; or other equivalent stabilization measures, such as permanent landscape mulches, rock rip-rap or washed/crushed stone have been applied on all disturbed areas that are not covered by permanent structures, concrete or pavement.
9. Upon final stabilization being met, Contractor shall clear the drainage system, drainage pipe, and all existing and new structures on site of any sediment which may have accumulated during construction.
10. Additional erosion control measures shall be installed, as may be necessary, required and/or requested by authorities, to prevent the incidental discharge of silt laden runoff from entering a



water course or a drainage system. The general permit for stormwater discharges from construction activities states that it is unlawful for any person to cause or contribute to a violation of water quality standards.

For additional, general Erosion and Sediment Control notes including seeding, please refer to the latest Erosion and Sediment Control Plans.

## VII. GOOD HOUSEKEEPING

Good housekeeping practices are inexpensive, relatively easy to implement and are often effective in preventing stormwater contamination. Specific activities that should be completed by the contractor are listed below:

### SPILL INVENTORY

The materials or substances listed below are expected to be present on-site during construction:

- Concrete
- Fertilizers
- Piping
- Paints (enamel & latex)
- Treated and non-treated wood
- Seed
- Tar
- Petroleum-based products
- Reinforcing steel
- Cleaning solvents
- Masonry block
- Paving materials

### MATERIAL MANAGEMENT PRACTICES

The following are the material management practices that shall be used to reduce the risk of spills or other accidental exposure of materials and substances to stormwater runoff:

- Products shall be kept in original containers unless they are not re-sealable.
- Original labels and material safety data sheets (MSDS) shall be retained; they contain important product information.
- An effort shall be made to store only enough products required to do the job.
- All materials stored onsite shall be stored in a neat, orderly manner in their appropriate containers, and if possible, under a roof or other enclosure and/or on non-porous blacktop.
- Products shall be kept in their original containers with the original manufacturer's label.
- Substances shall not be mixed with one another unless recommended by the manufacturer.
- Whenever possible, all of a product shall be used up before disposing of the container.
- Manufacturer's recommendations for proper use and disposal shall be followed.

- The contractor's site superintendent shall inspect daily to ensure proper use and disposal of materials on site.

#### SPILL CONTROL PRACTICES

In addition to the good housekeeping and material management practices discussed in the previous sections of this plan, the following practices shall be followed for spill prevention and cleanup.

- Spills, of any size, of toxic or hazardous material and/or petroleum products shall be reported to the NYSDEC and Central Hudson's Environmental Affairs division.
- Manufacturer's recommended methods for spill cleanup shall be clearly posted and site personnel shall be made aware of the procedures and the locations of the information and cleanup supplies.
- Materials and equipment necessary for spill cleanup shall be kept in the material storage area onsite. Equipment and materials shall include but not be limited to brooms, dust pans, mops, rags, gloves, kitty litter, sand, sawdust, and plastic and metal trash containers specifically for this purpose.
- All spills shall be cleaned up immediately after discovery.
- The spill area shall be kept well ventilated and personnel shall wear appropriate protective clothing to prevent injury from contact with a hazardous substance.
- The spill prevention plan shall be adjusted to include measures to prevent toxic or hazardous material of spills from recurring and how to clean up the spill. A description of the spill, what caused it, and the cleanup measures shall also be included.

The contractor's site superintendent is responsible for the day-to-day site operations and shall be the spill prevention and cleanup coordinator.

#### PRODUCT SPECIFIC PRACTICES

The following product specific practices shall be followed onsite.

- Petroleum Products – All onsite vehicles shall be monitored for leaks and receive regular preventive maintenance to reduce the chance of leakage. Petroleum products shall be stored in tightly sealed containers that are clearly labeled. Any asphalt substances used on site shall be applied according to manufacturer's recommendations.
- Fertilizers- Fertilizers shall be applied only in the minimum amounts recommended by the manufacturer. Use only fertilizers that have 5 or less parts phosphorous. Once applied, fertilizers shall be worked into the soil to limit exposure to stormwater. Storage shall be in a covered shed. The contents of any partially used bags of fertilizer shall be transferred to a sealable plastic bin to avoid spills.
- Paints – All containers shall be tightly sealed and stored when not required for use. Excess paint shall not be discharged to the storm sewer system but shall be properly disposed of according to the manufacturer's instructions or state and local regulations.
- Concrete Trucks – Concrete trucks shall not be allowed to wash out or discharge surplus concrete or drum wash water on the site, unless in approved clean-out areas.

- Waste Disposal – All waste materials shall be collected and stored in a securely lidded metal dumpster rented from a licensed solid waste management company. The dumpster shall meet all local and any State solid waste management regulations. All trash and construction debris from the site shall be deposited in the dumpster. The dumpster shall be emptied as necessary, and the trash shall be hauled to a NYSDEC permitted landfill. No construction waste materials shall be buried onsite. All personnel shall be instructed regarding the correct procedure for waste disposal.
- Hazardous Waste – All hazardous waste materials shall be disposed of in a manner specified by local or State regulations or the manufacturer. Site personnel shall be instructed in these practices.
- Sanitary Waste – All sanitary waste shall be collected from the portable units by a licensed sanitary waste management contractor, as required by local regulation and as required to protect public health and safety.
- Recyclable Waste – All recyclable waste (cardboard, wood, etc.) shall be collected and recycled on a weekly schedule.

## VIII. RESPONSIBLE PARTIES

### IMPLEMENTATION OF SWPPP

The owner/operator is responsible for implementing the provisions of the SWPPP and ensuring that the appropriate contractors and subcontractors on the site provide certification in accordance with the provisions of the GP-0-20-001.

The owner/operator is also responsible to have a trained contractor and Qualified Inspector inspect the active construction site in accordance with section 6.3 of this report and all provisions for inspections defined in the GP-0-20-001, (See Appendix 4). A trained contractor cannot conduct Qualified Inspector site inspections unless they meet the Qualified Inspector qualifications listed in appendices of the GP-0-20-001.

### INSPECTION REQUIREMENTS

The owner/operator is responsible for implementing inspections of all erosion and sediment control measures. To do so, the owner/operator shall have a Qualified Inspector inspect the site in accordance with the guidelines of Part IV of the GP-0-20-001. A sample inspection template is provided in the Appendix of this report.

The owner/operator shall maintain a record of all inspection reports in a site logbook. The site logbook shall be kept on site and be made available to the permitting authority upon request. The owner/operator shall also retain a copy of this SWPPP document at the construction site during the life of the project.

## IX. END OF PROJECT – TERMINATION OF PERMIT

### FINAL INSPECTION

Prior to filing the Notice of Termination (NOT), or at the end of permit term, the owner/operator shall have a *Qualified Inspector* perform a final site inspection. The inspector shall certify that the site has undergone final stabilization using either vegetative or structural stabilization methods. Final stabilization means that all soil-disturbing activities at the site have been completed and a uniform, perennial vegetative cover with a density of 80% has been established on all unpaved areas and areas not covered by permanent structures.

### NOTICE OF TERMINATION

When the site has been finally stabilized, the owner/operator must submit a Notice of Termination (NOT) form to terminate coverage under SPDES General Permit GP-0-20-001. The permittee must identify all of the permanent stormwater management structures that have been constructed. In addition, a manual describing the operation and maintenance practices that will be necessary for the structure(s) to function as designed after the site is stabilized must be developed and in place. The permittee must also certify that the permanent structure(s) have been constructed in conformance with this document. A copy of the Notice of Termination (NOT) is provided in the Appendix of this report.

### RECORD KEEPING

The owner/operator shall retain copies of SWPPP, any reports submitted in conjunction with this permit, and records of all data used to complete the NOI & NOT for a period of at least five (5) years from the date that the site is finally stabilized.

## X. SUMMARY OF PROPOSED STORMWATER IMPROVEMENTS

The site runoff has been attenuated for peak flows in the peak design storms. The new impervious area has been treated for the required water quality and runoff reduction through the use of bioretention ponds. The design utilizes DEC approved practices that help maintain the existing hydrology.

## XI. CONCLUSION

As the storm water pollution prevention plan provides water quality treatment and peak flow mitigation meeting the applicable standards, there should be no adverse impacts due to storm water, on-site or off-site, as a result of the proposed development.

r:\projects\2020\20006912a\reports\drainage\dewpoint south\jan 2023 - r1\pieces\report\230202 - r1 - swppp narrative - rdm dewpoint south.docx

# Appendix 1 | Watershed Maps

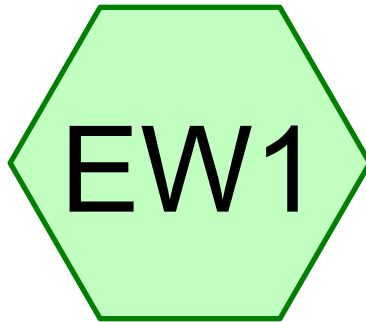




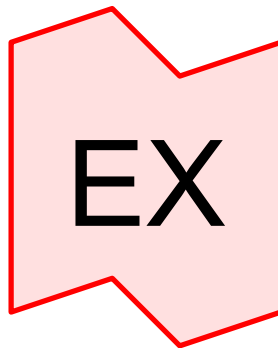


## Appendix 2a | HydroCAD Data (Existing)

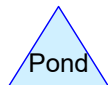
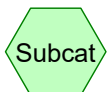




EW1



EXISTING



## 230119 - R1 - Dewpoint South

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Printed 2/2/2023

Page 2

### Rainfall Events Listing

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	1-yr	Type III 24-hr		Default	24.00	1	2.64	2
2	2-yr	Type III 24-hr		Default	24.00	1	3.17	2
3	10-yr	Type III 24-hr		Default	24.00	1	4.68	2
4	100-yr	Type III 24-hr		Default	24.00	1	8.22	2
5	WQv	Type III 24-hr		Default	24.00	1	1.40	2

**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 3

**Summary for Subcatchment EW1: EW1**

Runoff = 6.03 cfs @ 12.52 hrs, Volume= 37,256 cf, Depth= 0.88"  
 Routed to Link EX : EXISTING

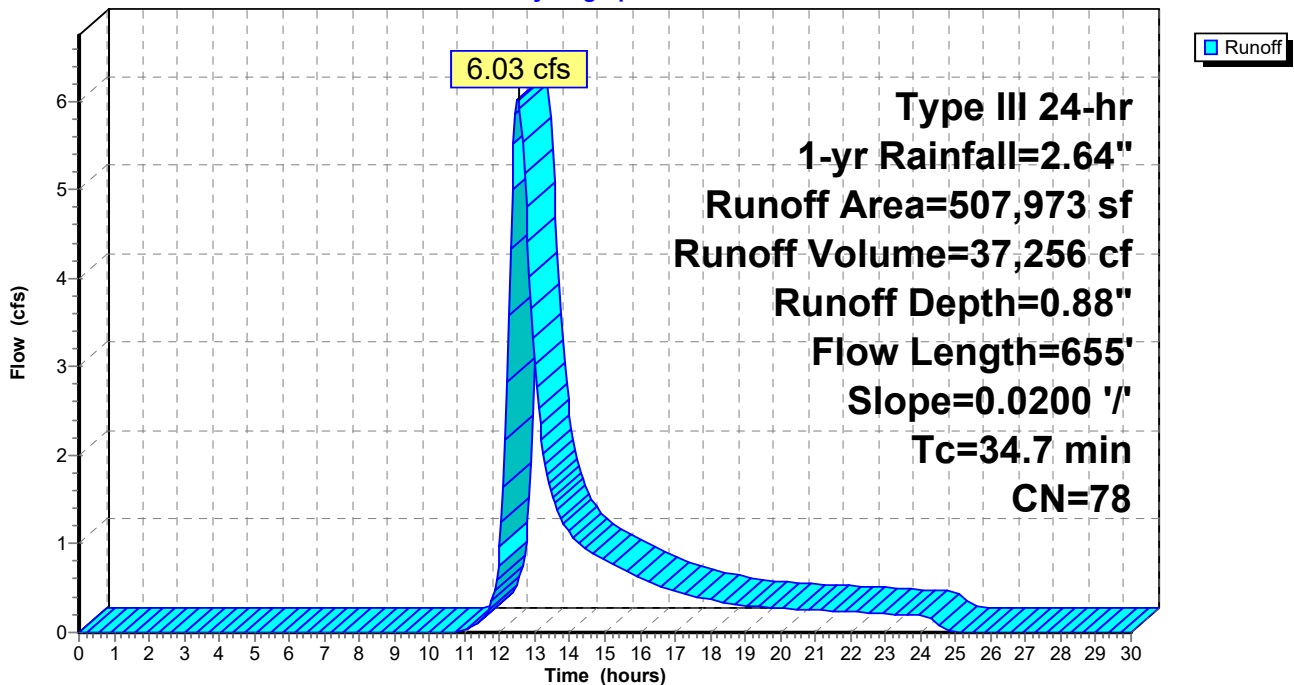
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
10,934	98	Paved parking, HSG D
26,543	84	50-75% Grass cover, Fair, HSG D
22,724	73	Brush, Good, HSG D
447,772	77	Woods, Good, HSG D
507,973	78	Weighted Average
497,039		97.85% Pervious Area
10,934		2.15% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment EW1: EW1**

Hydrograph



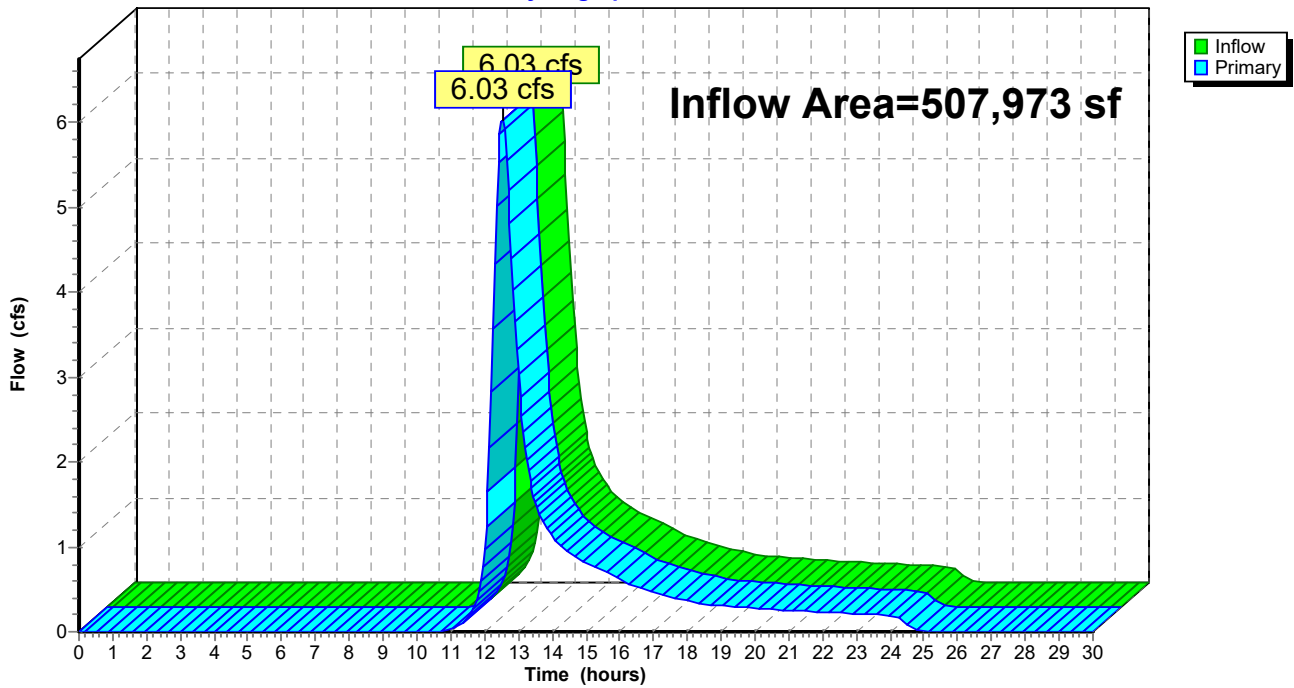
### Summary for Link EX: EXISTING

Inflow Area = 507,973 sf, 2.15% Impervious, Inflow Depth = 0.88" for 1-yr event  
Inflow = 6.03 cfs @ 12.52 hrs, Volume= 37,256 cf  
Primary = 6.03 cfs @ 12.52 hrs, Volume= 37,256 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link EX: EXISTING

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 5

**Summary for Subcatchment EW1: EW1**

Runoff = 8.80 cfs @ 12.51 hrs, Volume= 52,974 cf, Depth= 1.25"  
 Routed to Link EX : EXISTING

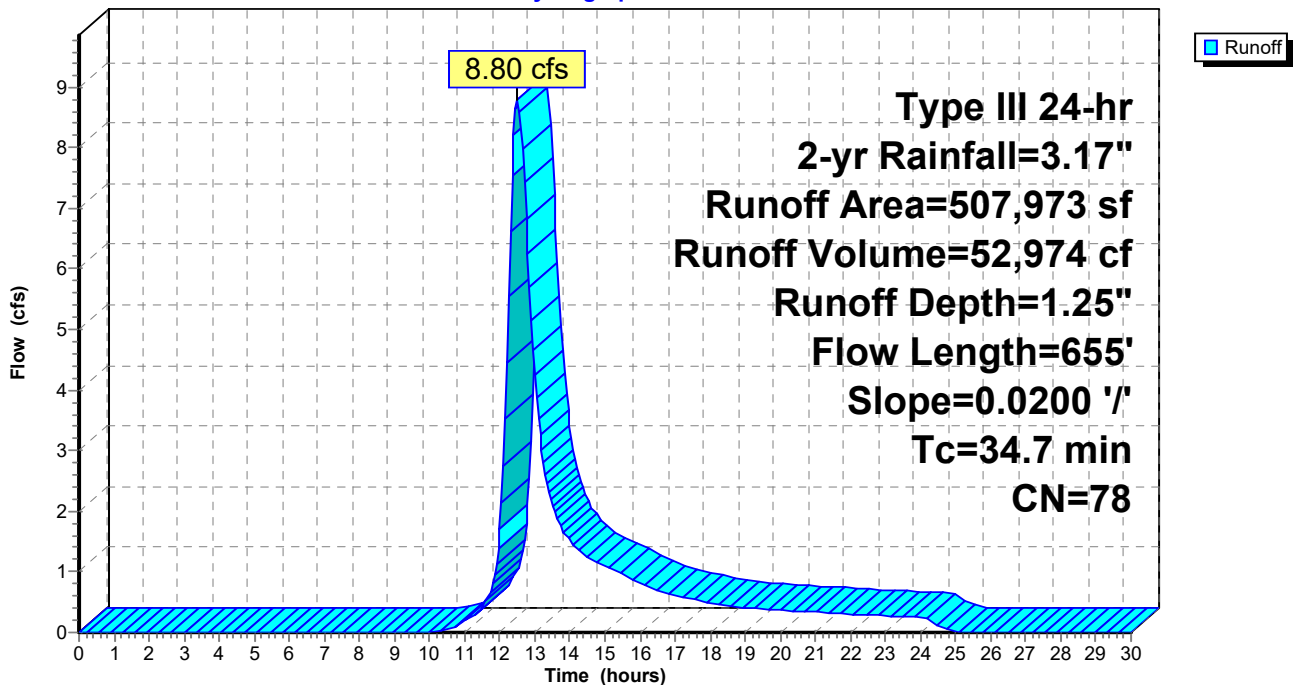
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
10,934	98	Paved parking, HSG D
26,543	84	50-75% Grass cover, Fair, HSG D
22,724	73	Brush, Good, HSG D
447,772	77	Woods, Good, HSG D
507,973	78	Weighted Average
497,039		97.85% Pervious Area
10,934		2.15% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment EW1: EW1**

Hydrograph



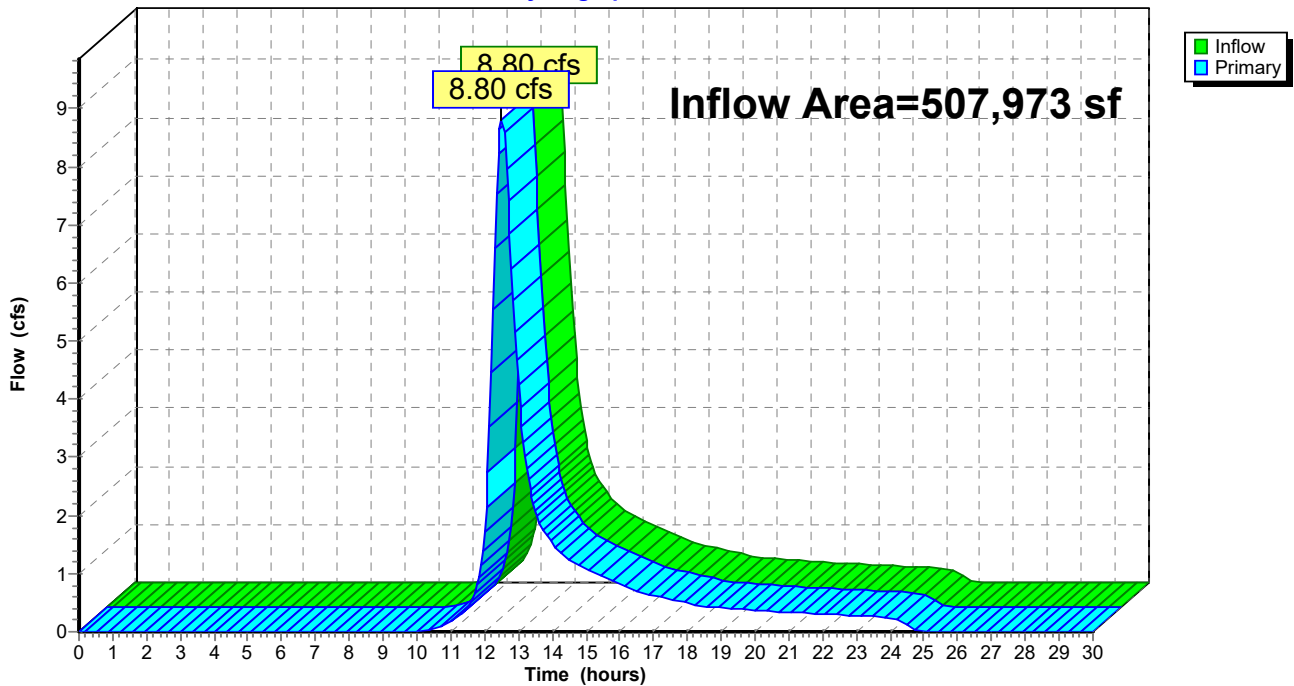
### Summary for Link EX: EXISTING

Inflow Area = 507,973 sf, 2.15% Impervious, Inflow Depth = 1.25" for 2-yr event  
Inflow = 8.80 cfs @ 12.51 hrs, Volume= 52,974 cf  
Primary = 8.80 cfs @ 12.51 hrs, Volume= 52,974 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link EX: EXISTING

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 7

**Summary for Subcatchment EW1: EW1**

Runoff = 17.57 cfs @ 12.49 hrs, Volume= 103,384 cf, Depth= 2.44"  
 Routed to Link EX : EXISTING

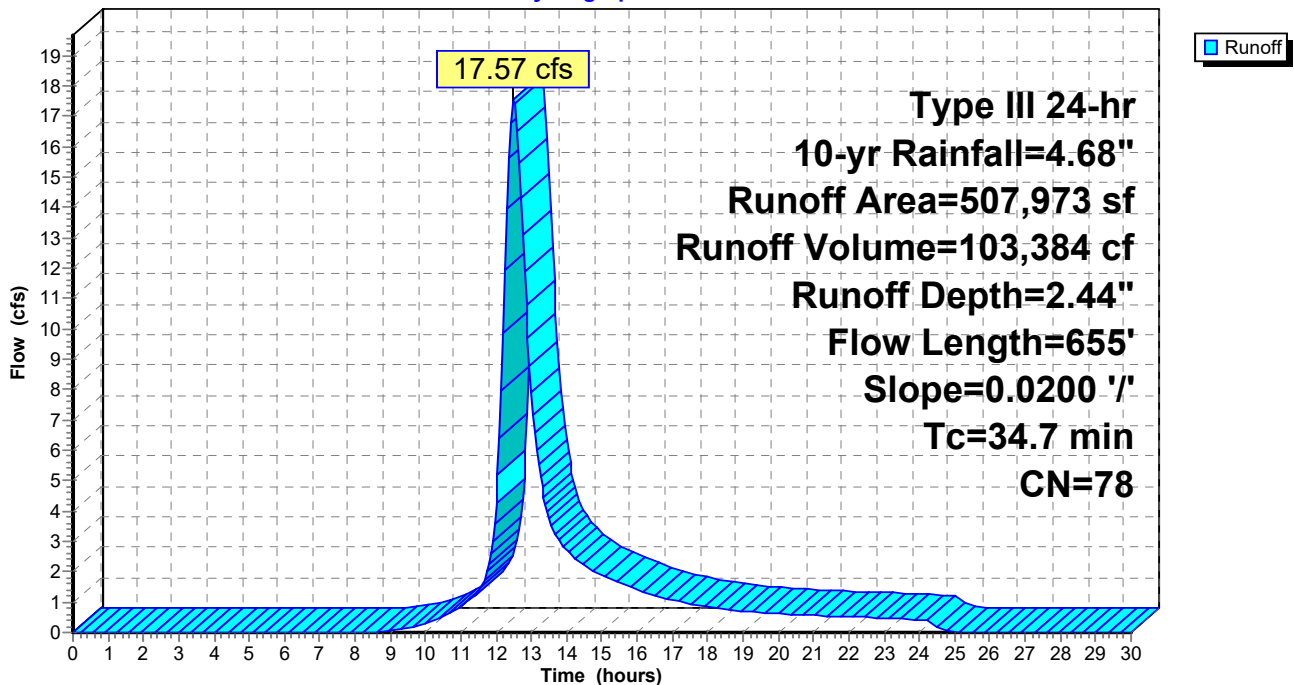
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
10,934	98	Paved parking, HSG D
26,543	84	50-75% Grass cover, Fair, HSG D
22,724	73	Brush, Good, HSG D
447,772	77	Woods, Good, HSG D
507,973	78	Weighted Average
497,039		97.85% Pervious Area
10,934		2.15% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment EW1: EW1**

Hydrograph



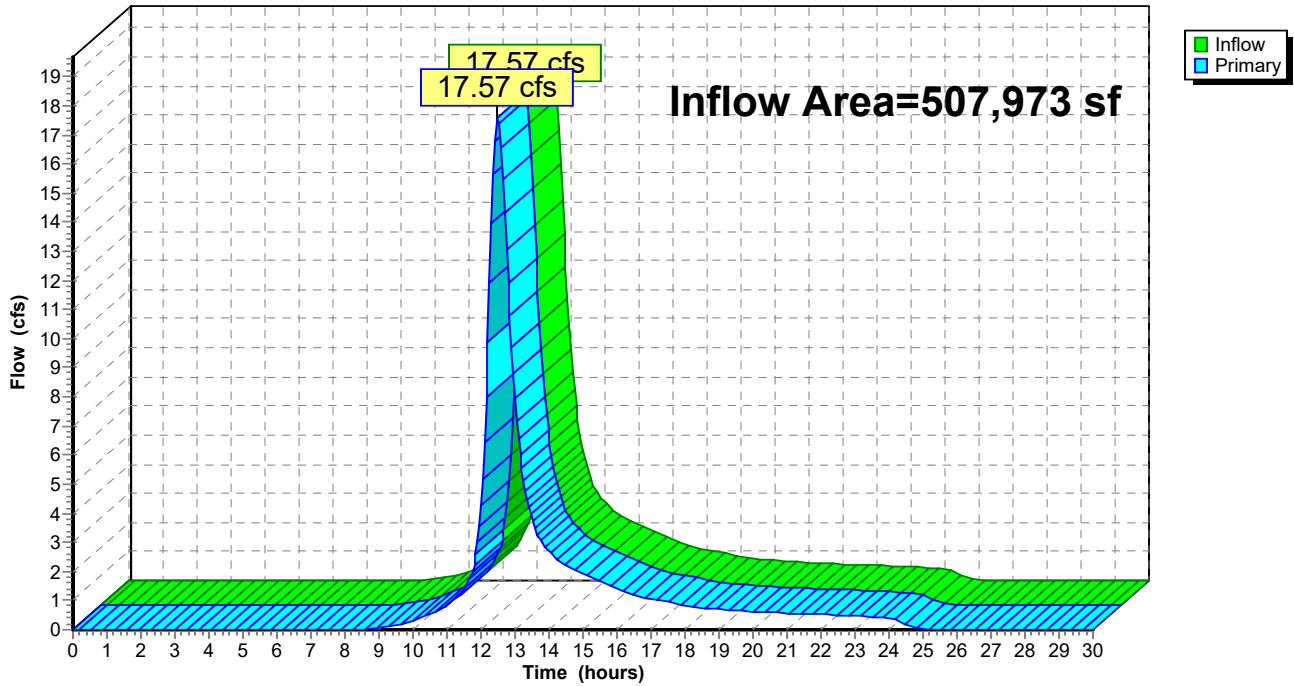
### Summary for Link EX: EXISTING

Inflow Area = 507,973 sf, 2.15% Impervious, Inflow Depth = 2.44" for 10-yr event  
Inflow = 17.57 cfs @ 12.49 hrs, Volume= 103,384 cf  
Primary = 17.57 cfs @ 12.49 hrs, Volume= 103,384 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link EX: EXISTING

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 9

**Summary for Subcatchment EW1: EW1**

Runoff = 40.06 cfs @ 12.47 hrs, Volume= 236,831 cf, Depth= 5.59"  
 Routed to Link EX : EXISTING

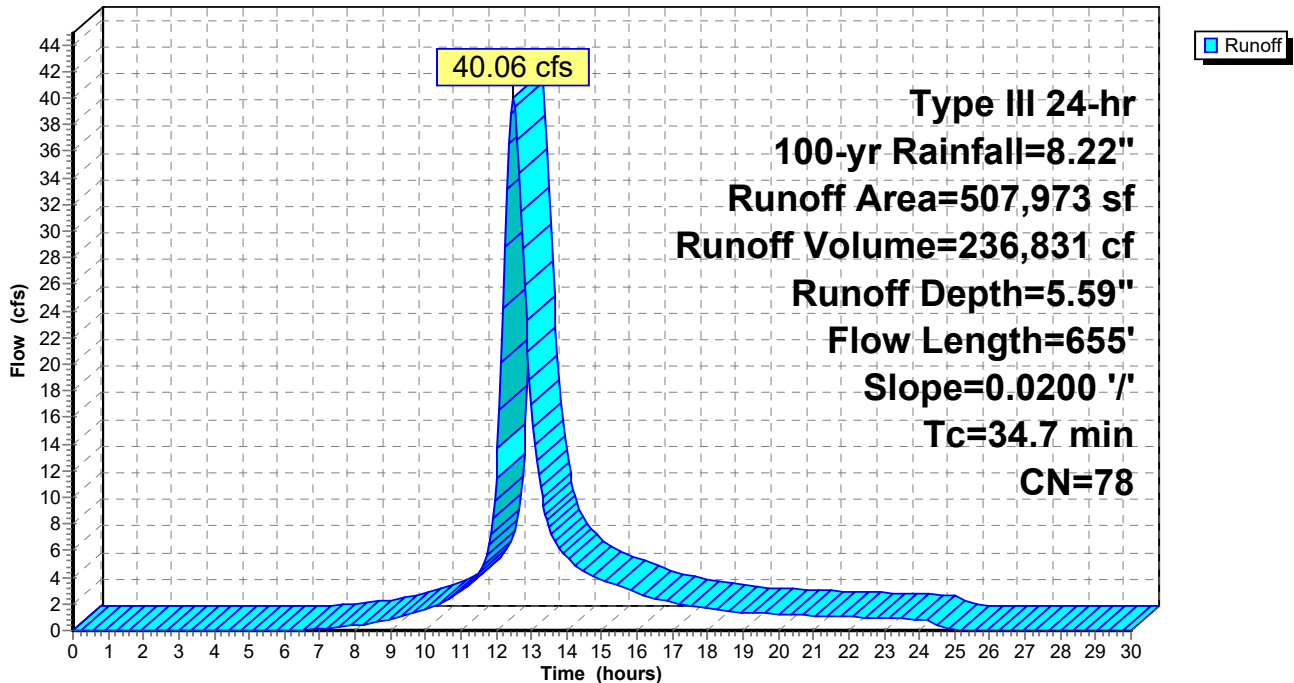
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
10,934	98	Paved parking, HSG D
26,543	84	50-75% Grass cover, Fair, HSG D
22,724	73	Brush, Good, HSG D
447,772	77	Woods, Good, HSG D
507,973	78	Weighted Average
497,039		97.85% Pervious Area
10,934		2.15% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment EW1: EW1**

Hydrograph



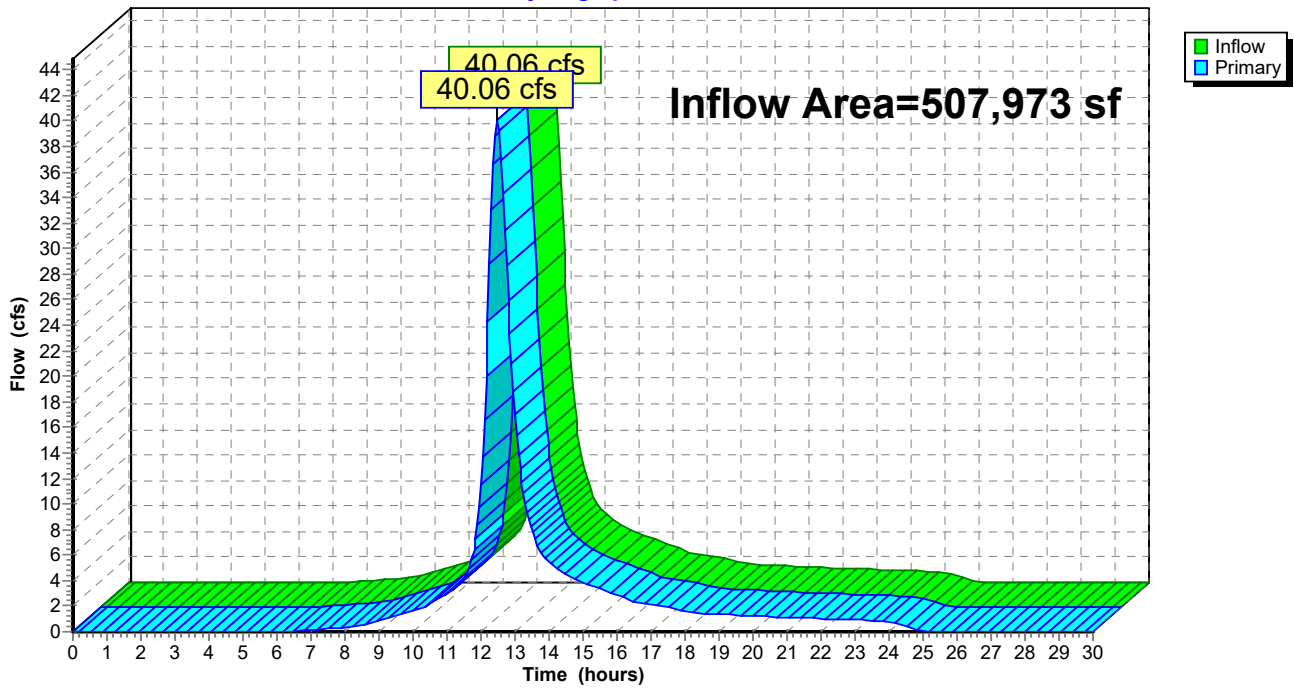
### Summary for Link EX: EXISTING

Inflow Area = 507,973 sf, 2.15% Impervious, Inflow Depth = 5.59" for 100-yr event  
Inflow = 40.06 cfs @ 12.47 hrs, Volume= 236,831 cf  
Primary = 40.06 cfs @ 12.47 hrs, Volume= 236,831 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link EX: EXISTING

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 11

**Summary for Subcatchment EW1: EW1**

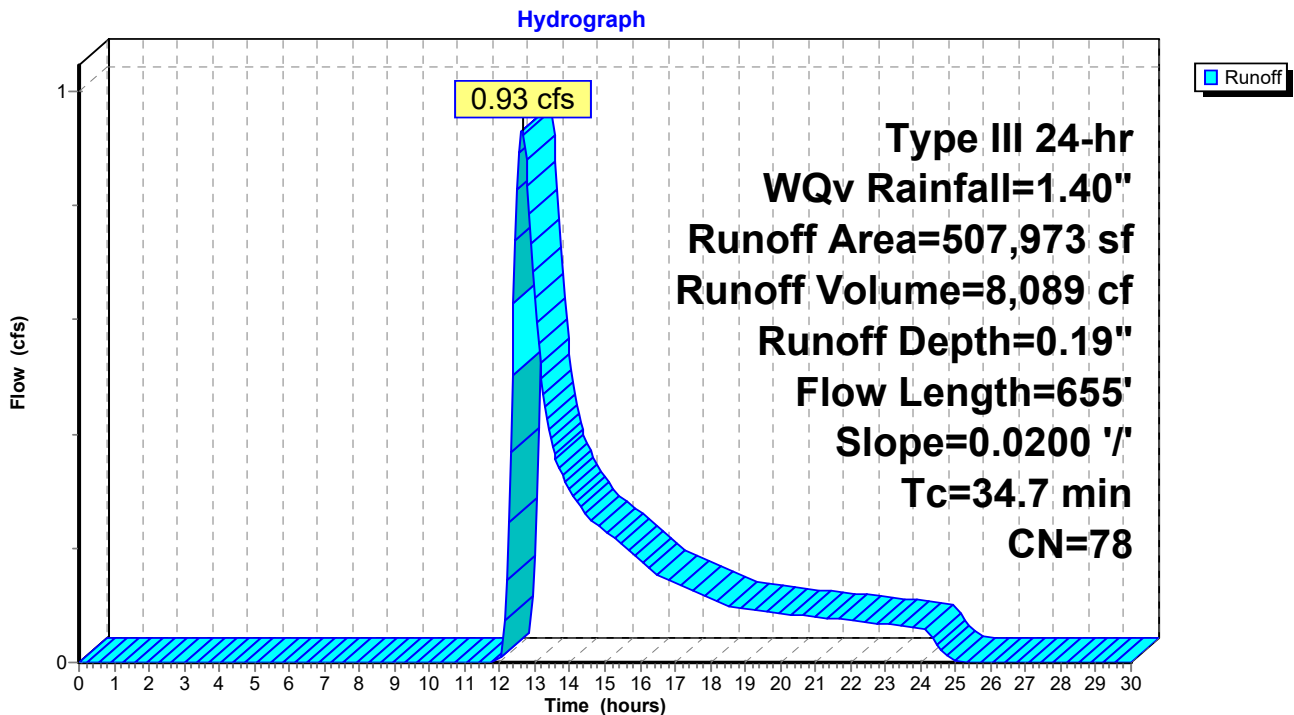
Runoff = 0.93 cfs @ 12.64 hrs, Volume= 8,089 cf, Depth= 0.19"  
 Routed to Link EX : EXISTING

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
10,934	98	Paved parking, HSG D
26,543	84	50-75% Grass cover, Fair, HSG D
22,724	73	Brush, Good, HSG D
447,772	77	Woods, Good, HSG D
507,973	78	Weighted Average
497,039		97.85% Pervious Area
10,934		2.15% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment EW1: EW1**



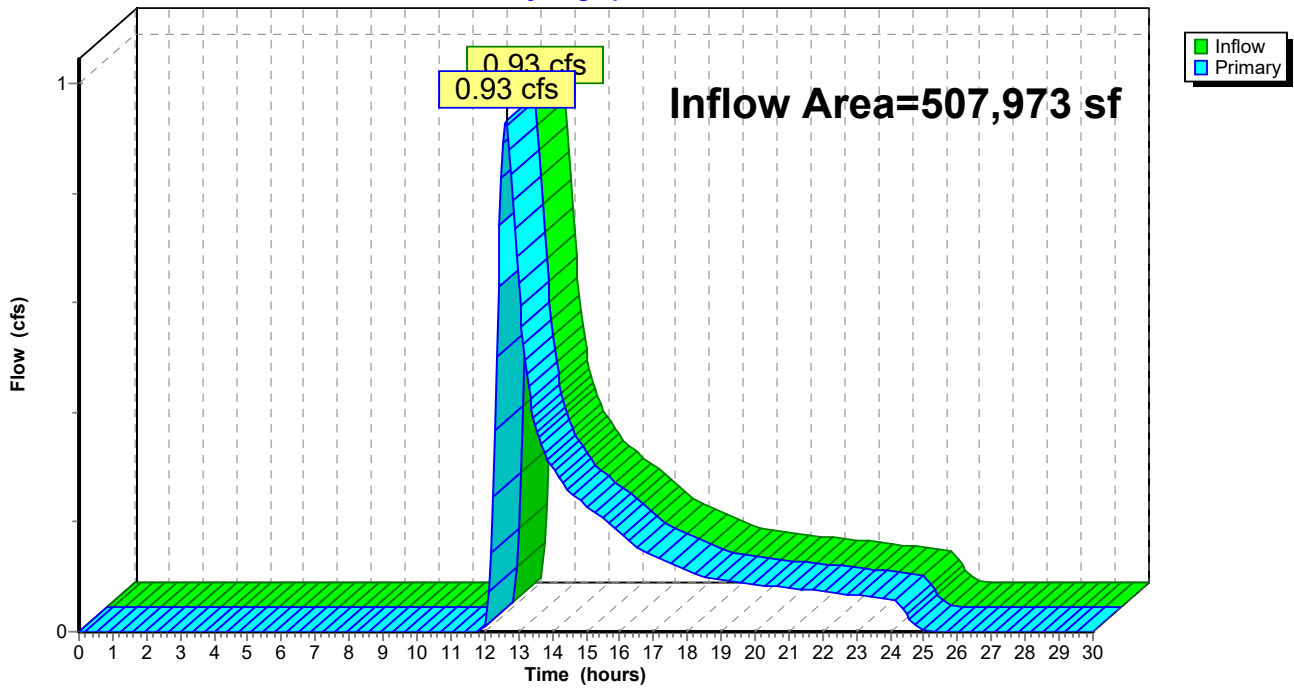
### Summary for Link EX: EXISTING

Inflow Area = 507,973 sf, 2.15% Impervious, Inflow Depth = 0.19" for WQv event  
Inflow = 0.93 cfs @ 12.64 hrs, Volume= 8,089 cf  
Primary = 0.93 cfs @ 12.64 hrs, Volume= 8,089 cf, Atten= 0%, Lag= 0.0 min

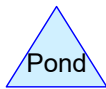
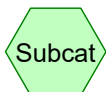
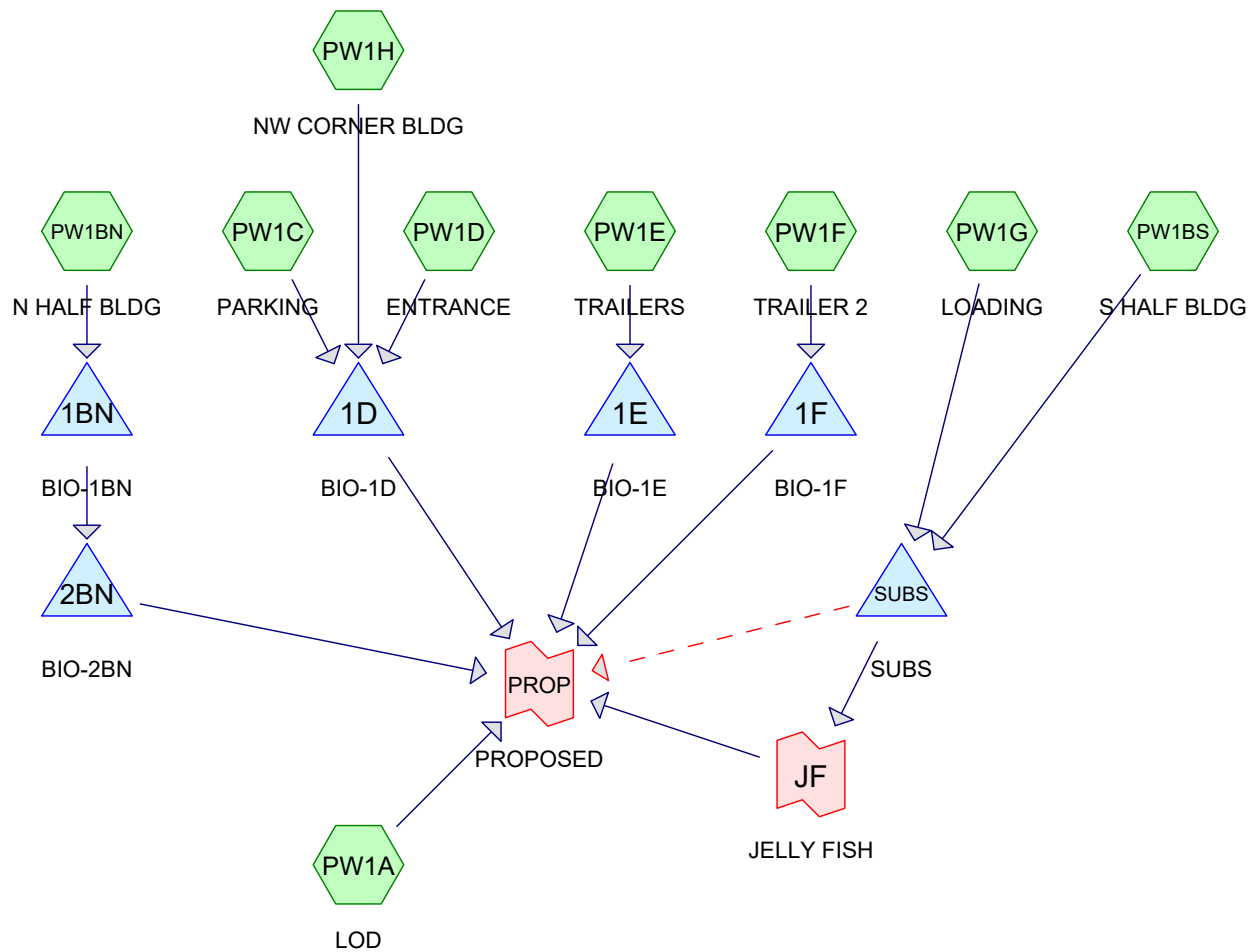
Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link EX: EXISTING

Hydrograph



## Appendix 2b | HydroCAD Data (Proposed)



**Routing Diagram for 230119 - R1 - Dewpoint South**  
 Prepared by Maser Consulting, Printed 2/2/2023  
 HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

## 230119 - R1 - Dewpoint South

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Printed 2/2/2023

Page 2

### Rainfall Events Listing

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	1-yr	Type III 24-hr		Default	24.00	1	2.64	2
2	2-yr	Type III 24-hr		Default	24.00	1	3.17	2
3	10-yr	Type III 24-hr		Default	24.00	1	4.68	2
4	100-yr	Type III 24-hr		Default	24.00	1	8.22	2
5	WQv	Type III 24-hr		Default	24.00	1	1.40	2

**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 3

**Summary for Subcatchment PW1A: LOD**

Runoff = 2.16 cfs @ 12.52 hrs, Volume= 13,330 cf, Depth= 0.88"  
 Routed to Link PROP : PROPOSED

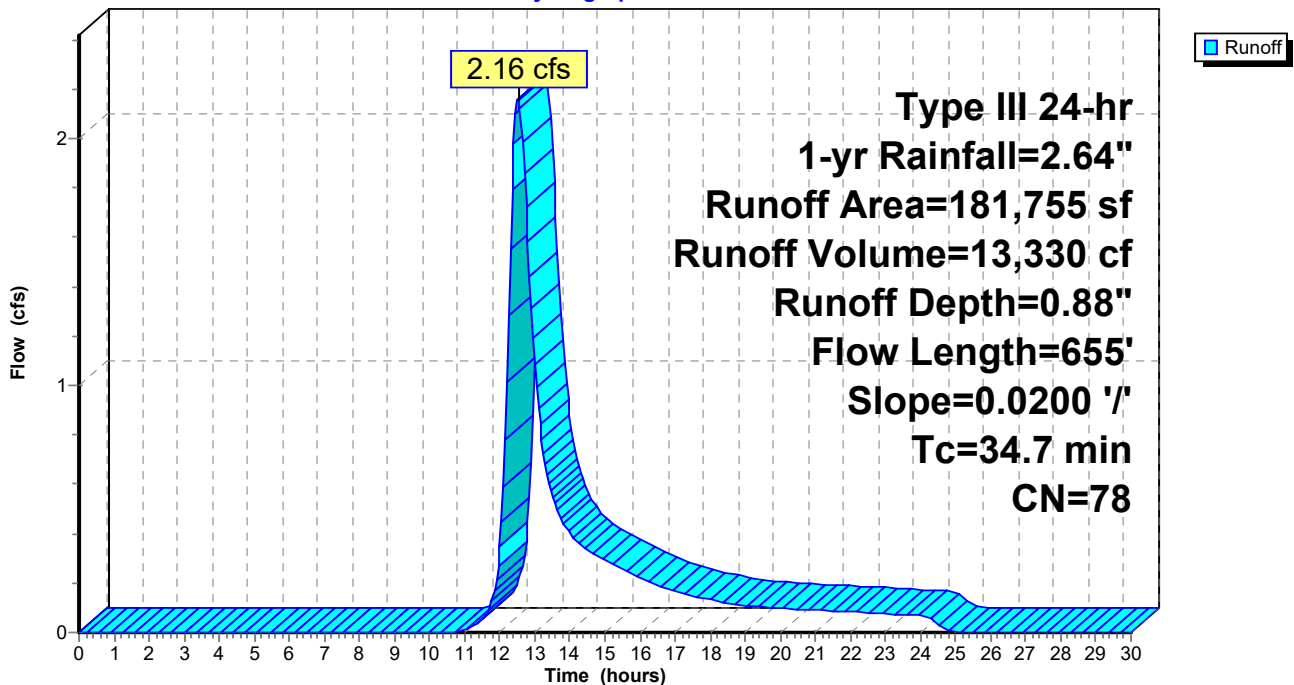
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
2,800	98	Paved parking, HSG D
73,077	80	>75% Grass cover, Good, HSG D
22,724	73	Brush, Good, HSG D
83,154	77	Woods, Good, HSG D
181,755	78	Weighted Average
178,955		98.46% Pervious Area
2,800		1.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment PW1A: LOD**

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 4

**Summary for Subcatchment PW1BN: N HALF BLDG**

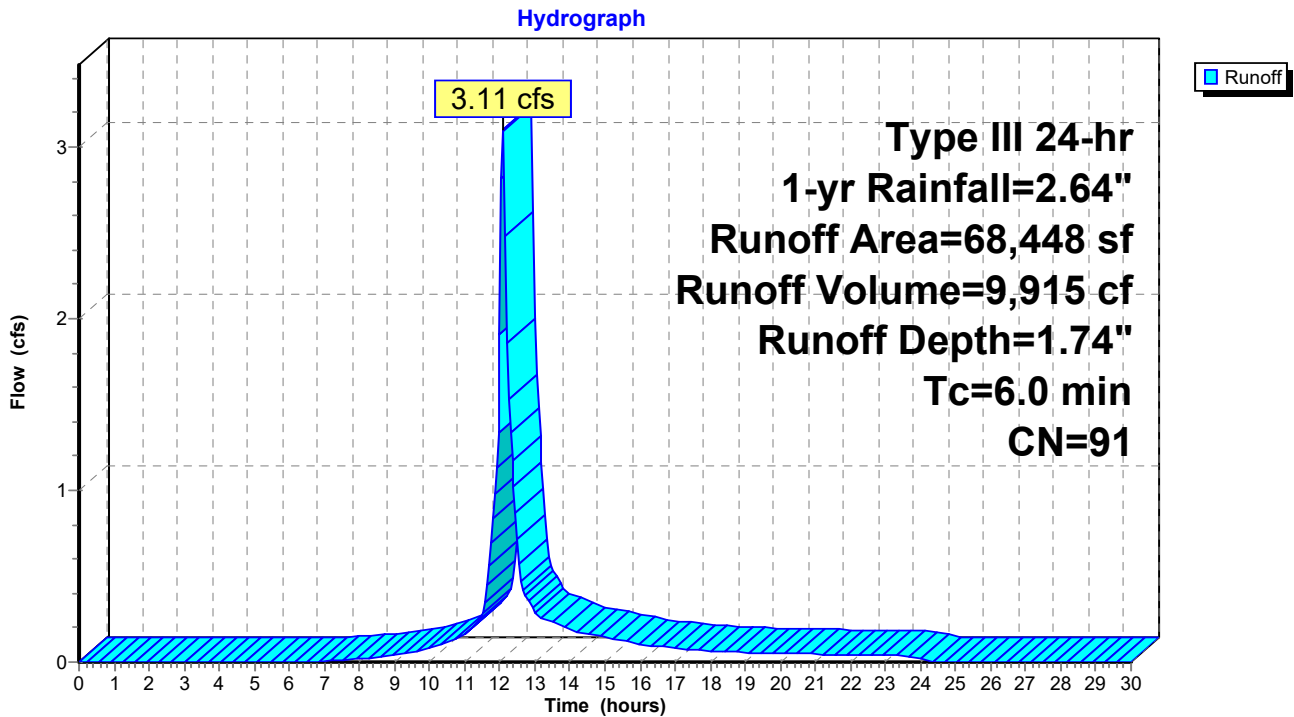
Runoff = 3.11 cfs @ 12.09 hrs, Volume= 9,915 cf, Depth= 1.74"  
 Routed to Pond 1BN : BIO-1BN

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
40,450	98	Paved parking, HSG D
27,998	80	>75% Grass cover, Good, HSG D
68,448	91	Weighted Average
27,998		40.90% Pervious Area
40,450		59.10% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BN: N HALF BLDG**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 5

**Summary for Subcatchment PW1BS: S HALF BLDG**

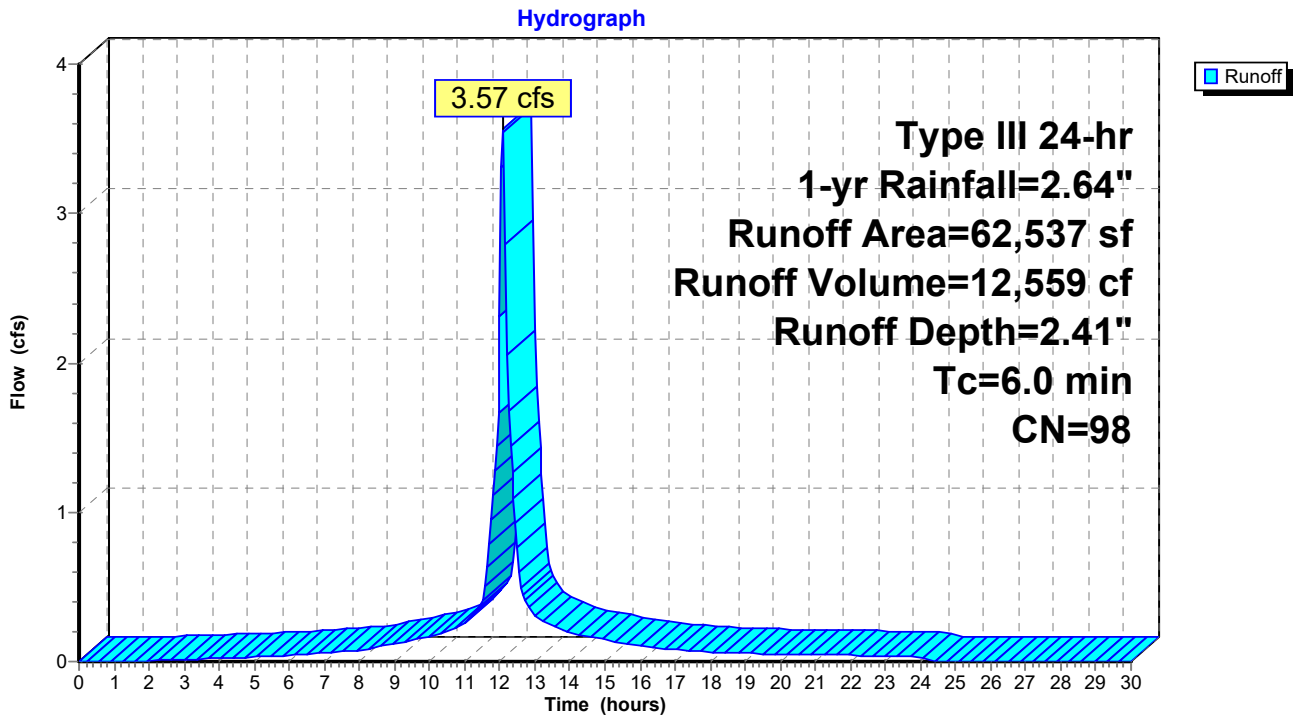
Runoff = 3.57 cfs @ 12.09 hrs, Volume= 12,559 cf, Depth= 2.41"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
62,537	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
62,537	98	Weighted Average
62,537		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BS: S HALF BLDG**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 6

**Summary for Subcatchment PW1C: PARKING**

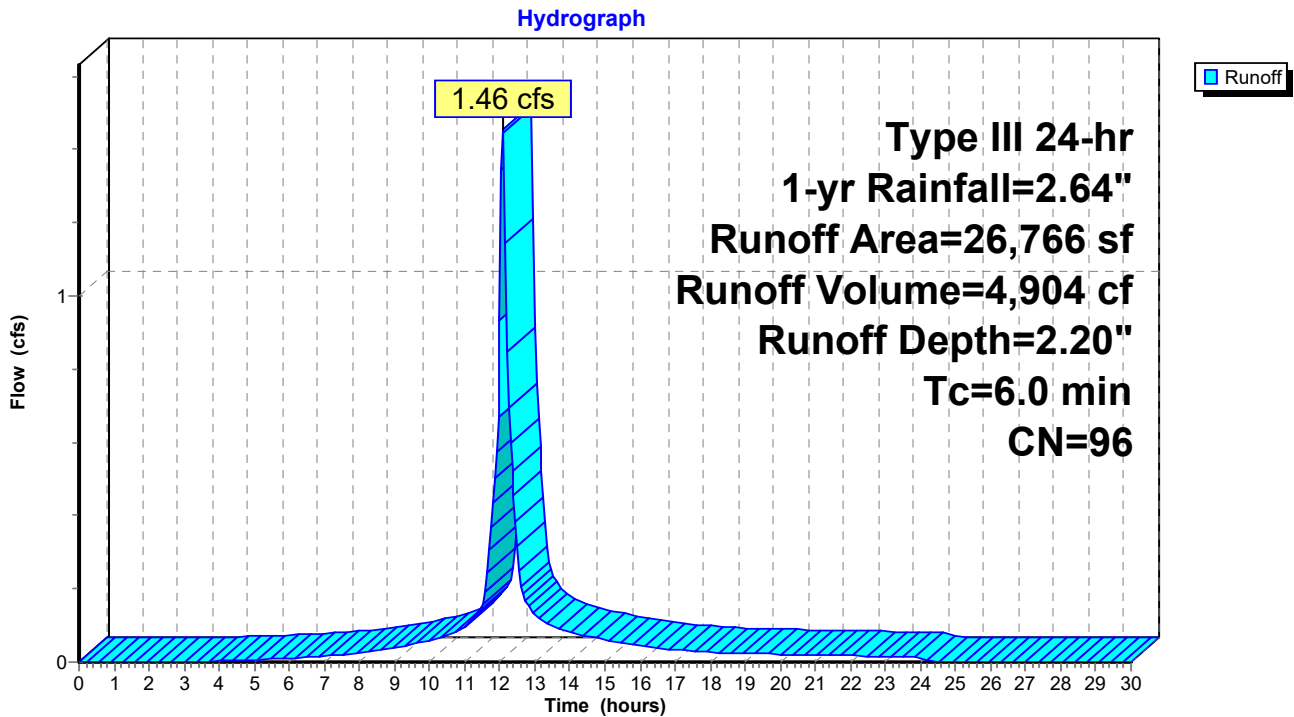
Runoff = 1.46 cfs @ 12.09 hrs, Volume= 4,904 cf, Depth= 2.20"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
23,545	98	Paved parking, HSG D
3,221	80	>75% Grass cover, Good, HSG D
26,766	96	Weighted Average
3,221		12.03% Pervious Area
23,545		87.97% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1C: PARKING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 7

**Summary for Subcatchment PW1D: ENTRANCE**

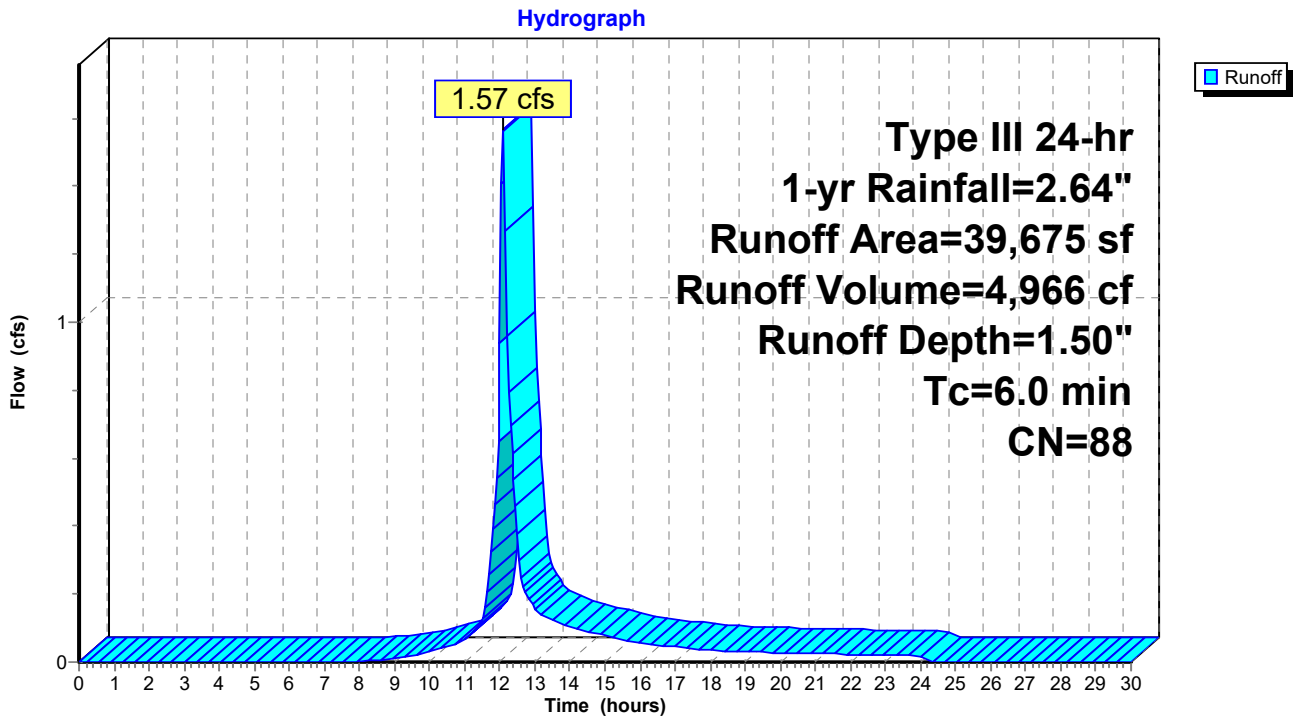
Runoff = 1.57 cfs @ 12.09 hrs, Volume= 4,966 cf, Depth= 1.50"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
17,739	98	Paved parking, HSG D
21,936	80	>75% Grass cover, Good, HSG D
39,675	88	Weighted Average
21,936		55.29% Pervious Area
17,739		44.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1D: ENTRANCE**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 8

**Summary for Subcatchment PW1E: TRAILERS**

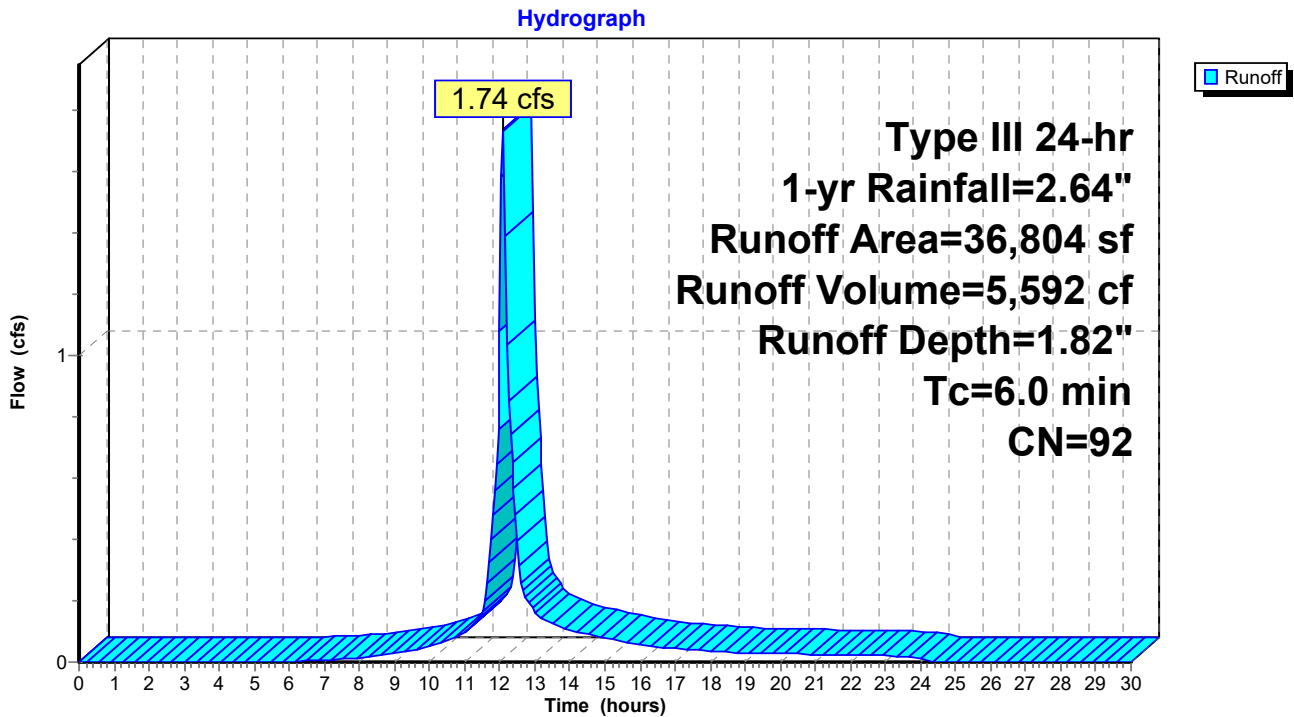
Runoff = 1.74 cfs @ 12.09 hrs, Volume= 5,592 cf, Depth= 1.82"  
 Routed to Pond 1E : BIO-1E

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
25,092	98	Paved parking, HSG D
11,712	80	>75% Grass cover, Good, HSG D
36,804	92	Weighted Average
11,712		31.82% Pervious Area
25,092		68.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1E: TRAILERS**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 9

**Summary for Subcatchment PW1F: TRAILER 2**

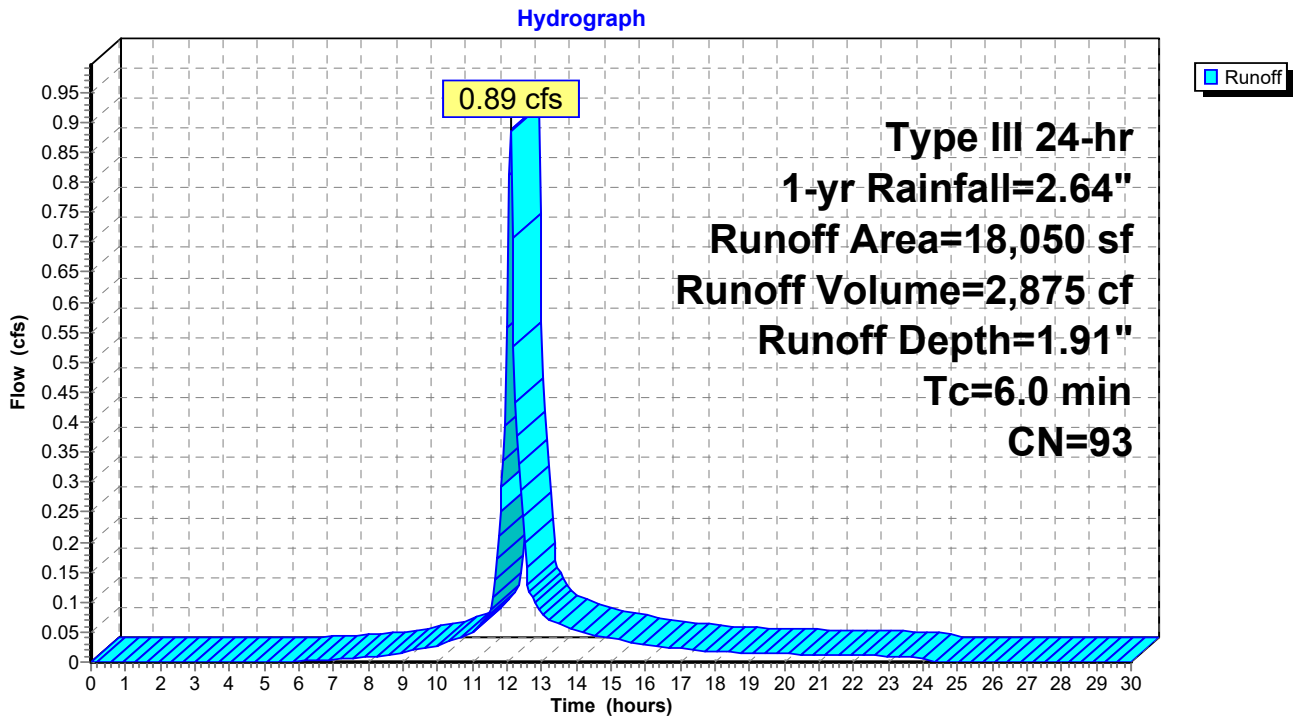
Runoff = 0.89 cfs @ 12.09 hrs, Volume= 2,875 cf, Depth= 1.91"  
 Routed to Pond 1F : BIO-1F

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
12,622	98	Paved parking, HSG D
5,428	80	>75% Grass cover, Good, HSG D
18,050	93	Weighted Average
5,428		30.07% Pervious Area
12,622		69.93% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1F: TRAILER 2**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 10

**Summary for Subcatchment PW1G: LOADING**

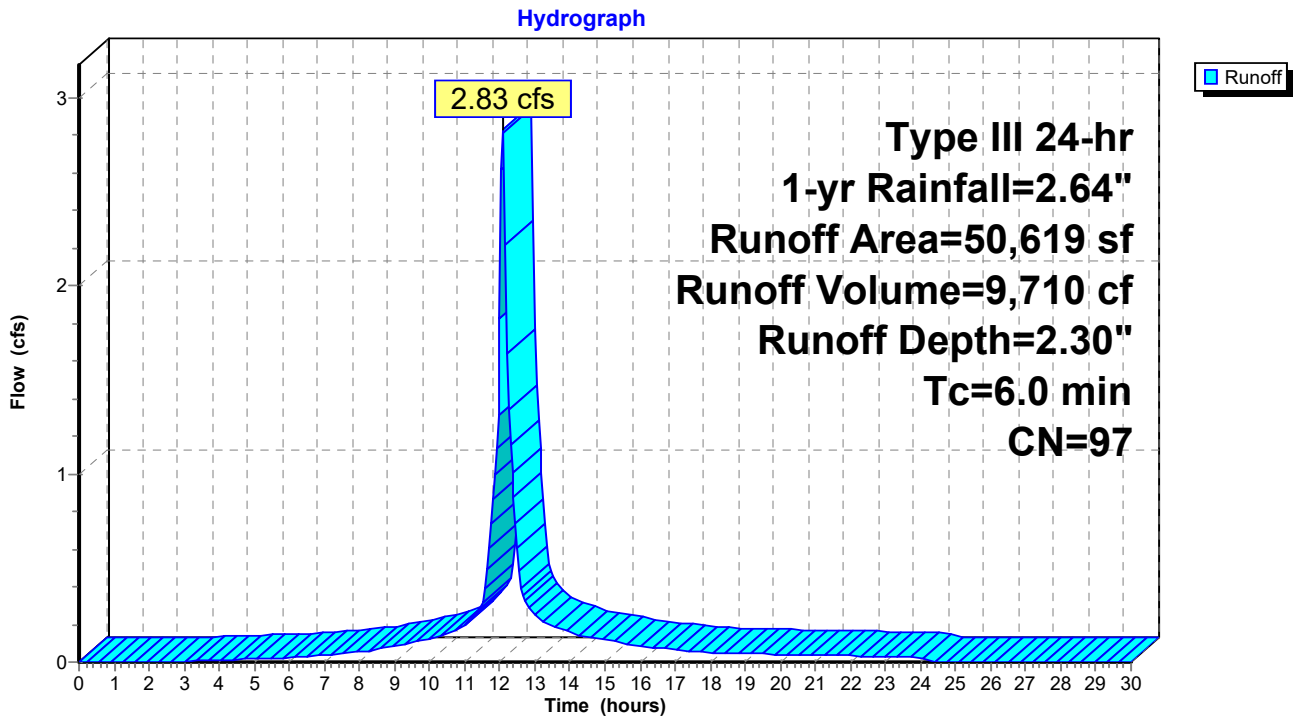
Runoff = 2.83 cfs @ 12.09 hrs, Volume= 9,710 cf, Depth= 2.30"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
46,810	98	Paved parking, HSG D
3,809	80	>75% Grass cover, Good, HSG D
50,619	97	Weighted Average
3,809		7.52% Pervious Area
46,810		92.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1G: LOADING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 11

**Summary for Subcatchment PW1H: NW CORNER BLDG**

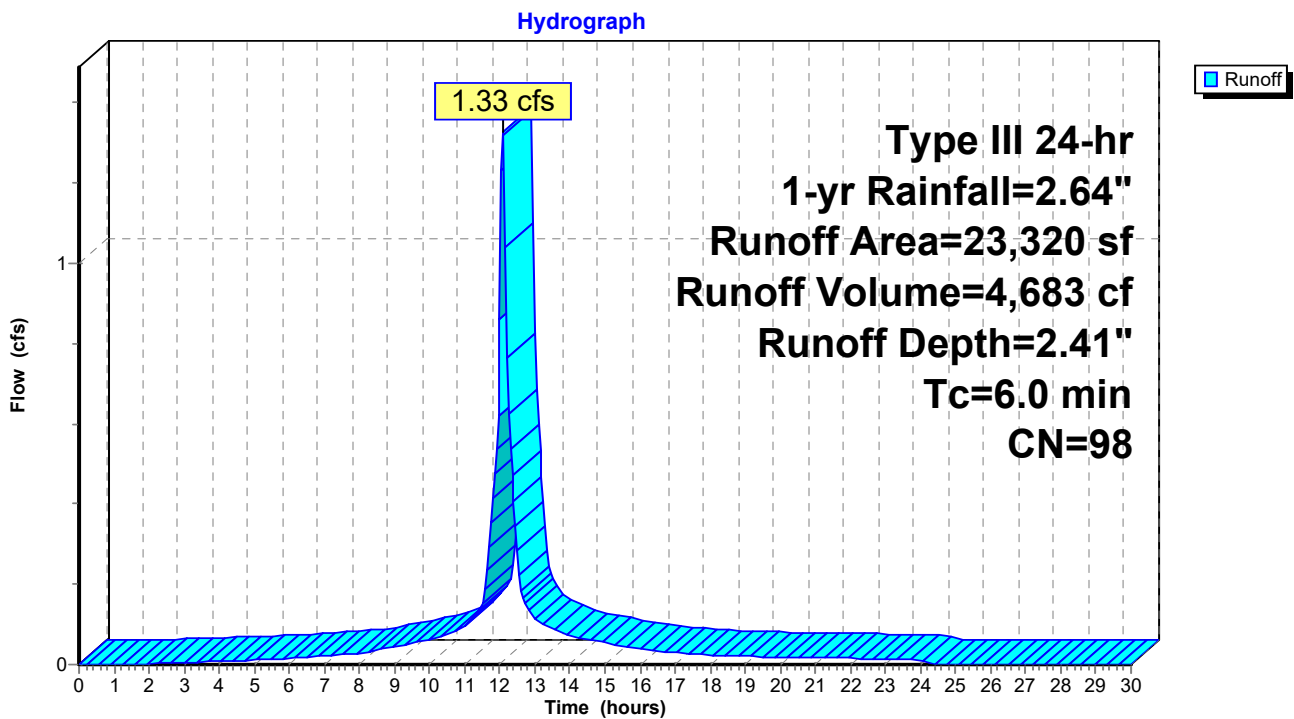
Runoff = 1.33 cfs @ 12.09 hrs, Volume= 4,683 cf, Depth= 2.41"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1-yr Rainfall=2.64"

Area (sf)	CN	Description
23,320	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
23,320	98	Weighted Average
23,320		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1H: NW CORNER BLDG**





**230119 - R1 - Dewpoint South**

Type III 24-hr 1-yr Rainfall=2.64"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 12

**Summary for Pond 1BN: BIO-1BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth = 1.74" for 1-yr event  
 Inflow = 3.11 cfs @ 12.09 hrs, Volume= 9,915 cf  
 Outflow = 0.65 cfs @ 12.53 hrs, Volume= 4,769 cf, Atten= 79%, Lag= 26.1 min  
 Primary = 0.65 cfs @ 12.53 hrs, Volume= 4,769 cf  
 Routed to Pond 2BN : BIO-2BN

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 492.56' @ 12.53 hrs Surf.Area= 2,898 sf Storage= 5,481 cf

Plug-Flow detention time= 267.6 min calculated for 4,761 cf (48% of inflow)  
 Center-of-Mass det. time= 154.4 min ( 964.2 - 809.9 )

Volume	Invert	Avail.Storage	Storage Description		
#1	490.00'	10,349 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
490.00	1,454	0	0	1,454	
492.00	2,555	3,958	3,958	2,611	
494.00	3,883	6,392	10,349	4,013	

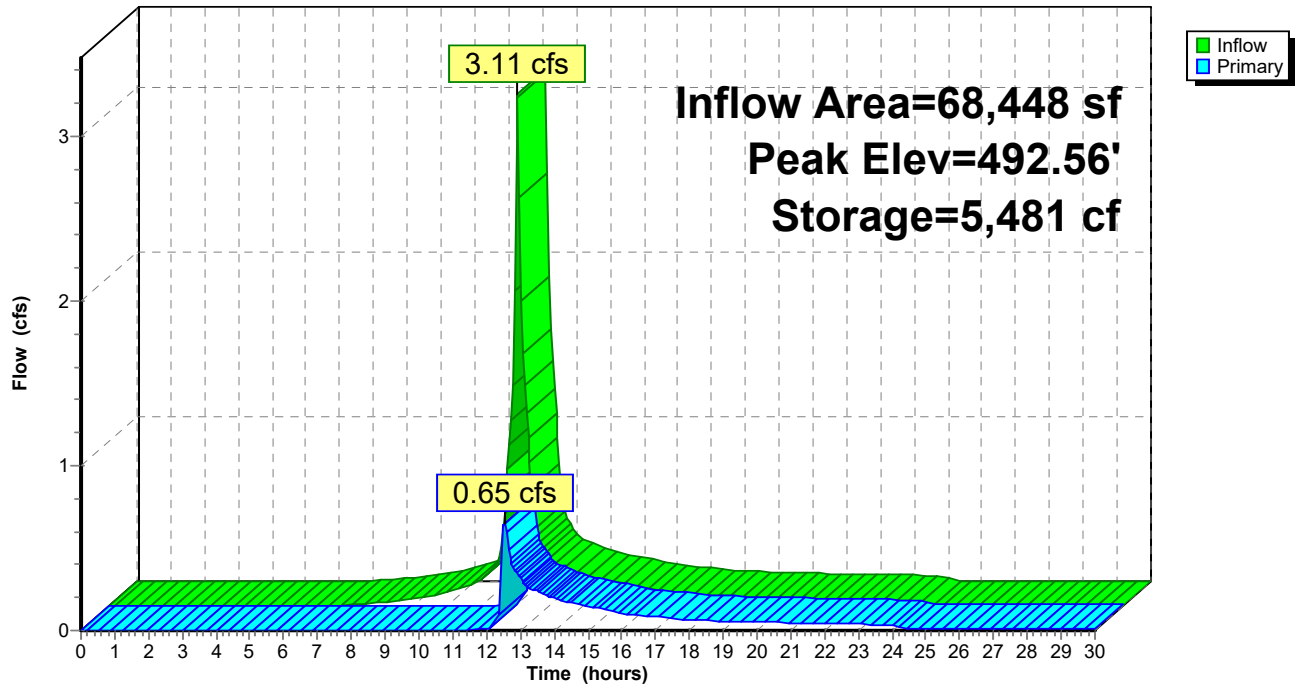
Device	Routing	Invert	Outlet Devices
#1	Primary	483.15'	<b>18.0" Round Culvert</b> L= 26.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 483.15' / 482.62' S= 0.0204 ' S= 0.0204 ' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	492.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	490.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.64 cfs @ 12.53 hrs HW=492.56' TW=484.06' (Dynamic Tailwater)

- 1=Culvert (Passes 0.64 cfs of 24.80 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 0.63 cfs @ 0.68 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 1BN: BIO-1BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 14

**Stage-Area-Storage for Pond 1BN: BIO-1BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
490.00	1,454	0	492.65	2,956	5,747
490.05	1,478	73	492.70	2,988	5,896
490.10	1,502	148	492.75	3,021	6,046
490.15	1,526	223	492.80	3,053	6,198
490.20	1,550	300	492.85	3,086	6,351
490.25	1,575	378	492.90	3,118	6,506
490.30	1,599	458	492.95	3,151	6,663
490.35	1,624	538	493.00	3,184	6,822
490.40	1,650	620	493.05	3,218	6,982
490.45	1,675	703	493.10	3,251	7,143
490.50	1,700	788	493.15	3,285	7,307
490.55	1,726	873	493.20	3,319	7,472
490.60	1,752	960	493.25	3,353	7,639
490.65	1,778	1,049	493.30	3,387	7,807
490.70	1,804	1,138	493.35	3,421	7,977
490.75	1,831	1,229	493.40	3,456	8,149
490.80	1,857	1,321	493.45	3,490	8,323
490.85	1,884	1,415	493.50	3,525	8,498
490.90	1,911	1,510	493.55	3,560	8,675
490.95	1,939	1,606	493.60	3,595	8,854
491.00	1,966	1,704	493.65	3,631	9,035
491.05	1,994	1,803	493.70	3,666	9,217
491.10	2,021	1,903	493.75	3,702	9,401
491.15	2,049	2,005	493.80	3,738	9,587
491.20	2,078	2,108	493.85	3,774	9,775
491.25	2,106	2,212	493.90	3,810	9,965
491.30	2,135	2,318	493.95	3,846	10,156
491.35	2,163	2,426	494.00	<b>3,883</b>	<b>10,349</b>
491.40	2,192	2,535			
491.45	2,221	2,645			
491.50	2,251	2,757			
491.55	2,280	2,870			
491.60	2,310	2,985			
491.65	2,340	3,101			
491.70	2,370	3,219			
491.75	2,401	3,338			
491.80	2,431	3,459			
491.85	2,462	3,581			
491.90	2,493	3,705			
491.95	2,524	3,831			
492.00	2,555	3,958			
492.05	2,585	4,086			
492.10	2,615	4,216			
492.15	2,645	4,348			
492.20	2,675	4,481			
492.25	2,706	4,615			
492.30	2,737	4,751			
492.35	2,767	4,889			
492.40	2,798	5,028			
492.45	2,830	5,169			
492.50	2,861	5,311			
492.55	2,893	5,455			
492.60	2,924	5,600			

**Summary for Pond 1D: BIO-1D**

Inflow Area = 89,761 sf, 71.97% Impervious, Inflow Depth = 1.95" for 1-yr event  
 Inflow = 4.36 cfs @ 12.09 hrs, Volume= 14,553 cf  
 Outflow = 2.93 cfs @ 12.19 hrs, Volume= 10,829 cf, Atten= 33%, Lag= 5.9 min  
 Primary = 2.93 cfs @ 12.19 hrs, Volume= 10,829 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.76' @ 12.19 hrs Surf.Area= 7,466 sf Storage= 5,326 cf

Plug-Flow detention time= 177.6 min calculated for 10,811 cf (74% of inflow)  
 Center-of-Mass det. time= 91.3 min ( 879.7 - 788.4 )

Volume	Invert	Avail.Storage	Storage Description		
#1	468.00'	15,581 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
468.00	6,529	0	0	6,529	
470.00	9,124	15,581	15,581	9,218	

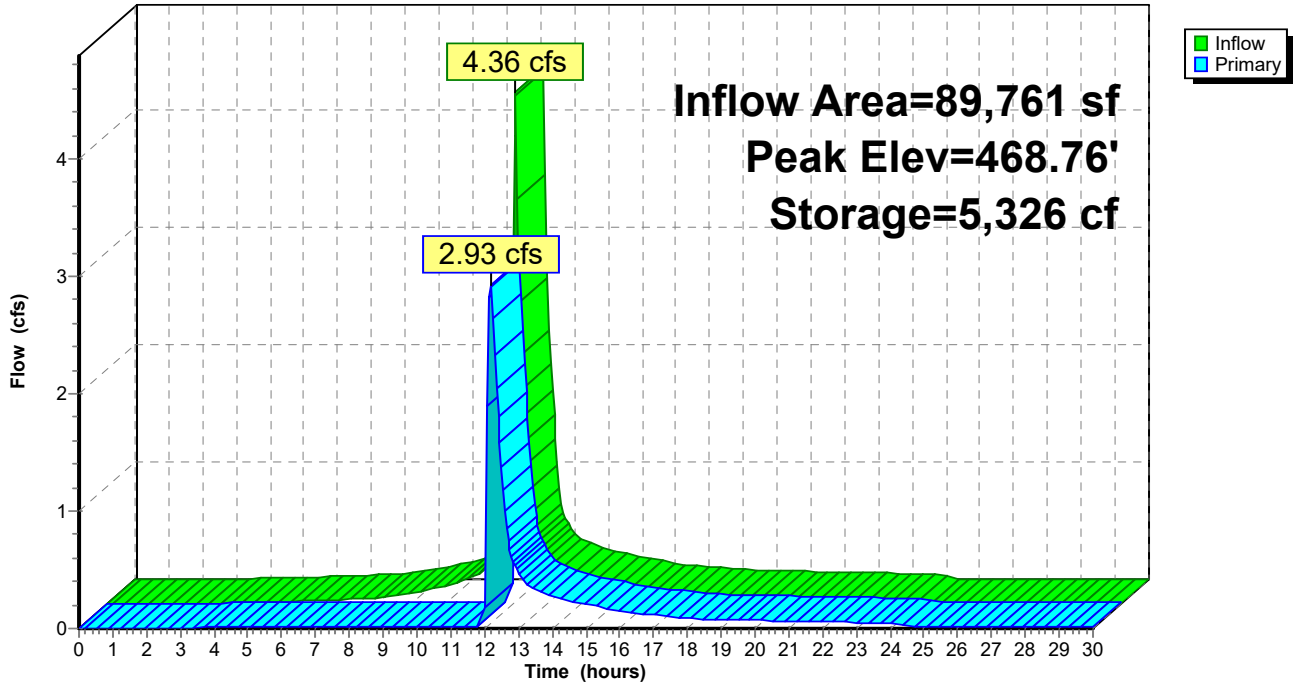
Device	Routing	Invert	Outlet Devices
#1	Primary	464.50'	<b>12.0" Round Culvert</b> L= 190.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 464.50' / 462.98' S= 0.0080 ' S= 0.0080 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.60'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	468.00'	<b>0.125 in/hr Exfiltration over Surface area</b>
#4	Primary	469.00'	<b>10.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83

**Primary OutFlow** Max=2.90 cfs @ 12.19 hrs HW=468.76' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 2.90 cfs of 5.37 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 2.88 cfs @ 1.12 fps)
- 3=Exfiltration (Exfiltration Controls 0.02 cfs)
- 4=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

Pond 1D: BIO-1D

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 17

**Stage-Area-Storage for Pond 1D: BIO-1D**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
468.00	6,529	0	469.06	7,850	7,610
468.02	6,553	131	469.08	7,876	7,768
468.04	6,577	262	469.10	7,903	7,925
468.06	6,601	394	469.12	7,929	8,084
468.08	6,624	526	469.14	7,955	8,243
468.10	6,648	659	469.16	7,981	8,402
468.12	6,672	792	469.18	8,008	8,562
468.14	6,697	926	469.20	8,034	8,722
468.16	6,721	1,060	469.22	8,060	8,883
468.18	6,745	1,195	469.24	8,087	9,045
468.20	6,769	1,330	469.26	8,113	9,207
468.22	6,793	1,465	469.28	8,140	9,369
468.24	6,818	1,601	469.30	8,166	9,532
468.26	6,842	1,738	469.32	8,193	9,696
468.28	6,866	1,875	469.34	8,220	9,860
468.30	6,891	2,013	469.36	8,246	10,025
468.32	6,915	2,151	469.38	8,273	10,190
468.34	6,940	2,289	469.40	8,300	10,356
468.36	6,964	2,428	469.42	8,327	10,522
468.38	6,989	2,568	469.44	8,354	10,689
468.40	7,013	2,708	469.46	8,381	10,856
468.42	7,038	2,848	469.48	8,408	11,024
468.44	7,063	2,989	469.50	8,435	11,192
468.46	7,087	3,131	469.52	8,462	11,361
468.48	7,112	3,273	469.54	8,489	11,531
468.50	7,137	3,415	469.56	8,516	11,701
468.52	7,162	3,558	469.58	8,543	11,871
468.54	7,187	3,702	469.60	8,570	12,043
468.56	7,212	3,846	469.62	8,598	12,214
468.58	7,237	3,990	469.64	8,625	12,386
468.60	7,262	4,135	469.66	8,652	12,559
468.62	7,287	4,281	469.68	8,680	12,733
468.64	7,312	4,427	469.70	8,707	12,906
468.66	7,337	4,573	469.72	8,735	13,081
468.68	7,363	4,720	469.74	8,762	13,256
468.70	7,388	4,868	469.76	8,790	13,431
468.72	7,413	5,016	469.78	8,817	13,607
468.74	7,439	5,164	469.80	8,845	13,784
468.76	7,464	5,313	469.82	8,873	13,961
468.78	7,490	5,463	469.84	8,900	14,139
468.80	7,515	5,613	469.86	8,928	14,317
468.82	7,541	5,764	469.88	8,956	14,496
468.84	7,566	5,915	469.90	8,984	14,675
468.86	7,592	6,066	469.92	9,012	14,855
468.88	7,617	6,218	469.94	9,040	15,036
468.90	7,643	6,371	469.96	9,068	15,217
468.92	7,669	6,524	469.98	9,096	15,399
468.94	7,695	6,678	470.00	<b>9,124</b>	<b>15,581</b>
468.96	7,721	6,832			
468.98	7,746	6,986			
469.00	7,772	7,142			
469.02	7,798	7,297			
469.04	7,824	7,454			

**230119 - R1 - Dewpoint South**

Type III 24-hr 1-yr Rainfall=2.64"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 18

**Summary for Pond 1E: BIO-1E**

Inflow Area = 36,804 sf, 68.18% Impervious, Inflow Depth = 1.82" for 1-yr event  
 Inflow = 1.74 cfs @ 12.09 hrs, Volume= 5,592 cf  
 Outflow = 0.01 cfs @ 24.07 hrs, Volume= 913 cf, Atten= 99%, Lag= 718.6 min  
 Primary = 0.01 cfs @ 24.07 hrs, Volume= 913 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.41' @ 24.07 hrs Surf.Area= 4,059 sf Storage= 4,927 cf

Plug-Flow detention time= 509.9 min calculated for 913 cf (16% of inflow)  
 Center-of-Mass det. time= 334.0 min ( 1,138.8 - 804.9 )

Volume	Invert	Avail.Storage	Storage Description		
#1	467.00'	12,471 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
467.00	2,940	0	0	2,940	
468.00	3,728	3,326	3,326	3,761	
470.00	5,472	9,144	12,471	5,587	

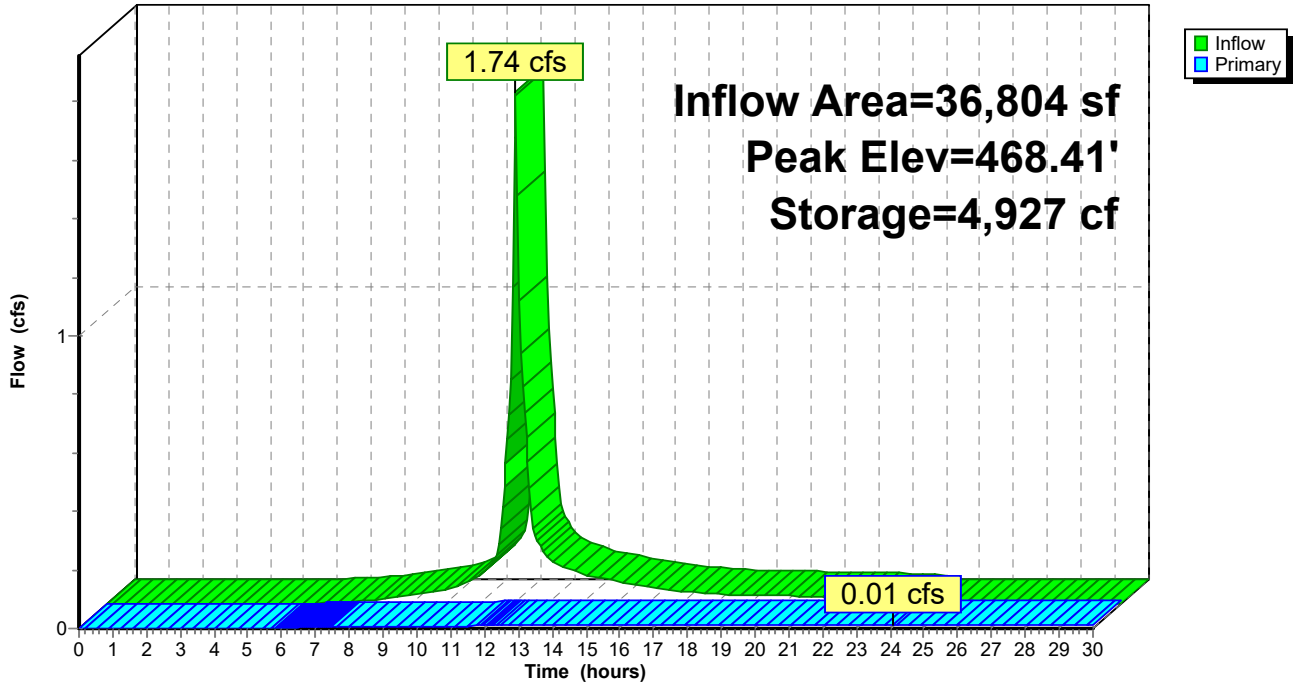
Device	Routing	Invert	Outlet Devices
#1	Primary	463.50'	<b>12.0" Round Culvert</b> L= 23.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 463.50' / 462.93' S= 0.0248 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	467.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.01 cfs @ 24.07 hrs HW=468.41' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.01 cfs of 7.94 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1E: BIO-1E

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 20

**Stage-Area-Storage for Pond 1E: BIO-1E**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
467.00	2,940	0	469.65	5,143	10,613
467.05	2,977	148	469.70	5,189	10,872
467.10	3,015	298	469.75	5,236	11,132
467.15	3,052	449	469.80	5,283	11,395
467.20	3,090	603	469.85	5,330	11,661
467.25	3,128	758	469.90	5,377	11,928
467.30	3,167	916	469.95	5,424	12,198
467.35	3,205	1,075	470.00	<b>5,472</b>	<b>12,471</b>
467.40	3,244	1,236			
467.45	3,283	1,399			
467.50	3,322	1,565			
467.55	3,362	1,732			
467.60	3,402	1,901			
467.65	3,442	2,072			
467.70	3,482	2,245			
467.75	3,522	2,420			
467.80	3,563	2,597			
467.85	3,604	2,776			
467.90	3,645	2,958			
467.95	3,686	3,141			
468.00	3,728	3,326			
468.05	3,768	3,514			
468.10	3,807	3,703			
468.15	3,847	3,894			
468.20	3,887	4,088			
468.25	3,928	4,283			
468.30	3,968	4,480			
468.35	4,009	4,680			
468.40	4,050	4,881			
468.45	4,091	5,085			
468.50	4,133	5,291			
468.55	4,174	5,498			
468.60	4,216	5,708			
468.65	4,258	5,920			
468.70	4,300	6,134			
468.75	4,343	6,350			
468.80	4,386	6,568			
468.85	4,428	6,788			
468.90	4,472	7,011			
468.95	4,515	7,236			
469.00	4,558	7,462			
469.05	4,602	7,691			
469.10	4,646	7,923			
469.15	4,690	8,156			
469.20	4,734	8,392			
469.25	4,779	8,629			
469.30	4,824	8,870			
469.35	4,869	9,112			
469.40	4,914	9,356			
469.45	4,959	9,603			
469.50	5,005	9,852			
469.55	5,051	10,104			
469.60	5,097	10,357			

**230119 - R1 - Dewpoint South**

Type III 24-hr 1-yr Rainfall=2.64"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 21

**Summary for Pond 1F: BIO-1F**

Inflow Area = 18,050 sf, 69.93% Impervious, Inflow Depth = 1.91" for 1-yr event  
 Inflow = 0.89 cfs @ 12.09 hrs, Volume= 2,875 cf  
 Outflow = 0.01 cfs @ 24.06 hrs, Volume= 484 cf, Atten= 99%, Lag= 718.2 min  
 Primary = 0.01 cfs @ 24.06 hrs, Volume= 484 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 478.44' @ 24.06 hrs Surf.Area= 2,183 sf Storage= 2,524 cf

Plug-Flow detention time= 522.5 min calculated for 484 cf (17% of inflow)  
 Center-of-Mass det. time= 342.1 min ( 1,141.6 - 799.5 )

Volume	Invert	Avail.Storage	Storage Description		
#1	477.00'	6,744 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
477.00	1,347	0	0	1,347	
478.00	1,919	1,625	1,625	1,941	
480.00	3,259	5,119	6,744	3,341	

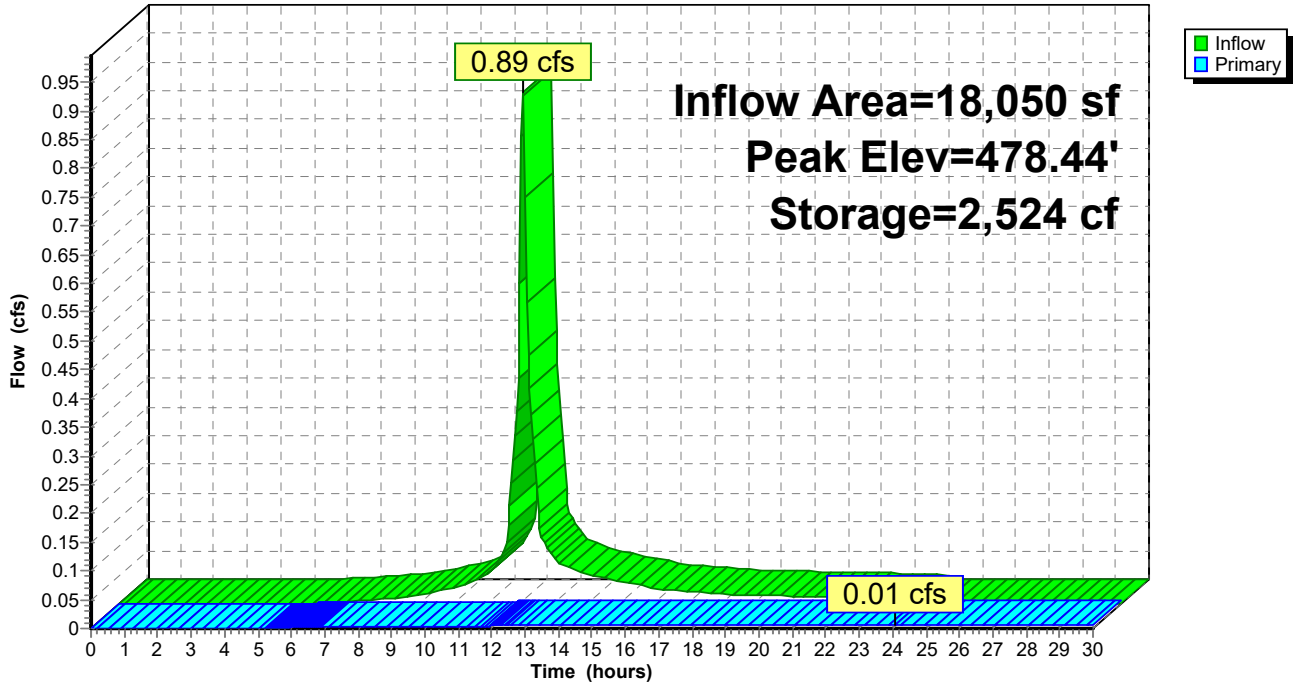
Device	Routing	Invert	Outlet Devices
#1	Primary	473.50'	<b>12.0" Round Culvert</b> L= 115.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 473.50' / 471.21' S= 0.0199 ' S= 0.0199 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	478.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	477.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.01 cfs @ 24.06 hrs HW=478.44' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.01 cfs of 7.35 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 1F: BIO-1F

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 23

**Stage-Area-Storage for Pond 1F: BIO-1F**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
477.00	1,347	0	479.65	2,999	5,649
477.05	1,373	68	479.70	3,036	5,800
477.10	1,400	137	479.75	3,072	5,953
477.15	1,426	208	479.80	3,109	6,107
477.20	1,453	280	479.85	3,146	6,263
477.25	1,481	353	479.90	3,184	6,422
477.30	1,508	428	479.95	3,221	6,582
477.35	1,536	504	480.00	<b>3,259</b>	<b>6,744</b>
477.40	1,564	582			
477.45	1,592	660			
477.50	1,620	741			
477.55	1,649	823			
477.60	1,678	906			
477.65	1,707	990			
477.70	1,737	1,076			
477.75	1,767	1,164			
477.80	1,797	1,253			
477.85	1,827	1,344			
477.90	1,857	1,436			
477.95	1,888	1,529			
478.00	1,919	1,625			
478.05	1,948	1,721			
478.10	1,978	1,819			
478.15	2,007	1,919			
478.20	2,037	2,020			
478.25	2,067	2,123			
478.30	2,098	2,227			
478.35	2,128	2,333			
478.40	2,159	2,440			
478.45	2,190	2,548			
478.50	2,221	2,659			
478.55	2,252	2,770			
478.60	2,284	2,884			
478.65	2,316	2,999			
478.70	2,348	3,115			
478.75	2,380	3,234			
478.80	2,413	3,353			
478.85	2,445	3,475			
478.90	2,478	3,598			
478.95	2,512	3,723			
479.00	2,545	3,849			
479.05	2,579	3,977			
479.10	2,612	4,107			
479.15	2,646	4,239			
479.20	2,681	4,372			
479.25	2,715	4,507			
479.30	2,750	4,643			
479.35	2,785	4,782			
479.40	2,820	4,922			
479.45	2,855	5,064			
479.50	2,891	5,207			
479.55	2,927	5,353			
479.60	2,963	5,500			

**230119 - R1 - Dewpoint South**

Type III 24-hr 1-yr Rainfall=2.64"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 24

**Summary for Pond 2BN: BIO-2BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth > 0.84" for 1-yr event  
 Inflow = 0.65 cfs @ 12.53 hrs, Volume= 4,769 cf  
 Outflow = 0.14 cfs @ 15.07 hrs, Volume= 3,260 cf, Atten= 78%, Lag= 152.4 min  
 Primary = 0.14 cfs @ 15.07 hrs, Volume= 3,260 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 484.62' @ 15.07 hrs Surf.Area= 3,262 sf Storage= 1,895 cf

Plug-Flow detention time= 266.6 min calculated for 3,260 cf (68% of inflow)  
 Center-of-Mass det. time= 134.4 min ( 1,098.6 - 964.2 )

Volume	Invert	Avail.Storage	Storage Description		
#1	484.00'	17,309 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
484.00	2,843	0	0	2,843	
486.00	4,295	7,088	7,088	4,371	
488.00	5,972	10,221	17,309	6,142	

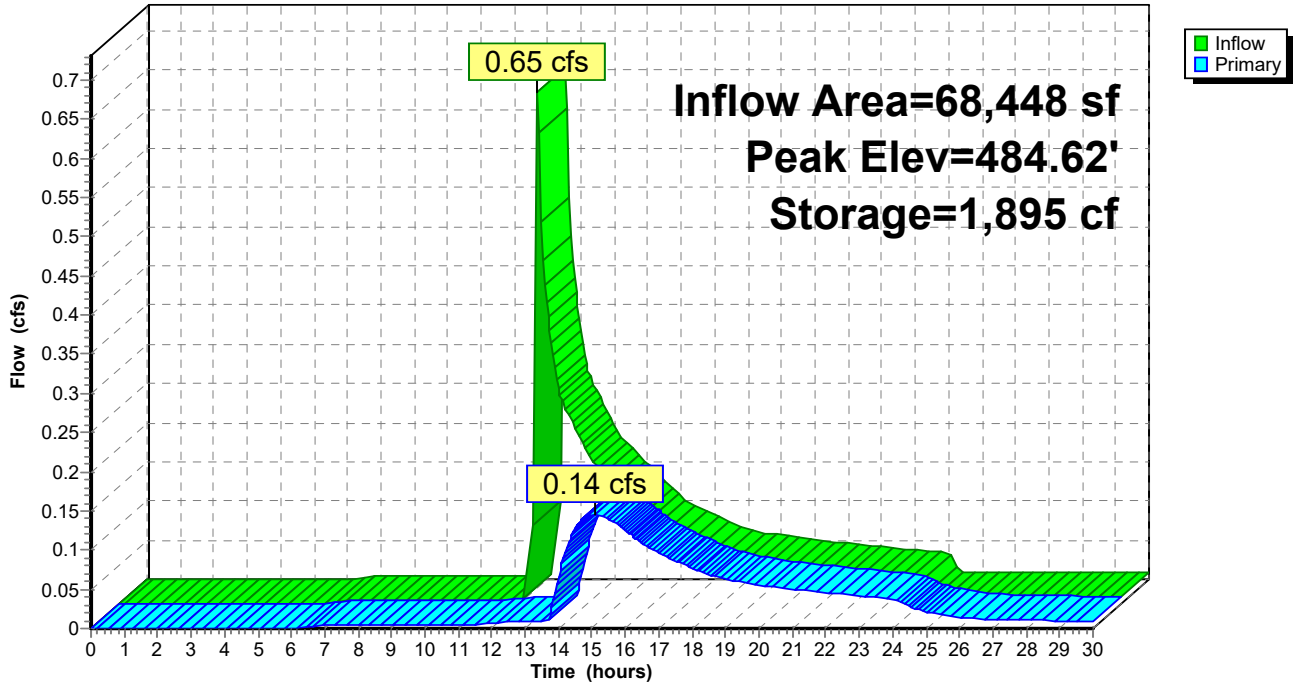
Device	Routing	Invert	Outlet Devices
#1	Primary	480.50'	<b>18.0" Round Culvert</b> L= 52.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 480.50' / 478.00' S= 0.0481 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	486.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	484.50'	<b>12.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	484.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.14 cfs @ 15.07 hrs HW=484.62' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.14 cfs of 15.62 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Orifice/Grate (Orifice Controls 0.14 cfs @ 1.12 fps)
- 4=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 2BN: BIO-2BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 26

**Stage-Area-Storage for Pond 2BN: BIO-2BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
484.00	2,843	0	486.65	4,810	10,046
484.05	2,876	143	486.70	4,851	10,287
484.10	2,909	288	486.75	4,892	10,531
484.15	2,942	434	486.80	4,933	10,776
484.20	2,975	582	486.85	4,974	11,024
484.25	3,008	731	486.90	5,016	11,274
484.30	3,042	883	486.95	5,057	11,526
484.35	3,076	1,035	487.00	5,099	11,780
484.40	3,110	1,190	487.05	5,141	12,036
484.45	3,144	1,346	487.10	5,183	12,294
484.50	3,178	1,504	487.15	5,226	12,554
484.55	3,213	1,664	487.20	5,268	12,816
484.60	3,247	1,826	487.25	5,311	13,081
484.65	3,282	1,989	487.30	5,354	13,347
484.70	3,317	2,154	487.35	5,397	13,616
484.75	3,353	2,321	487.40	5,440	13,887
484.80	3,388	2,489	487.45	5,483	14,160
484.85	3,424	2,659	487.50	5,527	14,435
484.90	3,459	2,832	487.55	5,571	14,713
484.95	3,495	3,005	487.60	5,615	14,992
485.00	3,532	3,181	487.65	5,659	15,274
485.05	3,568	3,359	487.70	5,703	15,558
485.10	3,605	3,538	487.75	5,747	15,844
485.15	3,641	3,719	487.80	5,792	16,133
485.20	3,678	3,902	487.85	5,837	16,424
485.25	3,716	4,087	487.90	5,882	16,717
485.30	3,753	4,274	487.95	5,927	17,012
485.35	3,790	4,462	488.00	<b>5,972</b>	<b>17,309</b>
485.40	3,828	4,653			
485.45	3,866	4,845			
485.50	3,904	5,039			
485.55	3,942	5,235			
485.60	3,981	5,434			
485.65	4,019	5,634			
485.70	4,058	5,835			
485.75	4,097	6,039			
485.80	4,136	6,245			
485.85	4,176	6,453			
485.90	4,215	6,663			
485.95	4,255	6,875			
486.00	4,295	7,088			
486.05	4,334	7,304			
486.10	4,372	7,522			
486.15	4,411	7,741			
486.20	4,450	7,963			
486.25	4,490	8,186			
486.30	4,529	8,412			
486.35	4,569	8,639			
486.40	4,608	8,869			
486.45	4,648	9,100			
486.50	4,688	9,333			
486.55	4,729	9,569			
486.60	4,769	9,806			

**Summary for Pond SUBS: SUBS**

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth = 2.36" for 1-yr event  
 Inflow = 6.40 cfs @ 12.09 hrs, Volume= 22,270 cf  
 Outflow = 0.55 cfs @ 13.01 hrs, Volume= 22,073 cf, Atten= 91%, Lag= 55.7 min  
 Primary = 0.55 cfs @ 13.01 hrs, Volume= 22,073 cf  
 Routed to Link JF : JELLY FISH  
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 476.86' @ 13.01 hrs Surf.Area= 8,608 sf Storage= 10,797 cf

Plug-Flow detention time= 224.9 min calculated for 22,073 cf (99% of inflow)  
 Center-of-Mass det. time= 219.1 min ( 984.3 - 765.2 )

Volume	Invert	Avail.Storage	Storage Description
#1A	475.00'	13,785 cf	<b>83.00'W x 103.72'L x 6.75'H Field A</b> 58,107 cf Overall - 23,645 cf Embedded = 34,463 cf x 40.0% Voids
#2A	475.75'	23,645 cf	<b>ADS_StormTech MC-4500 +Cap x 216 Inside #1</b> Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 216 Chambers in 9 Rows Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf
		37,430 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	472.00'	<b>12.0" Round Culvert</b> L= 30.9' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 472.00' / 471.69' S= 0.0100 1/ S= 0.0100 1/ Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	475.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Device 1	480.25'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Secondary	479.00'	<b>18.0" Round Culvert</b> L= 46.5' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 479.00' / 477.56' S= 0.0310 1/ Cc= 0.900 n= 0.012, Flow Area= 1.77 sf

**Primary OutFlow** Max=0.55 cfs @ 13.01 hrs HW=476.86' TW=0.00' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 0.55 cfs of 9.04 cfs potential flow)
- ↑ 2=Orifice/Grate (Orifice Controls 0.55 cfs @ 6.27 fps)
- ↑ 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=475.00' TW=0.00' (Dynamic Tailwater)

- ↑ 4=Culvert ( Controls 0.00 cfs)



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 28

**Pond SUBS: SUBS - Chamber Wizard Field A**

**Chamber Model = ADS\_StormTech MC-4500 +Cap (ADS StormTech® MC-4500 with cap, use MC-4500 b for new designs)**

Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf

Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap

Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf

100.0" Wide + 9.0" Spacing = 109.0" C-C Row Spacing

24 Chambers/Row x 4.02' Long +2.56' Cap Length x 2 = 101.72' Row Length +12.0" End Stone x 2 = 103.72' Base Length

9 Rows x 100.0" Wide + 9.0" Spacing x 8 + 12.0" Side Stone x 2 = 83.00' Base Width

9.0" Stone Base + 60.0" Chamber Height + 12.0" Stone Cover = 6.75' Field Height

216 Chambers x 106.5 cf + 35.7 cf Cap Volume x 2 x 9 Rows = 23,644.5 cf Chamber Storage

58,107.3 cf Field - 23,644.5 cf Chambers = 34,462.7 cf Stone x 40.0% Voids = 13,785.1 cf Stone Storage

Chamber Storage + Stone Storage = 37,429.6 cf = 0.859 af

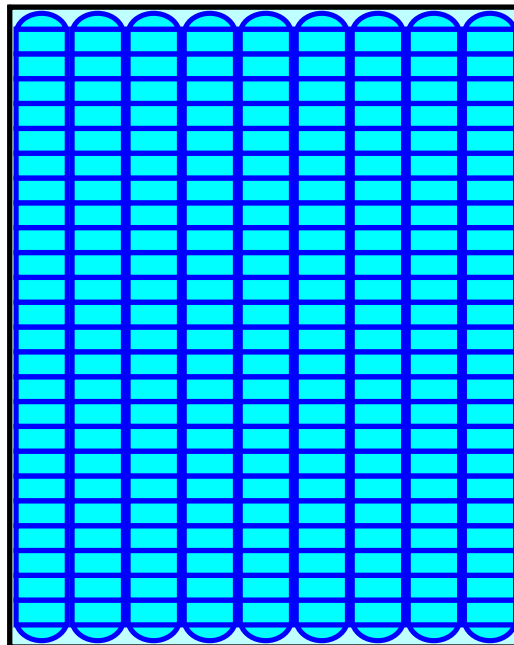
Overall Storage Efficiency = 64.4%

Overall System Size = 103.72' x 83.00' x 6.75'

216 Chambers

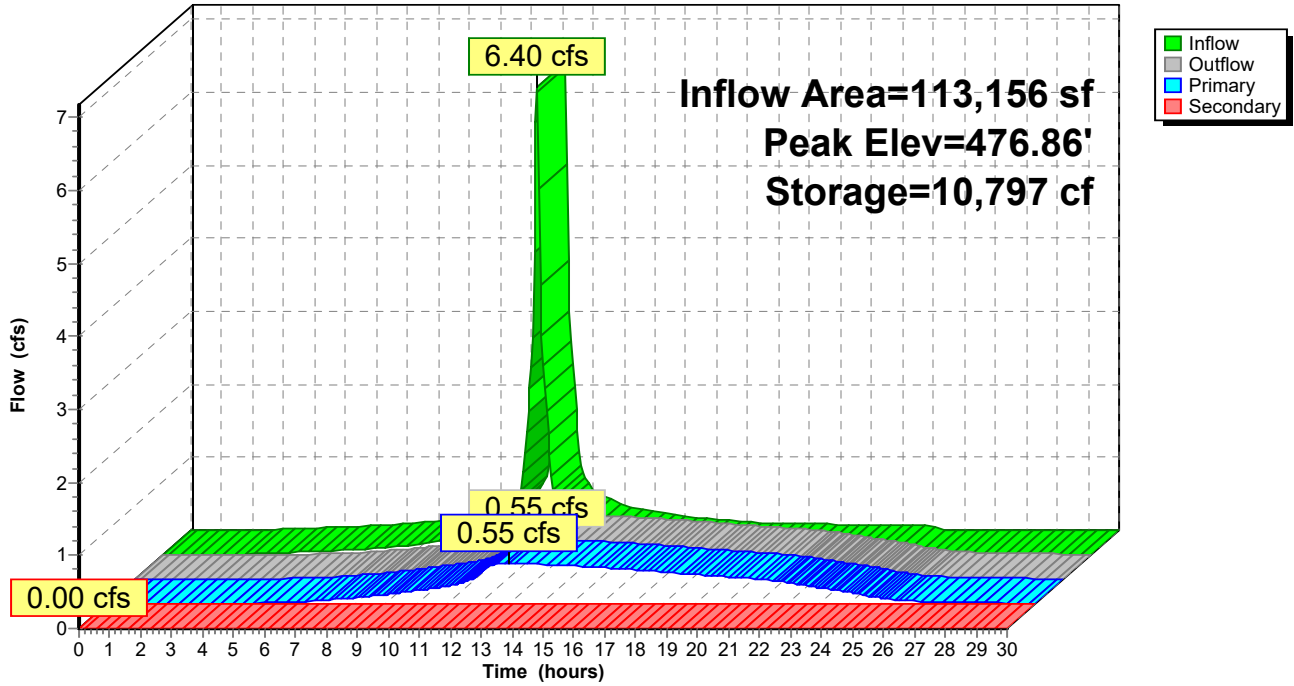
2,152.1 cy Field

1,276.4 cy Stone



### Pond SUBS: SUBS

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 1-yr Rainfall=2.64"

Printed 2/2/2023

Page 30

**Stage-Area-Storage for Pond SUBS: SUBS**

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
475.00	0	477.65	16,390	480.30	32,305
475.05	172	477.70	16,738	480.35	32,508
475.10	344	477.75	17,084	480.40	32,704
475.15	517	477.80	17,429	480.45	32,895
475.20	689	477.85	17,773	480.50	33,084
475.25	861	477.90	18,115	480.55	33,270
475.30	1,033	477.95	18,457	480.60	33,453
475.35	1,205	478.00	18,797	480.65	33,634
475.40	1,377	478.05	19,136	480.70	33,812
475.45	1,550	478.10	19,474	480.75	33,986
475.50	1,722	478.15	19,810	480.80	34,158
475.55	1,894	478.20	20,145	480.85	34,331
475.60	2,066	478.25	20,478	480.90	34,503
475.65	2,238	478.30	20,811	480.95	34,675
475.70	2,410	478.35	21,141	481.00	34,847
475.75	2,583	478.40	21,470	481.05	35,019
475.80	2,957	478.45	21,798	481.10	35,191
475.85	3,330	478.50	22,124	481.15	35,364
475.90	3,704	478.55	22,449	481.20	35,536
475.95	4,077	478.60	22,771	481.25	35,708
476.00	4,449	478.65	23,093	481.30	35,880
476.05	4,821	478.70	23,412	481.35	36,052
476.10	5,193	478.75	23,730	481.40	36,224
476.15	5,564	478.80	24,045	481.45	36,397
476.20	5,934	478.85	24,360	481.50	36,569
476.25	6,304	478.90	24,672	481.55	36,741
476.30	6,674	478.95	24,982	481.60	36,913
476.35	7,043	479.00	25,290	481.65	37,085
476.40	7,411	479.05	25,596	481.70	37,257
476.45	7,779	479.10	25,900	481.75	<b>37,430</b>
476.50	8,147	479.15	26,202		
476.55	8,513	479.20	26,501		
476.60	8,879	479.25	26,798		
476.65	9,245	479.30	27,093		
476.70	9,610	479.35	27,386		
476.75	9,974	479.40	27,675		
476.80	10,338	479.45	27,963		
476.85	10,700	479.50	28,247		
476.90	11,062	479.55	28,529		
476.95	11,424	479.60	28,808		
477.00	11,784	479.65	29,084		
477.05	12,144	479.70	29,357		
477.10	12,503	479.75	29,627		
477.15	12,861	479.80	29,893		
477.20	13,218	479.85	30,156		
477.25	13,574	479.90	30,414		
477.30	13,930	479.95	30,669		
477.35	14,284	480.00	30,920		
477.40	14,638	480.05	31,166		
477.45	14,990	480.10	31,407		
477.50	15,342	480.15	31,643		
477.55	15,692	480.20	31,872		
477.60	16,042	480.25	32,093		

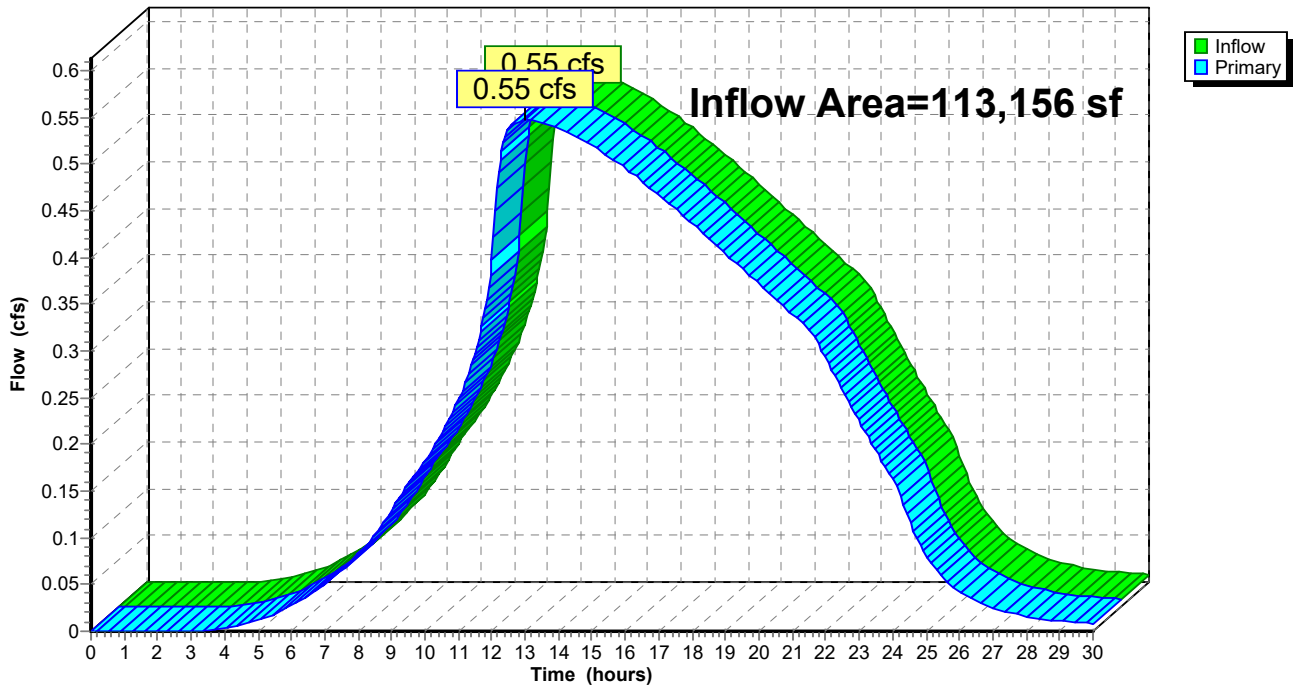
### Summary for Link JF: JELLY FISH

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth > 2.34" for 1-yr event  
Inflow = 0.55 cfs @ 13.01 hrs, Volume= 22,073 cf  
Primary = 0.55 cfs @ 13.01 hrs, Volume= 22,073 cf, Atten= 0%, Lag= 0.0 min  
Routed to Link PROP : PROPOSED

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link JF: JELLY FISH

Hydrograph

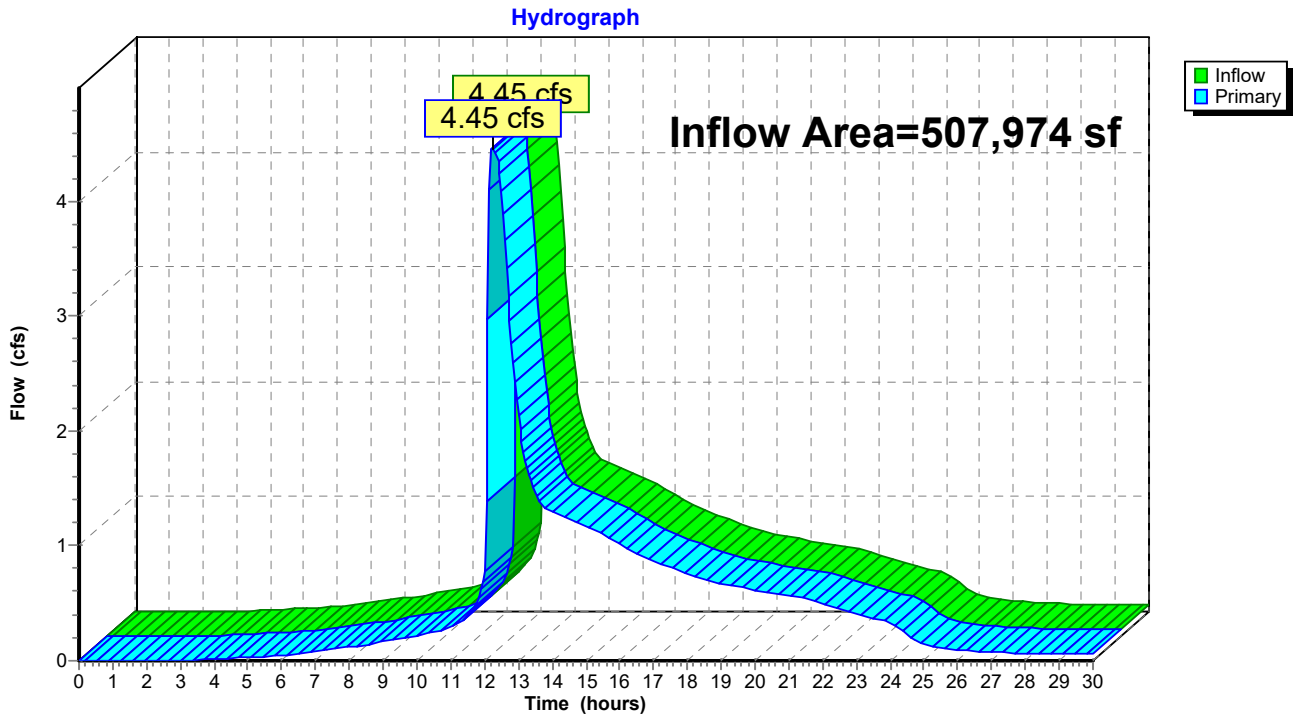


### Summary for Link PROP: PROPOSED

Inflow Area = 507,974 sf, 50.18% Impervious, Inflow Depth > 1.20" for 1-yr event  
Inflow = 4.45 cfs @ 12.23 hrs, Volume= 50,889 cf  
Primary = 4.45 cfs @ 12.23 hrs, Volume= 50,889 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link PROP: PROPOSED



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 33

**Summary for Subcatchment PW1A: LOD**

Runoff = 3.15 cfs @ 12.51 hrs, Volume= 18,954 cf, Depth= 1.25"  
 Routed to Link PROP : PROPOSED

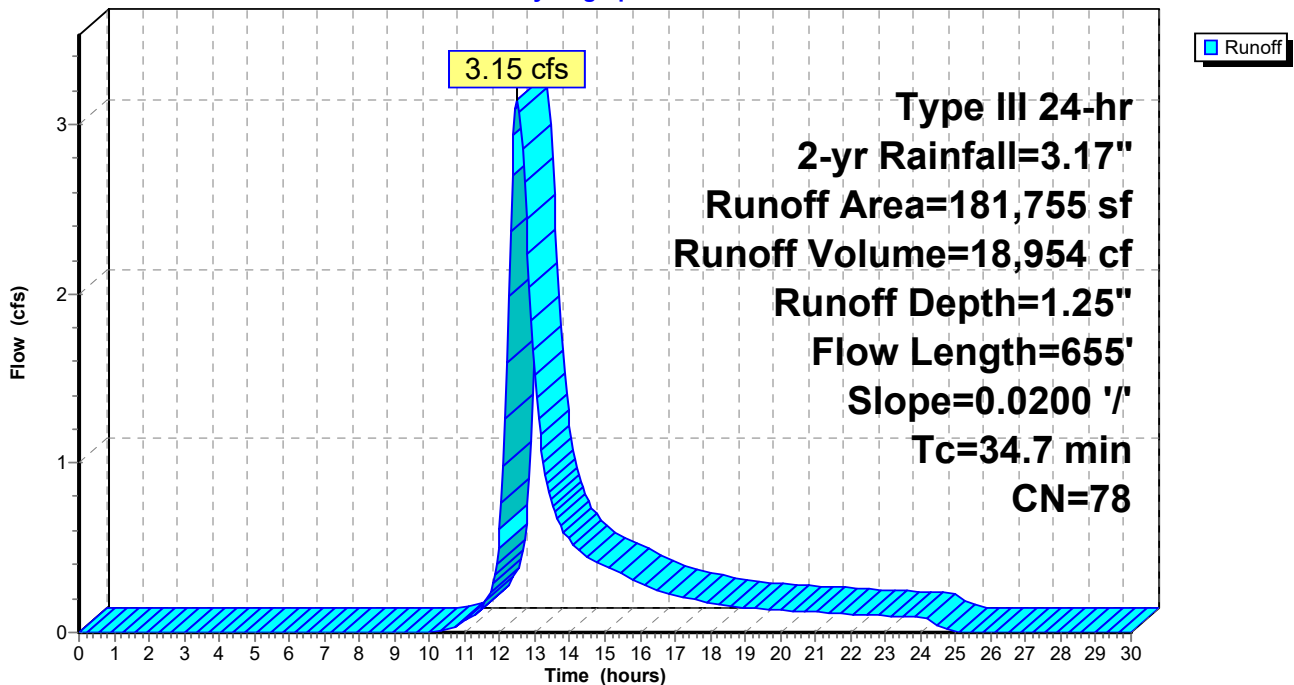
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
2,800	98	Paved parking, HSG D
73,077	80	>75% Grass cover, Good, HSG D
22,724	73	Brush, Good, HSG D
83,154	77	Woods, Good, HSG D
181,755	78	Weighted Average
178,955		98.46% Pervious Area
2,800		1.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment PW1A: LOD**

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 34

**Summary for Subcatchment PW1BN: N HALF BLDG**

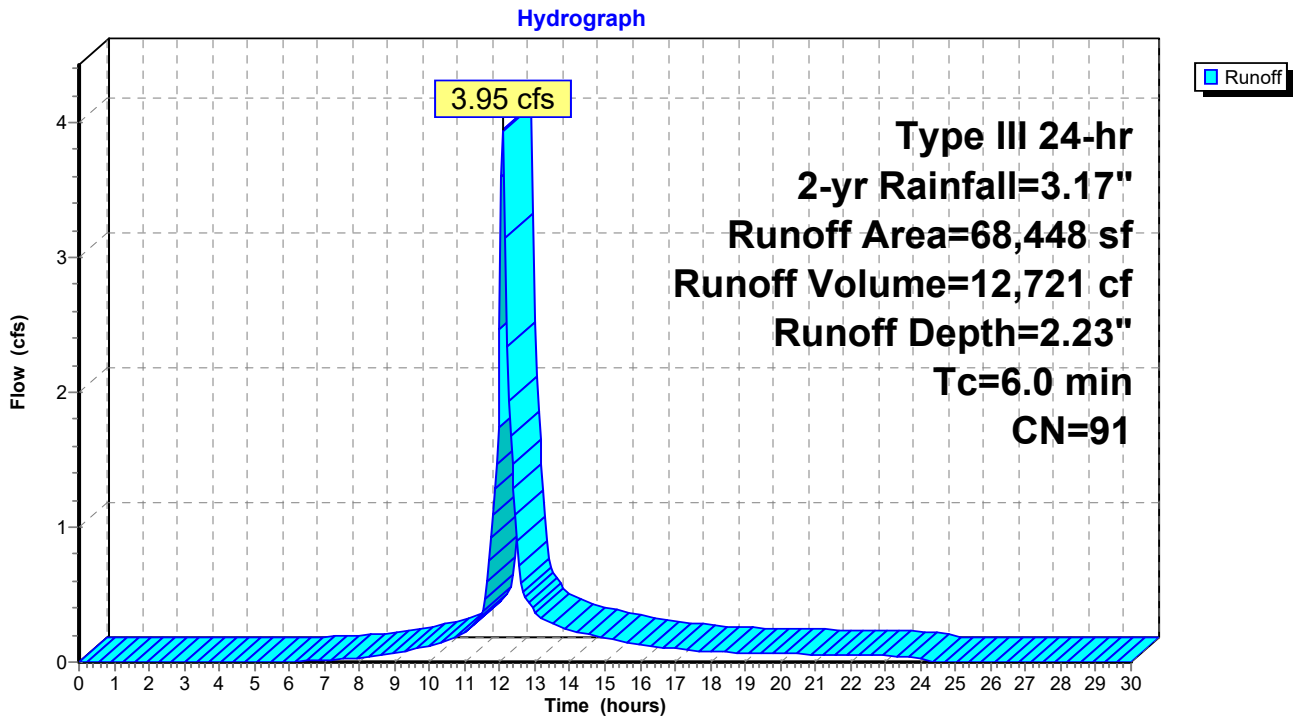
Runoff = 3.95 cfs @ 12.09 hrs, Volume= 12,721 cf, Depth= 2.23"  
 Routed to Pond 1BN : BIO-1BN

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
40,450	98	Paved parking, HSG D
27,998	80	>75% Grass cover, Good, HSG D
68,448	91	Weighted Average
27,998		40.90% Pervious Area
40,450		59.10% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BN: N HALF BLDG**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 35

**Summary for Subcatchment PW1BS: S HALF BLDG**

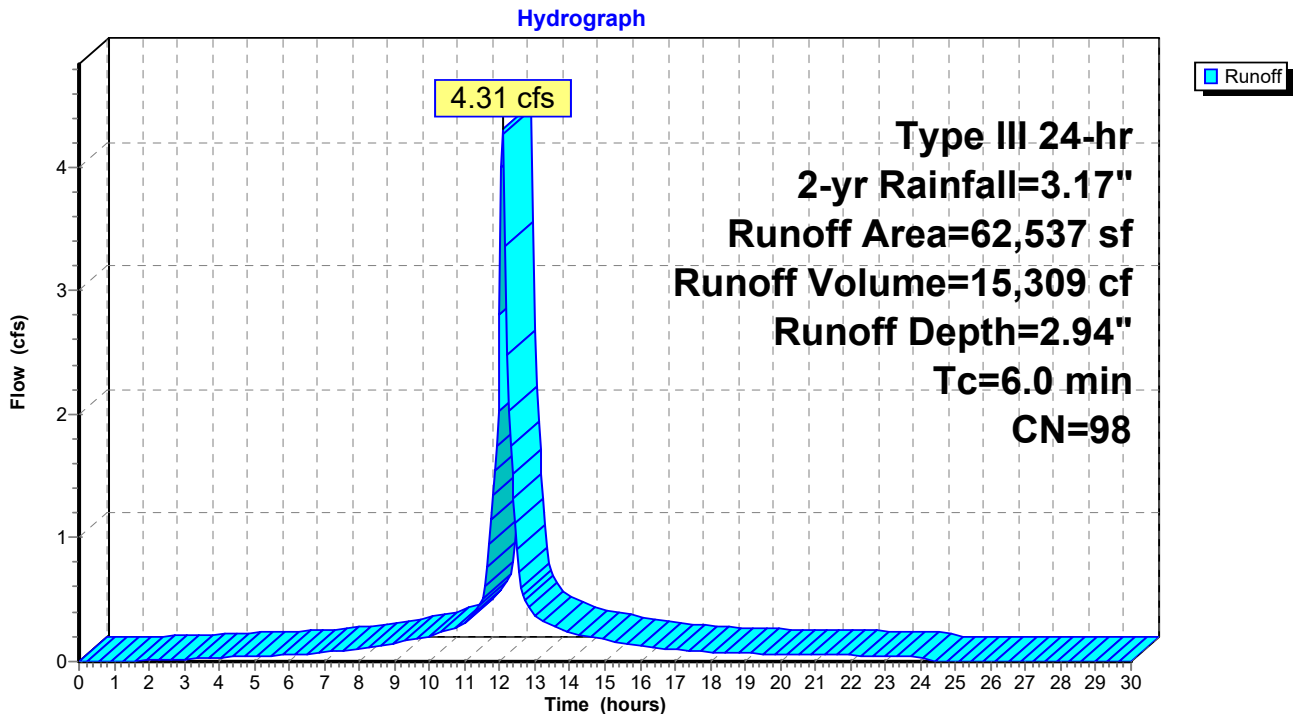
Runoff = 4.31 cfs @ 12.09 hrs, Volume= 15,309 cf, Depth= 2.94"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
62,537	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
62,537	98	Weighted Average
62,537		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BS: S HALF BLDG**





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 36

**Summary for Subcatchment PW1C: PARKING**

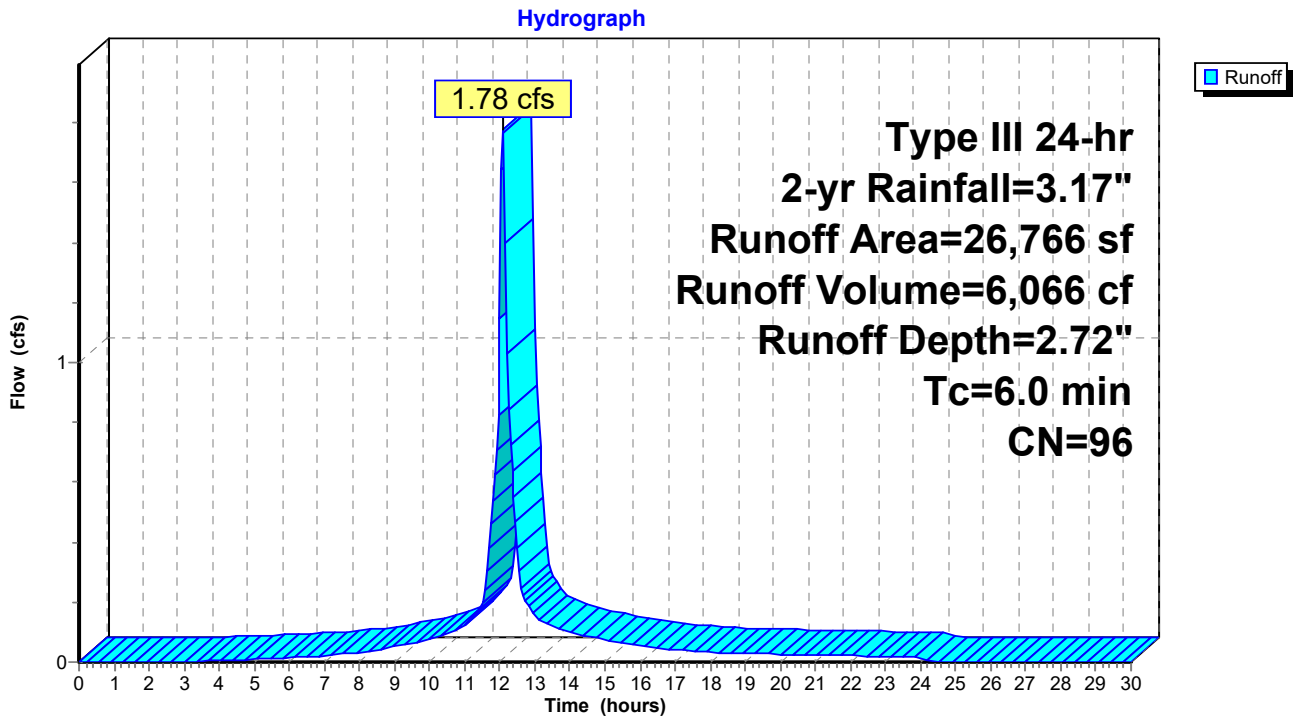
Runoff = 1.78 cfs @ 12.09 hrs, Volume= 6,066 cf, Depth= 2.72"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
23,545	98	Paved parking, HSG D
3,221	80	>75% Grass cover, Good, HSG D
26,766	96	Weighted Average
3,221		12.03% Pervious Area
23,545		87.97% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1C: PARKING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 37

**Summary for Subcatchment PW1D: ENTRANCE**

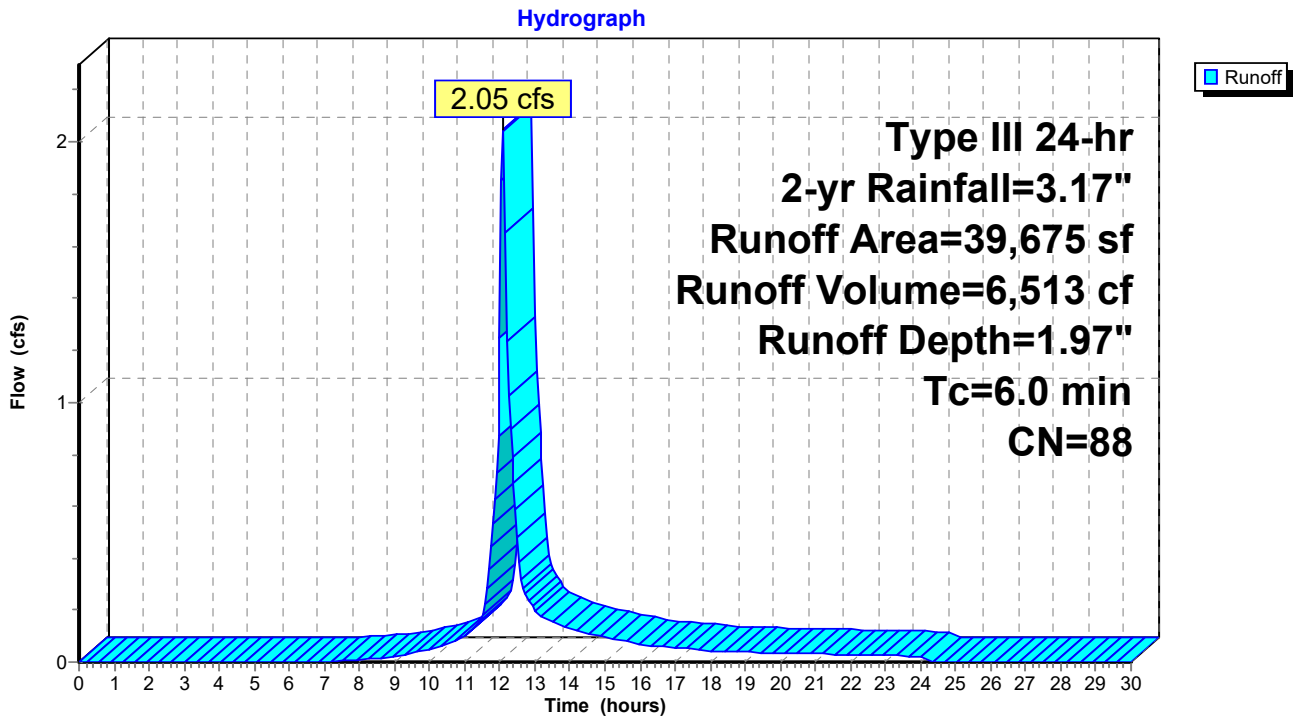
Runoff = 2.05 cfs @ 12.09 hrs, Volume= 6,513 cf, Depth= 1.97"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
17,739	98	Paved parking, HSG D
21,936	80	>75% Grass cover, Good, HSG D
39,675	88	Weighted Average
21,936		55.29% Pervious Area
17,739		44.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1D: ENTRANCE**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 38

**Summary for Subcatchment PW1E: TRAILERS**

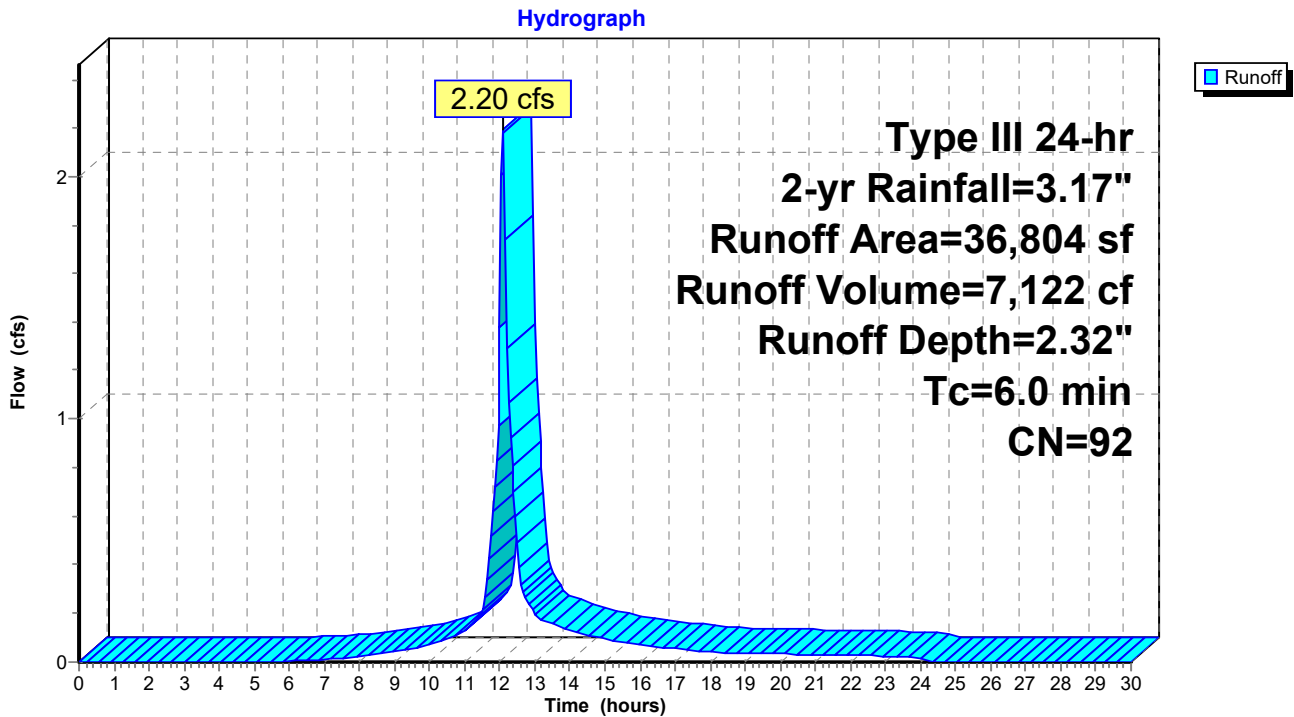
Runoff = 2.20 cfs @ 12.09 hrs, Volume= 7,122 cf, Depth= 2.32"  
 Routed to Pond 1E : BIO-1E

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
25,092	98	Paved parking, HSG D
11,712	80	>75% Grass cover, Good, HSG D
36,804	92	Weighted Average
11,712		31.82% Pervious Area
25,092		68.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1E: TRAILERS**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 39

**Summary for Subcatchment PW1F: TRAILER 2**

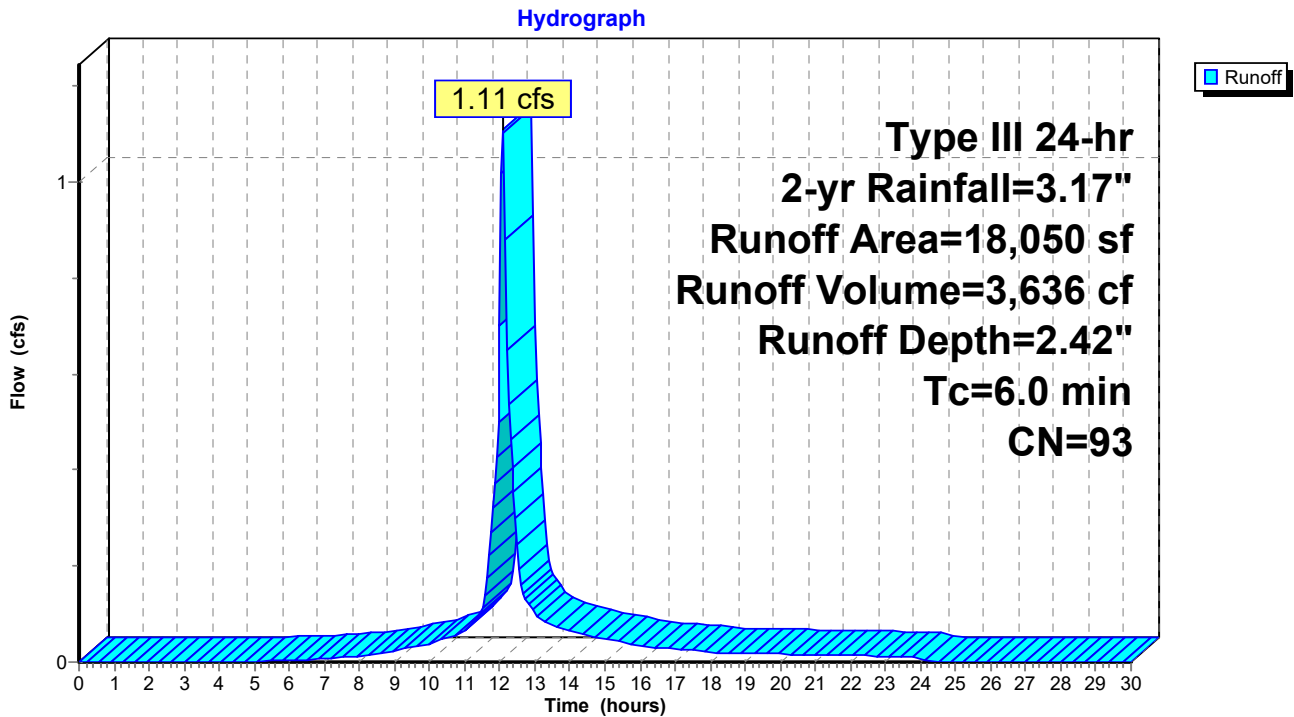
Runoff = 1.11 cfs @ 12.09 hrs, Volume= 3,636 cf, Depth= 2.42"  
 Routed to Pond 1F : BIO-1F

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
12,622	98	Paved parking, HSG D
5,428	80	>75% Grass cover, Good, HSG D
18,050	93	Weighted Average
5,428		30.07% Pervious Area
12,622		69.93% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1F: TRAILER 2**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 40

**Summary for Subcatchment PW1G: LOADING**

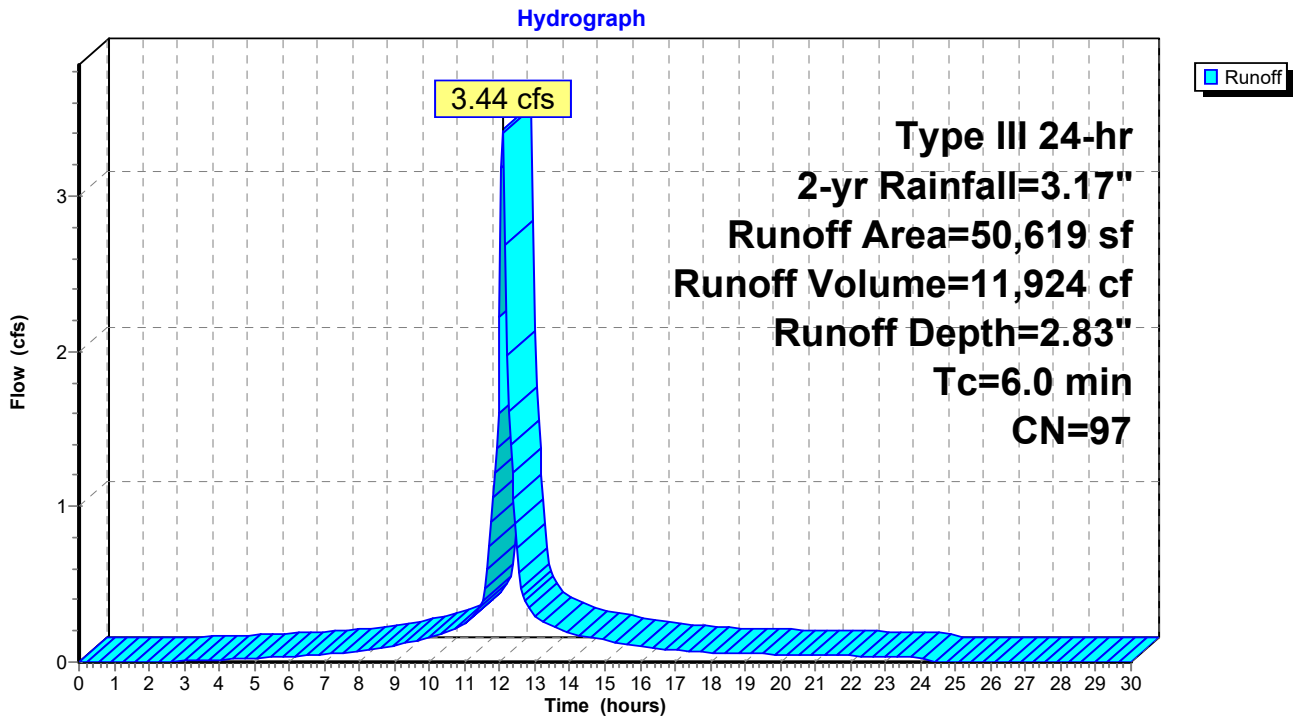
Runoff = 3.44 cfs @ 12.09 hrs, Volume= 11,924 cf, Depth= 2.83"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
46,810	98	Paved parking, HSG D
3,809	80	>75% Grass cover, Good, HSG D
50,619	97	Weighted Average
3,809		7.52% Pervious Area
46,810		92.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1G: LOADING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 41

**Summary for Subcatchment PW1H: NW CORNER BLDG**

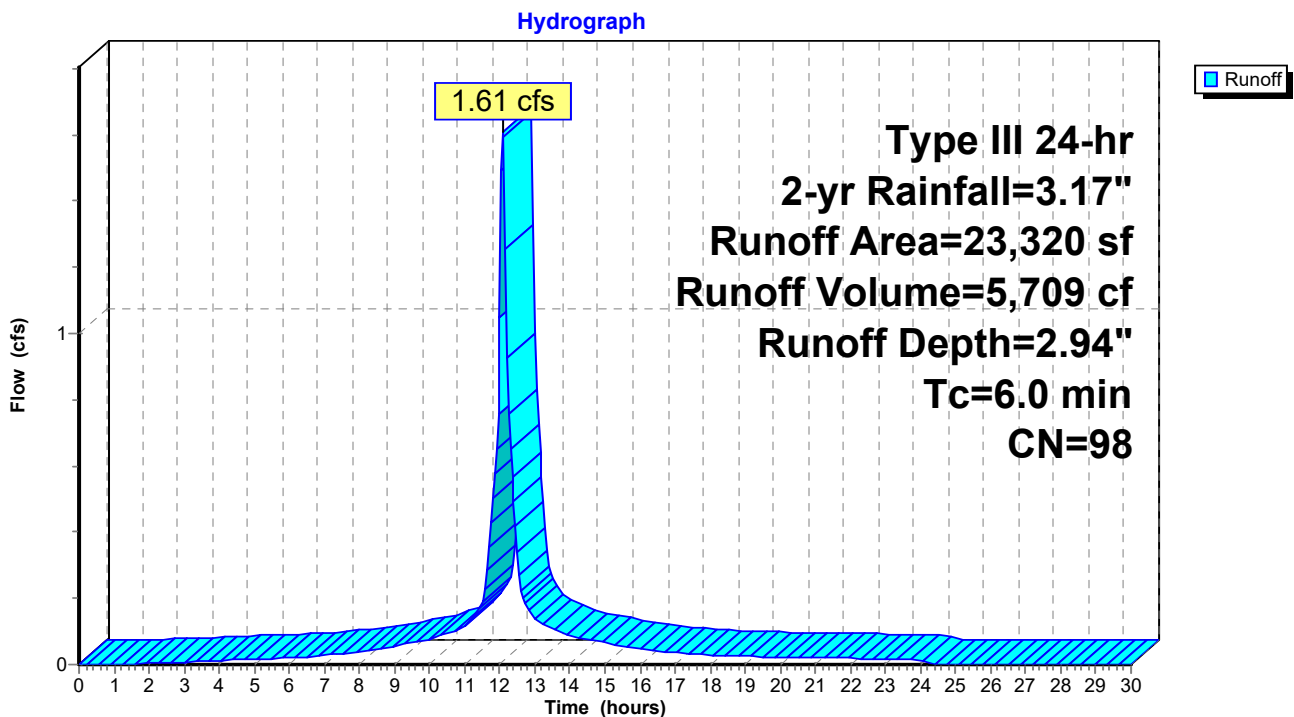
Runoff = 1.61 cfs @ 12.09 hrs, Volume= 5,709 cf, Depth= 2.94"  
Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
Type III 24-hr 2-yr Rainfall=3.17"

Area (sf)	CN	Description
23,320	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
23,320	98	Weighted Average
23,320		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1H: NW CORNER BLDG**



**230119 - R1 - Dewpoint South**

Type III 24-hr 2-yr Rainfall=3.17"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 42

**Summary for Pond 1BN: BIO-1BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth = 2.23" for 2-yr event  
 Inflow = 3.95 cfs @ 12.09 hrs, Volume= 12,721 cf  
 Outflow = 2.06 cfs @ 12.26 hrs, Volume= 7,574 cf, Atten= 48%, Lag= 10.1 min  
 Primary = 2.06 cfs @ 12.26 hrs, Volume= 7,574 cf  
 Routed to Pond 2BN : BIO-2BN

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 492.63' @ 12.26 hrs Surf.Area= 2,942 sf Storage= 5,682 cf

Plug-Flow detention time= 210.1 min calculated for 7,574 cf (60% of inflow)  
 Center-of-Mass det. time= 105.8 min ( 908.6 - 802.8 )

Volume	Invert	Avail.Storage	Storage Description		
#1	490.00'	10,349 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
490.00	1,454	0	0	1,454	
492.00	2,555	3,958	3,958	2,611	
494.00	3,883	6,392	10,349	4,013	

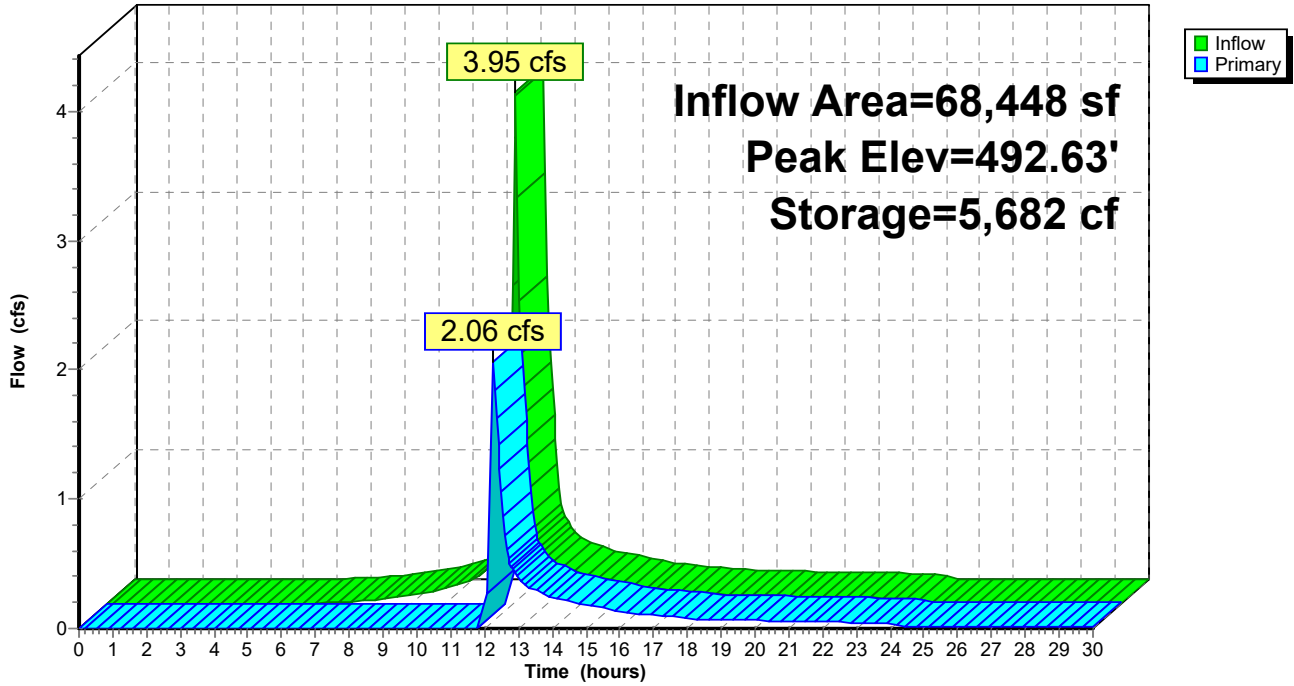
Device	Routing	Invert	Outlet Devices
#1	Primary	483.15'	<b>18.0" Round Culvert</b> L= 26.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 483.15' / 482.62' S= 0.0204 ' / Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	492.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	490.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=2.01 cfs @ 12.26 hrs HW=492.63' TW=484.18' (Dynamic Tailwater)

- 1=Culvert (Passes 2.01 cfs of 24.72 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 2.01 cfs @ 0.99 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1BN: BIO-1BN

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 44

**Stage-Area-Storage for Pond 1BN: BIO-1BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
490.00	1,454	0	492.65	2,956	5,747
490.05	1,478	73	492.70	2,988	5,896
490.10	1,502	148	492.75	3,021	6,046
490.15	1,526	223	492.80	3,053	6,198
490.20	1,550	300	492.85	3,086	6,351
490.25	1,575	378	492.90	3,118	6,506
490.30	1,599	458	492.95	3,151	6,663
490.35	1,624	538	493.00	3,184	6,822
490.40	1,650	620	493.05	3,218	6,982
490.45	1,675	703	493.10	3,251	7,143
490.50	1,700	788	493.15	3,285	7,307
490.55	1,726	873	493.20	3,319	7,472
490.60	1,752	960	493.25	3,353	7,639
490.65	1,778	1,049	493.30	3,387	7,807
490.70	1,804	1,138	493.35	3,421	7,977
490.75	1,831	1,229	493.40	3,456	8,149
490.80	1,857	1,321	493.45	3,490	8,323
490.85	1,884	1,415	493.50	3,525	8,498
490.90	1,911	1,510	493.55	3,560	8,675
490.95	1,939	1,606	493.60	3,595	8,854
491.00	1,966	1,704	493.65	3,631	9,035
491.05	1,994	1,803	493.70	3,666	9,217
491.10	2,021	1,903	493.75	3,702	9,401
491.15	2,049	2,005	493.80	3,738	9,587
491.20	2,078	2,108	493.85	3,774	9,775
491.25	2,106	2,212	493.90	3,810	9,965
491.30	2,135	2,318	493.95	3,846	10,156
491.35	2,163	2,426	494.00	<b>3,883</b>	<b>10,349</b>
491.40	2,192	2,535			
491.45	2,221	2,645			
491.50	2,251	2,757			
491.55	2,280	2,870			
491.60	2,310	2,985			
491.65	2,340	3,101			
491.70	2,370	3,219			
491.75	2,401	3,338			
491.80	2,431	3,459			
491.85	2,462	3,581			
491.90	2,493	3,705			
491.95	2,524	3,831			
492.00	2,555	3,958			
492.05	2,585	4,086			
492.10	2,615	4,216			
492.15	2,645	4,348			
492.20	2,675	4,481			
492.25	2,706	4,615			
492.30	2,737	4,751			
492.35	2,767	4,889			
492.40	2,798	5,028			
492.45	2,830	5,169			
492.50	2,861	5,311			
492.55	2,893	5,455			
492.60	2,924	5,600			

**Summary for Pond 1D: BIO-1D**

Inflow Area = 89,761 sf, 71.97% Impervious, Inflow Depth = 2.44" for 2-yr event  
 Inflow = 5.44 cfs @ 12.09 hrs, Volume= 18,288 cf  
 Outflow = 4.48 cfs @ 12.15 hrs, Volume= 14,559 cf, Atten= 18%, Lag= 3.8 min  
 Primary = 4.48 cfs @ 12.15 hrs, Volume= 14,559 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.81' @ 12.15 hrs Surf.Area= 7,533 sf Storage= 5,721 cf

Plug-Flow detention time= 152.7 min calculated for 14,535 cf (79% of inflow)  
 Center-of-Mass det. time= 76.4 min ( 859.9 - 783.4 )

Volume	Invert	Avail.Storage	Storage Description		
#1	468.00'	15,581 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
468.00	6,529	0	0	6,529	
470.00	9,124	15,581	15,581	9,218	

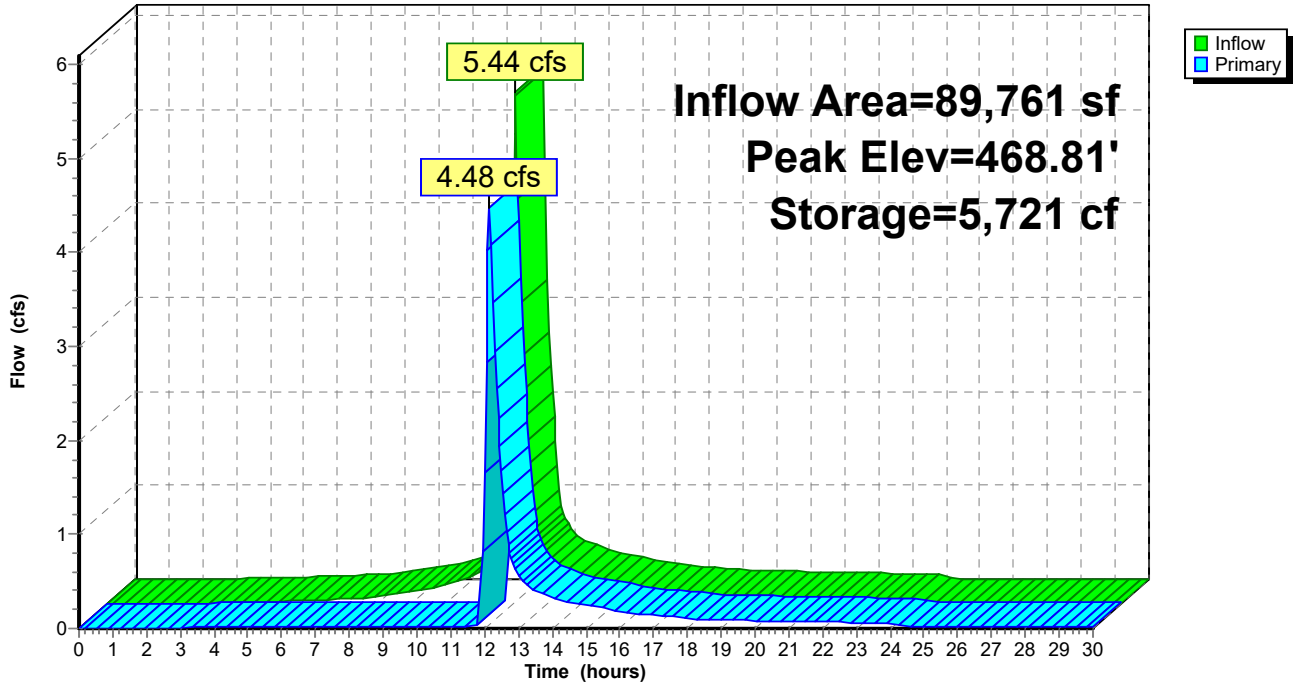
Device	Routing	Invert	Outlet Devices
#1	Primary	464.50'	<b>12.0" Round Culvert</b> L= 190.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 464.50' / 462.98' S= 0.0080 ' S= 0.0080 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.60'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	468.00'	<b>0.125 in/hr Exfiltration over Surface area</b>
#4	Primary	469.00'	<b>10.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83

**Primary OutFlow** Max=4.47 cfs @ 12.15 hrs HW=468.81' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 4.47 cfs of 5.40 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 4.45 cfs @ 1.30 fps)
- 3=Exfiltration (Exfiltration Controls 0.02 cfs)
- 4=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

Pond 1D: BIO-1D

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 47

**Stage-Area-Storage for Pond 1D: BIO-1D**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
468.00	6,529	0	469.06	7,850	7,610
468.02	6,553	131	469.08	7,876	7,768
468.04	6,577	262	469.10	7,903	7,925
468.06	6,601	394	469.12	7,929	8,084
468.08	6,624	526	469.14	7,955	8,243
468.10	6,648	659	469.16	7,981	8,402
468.12	6,672	792	469.18	8,008	8,562
468.14	6,697	926	469.20	8,034	8,722
468.16	6,721	1,060	469.22	8,060	8,883
468.18	6,745	1,195	469.24	8,087	9,045
468.20	6,769	1,330	469.26	8,113	9,207
468.22	6,793	1,465	469.28	8,140	9,369
468.24	6,818	1,601	469.30	8,166	9,532
468.26	6,842	1,738	469.32	8,193	9,696
468.28	6,866	1,875	469.34	8,220	9,860
468.30	6,891	2,013	469.36	8,246	10,025
468.32	6,915	2,151	469.38	8,273	10,190
468.34	6,940	2,289	469.40	8,300	10,356
468.36	6,964	2,428	469.42	8,327	10,522
468.38	6,989	2,568	469.44	8,354	10,689
468.40	7,013	2,708	469.46	8,381	10,856
468.42	7,038	2,848	469.48	8,408	11,024
468.44	7,063	2,989	469.50	8,435	11,192
468.46	7,087	3,131	469.52	8,462	11,361
468.48	7,112	3,273	469.54	8,489	11,531
468.50	7,137	3,415	469.56	8,516	11,701
468.52	7,162	3,558	469.58	8,543	11,871
468.54	7,187	3,702	469.60	8,570	12,043
468.56	7,212	3,846	469.62	8,598	12,214
468.58	7,237	3,990	469.64	8,625	12,386
468.60	7,262	4,135	469.66	8,652	12,559
468.62	7,287	4,281	469.68	8,680	12,733
468.64	7,312	4,427	469.70	8,707	12,906
468.66	7,337	4,573	469.72	8,735	13,081
468.68	7,363	4,720	469.74	8,762	13,256
468.70	7,388	4,868	469.76	8,790	13,431
468.72	7,413	5,016	469.78	8,817	13,607
468.74	7,439	5,164	469.80	8,845	13,784
468.76	7,464	5,313	469.82	8,873	13,961
468.78	7,490	5,463	469.84	8,900	14,139
468.80	7,515	5,613	469.86	8,928	14,317
468.82	7,541	5,764	469.88	8,956	14,496
468.84	7,566	5,915	469.90	8,984	14,675
468.86	7,592	6,066	469.92	9,012	14,855
468.88	7,617	6,218	469.94	9,040	15,036
468.90	7,643	6,371	469.96	9,068	15,217
468.92	7,669	6,524	469.98	9,096	15,399
468.94	7,695	6,678	470.00	<b>9,124</b>	<b>15,581</b>
468.96	7,721	6,832			
468.98	7,746	6,986			
469.00	7,772	7,142			
469.02	7,798	7,297			
469.04	7,824	7,454			

**230119 - R1 - Dewpoint South**

Type III 24-hr 2-yr Rainfall=3.17"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 48

**Summary for Pond 1E: BIO-1E**

Inflow Area = 36,804 sf, 68.18% Impervious, Inflow Depth = 2.32" for 2-yr event  
 Inflow = 2.20 cfs @ 12.09 hrs, Volume= 7,122 cf  
 Outflow = 0.10 cfs @ 15.08 hrs, Volume= 2,073 cf, Atten= 96%, Lag= 179.6 min  
 Primary = 0.10 cfs @ 15.08 hrs, Volume= 2,073 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.52' @ 15.08 hrs Surf.Area= 4,145 sf Storage= 5,353 cf

Plug-Flow detention time= 436.0 min calculated for 2,070 cf (29% of inflow)  
 Center-of-Mass det. time= 294.6 min ( 1,092.7 - 798.1 )

Volume	Invert	Avail.Storage	Storage Description		
#1	467.00'	12,471 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
467.00	2,940	0	0	2,940	
468.00	3,728	3,326	3,326	3,761	
470.00	5,472	9,144	12,471	5,587	

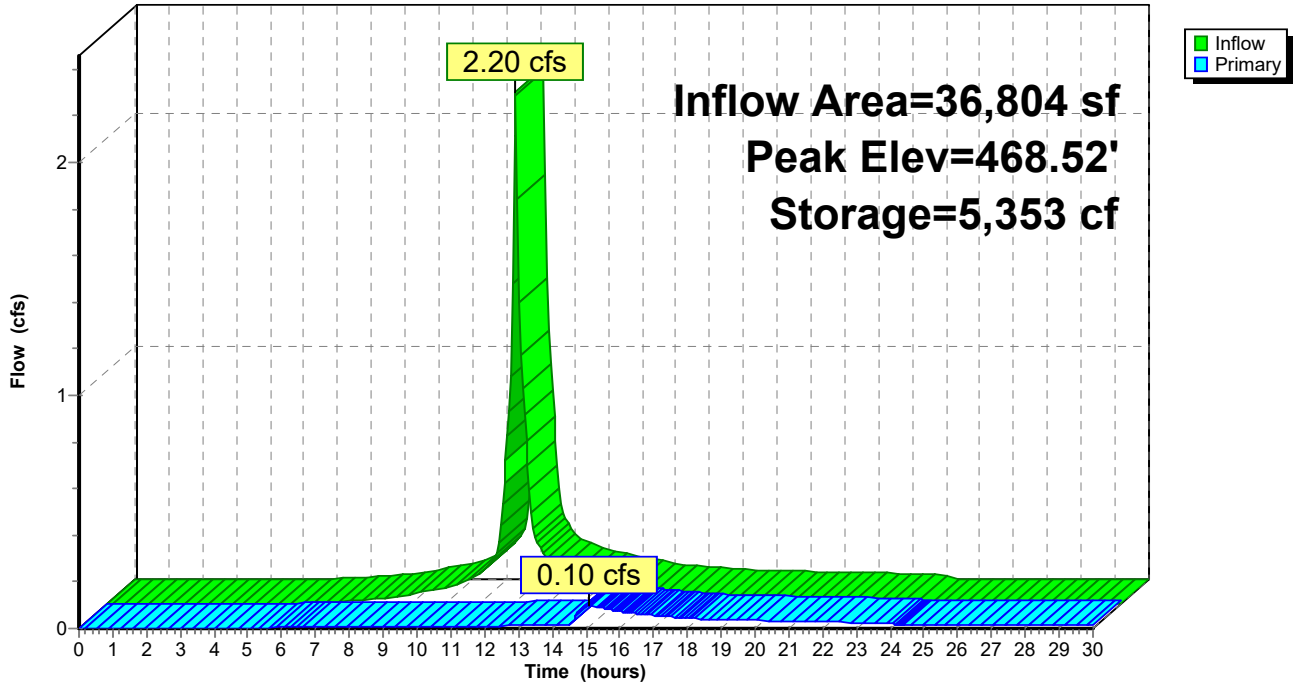
Device	Routing	Invert	Outlet Devices
#1	Primary	463.50'	<b>12.0" Round Culvert</b> L= 23.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 463.50' / 462.93' S= 0.0248 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	467.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.10 cfs @ 15.08 hrs HW=468.52' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.10 cfs of 8.04 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 0.08 cfs @ 0.34 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1E: BIO-1E

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

*Type III 24-hr 2-yr Rainfall=3.17"*

Printed 2/2/2023

Page 50

**Stage-Area-Storage for Pond 1E: BIO-1E**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
467.00	2,940	0	469.65	5,143	10,613
467.05	2,977	148	469.70	5,189	10,872
467.10	3,015	298	469.75	5,236	11,132
467.15	3,052	449	469.80	5,283	11,395
467.20	3,090	603	469.85	5,330	11,661
467.25	3,128	758	469.90	5,377	11,928
467.30	3,167	916	469.95	5,424	12,198
467.35	3,205	1,075	470.00	<b>5,472</b>	<b>12,471</b>
467.40	3,244	1,236			
467.45	3,283	1,399			
467.50	3,322	1,565			
467.55	3,362	1,732			
467.60	3,402	1,901			
467.65	3,442	2,072			
467.70	3,482	2,245			
467.75	3,522	2,420			
467.80	3,563	2,597			
467.85	3,604	2,776			
467.90	3,645	2,958			
467.95	3,686	3,141			
468.00	3,728	3,326			
468.05	3,768	3,514			
468.10	3,807	3,703			
468.15	3,847	3,894			
468.20	3,887	4,088			
468.25	3,928	4,283			
468.30	3,968	4,480			
468.35	4,009	4,680			
468.40	4,050	4,881			
468.45	4,091	5,085			
468.50	4,133	5,291			
468.55	4,174	5,498			
468.60	4,216	5,708			
468.65	4,258	5,920			
468.70	4,300	6,134			
468.75	4,343	6,350			
468.80	4,386	6,568			
468.85	4,428	6,788			
468.90	4,472	7,011			
468.95	4,515	7,236			
469.00	4,558	7,462			
469.05	4,602	7,691			
469.10	4,646	7,923			
469.15	4,690	8,156			
469.20	4,734	8,392			
469.25	4,779	8,629			
469.30	4,824	8,870			
469.35	4,869	9,112			
469.40	4,914	9,356			
469.45	4,959	9,603			
469.50	5,005	9,852			
469.55	5,051	10,104			
469.60	5,097	10,357			

**Summary for Pond 1F: BIO-1F**

Inflow Area = 18,050 sf, 69.93% Impervious, Inflow Depth = 2.42" for 2-yr event  
 Inflow = 1.11 cfs @ 12.09 hrs, Volume= 3,636 cf  
 Outflow = 0.05 cfs @ 14.62 hrs, Volume= 1,109 cf, Atten= 95%, Lag= 151.6 min  
 Primary = 0.05 cfs @ 14.62 hrs, Volume= 1,109 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 478.51' @ 14.62 hrs Surf.Area= 2,227 sf Storage= 2,682 cf

Plug-Flow detention time= 429.4 min calculated for 1,109 cf (31% of inflow)  
 Center-of-Mass det. time= 286.5 min ( 1,079.5 - 793.0 )

Volume	Invert	Avail.Storage	Storage Description		
#1	477.00'	6,744 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
477.00	1,347	0	0	1,347	
478.00	1,919	1,625	1,625	1,941	
480.00	3,259	5,119	6,744	3,341	

Device	Routing	Invert	Outlet Devices
#1	Primary	473.50'	<b>12.0" Round Culvert</b> L= 115.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 473.50' / 471.21' S= 0.0199 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	478.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	477.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

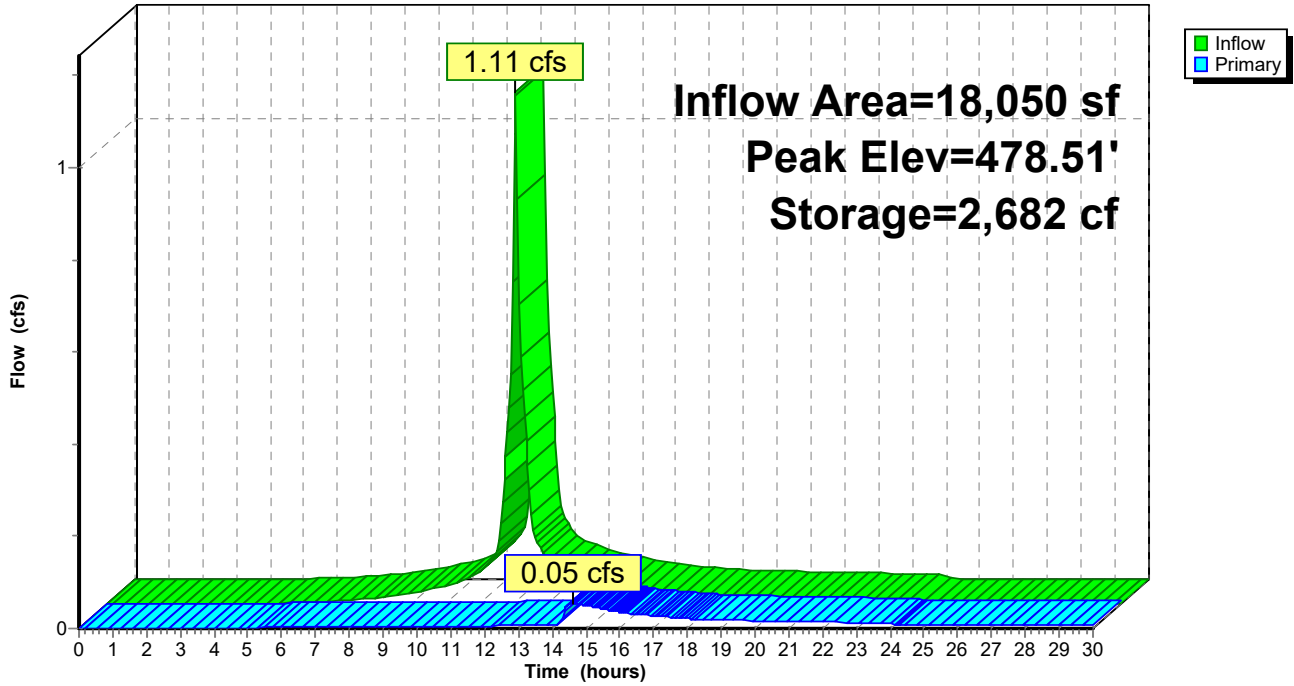
**Primary OutFlow** Max=0.05 cfs @ 14.62 hrs HW=478.51' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.05 cfs of 7.40 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 0.05 cfs @ 0.29 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)



### Pond 1F: BIO-1F

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 53

**Stage-Area-Storage for Pond 1F: BIO-1F**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
477.00	1,347	0	479.65	2,999	5,649
477.05	1,373	68	479.70	3,036	5,800
477.10	1,400	137	479.75	3,072	5,953
477.15	1,426	208	479.80	3,109	6,107
477.20	1,453	280	479.85	3,146	6,263
477.25	1,481	353	479.90	3,184	6,422
477.30	1,508	428	479.95	3,221	6,582
477.35	1,536	504	480.00	<b>3,259</b>	<b>6,744</b>
477.40	1,564	582			
477.45	1,592	660			
477.50	1,620	741			
477.55	1,649	823			
477.60	1,678	906			
477.65	1,707	990			
477.70	1,737	1,076			
477.75	1,767	1,164			
477.80	1,797	1,253			
477.85	1,827	1,344			
477.90	1,857	1,436			
477.95	1,888	1,529			
478.00	1,919	1,625			
478.05	1,948	1,721			
478.10	1,978	1,819			
478.15	2,007	1,919			
478.20	2,037	2,020			
478.25	2,067	2,123			
478.30	2,098	2,227			
478.35	2,128	2,333			
478.40	2,159	2,440			
478.45	2,190	2,548			
478.50	2,221	2,659			
478.55	2,252	2,770			
478.60	2,284	2,884			
478.65	2,316	2,999			
478.70	2,348	3,115			
478.75	2,380	3,234			
478.80	2,413	3,353			
478.85	2,445	3,475			
478.90	2,478	3,598			
478.95	2,512	3,723			
479.00	2,545	3,849			
479.05	2,579	3,977			
479.10	2,612	4,107			
479.15	2,646	4,239			
479.20	2,681	4,372			
479.25	2,715	4,507			
479.30	2,750	4,643			
479.35	2,785	4,782			
479.40	2,820	4,922			
479.45	2,855	5,064			
479.50	2,891	5,207			
479.55	2,927	5,353			
479.60	2,963	5,500			

**230119 - R1 - Dewpoint South**

Type III 24-hr 2-yr Rainfall=3.17"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 54

**Summary for Pond 2BN: BIO-2BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth > 1.33" for 2-yr event  
 Inflow = 2.06 cfs @ 12.26 hrs, Volume= 7,574 cf  
 Outflow = 0.39 cfs @ 13.00 hrs, Volume= 6,063 cf, Atten= 81%, Lag= 44.7 min  
 Primary = 0.39 cfs @ 13.00 hrs, Volume= 6,063 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 484.74' @ 13.00 hrs Surf.Area= 3,347 sf Storage= 2,294 cf

Plug-Flow detention time= 176.4 min calculated for 6,053 cf (80% of inflow)  
 Center-of-Mass det. time= 84.2 min ( 992.8 - 908.6 )

Volume	Invert	Avail.Storage	Storage Description		
#1	484.00'	17,309 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
484.00	2,843	0	0	2,843	
486.00	4,295	7,088	7,088	4,371	
488.00	5,972	10,221	17,309	6,142	

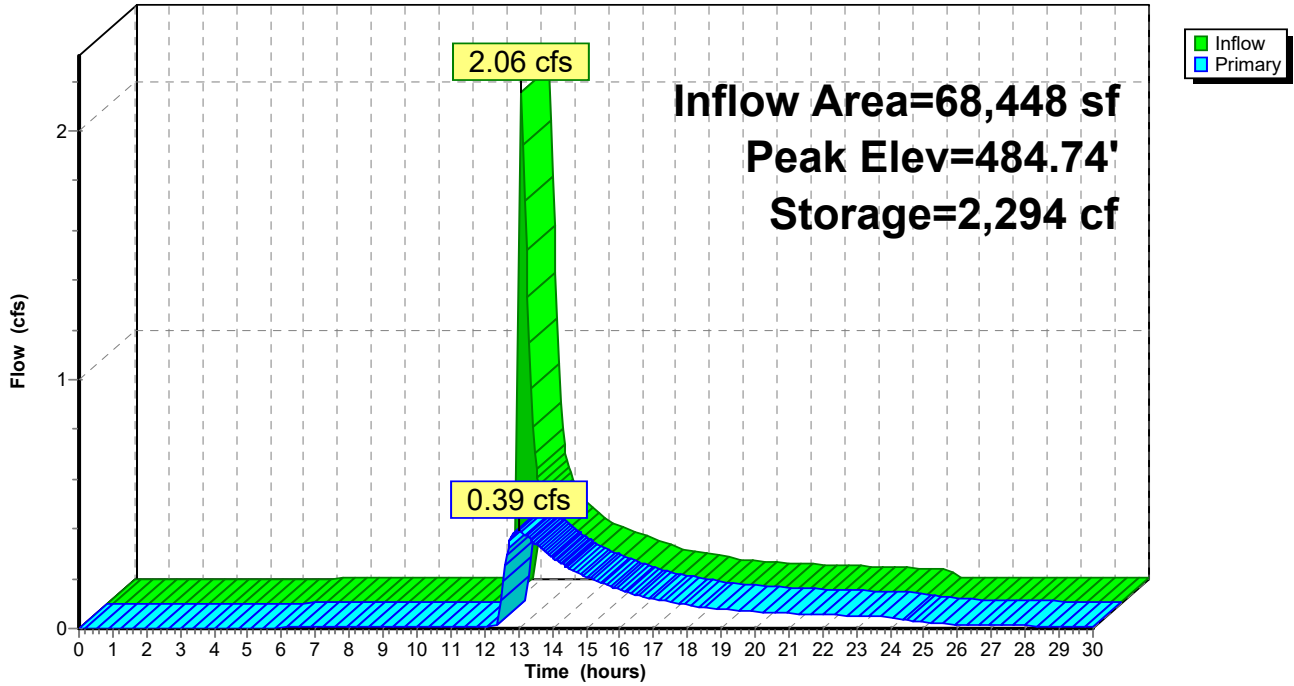
Device	Routing	Invert	Outlet Devices
#1	Primary	480.50'	<b>18.0" Round Culvert</b> L= 52.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 480.50' / 478.00' S= 0.0481 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	486.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	484.50'	<b>12.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	484.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.39 cfs @ 13.00 hrs HW=484.74' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.39 cfs of 15.90 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Orifice/Grate (Orifice Controls 0.38 cfs @ 1.58 fps)
- 4=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 2BN: BIO-2BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 56

**Stage-Area-Storage for Pond 2BN: BIO-2BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
484.00	2,843	0	486.65	4,810	10,046
484.05	2,876	143	486.70	4,851	10,287
484.10	2,909	288	486.75	4,892	10,531
484.15	2,942	434	486.80	4,933	10,776
484.20	2,975	582	486.85	4,974	11,024
484.25	3,008	731	486.90	5,016	11,274
484.30	3,042	883	486.95	5,057	11,526
484.35	3,076	1,035	487.00	5,099	11,780
484.40	3,110	1,190	487.05	5,141	12,036
484.45	3,144	1,346	487.10	5,183	12,294
484.50	3,178	1,504	487.15	5,226	12,554
484.55	3,213	1,664	487.20	5,268	12,816
484.60	3,247	1,826	487.25	5,311	13,081
484.65	3,282	1,989	487.30	5,354	13,347
484.70	3,317	2,154	487.35	5,397	13,616
484.75	3,353	2,321	487.40	5,440	13,887
484.80	3,388	2,489	487.45	5,483	14,160
484.85	3,424	2,659	487.50	5,527	14,435
484.90	3,459	2,832	487.55	5,571	14,713
484.95	3,495	3,005	487.60	5,615	14,992
485.00	3,532	3,181	487.65	5,659	15,274
485.05	3,568	3,359	487.70	5,703	15,558
485.10	3,605	3,538	487.75	5,747	15,844
485.15	3,641	3,719	487.80	5,792	16,133
485.20	3,678	3,902	487.85	5,837	16,424
485.25	3,716	4,087	487.90	5,882	16,717
485.30	3,753	4,274	487.95	5,927	17,012
485.35	3,790	4,462	488.00	<b>5,972</b>	<b>17,309</b>
485.40	3,828	4,653			
485.45	3,866	4,845			
485.50	3,904	5,039			
485.55	3,942	5,235			
485.60	3,981	5,434			
485.65	4,019	5,634			
485.70	4,058	5,835			
485.75	4,097	6,039			
485.80	4,136	6,245			
485.85	4,176	6,453			
485.90	4,215	6,663			
485.95	4,255	6,875			
486.00	4,295	7,088			
486.05	4,334	7,304			
486.10	4,372	7,522			
486.15	4,411	7,741			
486.20	4,450	7,963			
486.25	4,490	8,186			
486.30	4,529	8,412			
486.35	4,569	8,639			
486.40	4,608	8,869			
486.45	4,648	9,100			
486.50	4,688	9,333			
486.55	4,729	9,569			
486.60	4,769	9,806			

**Summary for Pond SUBS: SUBS**

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth = 2.89" for 2-yr event  
 Inflow = 7.75 cfs @ 12.09 hrs, Volume= 27,233 cf  
 Outflow = 0.60 cfs @ 13.11 hrs, Volume= 26,987 cf, Atten= 92%, Lag= 61.5 min  
 Primary = 0.60 cfs @ 13.11 hrs, Volume= 26,987 cf  
 Routed to Link JF : JELLY FISH  
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 477.24' @ 13.11 hrs Surf.Area= 8,608 sf Storage= 13,490 cf

Plug-Flow detention time= 253.3 min calculated for 26,987 cf (99% of inflow)  
 Center-of-Mass det. time= 247.4 min ( 1,008.2 - 760.8 )

Volume	Invert	Avail.Storage	Storage Description
#1A	475.00'	13,785 cf	<b>83.00'W x 103.72'L x 6.75'H Field A</b> 58,107 cf Overall - 23,645 cf Embedded = 34,463 cf x 40.0% Voids
#2A	475.75'	23,645 cf	<b>ADS_StormTech MC-4500 +Cap</b> x 216 Inside #1 Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 216 Chambers in 9 Rows Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf
		37,430 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	472.00'	<b>12.0" Round Culvert</b> L= 30.9' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 472.00' / 471.69' S= 0.0100 1/ S= 0.0100 1/ Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	475.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Device 1	480.25'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Secondary	479.00'	<b>18.0" Round Culvert</b> L= 46.5' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 479.00' / 477.56' S= 0.0310 1/ Cc= 0.900 n= 0.012, Flow Area= 1.77 sf

**Primary OutFlow** Max=0.60 cfs @ 13.11 hrs HW=477.24' TW=0.00' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 0.60 cfs of 9.44 cfs potential flow)
- ↑ 2=Orifice/Grate (Orifice Controls 0.60 cfs @ 6.93 fps)
- ↑ 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=475.00' TW=0.00' (Dynamic Tailwater)

- ↑ 4=Culvert ( Controls 0.00 cfs)

**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 58

**Pond SUBS: SUBS - Chamber Wizard Field A**

**Chamber Model = ADS\_StormTech MC-4500 +Cap (ADS StormTech®MC-4500 with cap, use MC-4500 b for new designs)**

Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf

Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap

Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf

100.0" Wide + 9.0" Spacing = 109.0" C-C Row Spacing

24 Chambers/Row x 4.02' Long +2.56' Cap Length x 2 = 101.72' Row Length +12.0" End Stone x 2 = 103.72' Base Length

9 Rows x 100.0" Wide + 9.0" Spacing x 8 + 12.0" Side Stone x 2 = 83.00' Base Width

9.0" Stone Base + 60.0" Chamber Height + 12.0" Stone Cover = 6.75' Field Height

216 Chambers x 106.5 cf + 35.7 cf Cap Volume x 2 x 9 Rows = 23,644.5 cf Chamber Storage

58,107.3 cf Field - 23,644.5 cf Chambers = 34,462.7 cf Stone x 40.0% Voids = 13,785.1 cf Stone Storage

Chamber Storage + Stone Storage = 37,429.6 cf = 0.859 af

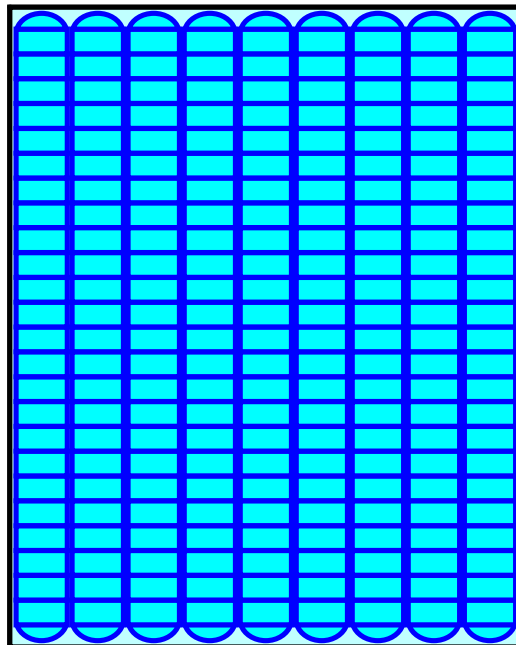
Overall Storage Efficiency = 64.4%

Overall System Size = 103.72' x 83.00' x 6.75'

216 Chambers

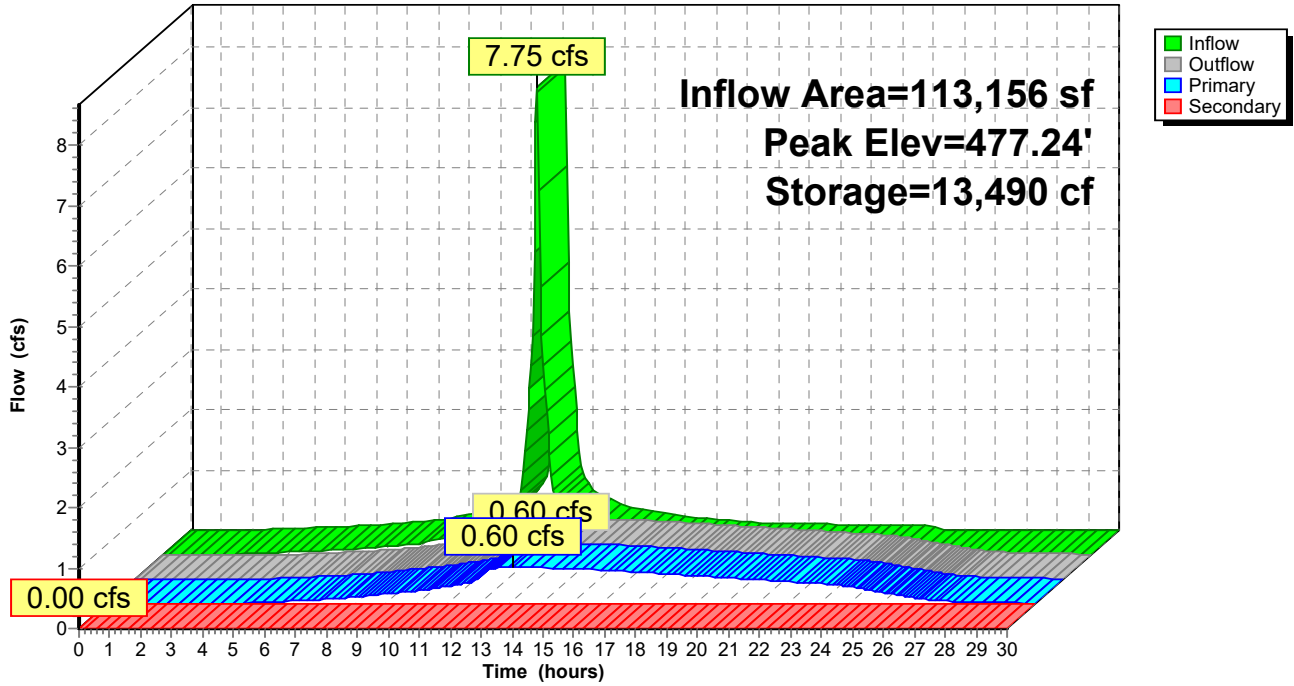
2,152.1 cy Field

1,276.4 cy Stone



### Pond SUBS: SUBS

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 2-yr Rainfall=3.17"

Printed 2/2/2023

Page 60

**Stage-Area-Storage for Pond SUBS: SUBS**

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
475.00	0	477.65	16,390	480.30	32,305
475.05	172	477.70	16,738	480.35	32,508
475.10	344	477.75	17,084	480.40	32,704
475.15	517	477.80	17,429	480.45	32,895
475.20	689	477.85	17,773	480.50	33,084
475.25	861	477.90	18,115	480.55	33,270
475.30	1,033	477.95	18,457	480.60	33,453
475.35	1,205	478.00	18,797	480.65	33,634
475.40	1,377	478.05	19,136	480.70	33,812
475.45	1,550	478.10	19,474	480.75	33,986
475.50	1,722	478.15	19,810	480.80	34,158
475.55	1,894	478.20	20,145	480.85	34,331
475.60	2,066	478.25	20,478	480.90	34,503
475.65	2,238	478.30	20,811	480.95	34,675
475.70	2,410	478.35	21,141	481.00	34,847
475.75	2,583	478.40	21,470	481.05	35,019
475.80	2,957	478.45	21,798	481.10	35,191
475.85	3,330	478.50	22,124	481.15	35,364
475.90	3,704	478.55	22,449	481.20	35,536
475.95	4,077	478.60	22,771	481.25	35,708
476.00	4,449	478.65	23,093	481.30	35,880
476.05	4,821	478.70	23,412	481.35	36,052
476.10	5,193	478.75	23,730	481.40	36,224
476.15	5,564	478.80	24,045	481.45	36,397
476.20	5,934	478.85	24,360	481.50	36,569
476.25	6,304	478.90	24,672	481.55	36,741
476.30	6,674	478.95	24,982	481.60	36,913
476.35	7,043	479.00	25,290	481.65	37,085
476.40	7,411	479.05	25,596	481.70	37,257
476.45	7,779	479.10	25,900	481.75	<b>37,430</b>
476.50	8,147	479.15	26,202		
476.55	8,513	479.20	26,501		
476.60	8,879	479.25	26,798		
476.65	9,245	479.30	27,093		
476.70	9,610	479.35	27,386		
476.75	9,974	479.40	27,675		
476.80	10,338	479.45	27,963		
476.85	10,700	479.50	28,247		
476.90	11,062	479.55	28,529		
476.95	11,424	479.60	28,808		
477.00	11,784	479.65	29,084		
477.05	12,144	479.70	29,357		
477.10	12,503	479.75	29,627		
477.15	12,861	479.80	29,893		
477.20	13,218	479.85	30,156		
477.25	13,574	479.90	30,414		
477.30	13,930	479.95	30,669		
477.35	14,284	480.00	30,920		
477.40	14,638	480.05	31,166		
477.45	14,990	480.10	31,407		
477.50	15,342	480.15	31,643		
477.55	15,692	480.20	31,872		
477.60	16,042	480.25	32,093		

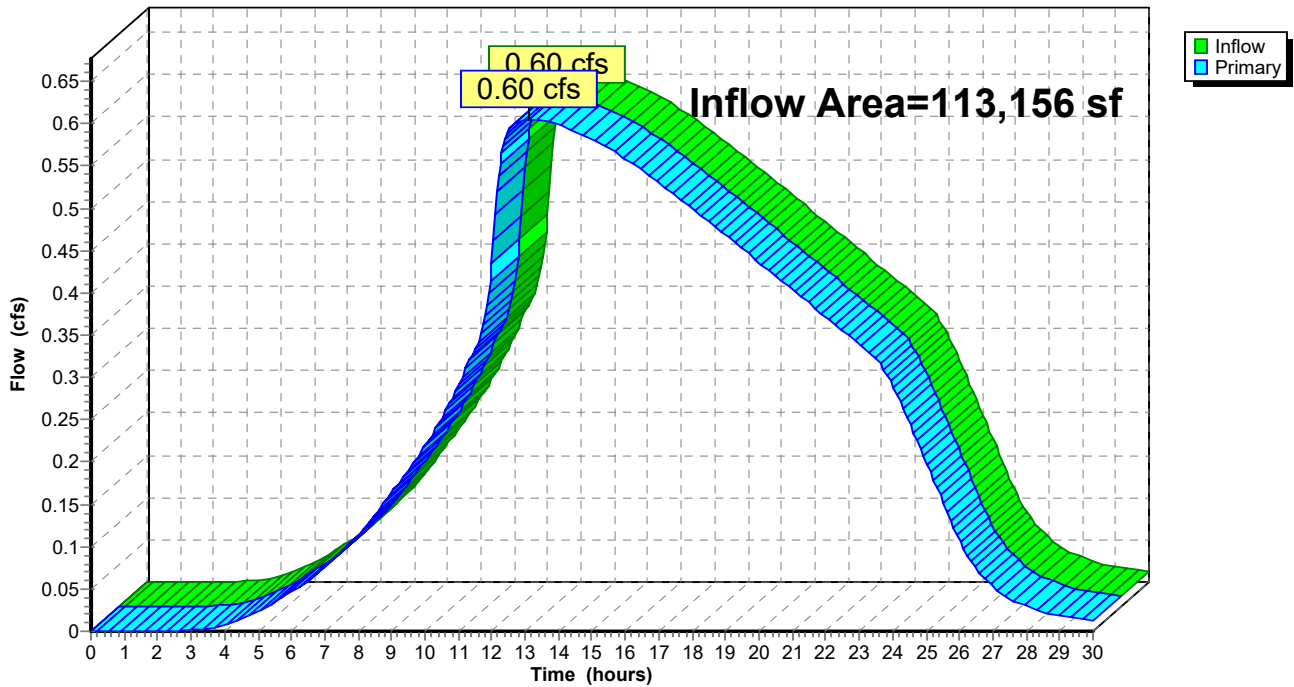
### Summary for Link JF: JELLY FISH

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth > 2.86" for 2-yr event  
Inflow = 0.60 cfs @ 13.11 hrs, Volume= 26,987 cf  
Primary = 0.60 cfs @ 13.11 hrs, Volume= 26,987 cf, Atten= 0%, Lag= 0.0 min  
Routed to Link PROP : PROPOSED

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link JF: JELLY FISH

Hydrograph

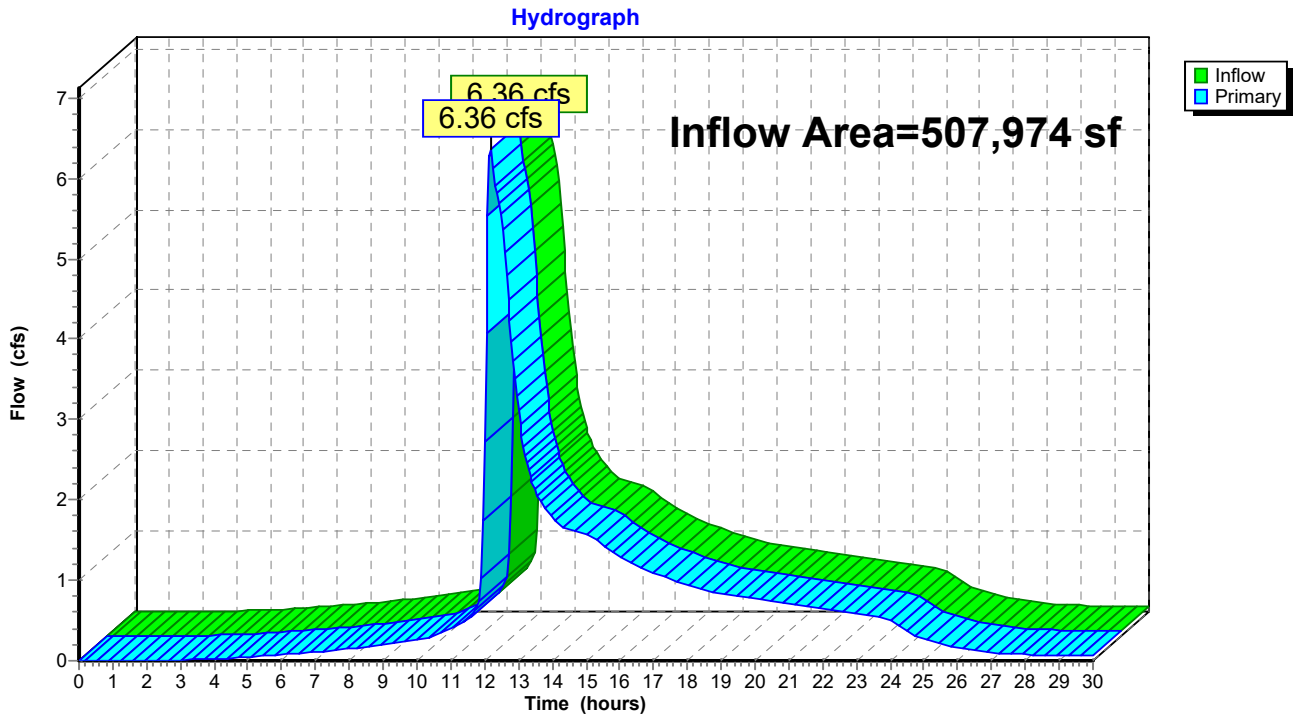


### Summary for Link PROP: PROPOSED

Inflow Area = 507,974 sf, 50.18% Impervious, Inflow Depth > 1.65" for 2-yr event  
Inflow = 6.36 cfs @ 12.17 hrs, Volume= 69,746 cf  
Primary = 6.36 cfs @ 12.17 hrs, Volume= 69,746 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link PROP: PROPOSED



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 63

**Summary for Subcatchment PW1A: LOD**

Runoff = 6.29 cfs @ 12.49 hrs, Volume= 36,991 cf, Depth= 2.44"  
 Routed to Link PROP : PROPOSED

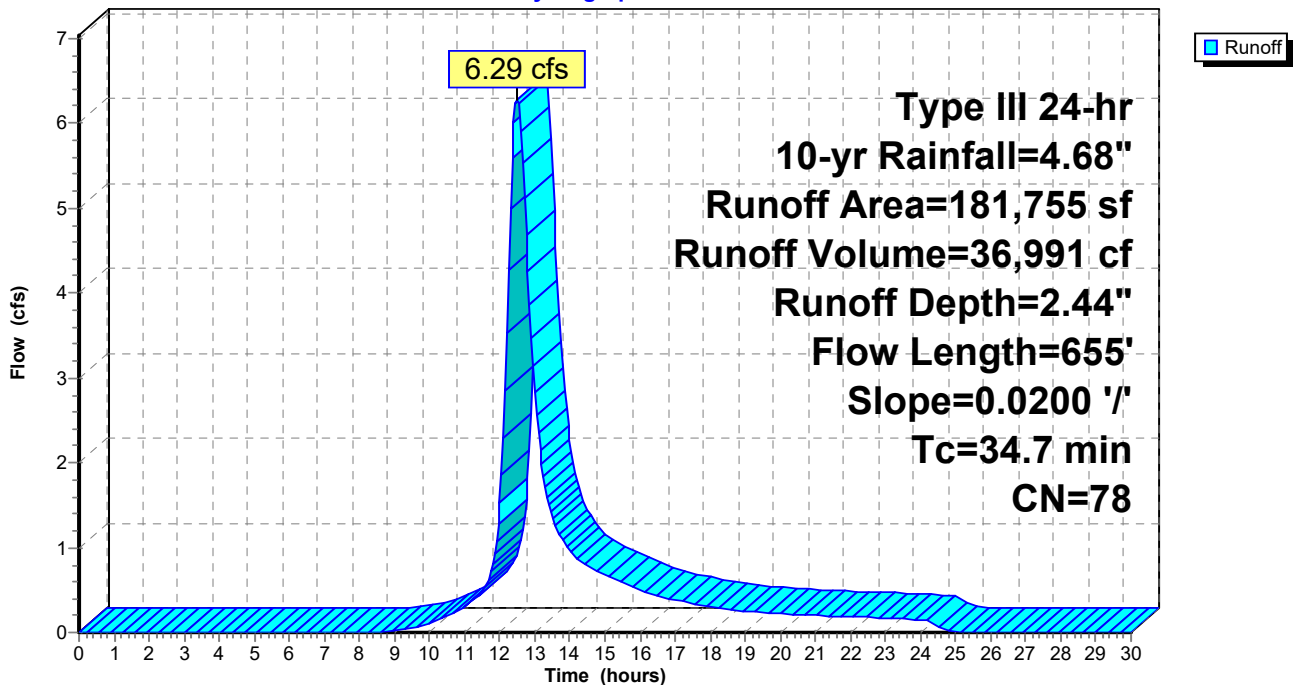
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
2,800	98	Paved parking, HSG D
73,077	80	>75% Grass cover, Good, HSG D
22,724	73	Brush, Good, HSG D
83,154	77	Woods, Good, HSG D
181,755	78	Weighted Average
178,955		98.46% Pervious Area
2,800		1.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment PW1A: LOD**

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 64

**Summary for Subcatchment PW1BN: N HALF BLDG**

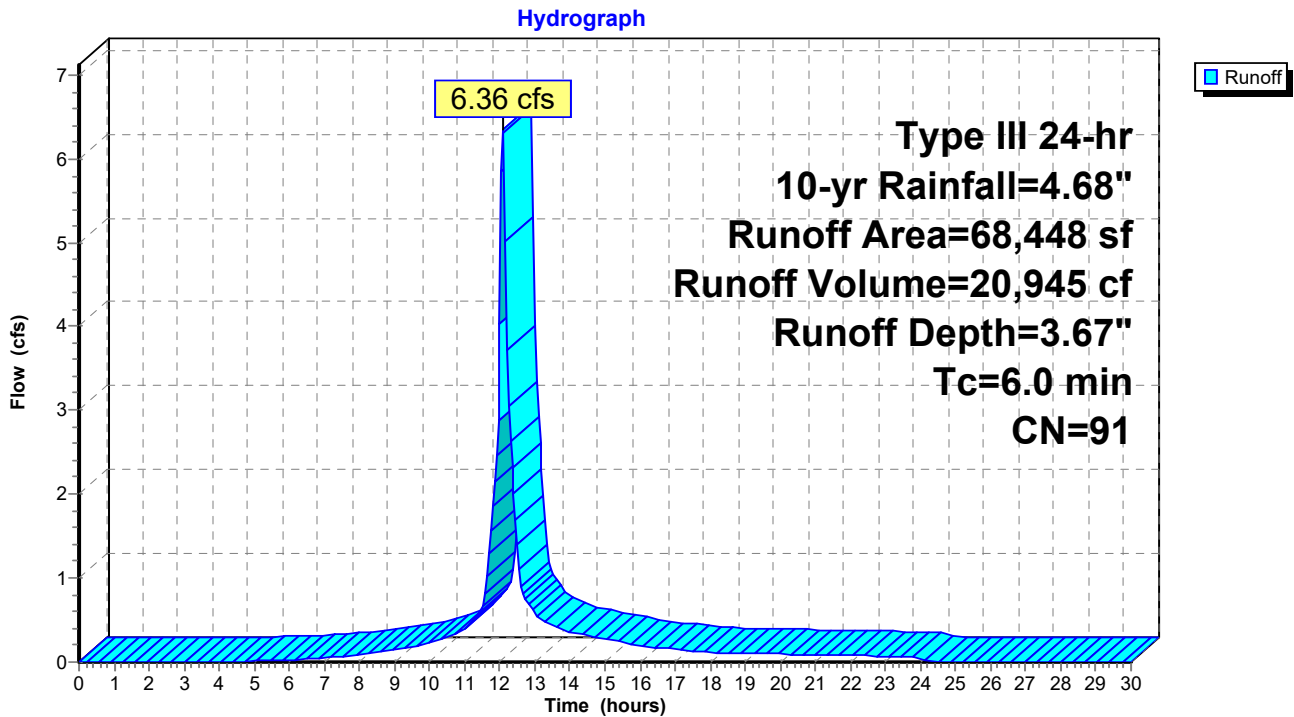
Runoff = 6.36 cfs @ 12.09 hrs, Volume= 20,945 cf, Depth= 3.67"  
 Routed to Pond 1BN : BIO-1BN

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
40,450	98	Paved parking, HSG D
27,998	80	>75% Grass cover, Good, HSG D
68,448	91	Weighted Average
27,998		40.90% Pervious Area
40,450		59.10% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BN: N HALF BLDG**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 65

**Summary for Subcatchment PW1BS: S HALF BLDG**

Runoff = 6.41 cfs @ 12.09 hrs, Volume= 23,158 cf, Depth= 4.44"  
Routed to Pond SUBS : SUBS

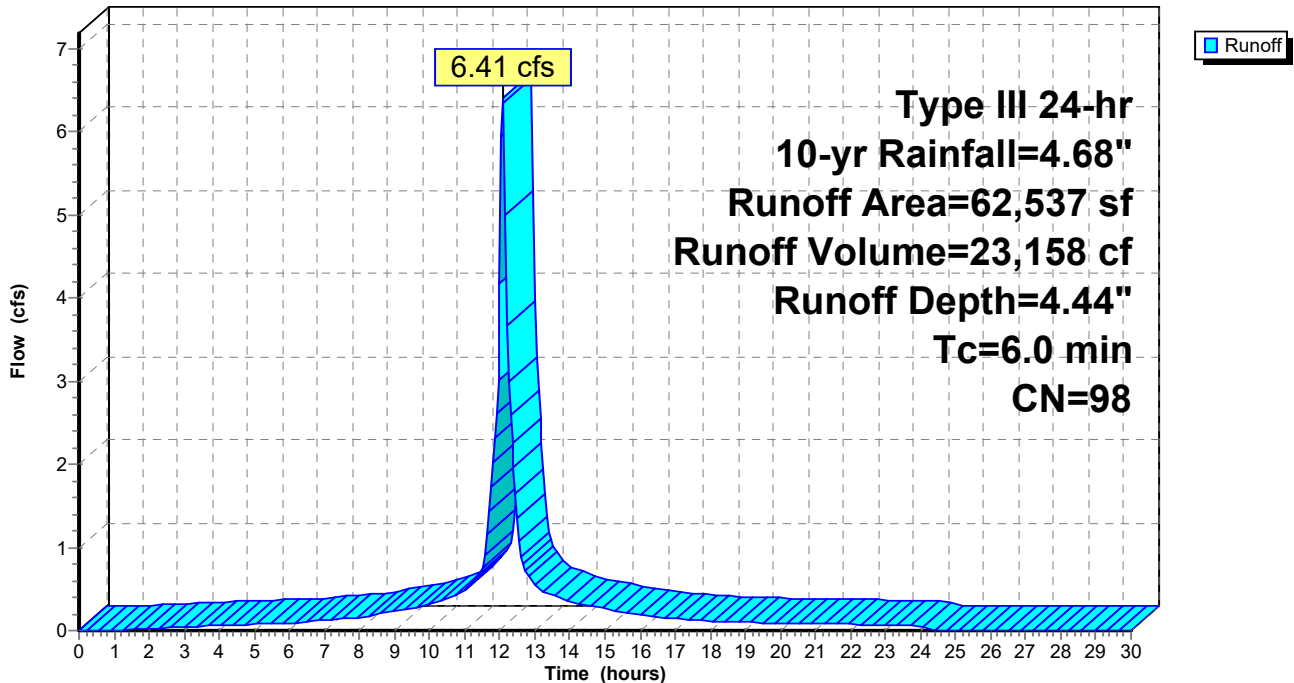
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
62,537	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
62,537	98	Weighted Average
62,537		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BS: S HALF BLDG**

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 66

**Summary for Subcatchment PW1C: PARKING**

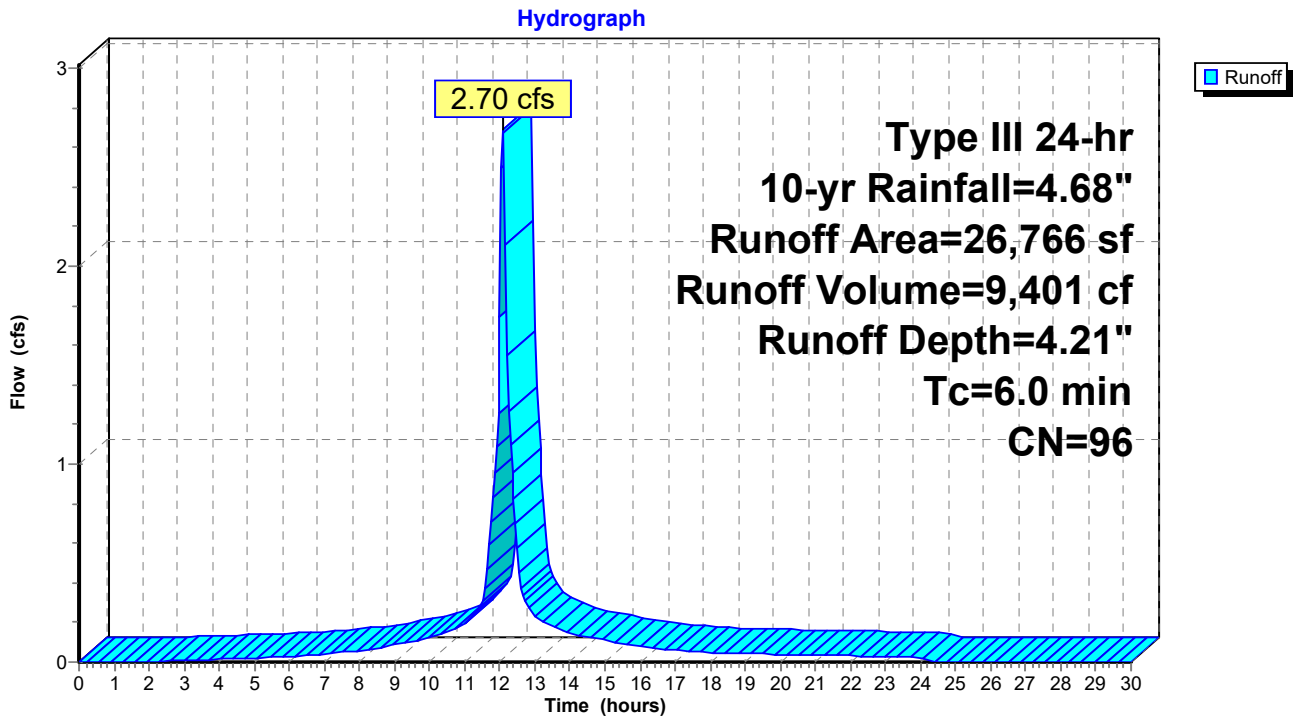
Runoff = 2.70 cfs @ 12.09 hrs, Volume= 9,401 cf, Depth= 4.21"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
23,545	98	Paved parking, HSG D
3,221	80	>75% Grass cover, Good, HSG D
26,766	96	Weighted Average
3,221		12.03% Pervious Area
23,545		87.97% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1C: PARKING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 67

**Summary for Subcatchment PW1D: ENTRANCE**

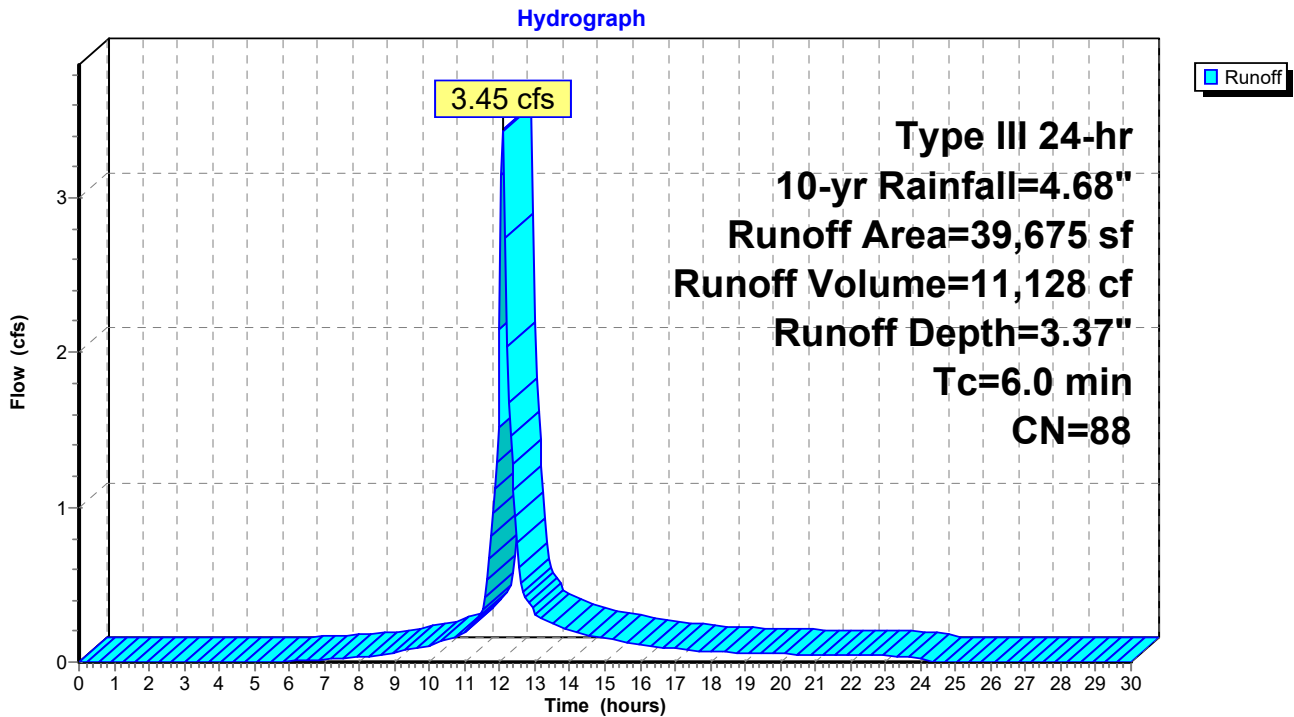
Runoff = 3.45 cfs @ 12.09 hrs, Volume= 11,128 cf, Depth= 3.37"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
17,739	98	Paved parking, HSG D
21,936	80	>75% Grass cover, Good, HSG D
39,675	88	Weighted Average
21,936		55.29% Pervious Area
17,739		44.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1D: ENTRANCE**





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 68

**Summary for Subcatchment PW1E: TRAILERS**

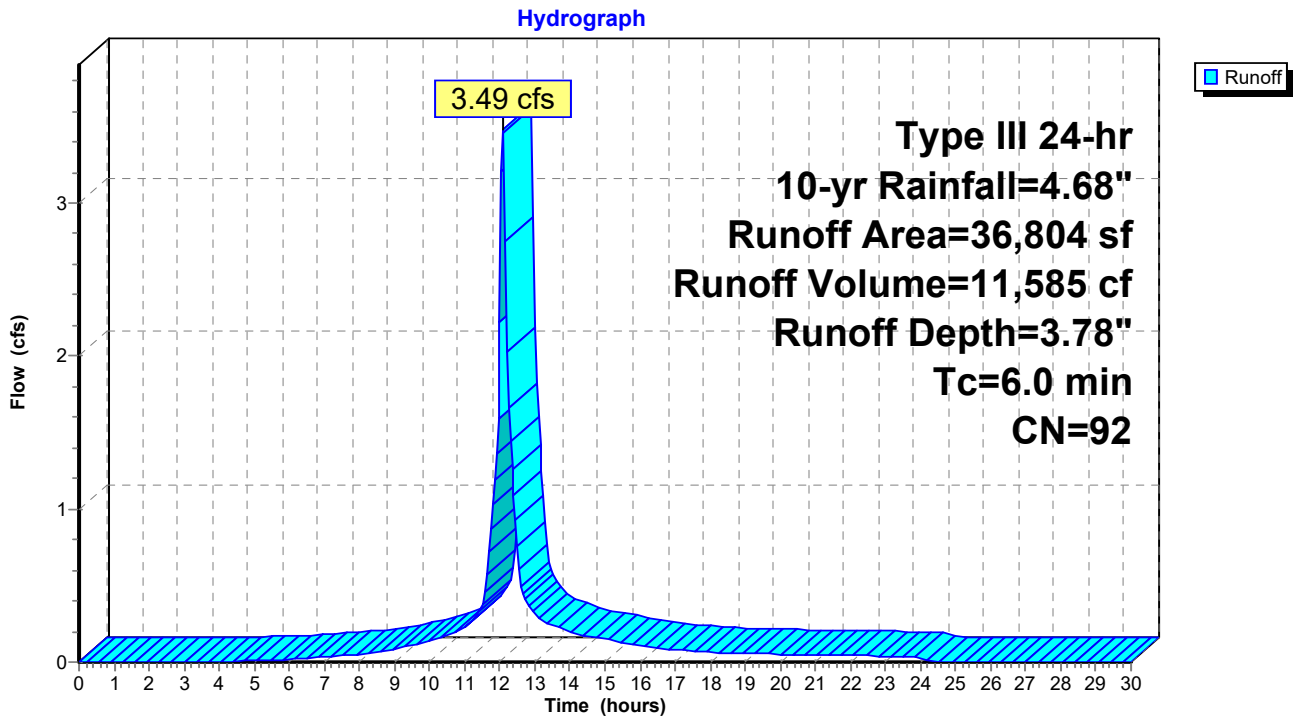
Runoff = 3.49 cfs @ 12.09 hrs, Volume= 11,585 cf, Depth= 3.78"  
Routed to Pond 1E : BIO-1E

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
25,092	98	Paved parking, HSG D
11,712	80	>75% Grass cover, Good, HSG D
36,804	92	Weighted Average
11,712		31.82% Pervious Area
25,092		68.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1E: TRAILERS**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 69

**Summary for Subcatchment PW1F: TRAILER 2**

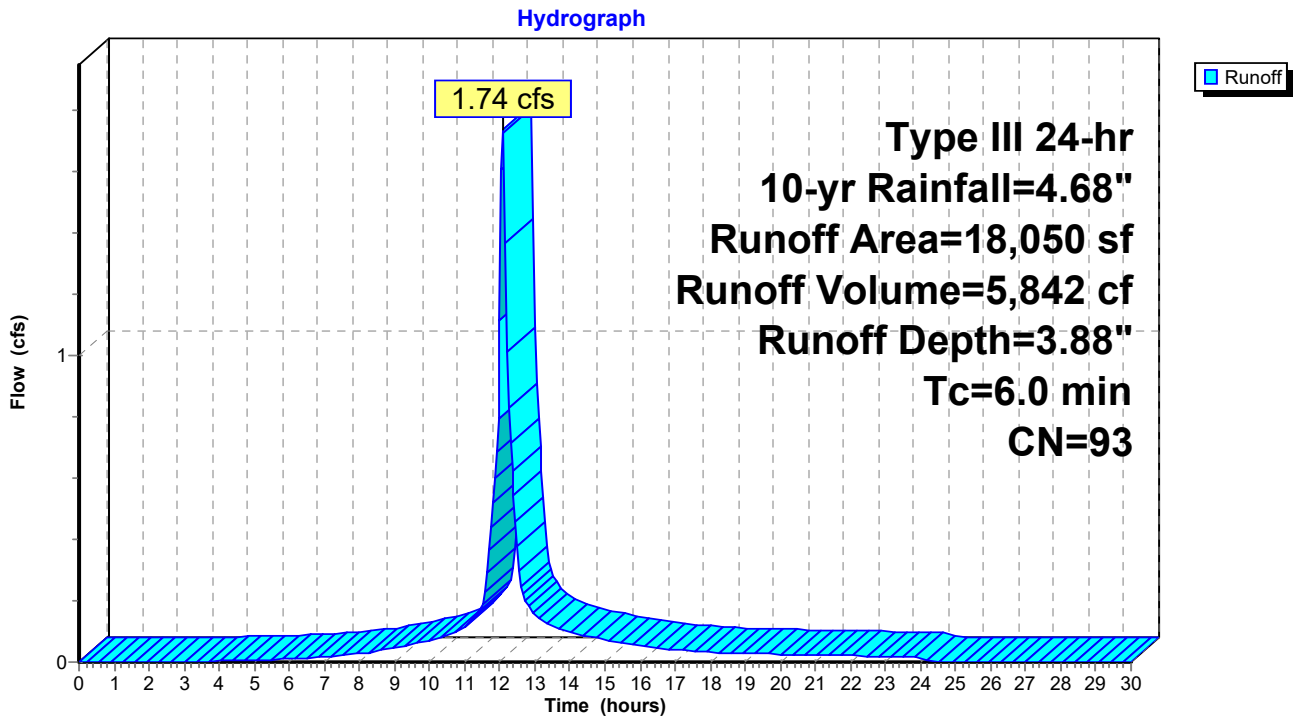
Runoff = 1.74 cfs @ 12.09 hrs, Volume= 5,842 cf, Depth= 3.88"  
 Routed to Pond 1F : BIO-1F

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
12,622	98	Paved parking, HSG D
5,428	80	>75% Grass cover, Good, HSG D
18,050	93	Weighted Average
5,428		30.07% Pervious Area
12,622		69.93% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1F: TRAILER 2**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 70

**Summary for Subcatchment PW1G: LOADING**

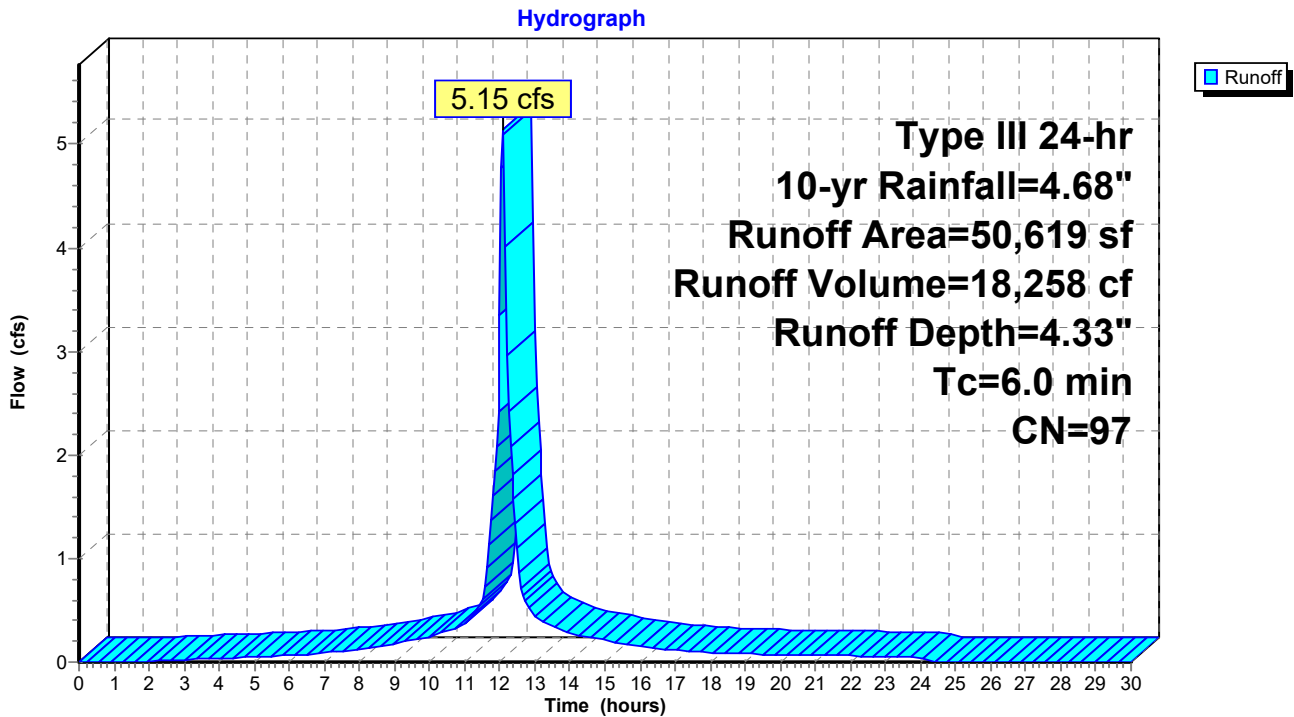
Runoff = 5.15 cfs @ 12.09 hrs, Volume= 18,258 cf, Depth= 4.33"  
Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
46,810	98	Paved parking, HSG D
3,809	80	>75% Grass cover, Good, HSG D
50,619	97	Weighted Average
3,809		7.52% Pervious Area
46,810		92.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1G: LOADING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 71

**Summary for Subcatchment PW1H: NW CORNER BLDG**

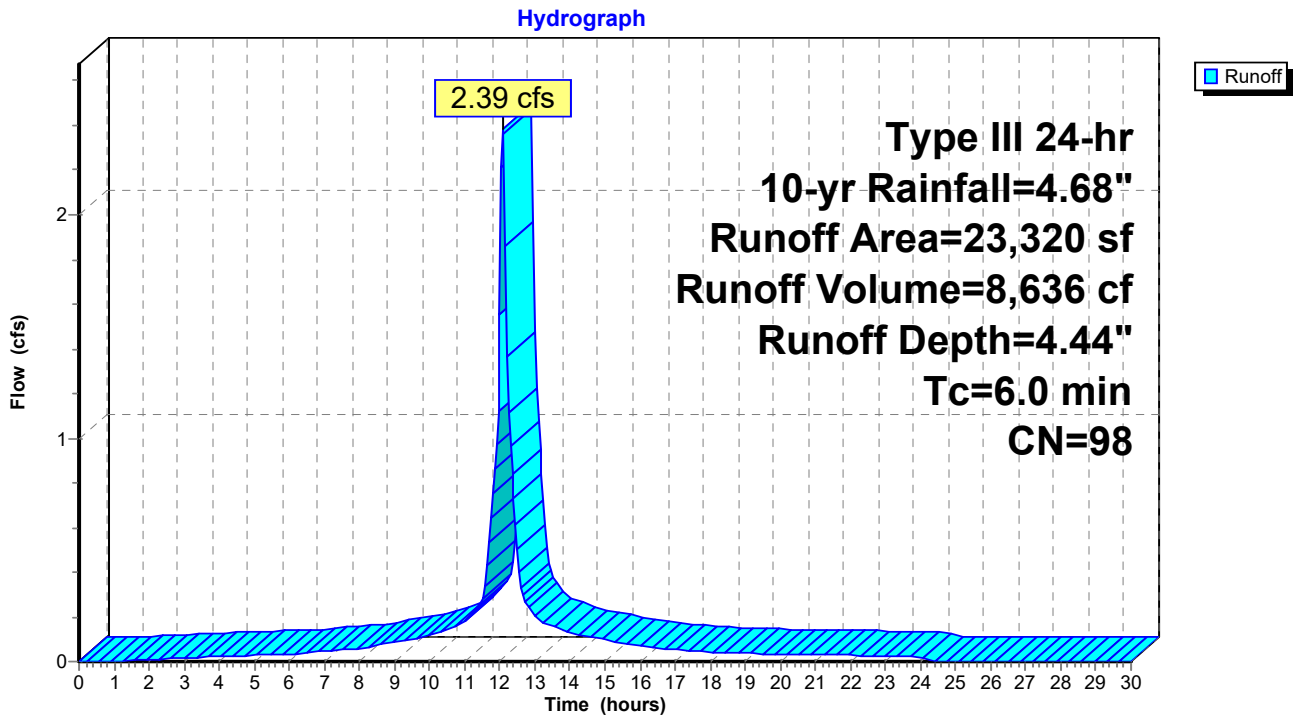
Runoff = 2.39 cfs @ 12.09 hrs, Volume= 8,636 cf, Depth= 4.44"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10-yr Rainfall=4.68"

Area (sf)	CN	Description
23,320	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
23,320	98	Weighted Average
23,320		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1H: NW CORNER BLDG**



**Summary for Pond 1BN: BIO-1BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth = 3.67" for 10-yr event  
 Inflow = 6.36 cfs @ 12.09 hrs, Volume= 20,945 cf  
 Outflow = 6.14 cfs @ 12.11 hrs, Volume= 15,797 cf, Atten= 3%, Lag= 1.4 min  
 Primary = 6.14 cfs @ 12.11 hrs, Volume= 15,797 cf  
 Routed to Pond 2BN : BIO-2BN

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 492.76' @ 12.11 hrs Surf.Area= 3,029 sf Storage= 6,086 cf

Plug-Flow detention time= 147.8 min calculated for 15,770 cf (75% of inflow)  
 Center-of-Mass det. time= 65.2 min ( 854.2 - 789.0 )

Volume	Invert	Avail.Storage	Storage Description		
#1	490.00'	10,349 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
490.00	1,454	0	0	1,454	
492.00	2,555	3,958	3,958	2,611	
494.00	3,883	6,392	10,349	4,013	

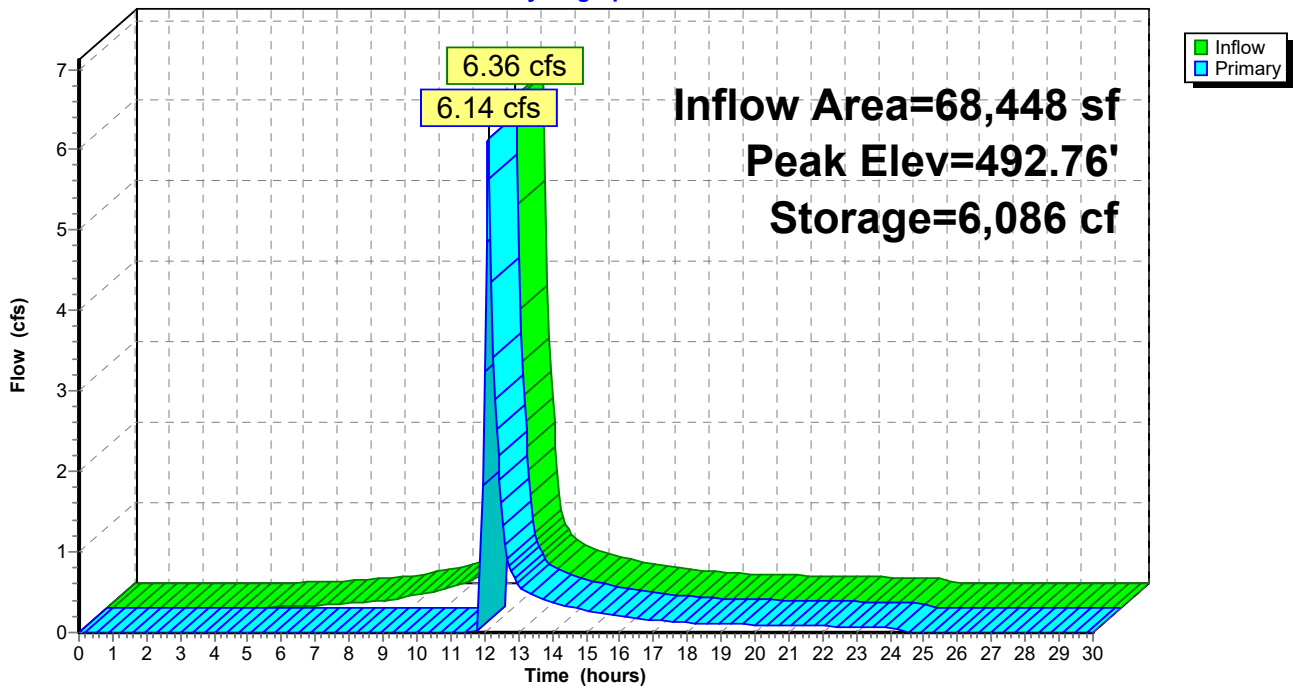
Device	Routing	Invert	Outlet Devices
#1	Primary	483.15'	<b>18.0" Round Culvert</b> L= 26.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 483.15' / 482.62' S= 0.0204 ' / Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	492.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	490.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=5.99 cfs @ 12.11 hrs HW=492.76' TW=484.81' (Dynamic Tailwater)

- 1=Culvert (Passes 5.99 cfs of 23.99 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 5.98 cfs @ 1.44 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1BN: BIO-1BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 74

**Stage-Area-Storage for Pond 1BN: BIO-1BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
490.00	1,454	0	492.65	2,956	5,747
490.05	1,478	73	492.70	2,988	5,896
490.10	1,502	148	492.75	3,021	6,046
490.15	1,526	223	492.80	3,053	6,198
490.20	1,550	300	492.85	3,086	6,351
490.25	1,575	378	492.90	3,118	6,506
490.30	1,599	458	492.95	3,151	6,663
490.35	1,624	538	493.00	3,184	6,822
490.40	1,650	620	493.05	3,218	6,982
490.45	1,675	703	493.10	3,251	7,143
490.50	1,700	788	493.15	3,285	7,307
490.55	1,726	873	493.20	3,319	7,472
490.60	1,752	960	493.25	3,353	7,639
490.65	1,778	1,049	493.30	3,387	7,807
490.70	1,804	1,138	493.35	3,421	7,977
490.75	1,831	1,229	493.40	3,456	8,149
490.80	1,857	1,321	493.45	3,490	8,323
490.85	1,884	1,415	493.50	3,525	8,498
490.90	1,911	1,510	493.55	3,560	8,675
490.95	1,939	1,606	493.60	3,595	8,854
491.00	1,966	1,704	493.65	3,631	9,035
491.05	1,994	1,803	493.70	3,666	9,217
491.10	2,021	1,903	493.75	3,702	9,401
491.15	2,049	2,005	493.80	3,738	9,587
491.20	2,078	2,108	493.85	3,774	9,775
491.25	2,106	2,212	493.90	3,810	9,965
491.30	2,135	2,318	493.95	3,846	10,156
491.35	2,163	2,426	494.00	<b>3,883</b>	<b>10,349</b>
491.40	2,192	2,535			
491.45	2,221	2,645			
491.50	2,251	2,757			
491.55	2,280	2,870			
491.60	2,310	2,985			
491.65	2,340	3,101			
491.70	2,370	3,219			
491.75	2,401	3,338			
491.80	2,431	3,459			
491.85	2,462	3,581			
491.90	2,493	3,705			
491.95	2,524	3,831			
492.00	2,555	3,958			
492.05	2,585	4,086			
492.10	2,615	4,216			
492.15	2,645	4,348			
492.20	2,675	4,481			
492.25	2,706	4,615			
492.30	2,737	4,751			
492.35	2,767	4,889			
492.40	2,798	5,028			
492.45	2,830	5,169			
492.50	2,861	5,311			
492.55	2,893	5,455			
492.60	2,924	5,600			

**Summary for Pond 1D: BIO-1D**

Inflow Area = 89,761 sf, 71.97% Impervious, Inflow Depth = 3.90" for 10-yr event  
 Inflow = 8.53 cfs @ 12.09 hrs, Volume= 29,165 cf  
 Outflow = 5.49 cfs @ 12.19 hrs, Volume= 25,427 cf, Atten= 36%, Lag= 6.0 min  
 Primary = 5.49 cfs @ 12.19 hrs, Volume= 25,427 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.97' @ 12.19 hrs Surf.Area= 7,730 sf Storage= 6,887 cf

Plug-Flow detention time= 117.8 min calculated for 25,427 cf (87% of inflow)  
 Center-of-Mass det. time= 59.4 min ( 832.8 - 773.4 )

Volume	Invert	Avail.Storage	Storage Description		
#1	468.00'	15,581 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
468.00	6,529	0	0	6,529	
470.00	9,124	15,581	15,581	9,218	

Device	Routing	Invert	Outlet Devices
#1	Primary	464.50'	<b>12.0" Round Culvert</b> L= 190.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 464.50' / 462.98' S= 0.0080 ' S= 0.0080 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.60'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	468.00'	<b>0.125 in/hr Exfiltration over Surface area</b>
#4	Primary	469.00'	<b>10.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83

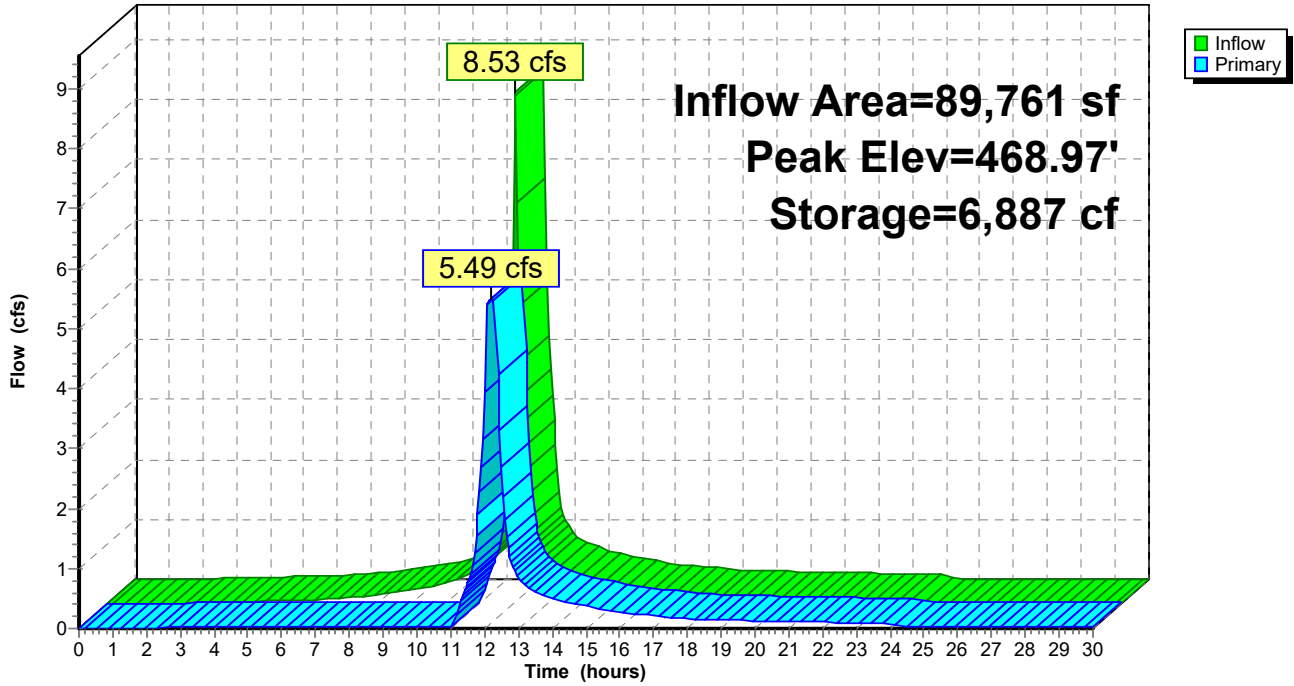
**Primary OutFlow** Max=5.48 cfs @ 12.19 hrs HW=468.96' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Barrel Controls 5.48 cfs @ 6.98 fps)
- 2=Broad-Crested Rectangular Weir (Passes < 10.20 cfs potential flow)
- 3=Exfiltration (Passes < 0.02 cfs potential flow)
- 4=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)



### Pond 1D: BIO-1D

Hydrograph



**Stage-Area-Storage for Pond 1D: BIO-1D**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
468.00	6,529	0	469.06	7,850	7,610
468.02	6,553	131	469.08	7,876	7,768
468.04	6,577	262	469.10	7,903	7,925
468.06	6,601	394	469.12	7,929	8,084
468.08	6,624	526	469.14	7,955	8,243
468.10	6,648	659	469.16	7,981	8,402
468.12	6,672	792	469.18	8,008	8,562
468.14	6,697	926	469.20	8,034	8,722
468.16	6,721	1,060	469.22	8,060	8,883
468.18	6,745	1,195	469.24	8,087	9,045
468.20	6,769	1,330	469.26	8,113	9,207
468.22	6,793	1,465	469.28	8,140	9,369
468.24	6,818	1,601	469.30	8,166	9,532
468.26	6,842	1,738	469.32	8,193	9,696
468.28	6,866	1,875	469.34	8,220	9,860
468.30	6,891	2,013	469.36	8,246	10,025
468.32	6,915	2,151	469.38	8,273	10,190
468.34	6,940	2,289	469.40	8,300	10,356
468.36	6,964	2,428	469.42	8,327	10,522
468.38	6,989	2,568	469.44	8,354	10,689
468.40	7,013	2,708	469.46	8,381	10,856
468.42	7,038	2,848	469.48	8,408	11,024
468.44	7,063	2,989	469.50	8,435	11,192
468.46	7,087	3,131	469.52	8,462	11,361
468.48	7,112	3,273	469.54	8,489	11,531
468.50	7,137	3,415	469.56	8,516	11,701
468.52	7,162	3,558	469.58	8,543	11,871
468.54	7,187	3,702	469.60	8,570	12,043
468.56	7,212	3,846	469.62	8,598	12,214
468.58	7,237	3,990	469.64	8,625	12,386
468.60	7,262	4,135	469.66	8,652	12,559
468.62	7,287	4,281	469.68	8,680	12,733
468.64	7,312	4,427	469.70	8,707	12,906
468.66	7,337	4,573	469.72	8,735	13,081
468.68	7,363	4,720	469.74	8,762	13,256
468.70	7,388	4,868	469.76	8,790	13,431
468.72	7,413	5,016	469.78	8,817	13,607
468.74	7,439	5,164	469.80	8,845	13,784
468.76	7,464	5,313	469.82	8,873	13,961
468.78	7,490	5,463	469.84	8,900	14,139
468.80	7,515	5,613	469.86	8,928	14,317
468.82	7,541	5,764	469.88	8,956	14,496
468.84	7,566	5,915	469.90	8,984	14,675
468.86	7,592	6,066	469.92	9,012	14,855
468.88	7,617	6,218	469.94	9,040	15,036
468.90	7,643	6,371	469.96	9,068	15,217
468.92	7,669	6,524	469.98	9,096	15,399
468.94	7,695	6,678	470.00	<b>9,124</b>	<b>15,581</b>
468.96	7,721	6,832			
468.98	7,746	6,986			
469.00	7,772	7,142			
469.02	7,798	7,297			
469.04	7,824	7,454			

**230119 - R1 - Dewpoint South**

Type III 24-hr 10-yr Rainfall=4.68"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 78

**Summary for Pond 1E: BIO-1E**

Inflow Area = 36,804 sf, 68.18% Impervious, Inflow Depth = 3.78" for 10-yr event  
 Inflow = 3.49 cfs @ 12.09 hrs, Volume= 11,585 cf  
 Outflow = 1.47 cfs @ 12.31 hrs, Volume= 6,531 cf, Atten= 58%, Lag= 13.2 min  
 Primary = 1.47 cfs @ 12.31 hrs, Volume= 6,531 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.60' @ 12.31 hrs Surf.Area= 4,218 sf Storage= 5,716 cf

Plug-Flow detention time= 233.0 min calculated for 6,521 cf (56% of inflow)  
 Center-of-Mass det. time= 127.2 min ( 912.0 - 784.8 )

Volume	Invert	Avail.Storage	Storage Description		
#1	467.00'	12,471 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
467.00	2,940	0	0	2,940	
468.00	3,728	3,326	3,326	3,761	
470.00	5,472	9,144	12,471	5,587	

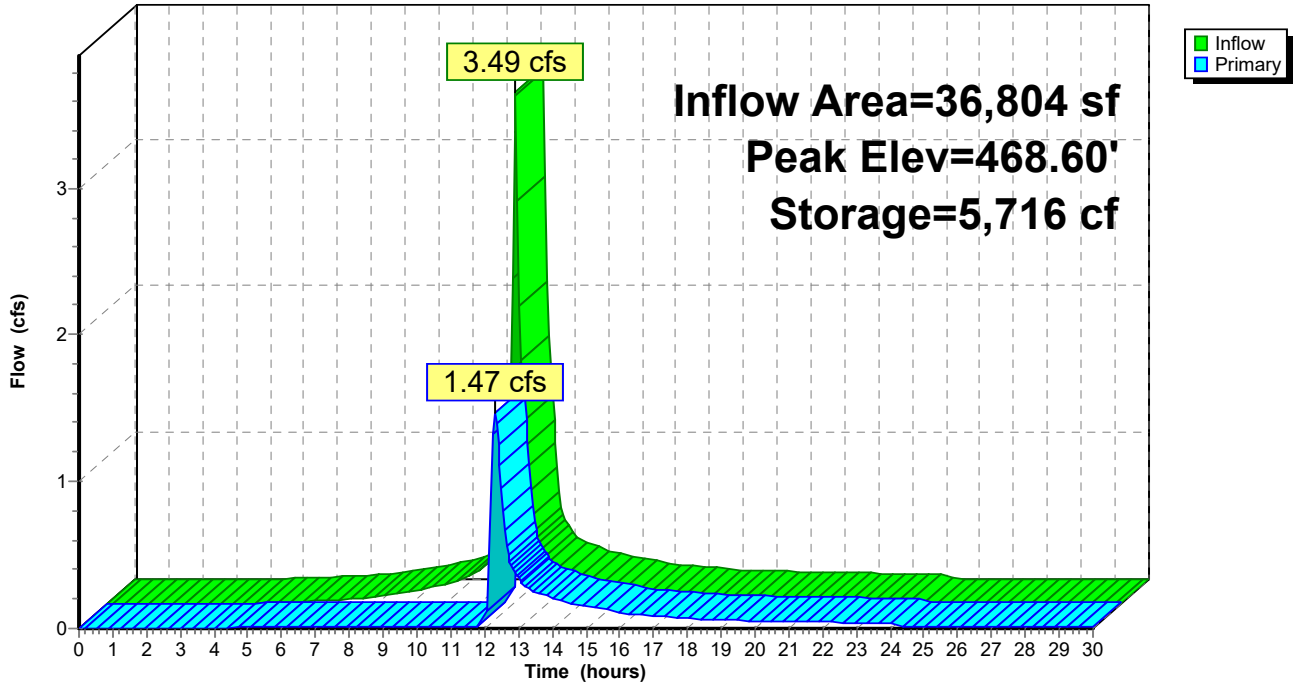
Device	Routing	Invert	Outlet Devices
#1	Primary	463.50'	<b>12.0" Round Culvert</b> L= 23.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 463.50' / 462.93' S= 0.0248 ' S= 0.0248 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	467.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=1.45 cfs @ 12.31 hrs HW=468.60' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 1.45 cfs of 8.11 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 1.44 cfs @ 0.89 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 1E: BIO-1E

Hydrograph



**Stage-Area-Storage for Pond 1E: BIO-1E**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
467.00	2,940	0	469.65	5,143	10,613
467.05	2,977	148	469.70	5,189	10,872
467.10	3,015	298	469.75	5,236	11,132
467.15	3,052	449	469.80	5,283	11,395
467.20	3,090	603	469.85	5,330	11,661
467.25	3,128	758	469.90	5,377	11,928
467.30	3,167	916	469.95	5,424	12,198
467.35	3,205	1,075	470.00	<b>5,472</b>	<b>12,471</b>
467.40	3,244	1,236			
467.45	3,283	1,399			
467.50	3,322	1,565			
467.55	3,362	1,732			
467.60	3,402	1,901			
467.65	3,442	2,072			
467.70	3,482	2,245			
467.75	3,522	2,420			
467.80	3,563	2,597			
467.85	3,604	2,776			
467.90	3,645	2,958			
467.95	3,686	3,141			
468.00	3,728	3,326			
468.05	3,768	3,514			
468.10	3,807	3,703			
468.15	3,847	3,894			
468.20	3,887	4,088			
468.25	3,928	4,283			
468.30	3,968	4,480			
468.35	4,009	4,680			
468.40	4,050	4,881			
468.45	4,091	5,085			
468.50	4,133	5,291			
468.55	4,174	5,498			
468.60	4,216	5,708			
468.65	4,258	5,920			
468.70	4,300	6,134			
468.75	4,343	6,350			
468.80	4,386	6,568			
468.85	4,428	6,788			
468.90	4,472	7,011			
468.95	4,515	7,236			
469.00	4,558	7,462			
469.05	4,602	7,691			
469.10	4,646	7,923			
469.15	4,690	8,156			
469.20	4,734	8,392			
469.25	4,779	8,629			
469.30	4,824	8,870			
469.35	4,869	9,112			
469.40	4,914	9,356			
469.45	4,959	9,603			
469.50	5,005	9,852			
469.55	5,051	10,104			
469.60	5,097	10,357			

**230119 - R1 - Dewpoint South**

Type III 24-hr 10-yr Rainfall=4.68"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 81

**Summary for Pond 1F: BIO-1F**

Inflow Area = 18,050 sf, 69.93% Impervious, Inflow Depth = 3.88" for 10-yr event  
 Inflow = 1.74 cfs @ 12.09 hrs, Volume= 5,842 cf  
 Outflow = 0.89 cfs @ 12.25 hrs, Volume= 3,314 cf, Atten= 49%, Lag= 10.0 min  
 Primary = 0.89 cfs @ 12.25 hrs, Volume= 3,314 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 478.57' @ 12.25 hrs Surf.Area= 2,267 sf Storage= 2,822 cf

Plug-Flow detention time= 233.3 min calculated for 3,309 cf (57% of inflow)  
 Center-of-Mass det. time= 127.3 min ( 907.6 - 780.3 )

Volume	Invert	Avail.Storage	Storage Description		
#1	477.00'	6,744 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
477.00	1,347	0	0	1,347	
478.00	1,919	1,625	1,625	1,941	
480.00	3,259	5,119	6,744	3,341	

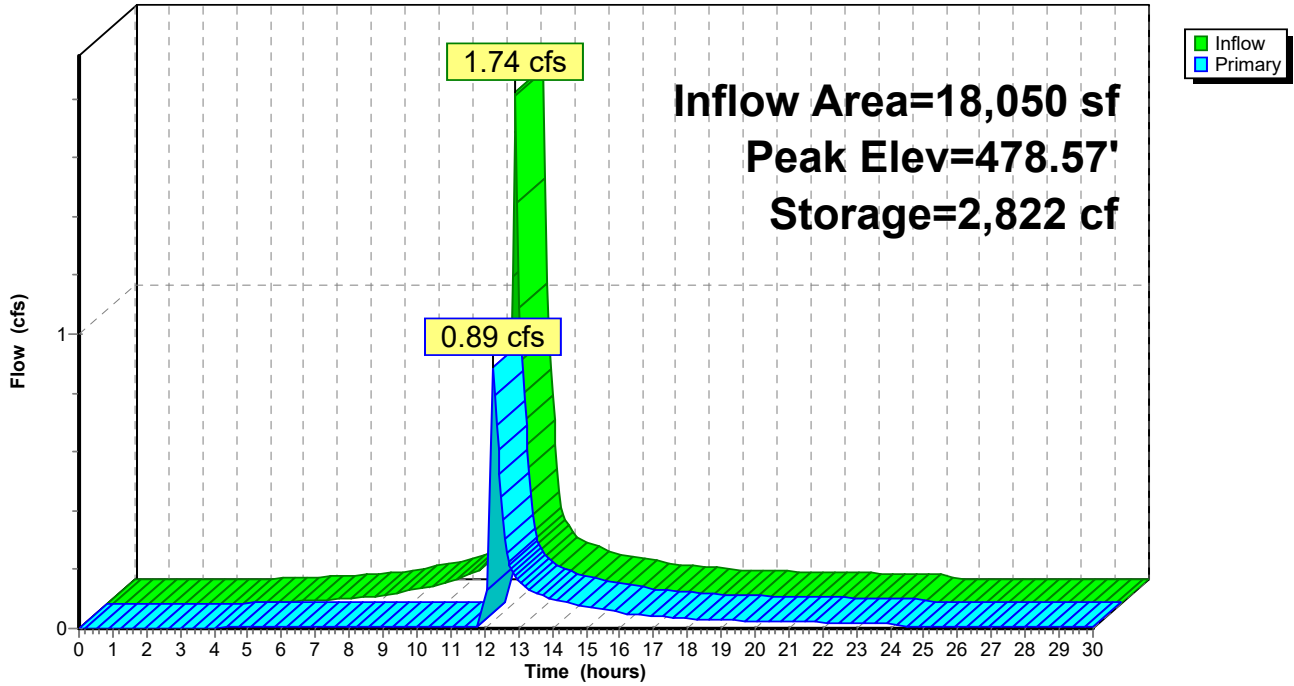
Device	Routing	Invert	Outlet Devices
#1	Primary	473.50'	<b>12.0" Round Culvert</b> L= 115.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 473.50' / 471.21' S= 0.0199 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	478.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	477.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.88 cfs @ 12.25 hrs HW=478.57' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.88 cfs of 7.43 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 0.87 cfs @ 0.75 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1F: BIO-1F

Hydrograph



**Stage-Area-Storage for Pond 1F: BIO-1F**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
477.00	1,347	0	479.65	2,999	5,649
477.05	1,373	68	479.70	3,036	5,800
477.10	1,400	137	479.75	3,072	5,953
477.15	1,426	208	479.80	3,109	6,107
477.20	1,453	280	479.85	3,146	6,263
477.25	1,481	353	479.90	3,184	6,422
477.30	1,508	428	479.95	3,221	6,582
477.35	1,536	504	480.00	<b>3,259</b>	<b>6,744</b>
477.40	1,564	582			
477.45	1,592	660			
477.50	1,620	741			
477.55	1,649	823			
477.60	1,678	906			
477.65	1,707	990			
477.70	1,737	1,076			
477.75	1,767	1,164			
477.80	1,797	1,253			
477.85	1,827	1,344			
477.90	1,857	1,436			
477.95	1,888	1,529			
478.00	1,919	1,625			
478.05	1,948	1,721			
478.10	1,978	1,819			
478.15	2,007	1,919			
478.20	2,037	2,020			
478.25	2,067	2,123			
478.30	2,098	2,227			
478.35	2,128	2,333			
478.40	2,159	2,440			
478.45	2,190	2,548			
478.50	2,221	2,659			
478.55	2,252	2,770			
478.60	2,284	2,884			
478.65	2,316	2,999			
478.70	2,348	3,115			
478.75	2,380	3,234			
478.80	2,413	3,353			
478.85	2,445	3,475			
478.90	2,478	3,598			
478.95	2,512	3,723			
479.00	2,545	3,849			
479.05	2,579	3,977			
479.10	2,612	4,107			
479.15	2,646	4,239			
479.20	2,681	4,372			
479.25	2,715	4,507			
479.30	2,750	4,643			
479.35	2,785	4,782			
479.40	2,820	4,922			
479.45	2,855	5,064			
479.50	2,891	5,207			
479.55	2,927	5,353			
479.60	2,963	5,500			



**Summary for Pond 2BN: BIO-2BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth > 2.77" for 10-yr event  
 Inflow = 6.14 cfs @ 12.11 hrs, Volume= 15,797 cf  
 Outflow = 1.98 cfs @ 12.44 hrs, Volume= 14,284 cf, Atten= 68%, Lag= 19.6 min  
 Primary = 1.98 cfs @ 12.44 hrs, Volume= 14,284 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 485.42' @ 12.44 hrs Surf.Area= 3,846 sf Storage= 4,743 cf

Plug-Flow detention time= 98.0 min calculated for 14,284 cf (90% of inflow)  
 Center-of-Mass det. time= 46.8 min ( 901.0 - 854.2 )

Volume	Invert	Avail.Storage	Storage Description		
#1	484.00'	17,309 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
484.00	2,843	0	0	2,843	
486.00	4,295	7,088	7,088	4,371	
488.00	5,972	10,221	17,309	6,142	

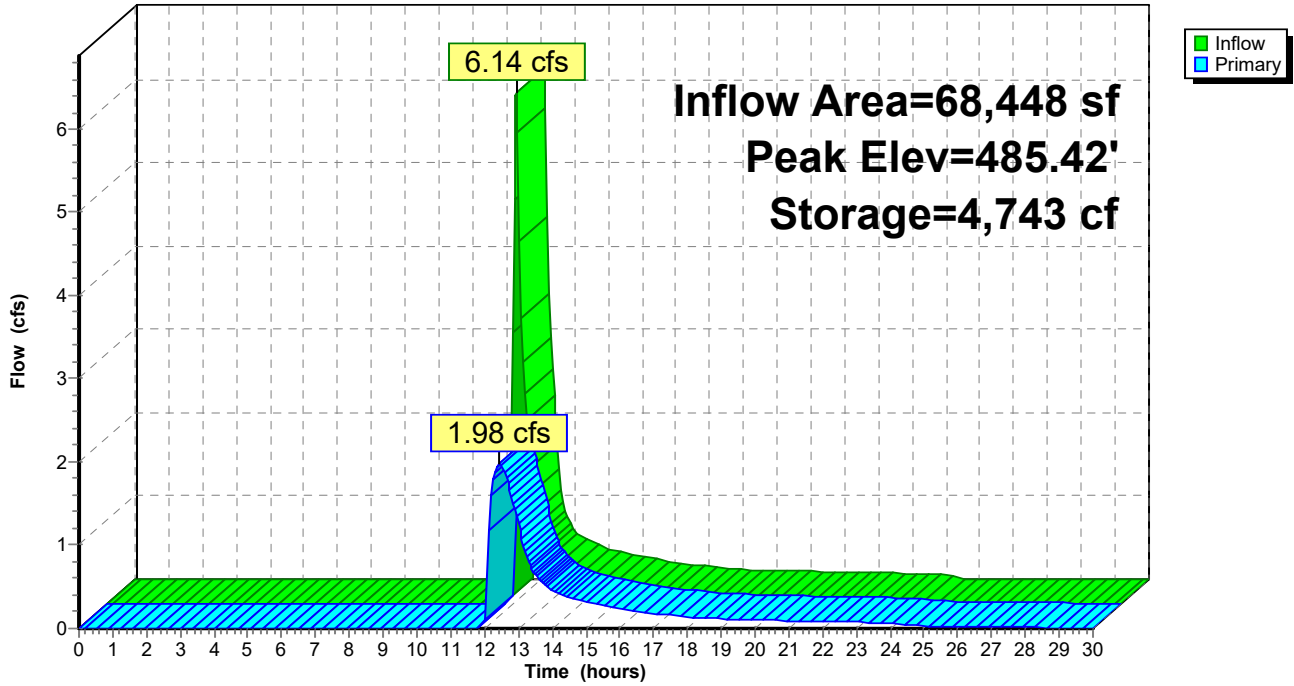
Device	Routing	Invert	Outlet Devices
#1	Primary	480.50'	<b>18.0" Round Culvert</b> L= 52.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 480.50' / 478.00' S= 0.0481 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	486.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	484.50'	<b>12.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	484.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=1.97 cfs @ 12.44 hrs HW=485.42' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 1.97 cfs of 17.38 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Orifice/Grate (Orifice Controls 1.96 cfs @ 3.93 fps)
- 4=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 2BN: BIO-2BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 86

**Stage-Area-Storage for Pond 2BN: BIO-2BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
484.00	2,843	0	486.65	4,810	10,046
484.05	2,876	143	486.70	4,851	10,287
484.10	2,909	288	486.75	4,892	10,531
484.15	2,942	434	486.80	4,933	10,776
484.20	2,975	582	486.85	4,974	11,024
484.25	3,008	731	486.90	5,016	11,274
484.30	3,042	883	486.95	5,057	11,526
484.35	3,076	1,035	487.00	5,099	11,780
484.40	3,110	1,190	487.05	5,141	12,036
484.45	3,144	1,346	487.10	5,183	12,294
484.50	3,178	1,504	487.15	5,226	12,554
484.55	3,213	1,664	487.20	5,268	12,816
484.60	3,247	1,826	487.25	5,311	13,081
484.65	3,282	1,989	487.30	5,354	13,347
484.70	3,317	2,154	487.35	5,397	13,616
484.75	3,353	2,321	487.40	5,440	13,887
484.80	3,388	2,489	487.45	5,483	14,160
484.85	3,424	2,659	487.50	5,527	14,435
484.90	3,459	2,832	487.55	5,571	14,713
484.95	3,495	3,005	487.60	5,615	14,992
485.00	3,532	3,181	487.65	5,659	15,274
485.05	3,568	3,359	487.70	5,703	15,558
485.10	3,605	3,538	487.75	5,747	15,844
485.15	3,641	3,719	487.80	5,792	16,133
485.20	3,678	3,902	487.85	5,837	16,424
485.25	3,716	4,087	487.90	5,882	16,717
485.30	3,753	4,274	487.95	5,927	17,012
485.35	3,790	4,462	488.00	<b>5,972</b>	<b>17,309</b>
485.40	3,828	4,653			
485.45	3,866	4,845			
485.50	3,904	5,039			
485.55	3,942	5,235			
485.60	3,981	5,434			
485.65	4,019	5,634			
485.70	4,058	5,835			
485.75	4,097	6,039			
485.80	4,136	6,245			
485.85	4,176	6,453			
485.90	4,215	6,663			
485.95	4,255	6,875			
486.00	4,295	7,088			
486.05	4,334	7,304			
486.10	4,372	7,522			
486.15	4,411	7,741			
486.20	4,450	7,963			
486.25	4,490	8,186			
486.30	4,529	8,412			
486.35	4,569	8,639			
486.40	4,608	8,869			
486.45	4,648	9,100			
486.50	4,688	9,333			
486.55	4,729	9,569			
486.60	4,769	9,806			

**Summary for Pond SUBS: SUBS**

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth = 4.39" for 10-yr event  
 Inflow = 11.56 cfs @ 12.09 hrs, Volume= 41,416 cf  
 Outflow = 0.76 cfs @ 13.55 hrs, Volume= 40,709 cf, Atten= 93%, Lag= 87.6 min  
 Primary = 0.76 cfs @ 13.55 hrs, Volume= 40,709 cf  
 Routed to Link JF : JELLY FISH  
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 478.42' @ 13.55 hrs Surf.Area= 8,608 sf Storage= 21,621 cf

Plug-Flow detention time= 323.9 min calculated for 40,641 cf (98% of inflow)  
 Center-of-Mass det. time= 313.1 min ( 1,065.8 - 752.7 )

Volume	Invert	Avail.Storage	Storage Description
#1A	475.00'	13,785 cf	<b>83.00'W x 103.72'L x 6.75'H Field A</b> 58,107 cf Overall - 23,645 cf Embedded = 34,463 cf x 40.0% Voids
#2A	475.75'	23,645 cf	<b>ADS_StormTech MC-4500 +Cap x 216 Inside #1</b> Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 216 Chambers in 9 Rows Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf
		37,430 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	472.00'	<b>12.0" Round Culvert</b> L= 30.9' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 472.00' / 471.69' S= 0.0100 '/ Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	475.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Device 1	480.25'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Secondary	479.00'	<b>18.0" Round Culvert</b> L= 46.5' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 479.00' / 477.56' S= 0.0310 '/ Cc= 0.900 n= 0.012, Flow Area= 1.77 sf

**Primary OutFlow** Max=0.76 cfs @ 13.55 hrs HW=478.42' TW=0.00' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 0.76 cfs of 10.60 cfs potential flow)
- ↑ 2=Orifice/Grate (Orifice Controls 0.76 cfs @ 8.69 fps)
- ↑ 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=475.00' TW=0.00' (Dynamic Tailwater)

- ↑ 4=Culvert ( Controls 0.00 cfs)

**Pond SUBS: SUBS - Chamber Wizard Field A**

**Chamber Model = ADS\_StormTech MC-4500 +Cap (ADS StormTech® MC-4500 with cap, use MC-4500 b for new designs)**

Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf

Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap

Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf

100.0" Wide + 9.0" Spacing = 109.0" C-C Row Spacing

24 Chambers/Row x 4.02' Long +2.56' Cap Length x 2 = 101.72' Row Length +12.0" End Stone x 2 = 103.72' Base Length

9 Rows x 100.0" Wide + 9.0" Spacing x 8 + 12.0" Side Stone x 2 = 83.00' Base Width

9.0" Stone Base + 60.0" Chamber Height + 12.0" Stone Cover = 6.75' Field Height

216 Chambers x 106.5 cf + 35.7 cf Cap Volume x 2 x 9 Rows = 23,644.5 cf Chamber Storage

58,107.3 cf Field - 23,644.5 cf Chambers = 34,462.7 cf Stone x 40.0% Voids = 13,785.1 cf Stone Storage

Chamber Storage + Stone Storage = 37,429.6 cf = 0.859 af

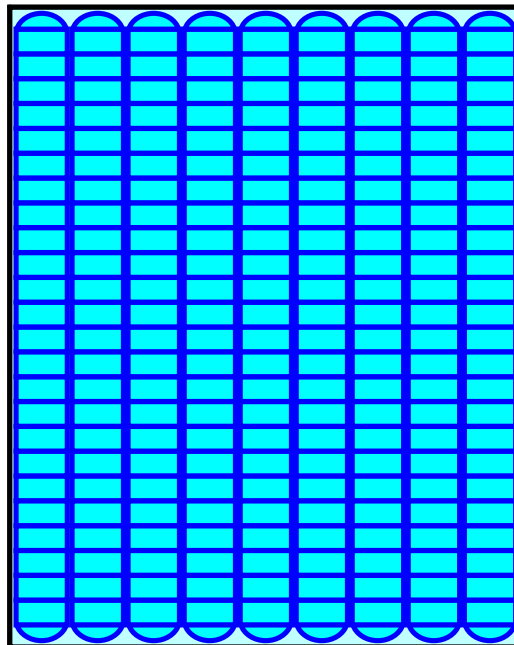
Overall Storage Efficiency = 64.4%

Overall System Size = 103.72' x 83.00' x 6.75'

216 Chambers

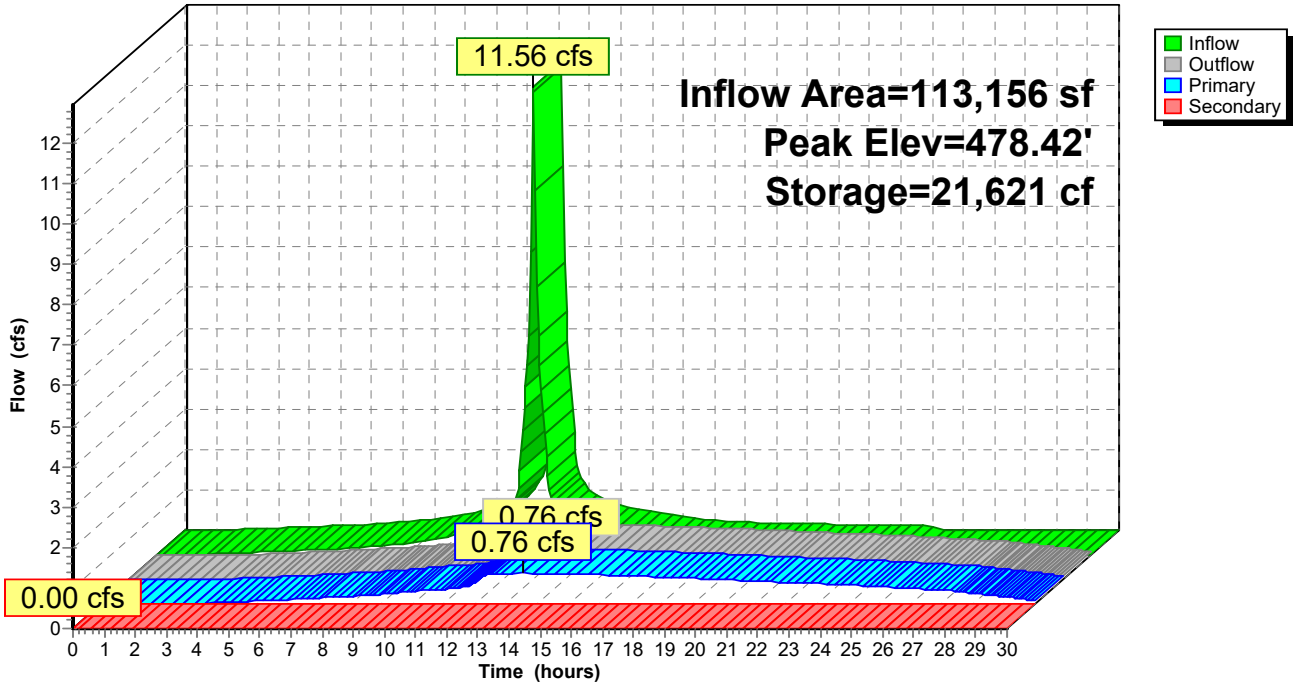
2,152.1 cy Field

1,276.4 cy Stone



### Pond SUBS: SUBS

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 10-yr Rainfall=4.68"

Printed 2/2/2023

Page 90

**Stage-Area-Storage for Pond SUBS: SUBS**

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
475.00	0	477.65	16,390	480.30	32,305
475.05	172	477.70	16,738	480.35	32,508
475.10	344	477.75	17,084	480.40	32,704
475.15	517	477.80	17,429	480.45	32,895
475.20	689	477.85	17,773	480.50	33,084
475.25	861	477.90	18,115	480.55	33,270
475.30	1,033	477.95	18,457	480.60	33,453
475.35	1,205	478.00	18,797	480.65	33,634
475.40	1,377	478.05	19,136	480.70	33,812
475.45	1,550	478.10	19,474	480.75	33,986
475.50	1,722	478.15	19,810	480.80	34,158
475.55	1,894	478.20	20,145	480.85	34,331
475.60	2,066	478.25	20,478	480.90	34,503
475.65	2,238	478.30	20,811	480.95	34,675
475.70	2,410	478.35	21,141	481.00	34,847
475.75	2,583	478.40	21,470	481.05	35,019
475.80	2,957	478.45	21,798	481.10	35,191
475.85	3,330	478.50	22,124	481.15	35,364
475.90	3,704	478.55	22,449	481.20	35,536
475.95	4,077	478.60	22,771	481.25	35,708
476.00	4,449	478.65	23,093	481.30	35,880
476.05	4,821	478.70	23,412	481.35	36,052
476.10	5,193	478.75	23,730	481.40	36,224
476.15	5,564	478.80	24,045	481.45	36,397
476.20	5,934	478.85	24,360	481.50	36,569
476.25	6,304	478.90	24,672	481.55	36,741
476.30	6,674	478.95	24,982	481.60	36,913
476.35	7,043	479.00	25,290	481.65	37,085
476.40	7,411	479.05	25,596	481.70	37,257
476.45	7,779	479.10	25,900	481.75	<b>37,430</b>
476.50	8,147	479.15	26,202		
476.55	8,513	479.20	26,501		
476.60	8,879	479.25	26,798		
476.65	9,245	479.30	27,093		
476.70	9,610	479.35	27,386		
476.75	9,974	479.40	27,675		
476.80	10,338	479.45	27,963		
476.85	10,700	479.50	28,247		
476.90	11,062	479.55	28,529		
476.95	11,424	479.60	28,808		
477.00	11,784	479.65	29,084		
477.05	12,144	479.70	29,357		
477.10	12,503	479.75	29,627		
477.15	12,861	479.80	29,893		
477.20	13,218	479.85	30,156		
477.25	13,574	479.90	30,414		
477.30	13,930	479.95	30,669		
477.35	14,284	480.00	30,920		
477.40	14,638	480.05	31,166		
477.45	14,990	480.10	31,407		
477.50	15,342	480.15	31,643		
477.55	15,692	480.20	31,872		
477.60	16,042	480.25	32,093		

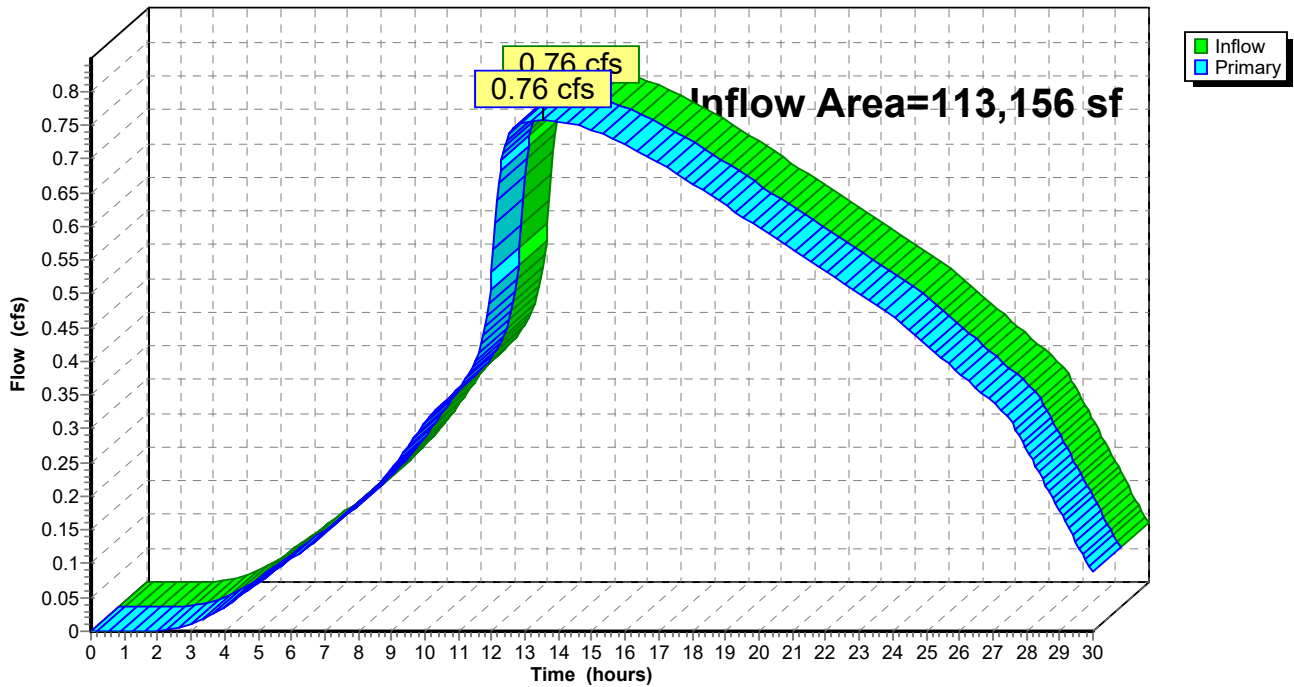
### Summary for Link JF: JELLY FISH

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth > 4.32" for 10-yr event  
Inflow = 0.76 cfs @ 13.55 hrs, Volume= 40,709 cf  
Primary = 0.76 cfs @ 13.55 hrs, Volume= 40,709 cf, Atten= 0%, Lag= 0.0 min  
Routed to Link PROP : PROPOSED

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link JF: JELLY FISH

Hydrograph



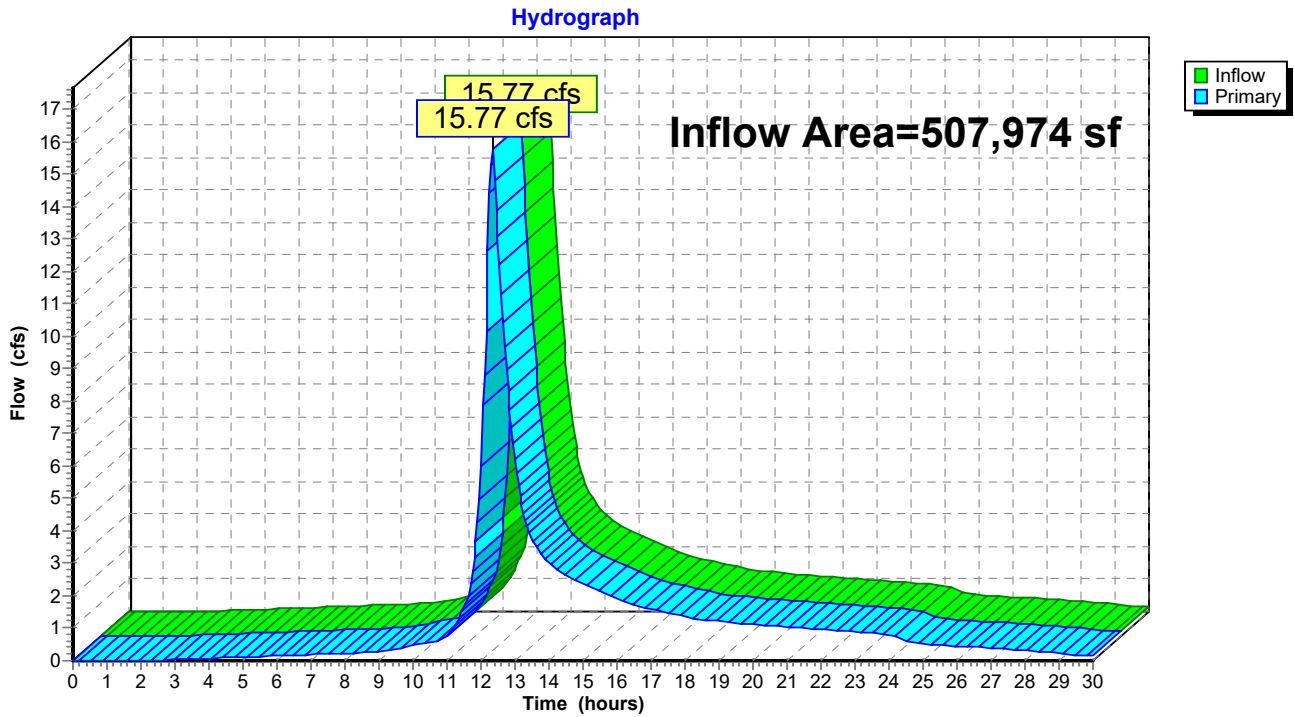


Summary for Link PROP: PROPOSED

Inflow Area = 507,974 sf, 50.18% Impervious, Inflow Depth > 3.01" for 10-yr event  
Inflow = 15.77 cfs @ 12.34 hrs, Volume= 127,256 cf  
Primary = 15.77 cfs @ 12.34 hrs, Volume= 127,256 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Link PROP: PROPOSED



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 93

**Summary for Subcatchment PW1A: LOD**

Runoff = 14.33 cfs @ 12.47 hrs, Volume= 84,739 cf, Depth= 5.59"  
 Routed to Link PROP : PROPOSED

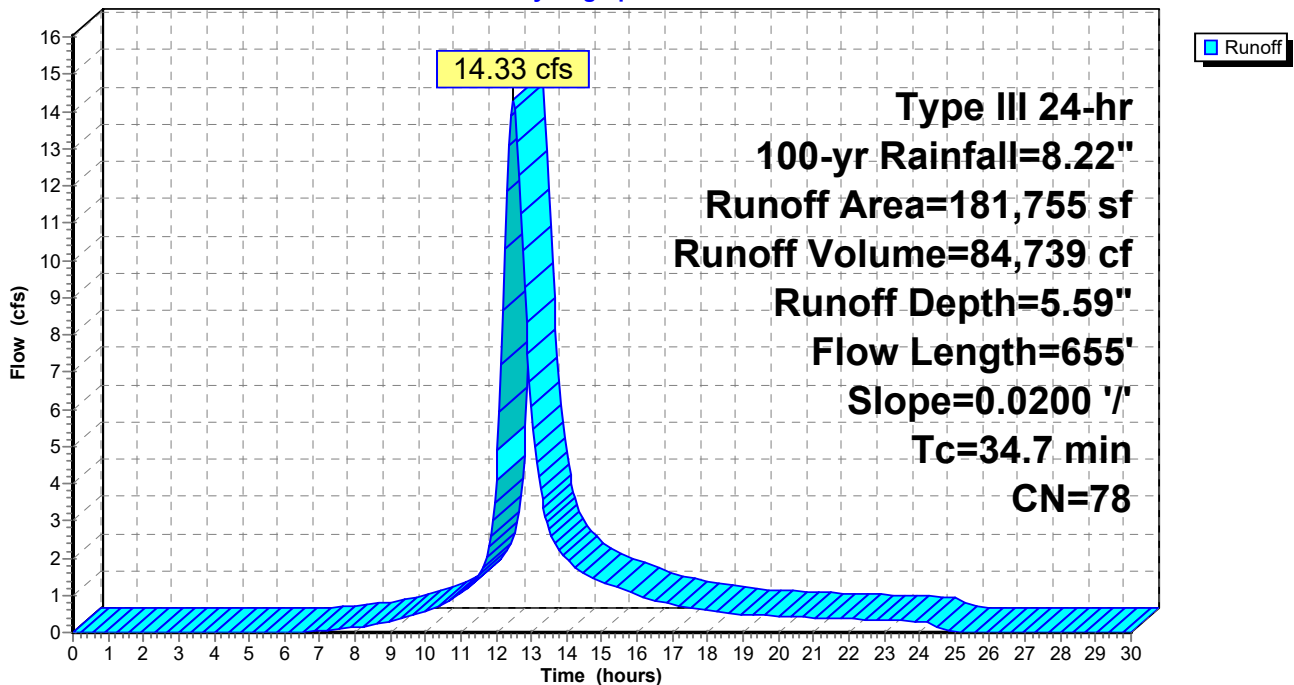
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
2,800	98	Paved parking, HSG D
73,077	80	>75% Grass cover, Good, HSG D
22,724	73	Brush, Good, HSG D
83,154	77	Woods, Good, HSG D
181,755	78	Weighted Average
178,955		98.46% Pervious Area
2,800		1.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment PW1A: LOD**

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 94

**Summary for Subcatchment PW1BN: N HALF BLDG**

Runoff = 11.90 cfs @ 12.09 hrs, Volume= 40,736 cf, Depth= 7.14"  
 Routed to Pond 1BN : BIO-1BN

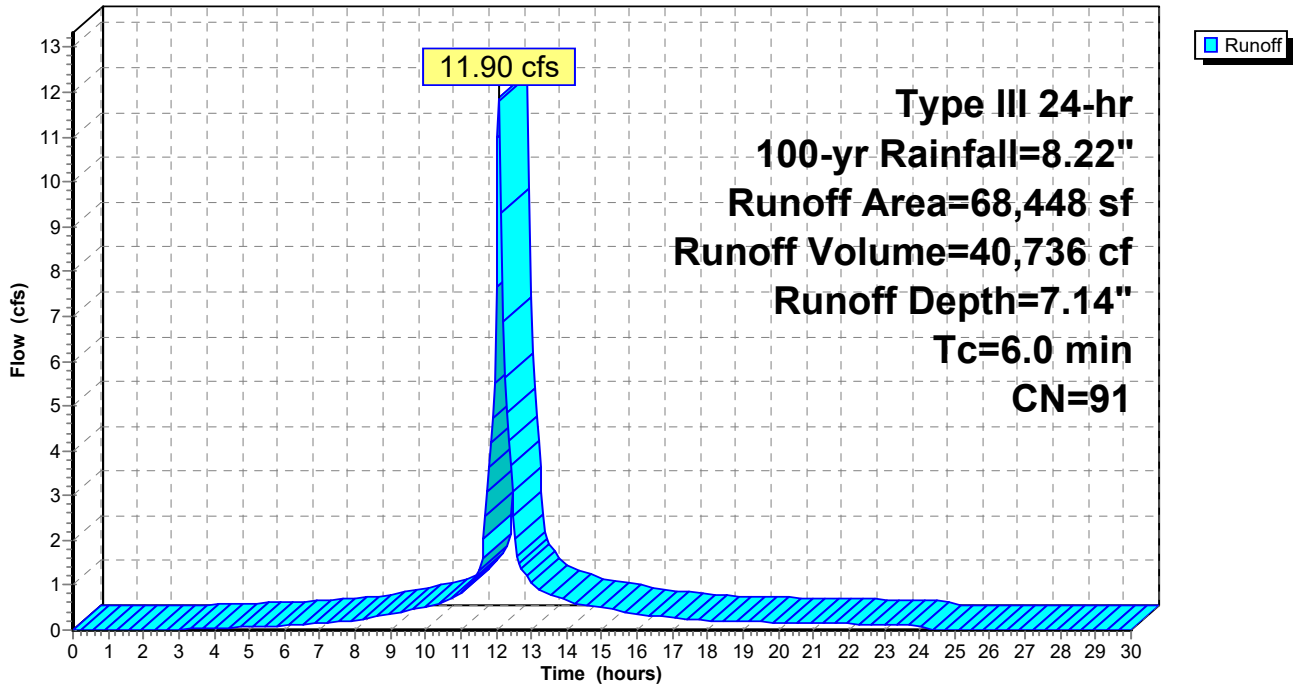
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
40,450	98	Paved parking, HSG D
27,998	80	>75% Grass cover, Good, HSG D
68,448	91	Weighted Average
27,998		40.90% Pervious Area
40,450		59.10% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BN: N HALF BLDG**

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 95

**Summary for Subcatchment PW1BS: S HALF BLDG**

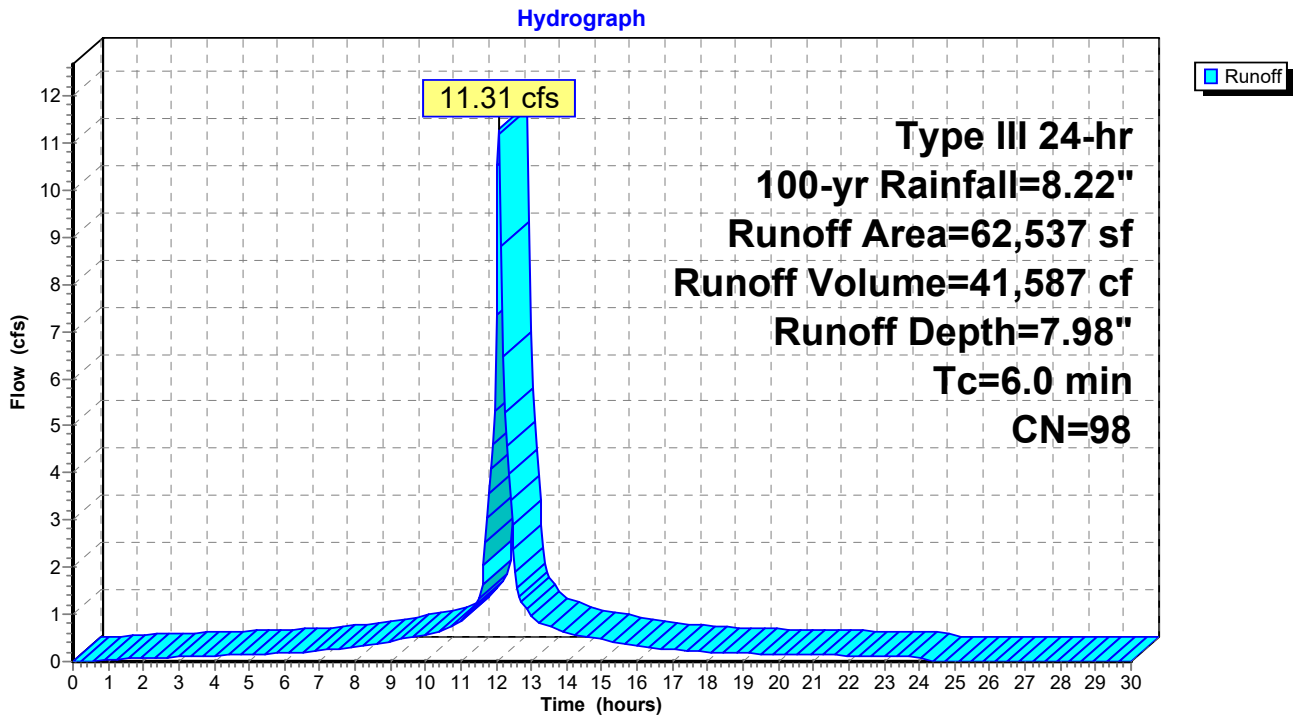
Runoff = 11.31 cfs @ 12.09 hrs, Volume= 41,587 cf, Depth= 7.98"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
62,537	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
62,537	98	Weighted Average
62,537		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BS: S HALF BLDG**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 96

**Summary for Subcatchment PW1C: PARKING**

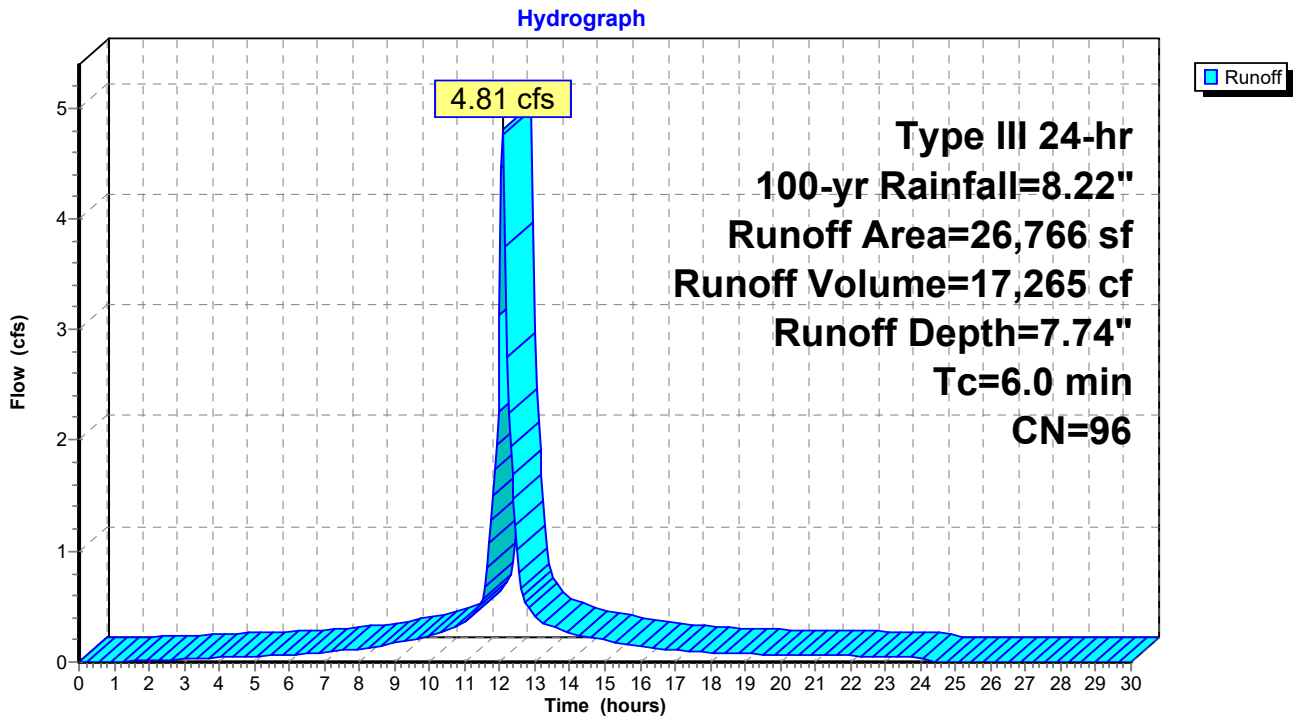
Runoff = 4.81 cfs @ 12.09 hrs, Volume= 17,265 cf, Depth= 7.74"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
23,545	98	Paved parking, HSG D
3,221	80	>75% Grass cover, Good, HSG D
26,766	96	Weighted Average
3,221		12.03% Pervious Area
23,545		87.97% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1C: PARKING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 97

**Summary for Subcatchment PW1D: ENTRANCE**

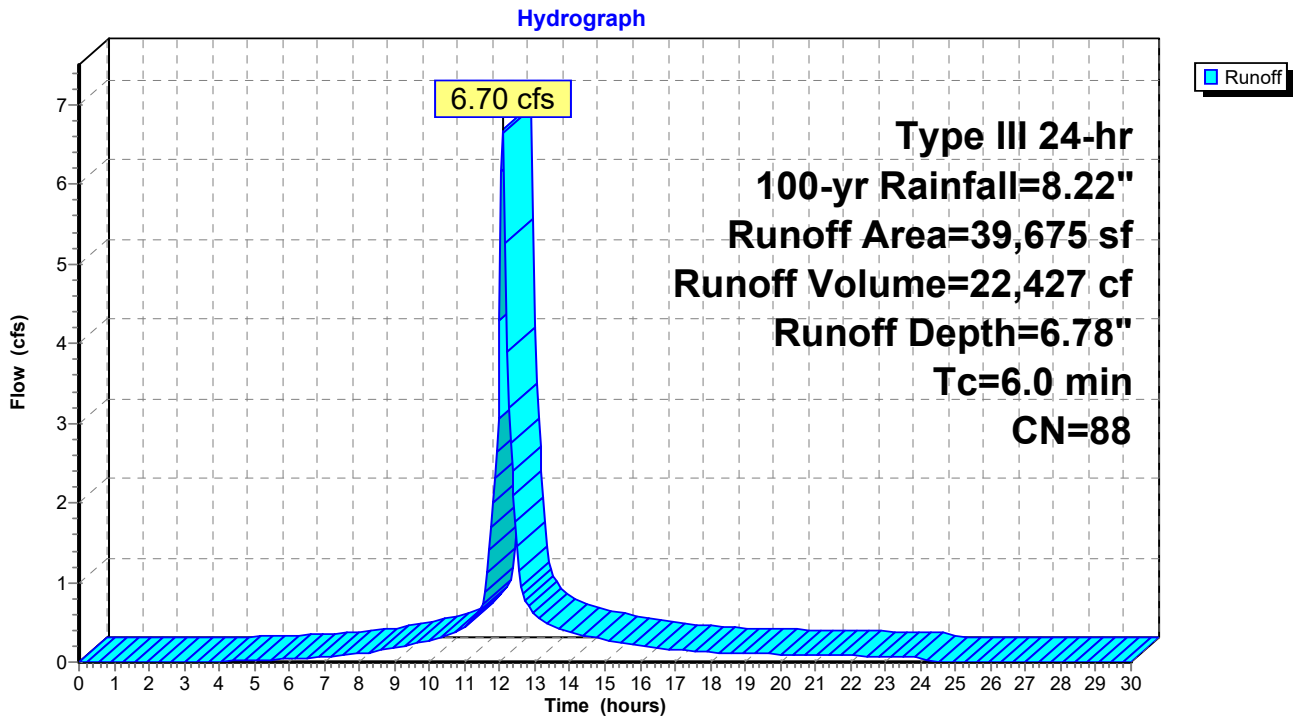
Runoff = 6.70 cfs @ 12.09 hrs, Volume= 22,427 cf, Depth= 6.78"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
17,739	98	Paved parking, HSG D
21,936	80	>75% Grass cover, Good, HSG D
39,675	88	Weighted Average
21,936		55.29% Pervious Area
17,739		44.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1D: ENTRANCE**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 98

**Summary for Subcatchment PW1E: TRAILERS**

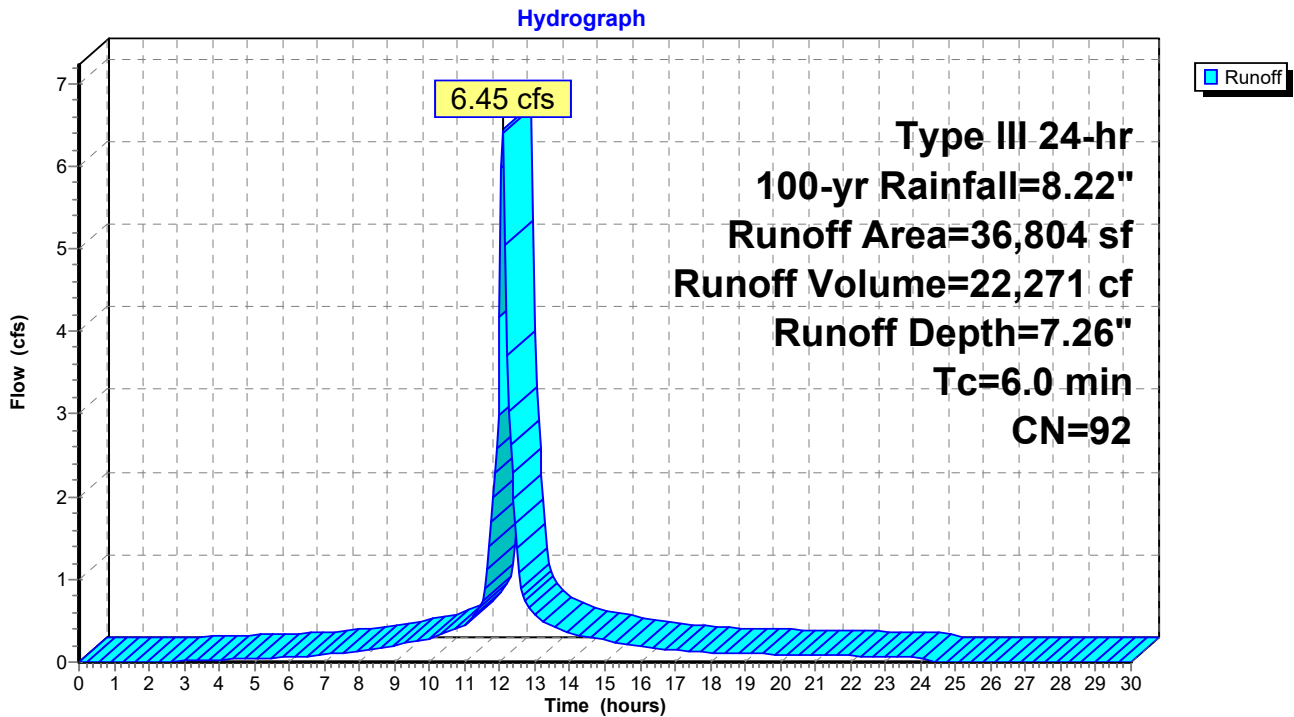
Runoff = 6.45 cfs @ 12.09 hrs, Volume= 22,271 cf, Depth= 7.26"  
 Routed to Pond 1E : BIO-1E

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
25,092	98	Paved parking, HSG D
11,712	80	>75% Grass cover, Good, HSG D
36,804	92	Weighted Average
11,712		31.82% Pervious Area
25,092		68.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1E: TRAILERS**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 99

**Summary for Subcatchment PW1F: TRAILER 2**

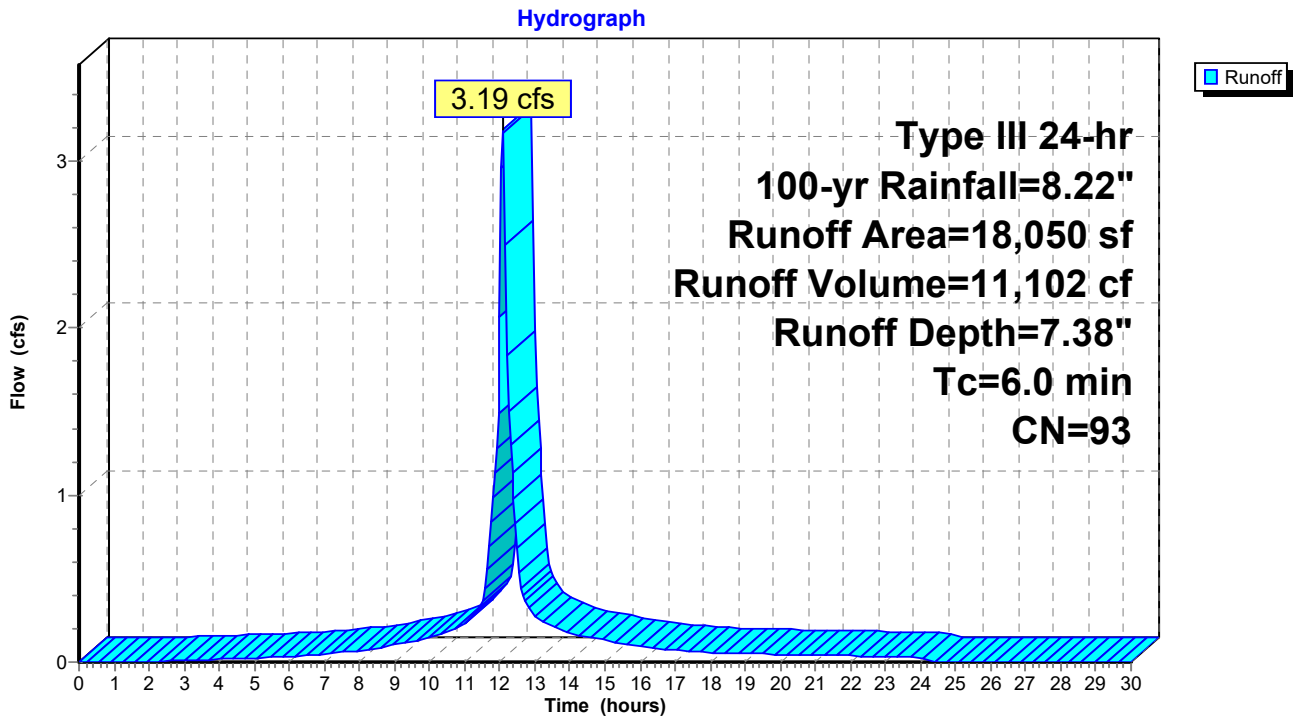
Runoff = 3.19 cfs @ 12.09 hrs, Volume= 11,102 cf, Depth= 7.38"  
 Routed to Pond 1F : BIO-1F

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
12,622	98	Paved parking, HSG D
5,428	80	>75% Grass cover, Good, HSG D
18,050	93	Weighted Average
5,428		30.07% Pervious Area
12,622		69.93% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1F: TRAILER 2**





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 100

**Summary for Subcatchment PW1G: LOADING**

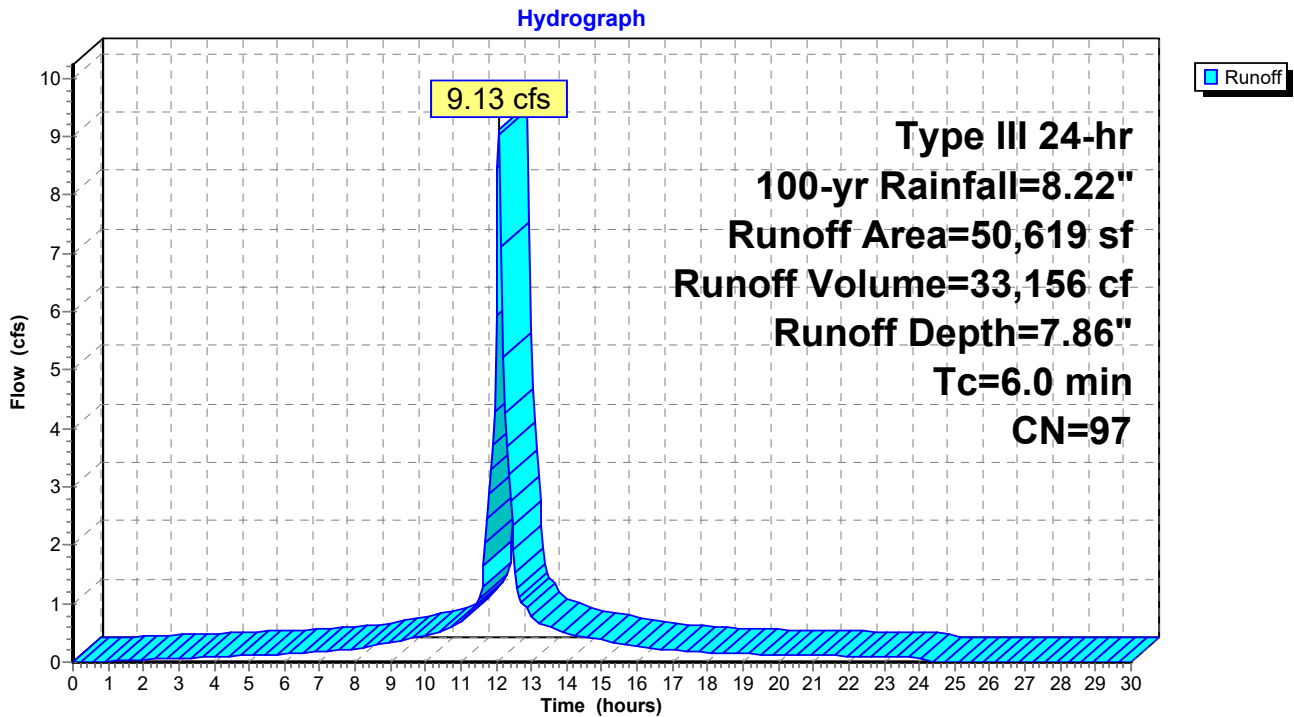
Runoff = 9.13 cfs @ 12.09 hrs, Volume= 33,156 cf, Depth= 7.86"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
46,810	98	Paved parking, HSG D
3,809	80	>75% Grass cover, Good, HSG D
50,619	97	Weighted Average
3,809		7.52% Pervious Area
46,810		92.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1G: LOADING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 101

**Summary for Subcatchment PW1H: NW CORNER BLDG**

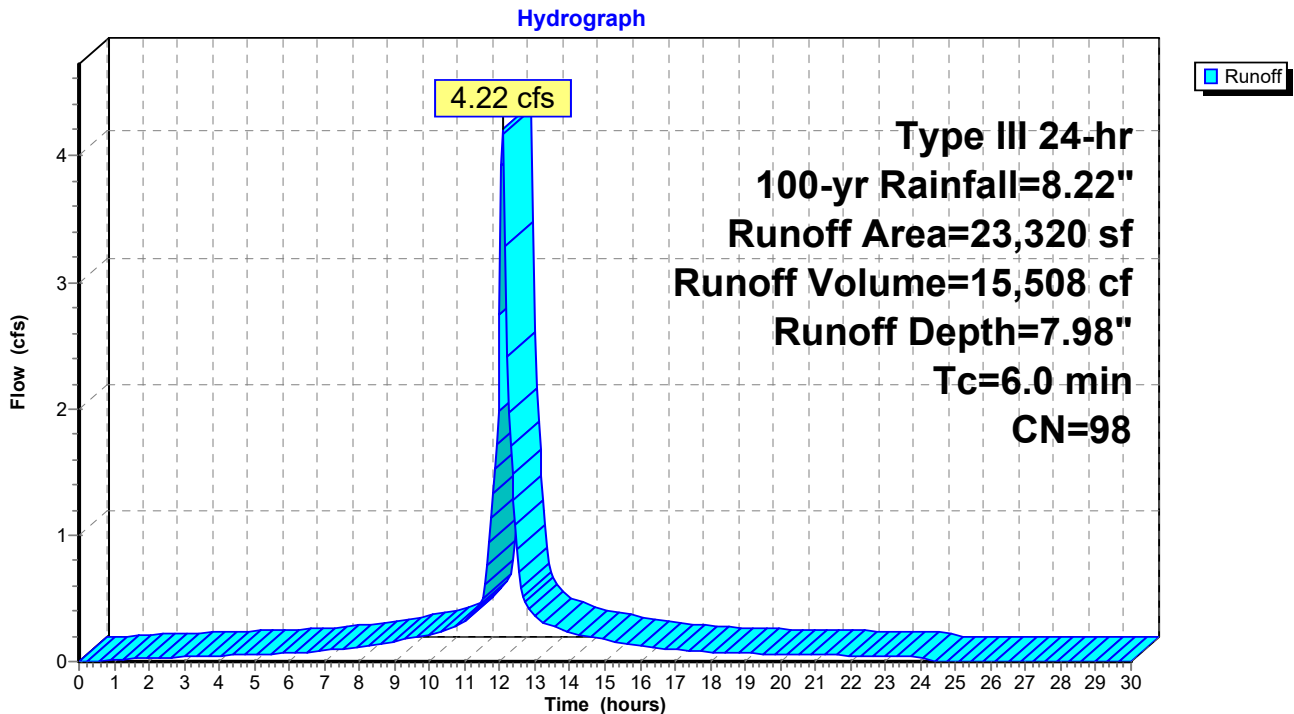
Runoff = 4.22 cfs @ 12.09 hrs, Volume= 15,508 cf, Depth= 7.98"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 100-yr Rainfall=8.22"

Area (sf)	CN	Description
23,320	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
23,320	98	Weighted Average
23,320		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1H: NW CORNER BLDG**



**230119 - R1 - Dewpoint South**

Type III 24-hr 100-yr Rainfall=8.22"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 102

**Summary for Pond 1BN: BIO-1BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth = 7.14" for 100-yr event  
 Inflow = 11.90 cfs @ 12.09 hrs, Volume= 40,736 cf  
 Outflow = 11.66 cfs @ 12.11 hrs, Volume= 35,586 cf, Atten= 2%, Lag= 1.2 min  
 Primary = 11.66 cfs @ 12.11 hrs, Volume= 35,586 cf  
 Routed to Pond 2BN : BIO-2BN

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 492.90' @ 12.11 hrs Surf.Area= 3,116 sf Storage= 6,495 cf

Plug-Flow detention time= 103.5 min calculated for 35,586 cf (87% of inflow)  
 Center-of-Mass det. time= 46.1 min ( 817.9 - 771.8 )

Volume	Invert	Avail.Storage	Storage Description		
#1	490.00'	10,349 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
	Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
	490.00	1,454	0	0	1,454
	492.00	2,555	3,958	3,958	2,611
	494.00	3,883	6,392	10,349	4,013

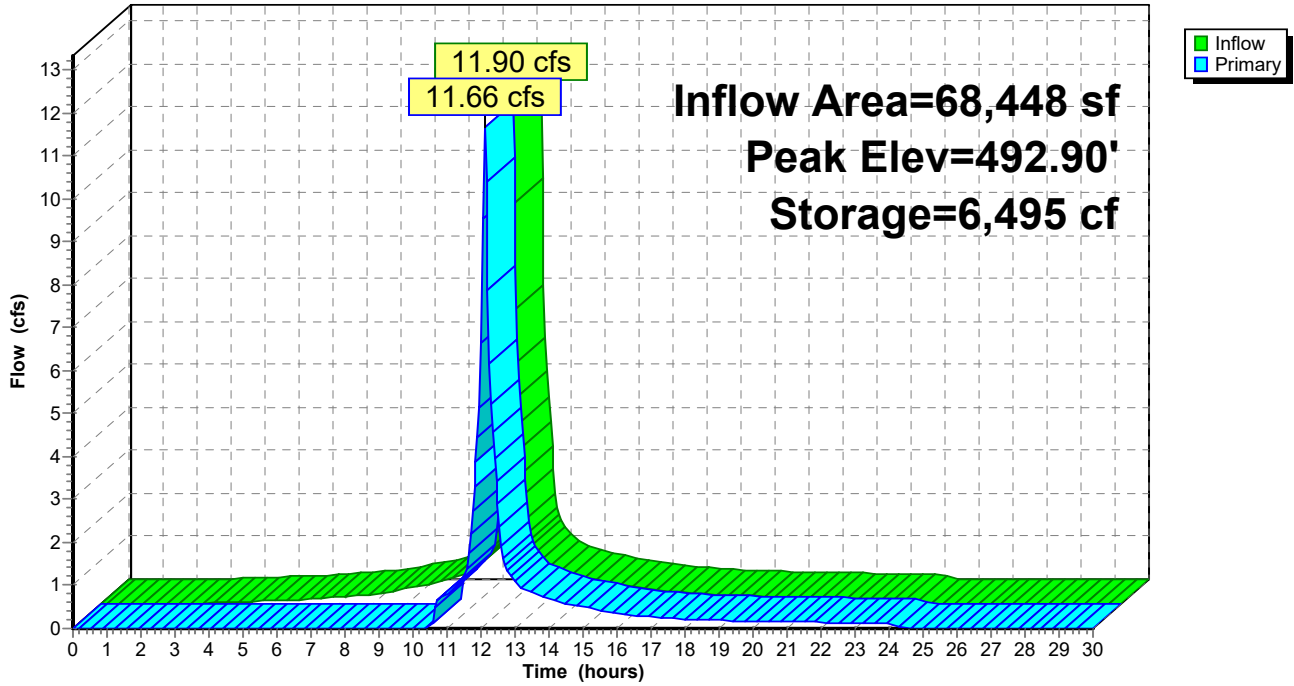
Device	Routing	Invert	Outlet Devices
#1	Primary	483.15'	<b>18.0" Round Culvert</b> L= 26.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 483.15' / 482.62' S= 0.0204 ' S= 0.0204 ' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	492.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	490.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=11.47 cfs @ 12.11 hrs HW=492.89' TW=486.25' (Dynamic Tailwater)

- 1=Culvert (Passes 11.47 cfs of 21.92 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 11.46 cfs @ 1.83 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 1BN: BIO-1BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 104

**Stage-Area-Storage for Pond 1BN: BIO-1BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
490.00	1,454	0	492.65	2,956	5,747
490.05	1,478	73	492.70	2,988	5,896
490.10	1,502	148	492.75	3,021	6,046
490.15	1,526	223	492.80	3,053	6,198
490.20	1,550	300	492.85	3,086	6,351
490.25	1,575	378	492.90	3,118	6,506
490.30	1,599	458	492.95	3,151	6,663
490.35	1,624	538	493.00	3,184	6,822
490.40	1,650	620	493.05	3,218	6,982
490.45	1,675	703	493.10	3,251	7,143
490.50	1,700	788	493.15	3,285	7,307
490.55	1,726	873	493.20	3,319	7,472
490.60	1,752	960	493.25	3,353	7,639
490.65	1,778	1,049	493.30	3,387	7,807
490.70	1,804	1,138	493.35	3,421	7,977
490.75	1,831	1,229	493.40	3,456	8,149
490.80	1,857	1,321	493.45	3,490	8,323
490.85	1,884	1,415	493.50	3,525	8,498
490.90	1,911	1,510	493.55	3,560	8,675
490.95	1,939	1,606	493.60	3,595	8,854
491.00	1,966	1,704	493.65	3,631	9,035
491.05	1,994	1,803	493.70	3,666	9,217
491.10	2,021	1,903	493.75	3,702	9,401
491.15	2,049	2,005	493.80	3,738	9,587
491.20	2,078	2,108	493.85	3,774	9,775
491.25	2,106	2,212	493.90	3,810	9,965
491.30	2,135	2,318	493.95	3,846	10,156
491.35	2,163	2,426	494.00	<b>3,883</b>	<b>10,349</b>
491.40	2,192	2,535			
491.45	2,221	2,645			
491.50	2,251	2,757			
491.55	2,280	2,870			
491.60	2,310	2,985			
491.65	2,340	3,101			
491.70	2,370	3,219			
491.75	2,401	3,338			
491.80	2,431	3,459			
491.85	2,462	3,581			
491.90	2,493	3,705			
491.95	2,524	3,831			
492.00	2,555	3,958			
492.05	2,585	4,086			
492.10	2,615	4,216			
492.15	2,645	4,348			
492.20	2,675	4,481			
492.25	2,706	4,615			
492.30	2,737	4,751			
492.35	2,767	4,889			
492.40	2,798	5,028			
492.45	2,830	5,169			
492.50	2,861	5,311			
492.55	2,893	5,455			
492.60	2,924	5,600			

**Summary for Pond 1D: BIO-1D**

Inflow Area = 89,761 sf, 71.97% Impervious, Inflow Depth = 7.38" for 100-yr event  
 Inflow = 15.73 cfs @ 12.09 hrs, Volume= 55,200 cf  
 Outflow = 11.13 cfs @ 12.17 hrs, Volume= 51,452 cf, Atten= 29%, Lag= 5.1 min  
 Primary = 11.13 cfs @ 12.17 hrs, Volume= 51,452 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 469.36' @ 12.17 hrs Surf.Area= 8,252 sf Storage= 10,056 cf

Plug-Flow detention time= 81.8 min calculated for 51,452 cf (93% of inflow)  
 Center-of-Mass det. time= 44.6 min ( 805.3 - 760.7 )

Volume	Invert	Avail.Storage	Storage Description		
#1	468.00'	15,581 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
	Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
	468.00	6,529	0	0	6,529
	470.00	9,124	15,581	15,581	9,218

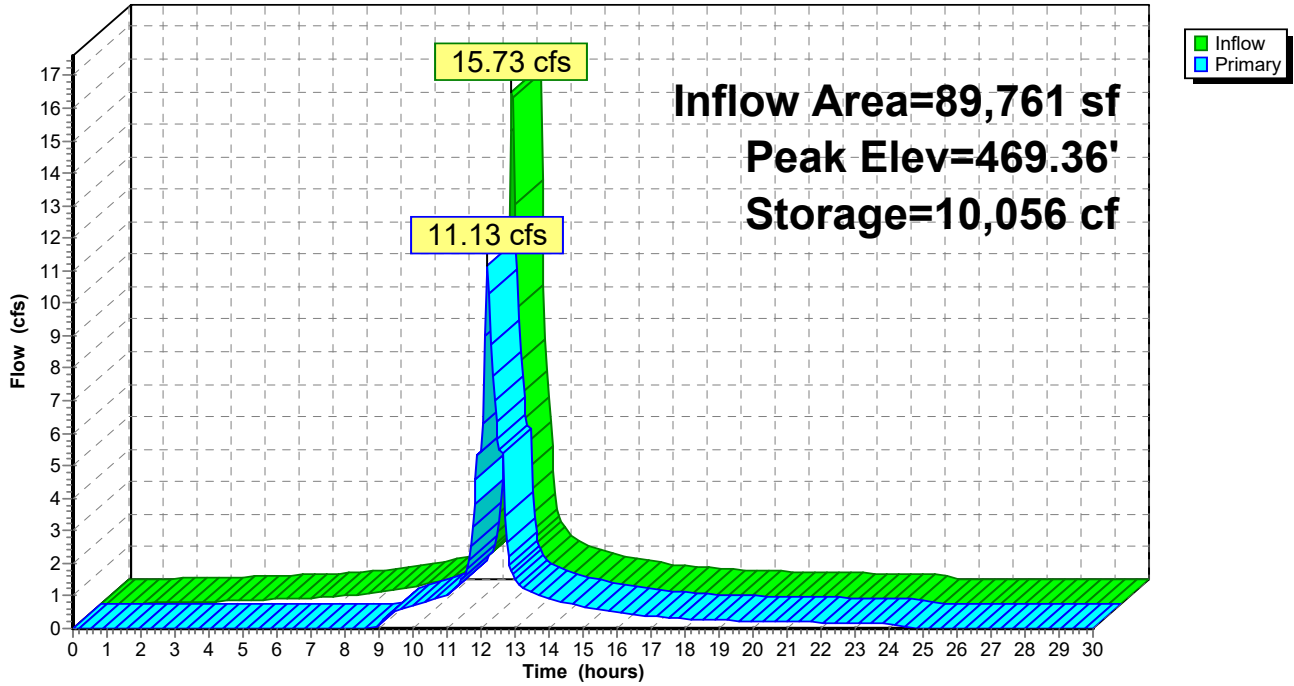
Device	Routing	Invert	Outlet Devices
#1	Primary	464.50'	<b>12.0" Round Culvert</b> L= 190.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 464.50' / 462.98' S= 0.0080 ' S= 0.0080 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.60'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	468.00'	<b>0.125 in/hr Exfiltration over Surface area</b>
#4	Primary	469.00'	<b>10.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83

**Primary OutFlow** Max=10.88 cfs @ 12.17 hrs HW=469.35' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Barrel Controls 5.69 cfs @ 7.25 fps)
- 2=Broad-Crested Rectangular Weir (Passes < 33.92 cfs potential flow)
- 3=Exfiltration (Passes < 0.02 cfs potential flow)
- 4=Broad-Crested Rectangular Weir (Weir Controls 5.18 cfs @ 1.47 fps)

Pond 1D: BIO-1D

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 107

**Stage-Area-Storage for Pond 1D: BIO-1D**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
468.00	6,529	0	469.06	7,850	7,610
468.02	6,553	131	469.08	7,876	7,768
468.04	6,577	262	469.10	7,903	7,925
468.06	6,601	394	469.12	7,929	8,084
468.08	6,624	526	469.14	7,955	8,243
468.10	6,648	659	469.16	7,981	8,402
468.12	6,672	792	469.18	8,008	8,562
468.14	6,697	926	469.20	8,034	8,722
468.16	6,721	1,060	469.22	8,060	8,883
468.18	6,745	1,195	469.24	8,087	9,045
468.20	6,769	1,330	469.26	8,113	9,207
468.22	6,793	1,465	469.28	8,140	9,369
468.24	6,818	1,601	469.30	8,166	9,532
468.26	6,842	1,738	469.32	8,193	9,696
468.28	6,866	1,875	469.34	8,220	9,860
468.30	6,891	2,013	469.36	8,246	10,025
468.32	6,915	2,151	469.38	8,273	10,190
468.34	6,940	2,289	469.40	8,300	10,356
468.36	6,964	2,428	469.42	8,327	10,522
468.38	6,989	2,568	469.44	8,354	10,689
468.40	7,013	2,708	469.46	8,381	10,856
468.42	7,038	2,848	469.48	8,408	11,024
468.44	7,063	2,989	469.50	8,435	11,192
468.46	7,087	3,131	469.52	8,462	11,361
468.48	7,112	3,273	469.54	8,489	11,531
468.50	7,137	3,415	469.56	8,516	11,701
468.52	7,162	3,558	469.58	8,543	11,871
468.54	7,187	3,702	469.60	8,570	12,043
468.56	7,212	3,846	469.62	8,598	12,214
468.58	7,237	3,990	469.64	8,625	12,386
468.60	7,262	4,135	469.66	8,652	12,559
468.62	7,287	4,281	469.68	8,680	12,733
468.64	7,312	4,427	469.70	8,707	12,906
468.66	7,337	4,573	469.72	8,735	13,081
468.68	7,363	4,720	469.74	8,762	13,256
468.70	7,388	4,868	469.76	8,790	13,431
468.72	7,413	5,016	469.78	8,817	13,607
468.74	7,439	5,164	469.80	8,845	13,784
468.76	7,464	5,313	469.82	8,873	13,961
468.78	7,490	5,463	469.84	8,900	14,139
468.80	7,515	5,613	469.86	8,928	14,317
468.82	7,541	5,764	469.88	8,956	14,496
468.84	7,566	5,915	469.90	8,984	14,675
468.86	7,592	6,066	469.92	9,012	14,855
468.88	7,617	6,218	469.94	9,040	15,036
468.90	7,643	6,371	469.96	9,068	15,217
468.92	7,669	6,524	469.98	9,096	15,399
468.94	7,695	6,678	470.00	<b>9,124</b>	<b>15,581</b>
468.96	7,721	6,832			
468.98	7,746	6,986			
469.00	7,772	7,142			
469.02	7,798	7,297			
469.04	7,824	7,454			



**230119 - R1 - Dewpoint South**

Type III 24-hr 100-yr Rainfall=8.22"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 108

**Summary for Pond 1E: BIO-1E**

Inflow Area = 36,804 sf, 68.18% Impervious, Inflow Depth = 7.26" for 100-yr event  
 Inflow = 6.45 cfs @ 12.09 hrs, Volume= 22,271 cf  
 Outflow = 6.03 cfs @ 12.12 hrs, Volume= 17,213 cf, Atten= 7%, Lag= 1.9 min  
 Primary = 6.03 cfs @ 12.12 hrs, Volume= 17,213 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.76' @ 12.12 hrs Surf.Area= 4,352 sf Storage= 6,394 cf

Plug-Flow detention time= 154.2 min calculated for 17,213 cf (77% of inflow)  
 Center-of-Mass det. time= 73.2 min ( 841.6 - 768.4 )

Volume	Invert	Avail.Storage	Storage Description		
#1	467.00'	12,471 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
467.00	2,940	0	0	2,940	
468.00	3,728	3,326	3,326	3,761	
470.00	5,472	9,144	12,471	5,587	

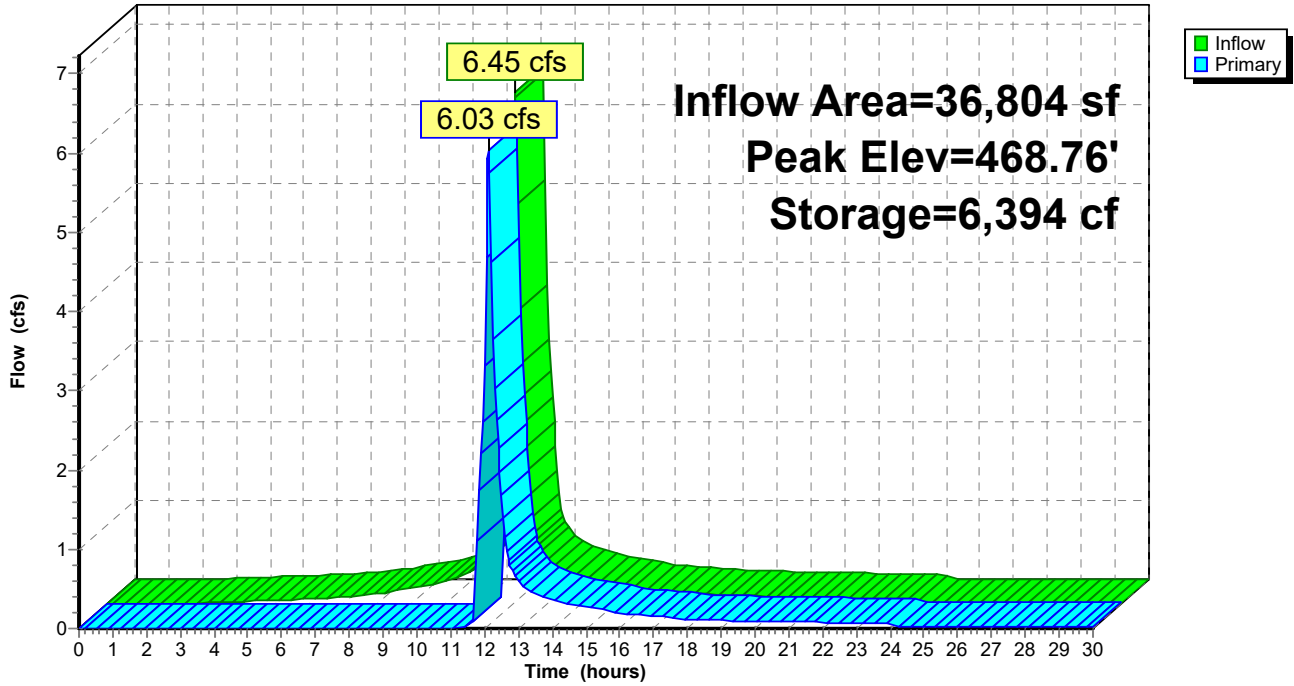
Device	Routing	Invert	Outlet Devices
#1	Primary	463.50'	<b>12.0" Round Culvert</b> L= 23.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 463.50' / 462.93' S= 0.0248 ' S= 0.0248 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	467.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=5.86 cfs @ 12.12 hrs HW=468.76' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 5.86 cfs of 8.25 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 5.85 cfs @ 1.43 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1E: BIO-1E

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 110

**Stage-Area-Storage for Pond 1E: BIO-1E**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
467.00	2,940	0	469.65	5,143	10,613
467.05	2,977	148	469.70	5,189	10,872
467.10	3,015	298	469.75	5,236	11,132
467.15	3,052	449	469.80	5,283	11,395
467.20	3,090	603	469.85	5,330	11,661
467.25	3,128	758	469.90	5,377	11,928
467.30	3,167	916	469.95	5,424	12,198
467.35	3,205	1,075	470.00	<b>5,472</b>	<b>12,471</b>
467.40	3,244	1,236			
467.45	3,283	1,399			
467.50	3,322	1,565			
467.55	3,362	1,732			
467.60	3,402	1,901			
467.65	3,442	2,072			
467.70	3,482	2,245			
467.75	3,522	2,420			
467.80	3,563	2,597			
467.85	3,604	2,776			
467.90	3,645	2,958			
467.95	3,686	3,141			
468.00	3,728	3,326			
468.05	3,768	3,514			
468.10	3,807	3,703			
468.15	3,847	3,894			
468.20	3,887	4,088			
468.25	3,928	4,283			
468.30	3,968	4,480			
468.35	4,009	4,680			
468.40	4,050	4,881			
468.45	4,091	5,085			
468.50	4,133	5,291			
468.55	4,174	5,498			
468.60	4,216	5,708			
468.65	4,258	5,920			
468.70	4,300	6,134			
468.75	4,343	6,350			
468.80	4,386	6,568			
468.85	4,428	6,788			
468.90	4,472	7,011			
468.95	4,515	7,236			
469.00	4,558	7,462			
469.05	4,602	7,691			
469.10	4,646	7,923			
469.15	4,690	8,156			
469.20	4,734	8,392			
469.25	4,779	8,629			
469.30	4,824	8,870			
469.35	4,869	9,112			
469.40	4,914	9,356			
469.45	4,959	9,603			
469.50	5,005	9,852			
469.55	5,051	10,104			
469.60	5,097	10,357			

**Summary for Pond 1F: BIO-1F**

Inflow Area = 18,050 sf, 69.93% Impervious, Inflow Depth = 7.38" for 100-yr event  
 Inflow = 3.19 cfs @ 12.09 hrs, Volume= 11,102 cf  
 Outflow = 3.08 cfs @ 12.11 hrs, Volume= 8,572 cf, Atten= 3%, Lag= 1.4 min  
 Primary = 3.08 cfs @ 12.11 hrs, Volume= 8,572 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 478.67' @ 12.11 hrs Surf.Area= 2,327 sf Storage= 3,040 cf

Plug-Flow detention time= 154.7 min calculated for 8,558 cf (77% of inflow)  
 Center-of-Mass det. time= 74.8 min ( 839.4 - 764.7 )

Volume	Invert	Avail.Storage	Storage Description		
#1	477.00'	6,744 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
477.00	1,347	0	0	1,347	
478.00	1,919	1,625	1,625	1,941	
480.00	3,259	5,119	6,744	3,341	

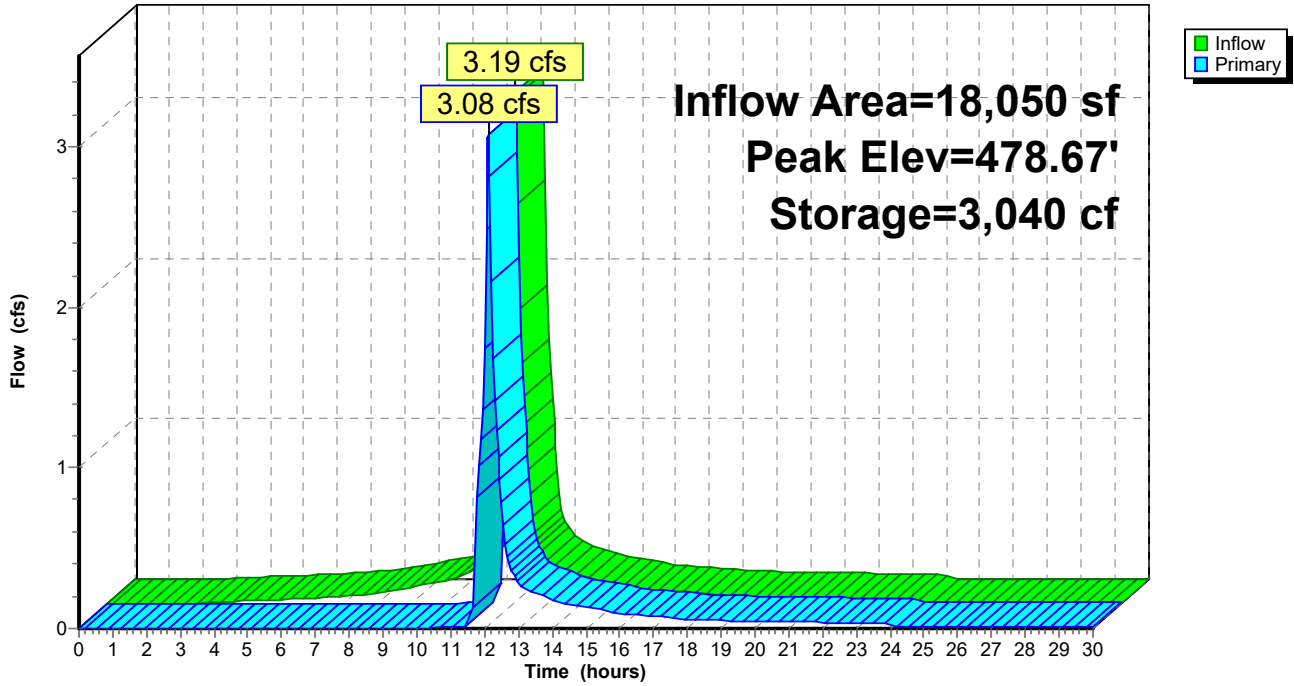
Device	Routing	Invert	Outlet Devices
#1	Primary	473.50'	<b>12.0" Round Culvert</b> L= 115.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 473.50' / 471.21' S= 0.0199 ' S= 0.0199 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	478.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	477.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=3.01 cfs @ 12.11 hrs HW=478.67' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 3.01 cfs of 7.49 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 3.01 cfs @ 1.14 fps)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1F: BIO-1F

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 113

**Stage-Area-Storage for Pond 1F: BIO-1F**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
477.00	1,347	0	479.65	2,999	5,649
477.05	1,373	68	479.70	3,036	5,800
477.10	1,400	137	479.75	3,072	5,953
477.15	1,426	208	479.80	3,109	6,107
477.20	1,453	280	479.85	3,146	6,263
477.25	1,481	353	479.90	3,184	6,422
477.30	1,508	428	479.95	3,221	6,582
477.35	1,536	504	480.00	<b>3,259</b>	<b>6,744</b>
477.40	1,564	582			
477.45	1,592	660			
477.50	1,620	741			
477.55	1,649	823			
477.60	1,678	906			
477.65	1,707	990			
477.70	1,737	1,076			
477.75	1,767	1,164			
477.80	1,797	1,253			
477.85	1,827	1,344			
477.90	1,857	1,436			
477.95	1,888	1,529			
478.00	1,919	1,625			
478.05	1,948	1,721			
478.10	1,978	1,819			
478.15	2,007	1,919			
478.20	2,037	2,020			
478.25	2,067	2,123			
478.30	2,098	2,227			
478.35	2,128	2,333			
478.40	2,159	2,440			
478.45	2,190	2,548			
478.50	2,221	2,659			
478.55	2,252	2,770			
478.60	2,284	2,884			
478.65	2,316	2,999			
478.70	2,348	3,115			
478.75	2,380	3,234			
478.80	2,413	3,353			
478.85	2,445	3,475			
478.90	2,478	3,598			
478.95	2,512	3,723			
479.00	2,545	3,849			
479.05	2,579	3,977			
479.10	2,612	4,107			
479.15	2,646	4,239			
479.20	2,681	4,372			
479.25	2,715	4,507			
479.30	2,750	4,643			
479.35	2,785	4,782			
479.40	2,820	4,922			
479.45	2,855	5,064			
479.50	2,891	5,207			
479.55	2,927	5,353			
479.60	2,963	5,500			

**230119 - R1 - Dewpoint South**

Type III 24-hr 100-yr Rainfall=8.22"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 114

**Summary for Pond 2BN: BIO-2BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth > 6.24" for 100-yr event  
 Inflow = 11.66 cfs @ 12.11 hrs, Volume= 35,586 cf  
 Outflow = 6.96 cfs @ 12.23 hrs, Volume= 34,072 cf, Atten= 40%, Lag= 7.7 min  
 Primary = 6.96 cfs @ 12.23 hrs, Volume= 34,072 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 486.69' @ 12.23 hrs Surf.Area= 4,839 sf Storage= 10,221 cf

Plug-Flow detention time= 63.8 min calculated for 34,015 cf (96% of inflow)  
 Center-of-Mass det. time= 38.9 min ( 856.9 - 817.9 )

Volume	Invert	Avail.Storage	Storage Description		
#1	484.00'	17,309 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
484.00	2,843	0	0	2,843	
486.00	4,295	7,088	7,088	4,371	
488.00	5,972	10,221	17,309	6,142	

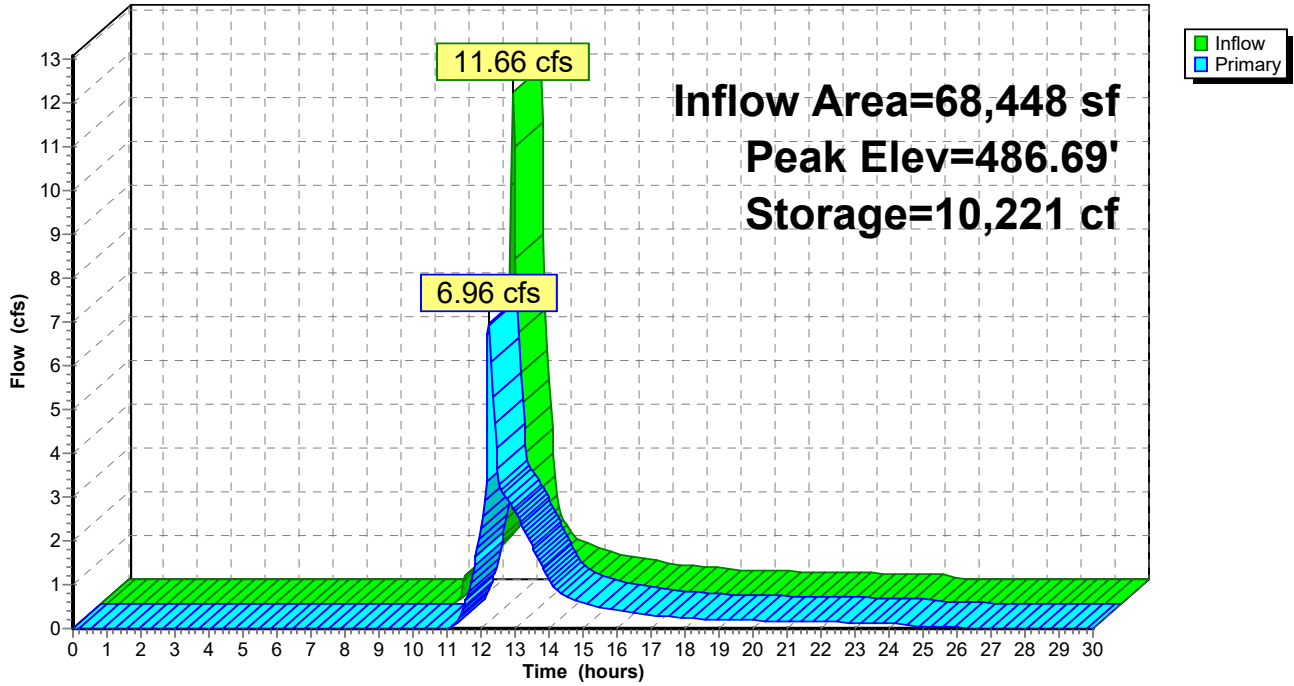
Device	Routing	Invert	Outlet Devices
#1	Primary	480.50'	<b>18.0" Round Culvert</b> L= 52.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 480.50' / 478.00' S= 0.0481 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	486.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	484.50'	<b>12.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	484.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=6.85 cfs @ 12.23 hrs HW=486.68' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 6.85 cfs of 19.83 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 3.49 cfs @ 1.20 fps)
- 3=Orifice/Grate (Orifice Controls 3.34 cfs @ 6.69 fps)
- 4=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 2BN: BIO-2BN

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 116

**Stage-Area-Storage for Pond 2BN: BIO-2BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
484.00	2,843	0	486.65	4,810	10,046
484.05	2,876	143	486.70	4,851	10,287
484.10	2,909	288	486.75	4,892	10,531
484.15	2,942	434	486.80	4,933	10,776
484.20	2,975	582	486.85	4,974	11,024
484.25	3,008	731	486.90	5,016	11,274
484.30	3,042	883	486.95	5,057	11,526
484.35	3,076	1,035	487.00	5,099	11,780
484.40	3,110	1,190	487.05	5,141	12,036
484.45	3,144	1,346	487.10	5,183	12,294
484.50	3,178	1,504	487.15	5,226	12,554
484.55	3,213	1,664	487.20	5,268	12,816
484.60	3,247	1,826	487.25	5,311	13,081
484.65	3,282	1,989	487.30	5,354	13,347
484.70	3,317	2,154	487.35	5,397	13,616
484.75	3,353	2,321	487.40	5,440	13,887
484.80	3,388	2,489	487.45	5,483	14,160
484.85	3,424	2,659	487.50	5,527	14,435
484.90	3,459	2,832	487.55	5,571	14,713
484.95	3,495	3,005	487.60	5,615	14,992
485.00	3,532	3,181	487.65	5,659	15,274
485.05	3,568	3,359	487.70	5,703	15,558
485.10	3,605	3,538	487.75	5,747	15,844
485.15	3,641	3,719	487.80	5,792	16,133
485.20	3,678	3,902	487.85	5,837	16,424
485.25	3,716	4,087	487.90	5,882	16,717
485.30	3,753	4,274	487.95	5,927	17,012
485.35	3,790	4,462	488.00	<b>5,972</b>	<b>17,309</b>
485.40	3,828	4,653			
485.45	3,866	4,845			
485.50	3,904	5,039			
485.55	3,942	5,235			
485.60	3,981	5,434			
485.65	4,019	5,634			
485.70	4,058	5,835			
485.75	4,097	6,039			
485.80	4,136	6,245			
485.85	4,176	6,453			
485.90	4,215	6,663			
485.95	4,255	6,875			
486.00	4,295	7,088			
486.05	4,334	7,304			
486.10	4,372	7,522			
486.15	4,411	7,741			
486.20	4,450	7,963			
486.25	4,490	8,186			
486.30	4,529	8,412			
486.35	4,569	8,639			
486.40	4,608	8,869			
486.45	4,648	9,100			
486.50	4,688	9,333			
486.55	4,729	9,569			
486.60	4,769	9,806			

**Summary for Pond SUBS: SUBS**

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth = 7.93" for 100-yr event  
 Inflow = 20.45 cfs @ 12.09 hrs, Volume= 74,744 cf  
 Outflow = 7.84 cfs @ 12.32 hrs, Volume= 71,416 cf, Atten= 62%, Lag= 14.2 min  
 Primary = 0.94 cfs @ 12.32 hrs, Volume= 53,602 cf  
 Routed to Link JF : JELLY FISH  
 Secondary = 6.90 cfs @ 12.32 hrs, Volume= 17,814 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 480.18' @ 12.32 hrs Surf.Area= 8,608 sf Storage= 31,786 cf

Plug-Flow detention time= 271.4 min calculated for 71,416 cf (96% of inflow)  
 Center-of-Mass det. time= 244.7 min ( 988.2 - 743.5 )

Volume	Invert	Avail.Storage	Storage Description
#1A	475.00'	13,785 cf	<b>83.00'W x 103.72'L x 6.75'H Field A</b> 58,107 cf Overall - 23,645 cf Embedded = 34,463 cf x 40.0% Voids
#2A	475.75'	23,645 cf	<b>ADS_StormTech MC-4500 +Cap x 216 Inside #1</b> Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 216 Chambers in 9 Rows Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf
		37,430 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	472.00'	<b>12.0" Round Culvert</b> L= 30.9' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 472.00' / 471.69' S= 0.0100 1/ S= 0.0100 1/ Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	475.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Device 1	480.25'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Secondary	479.00'	<b>18.0" Round Culvert</b> L= 46.5' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 479.00' / 477.56' S= 0.0310 1/ Cc= 0.900 n= 0.012, Flow Area= 1.77 sf

**Primary OutFlow** Max=0.94 cfs @ 12.32 hrs HW=480.17' TW=0.00' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 0.94 cfs of 12.11 cfs potential flow)
- ↑ 2=Orifice/Grate (Orifice Controls 0.94 cfs @ 10.77 fps)
- ↑ 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Secondary OutFlow** Max=6.85 cfs @ 12.32 hrs HW=480.17' TW=0.00' (Dynamic Tailwater)

- ↑ 4=Culvert (Inlet Controls 6.85 cfs @ 4.61 fps)

**Pond SUBS: SUBS - Chamber Wizard Field A**

**Chamber Model = ADS\_StormTech MC-4500 +Cap (ADS StormTech®MC-4500 with cap, use MC-4500 b for new designs)**

Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf

Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap

Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf

100.0" Wide + 9.0" Spacing = 109.0" C-C Row Spacing

24 Chambers/Row x 4.02' Long +2.56' Cap Length x 2 = 101.72' Row Length +12.0" End Stone x 2 = 103.72' Base Length

9 Rows x 100.0" Wide + 9.0" Spacing x 8 + 12.0" Side Stone x 2 = 83.00' Base Width

9.0" Stone Base + 60.0" Chamber Height + 12.0" Stone Cover = 6.75' Field Height

216 Chambers x 106.5 cf + 35.7 cf Cap Volume x 2 x 9 Rows = 23,644.5 cf Chamber Storage

58,107.3 cf Field - 23,644.5 cf Chambers = 34,462.7 cf Stone x 40.0% Voids = 13,785.1 cf Stone Storage

Chamber Storage + Stone Storage = 37,429.6 cf = 0.859 af

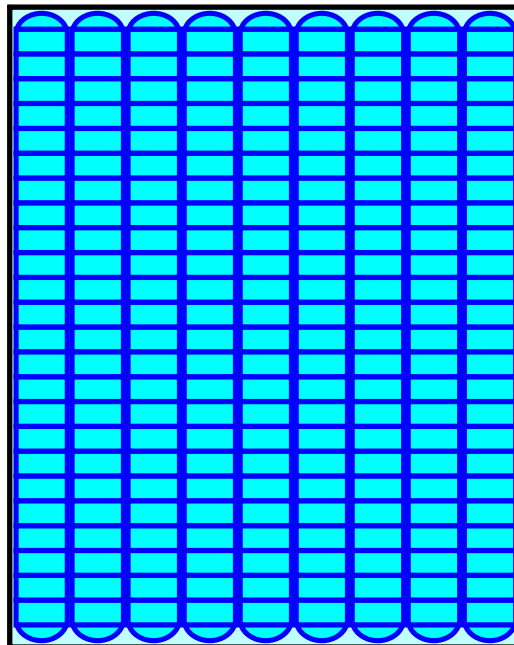
Overall Storage Efficiency = 64.4%

Overall System Size = 103.72' x 83.00' x 6.75'

216 Chambers

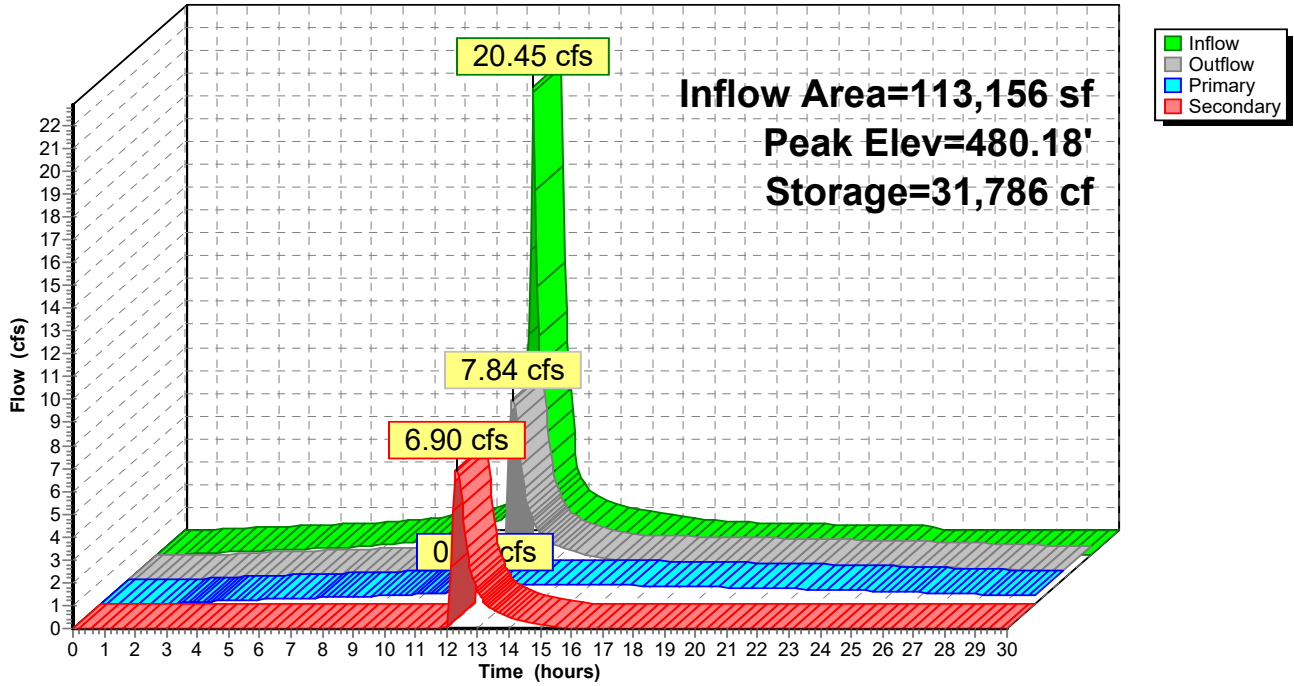
2,152.1 cy Field

1,276.4 cy Stone



### Pond SUBS: SUBS

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr 100-yr Rainfall=8.22"

Printed 2/2/2023

Page 120

**Stage-Area-Storage for Pond SUBS: SUBS**

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
475.00	0	477.65	16,390	480.30	32,305
475.05	172	477.70	16,738	480.35	32,508
475.10	344	477.75	17,084	480.40	32,704
475.15	517	477.80	17,429	480.45	32,895
475.20	689	477.85	17,773	480.50	33,084
475.25	861	477.90	18,115	480.55	33,270
475.30	1,033	477.95	18,457	480.60	33,453
475.35	1,205	478.00	18,797	480.65	33,634
475.40	1,377	478.05	19,136	480.70	33,812
475.45	1,550	478.10	19,474	480.75	33,986
475.50	1,722	478.15	19,810	480.80	34,158
475.55	1,894	478.20	20,145	480.85	34,331
475.60	2,066	478.25	20,478	480.90	34,503
475.65	2,238	478.30	20,811	480.95	34,675
475.70	2,410	478.35	21,141	481.00	34,847
475.75	2,583	478.40	21,470	481.05	35,019
475.80	2,957	478.45	21,798	481.10	35,191
475.85	3,330	478.50	22,124	481.15	35,364
475.90	3,704	478.55	22,449	481.20	35,536
475.95	4,077	478.60	22,771	481.25	35,708
476.00	4,449	478.65	23,093	481.30	35,880
476.05	4,821	478.70	23,412	481.35	36,052
476.10	5,193	478.75	23,730	481.40	36,224
476.15	5,564	478.80	24,045	481.45	36,397
476.20	5,934	478.85	24,360	481.50	36,569
476.25	6,304	478.90	24,672	481.55	36,741
476.30	6,674	478.95	24,982	481.60	36,913
476.35	7,043	479.00	25,290	481.65	37,085
476.40	7,411	479.05	25,596	481.70	37,257
476.45	7,779	479.10	25,900	481.75	<b>37,430</b>
476.50	8,147	479.15	26,202		
476.55	8,513	479.20	26,501		
476.60	8,879	479.25	26,798		
476.65	9,245	479.30	27,093		
476.70	9,610	479.35	27,386		
476.75	9,974	479.40	27,675		
476.80	10,338	479.45	27,963		
476.85	10,700	479.50	28,247		
476.90	11,062	479.55	28,529		
476.95	11,424	479.60	28,808		
477.00	11,784	479.65	29,084		
477.05	12,144	479.70	29,357		
477.10	12,503	479.75	29,627		
477.15	12,861	479.80	29,893		
477.20	13,218	479.85	30,156		
477.25	13,574	479.90	30,414		
477.30	13,930	479.95	30,669		
477.35	14,284	480.00	30,920		
477.40	14,638	480.05	31,166		
477.45	14,990	480.10	31,407		
477.50	15,342	480.15	31,643		
477.55	15,692	480.20	31,872		
477.60	16,042	480.25	32,093		

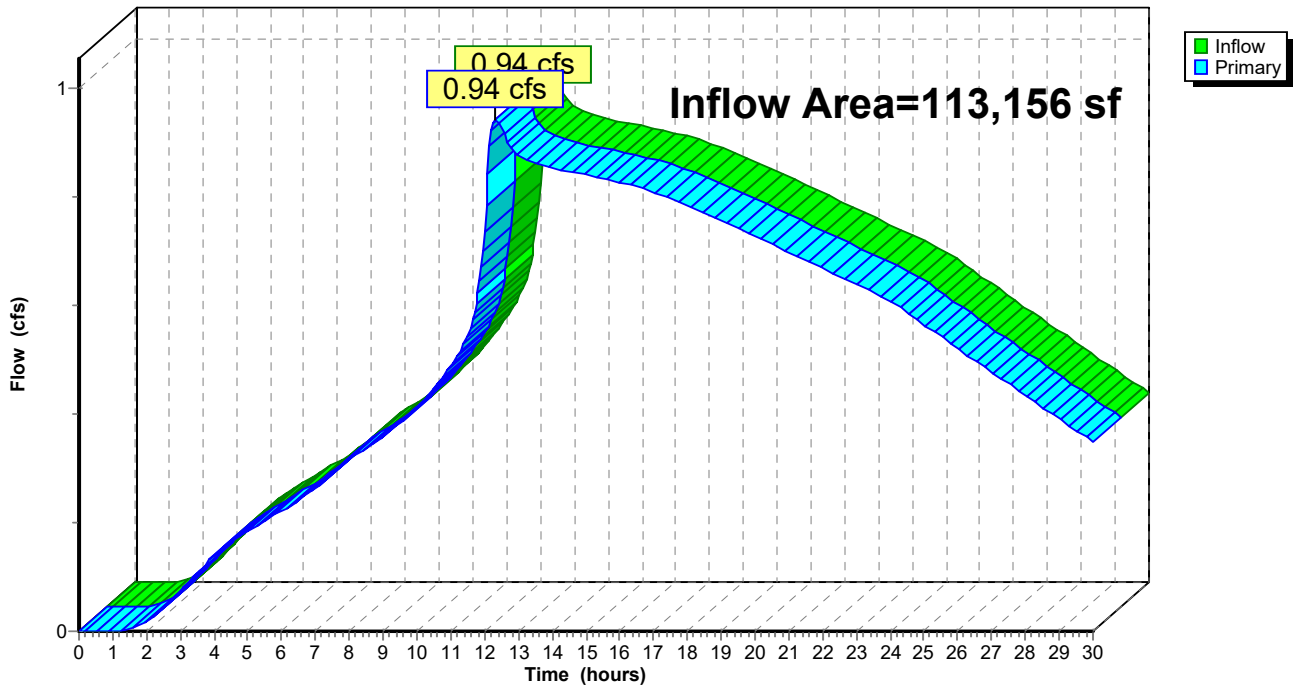
### Summary for Link JF: JELLY FISH

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth > 5.68" for 100-yr event  
Inflow = 0.94 cfs @ 12.32 hrs, Volume= 53,602 cf  
Primary = 0.94 cfs @ 12.32 hrs, Volume= 53,602 cf, Atten= 0%, Lag= 0.0 min  
Routed to Link PROP : PROPOSED

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link JF: JELLY FISH

Hydrograph

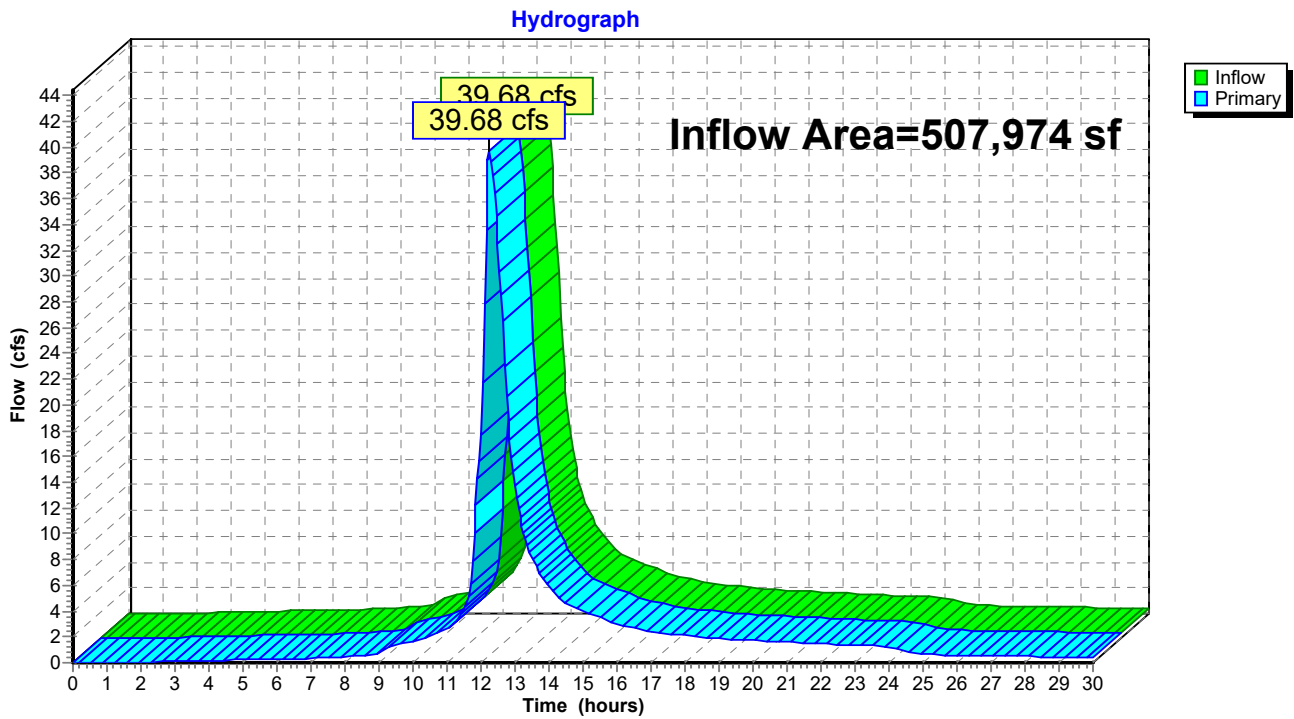


### Summary for Link PROP: PROPOSED

Inflow Area = 507,974 sf, 50.18% Impervious, Inflow Depth > 6.32" for 100-yr event  
Inflow = 39.68 cfs @ 12.25 hrs, Volume= 267,464 cf  
Primary = 39.68 cfs @ 12.25 hrs, Volume= 267,464 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link PROP: PROPOSED



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 123

**Summary for Subcatchment PW1A: LOD**

Runoff = 0.33 cfs @ 12.64 hrs, Volume= 2,894 cf, Depth= 0.19"  
 Routed to Link PROP : PROPOSED

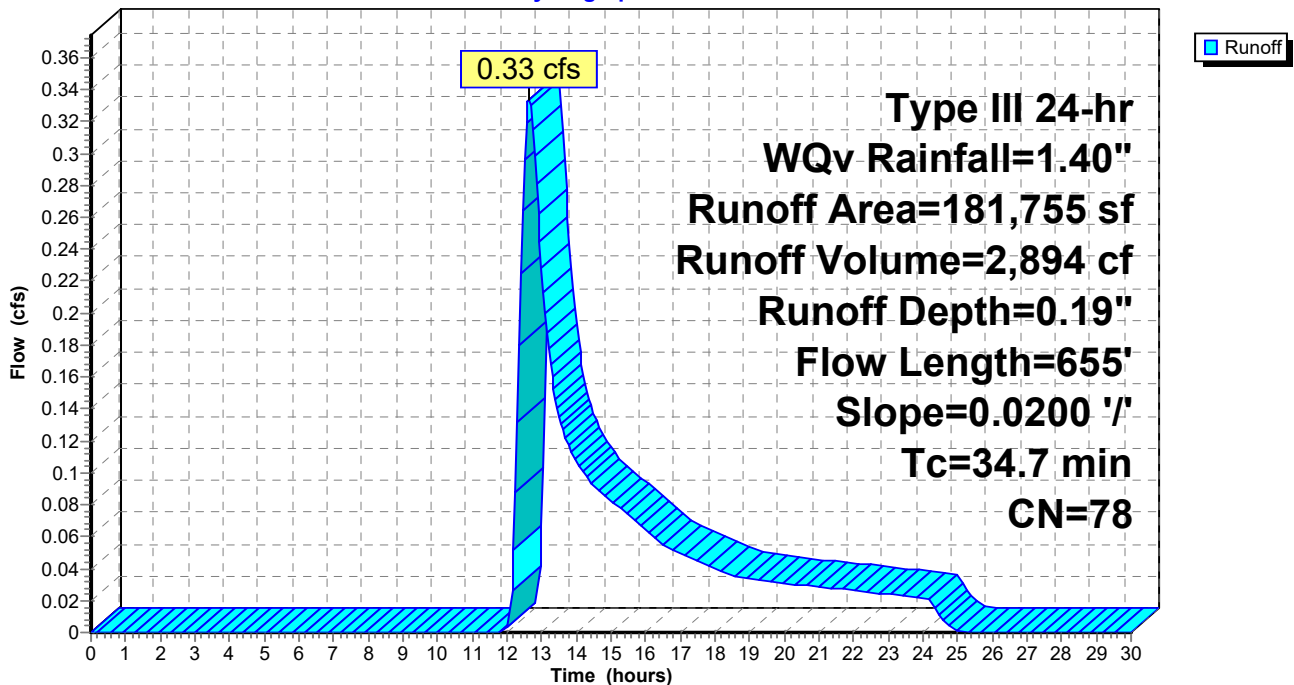
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
2,800	98	Paved parking, HSG D
73,077	80	>75% Grass cover, Good, HSG D
22,724	73	Brush, Good, HSG D
83,154	77	Woods, Good, HSG D
181,755	78	Weighted Average
178,955		98.46% Pervious Area
2,800		1.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.6	100	0.0200	0.08		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.17"
13.1	555	0.0200	0.71		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
34.7	655	Total			

**Subcatchment PW1A: LOD**

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 124

**Summary for Subcatchment PW1BN: N HALF BLDG**

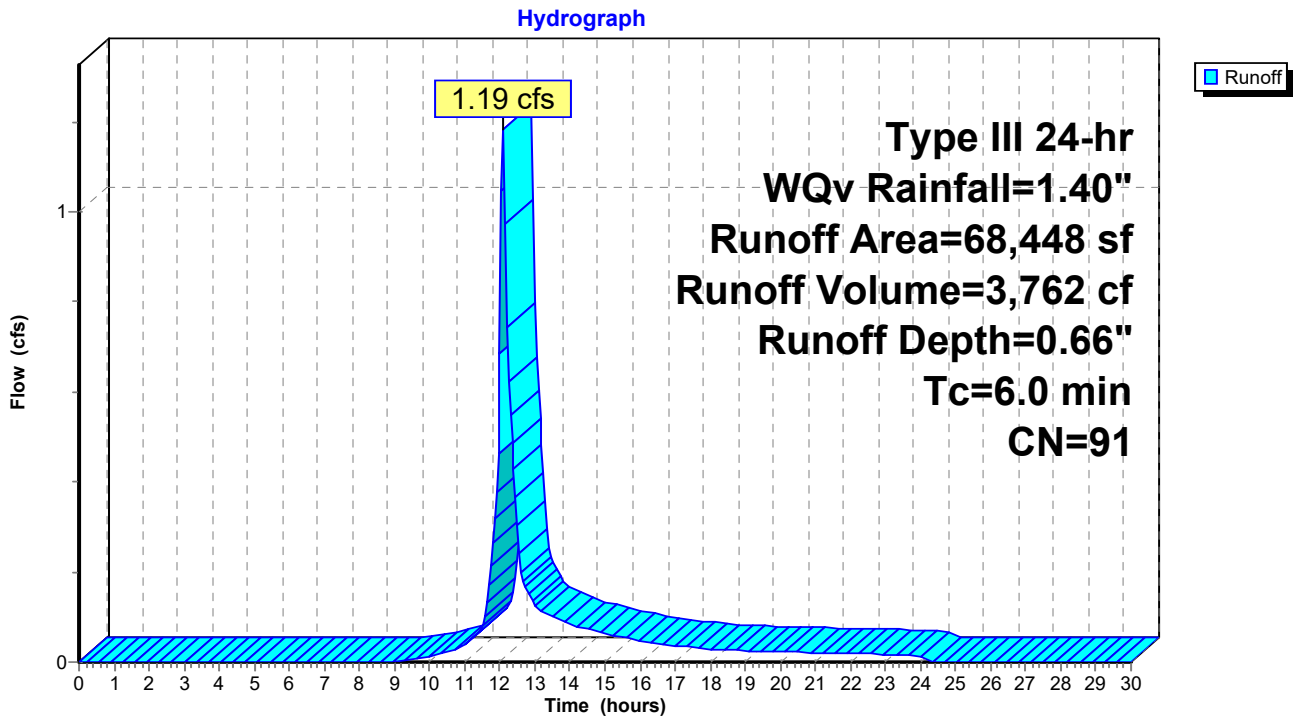
Runoff = 1.19 cfs @ 12.09 hrs, Volume= 3,762 cf, Depth= 0.66"  
 Routed to Pond 1BN : BIO-1BN

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
40,450	98	Paved parking, HSG D
27,998	80	>75% Grass cover, Good, HSG D
68,448	91	Weighted Average
27,998		40.90% Pervious Area
40,450		59.10% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BN: N HALF BLDG**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 125

**Summary for Subcatchment PW1BS: S HALF BLDG**

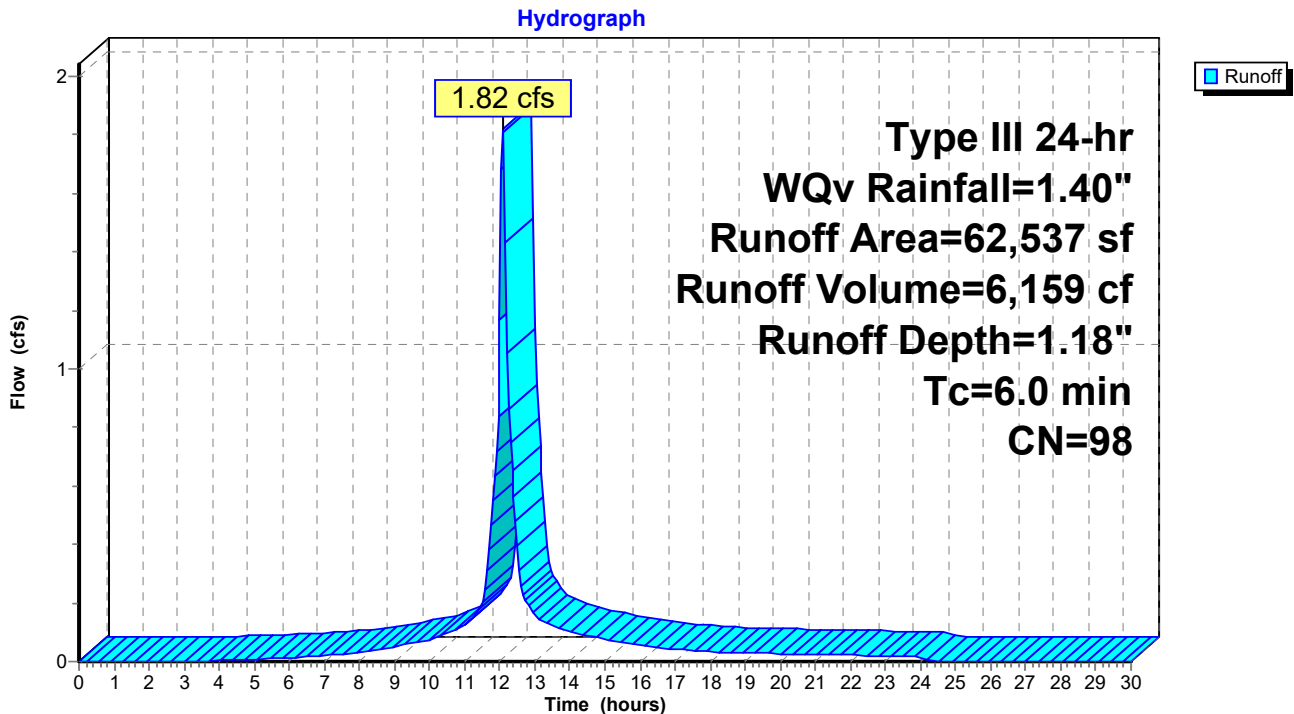
Runoff = 1.82 cfs @ 12.09 hrs, Volume= 6,159 cf, Depth= 1.18"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
62,537	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
62,537	98	Weighted Average
62,537		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1BS: S HALF BLDG**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 126

**Summary for Subcatchment PW1C: PARKING**

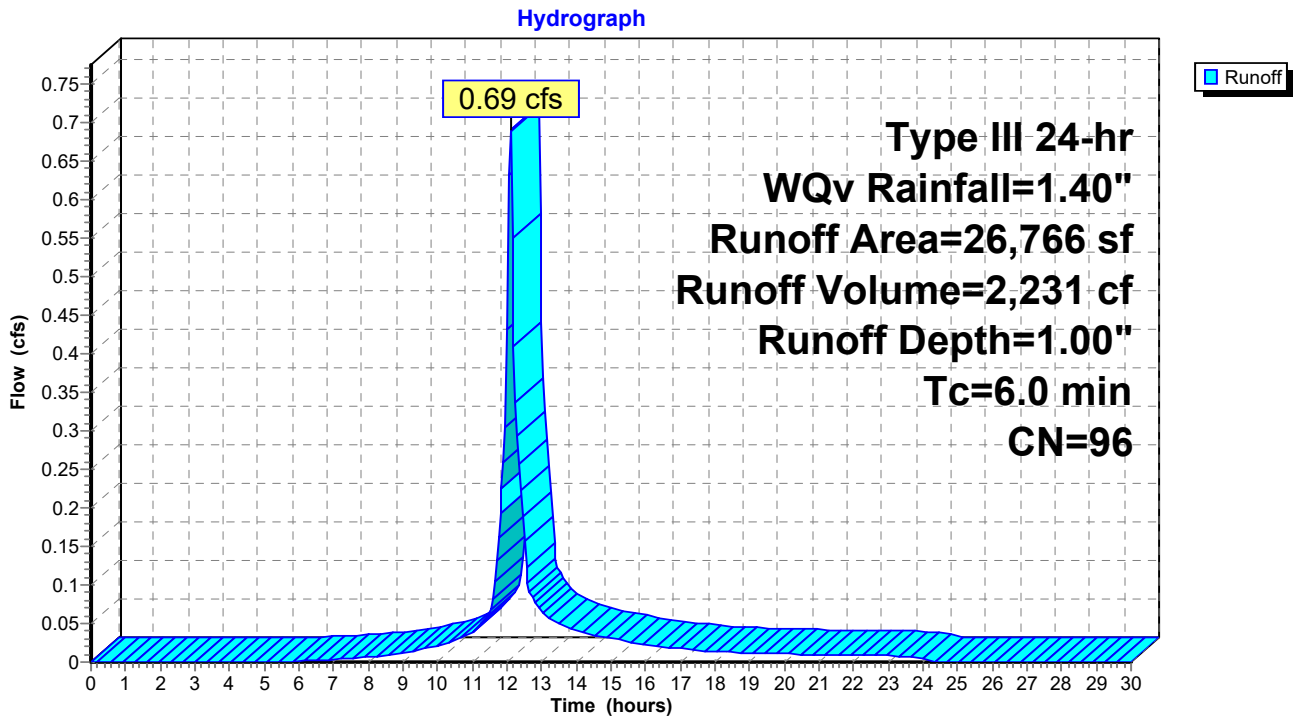
Runoff = 0.69 cfs @ 12.09 hrs, Volume= 2,231 cf, Depth= 1.00"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
23,545	98	Paved parking, HSG D
3,221	80	>75% Grass cover, Good, HSG D
26,766	96	Weighted Average
3,221		12.03% Pervious Area
23,545		87.97% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1C: PARKING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 127

**Summary for Subcatchment PW1D: ENTRANCE**

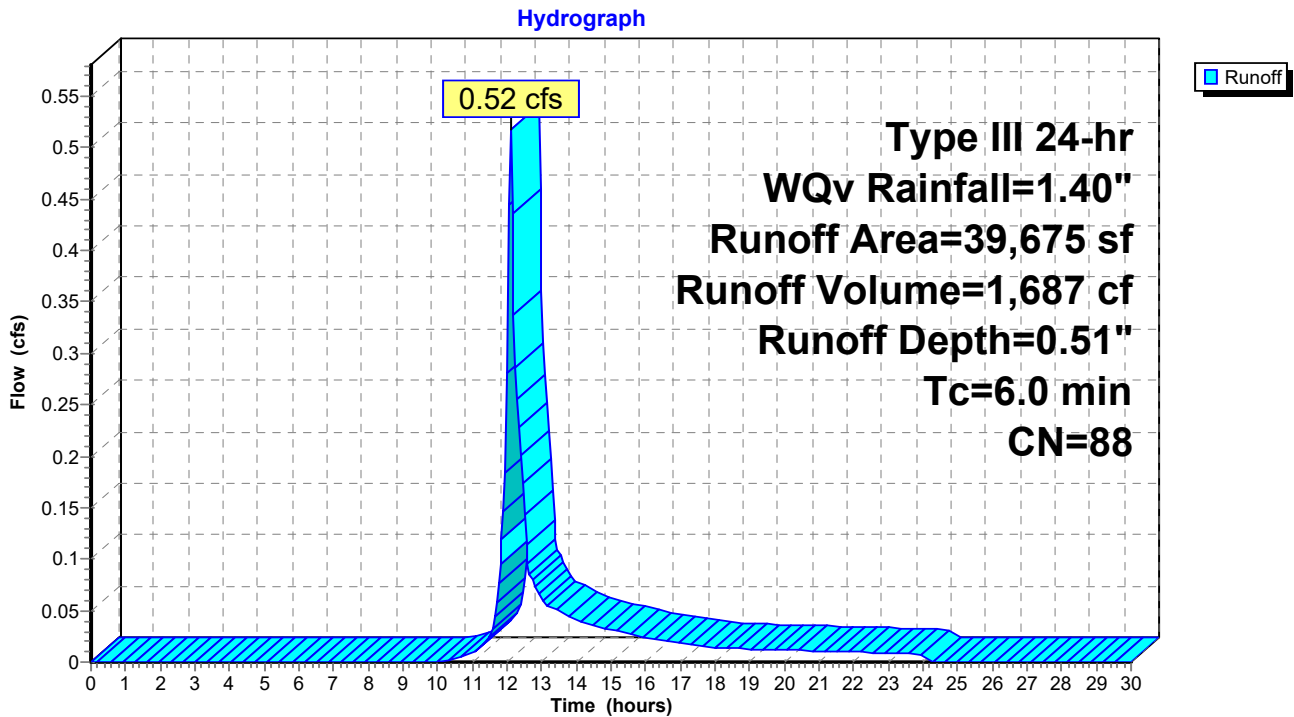
Runoff = 0.52 cfs @ 12.10 hrs, Volume= 1,687 cf, Depth= 0.51"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
17,739	98	Paved parking, HSG D
21,936	80	>75% Grass cover, Good, HSG D
39,675	88	Weighted Average
21,936		55.29% Pervious Area
17,739		44.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1D: ENTRANCE**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 128

**Summary for Subcatchment PW1E: TRAILERS**

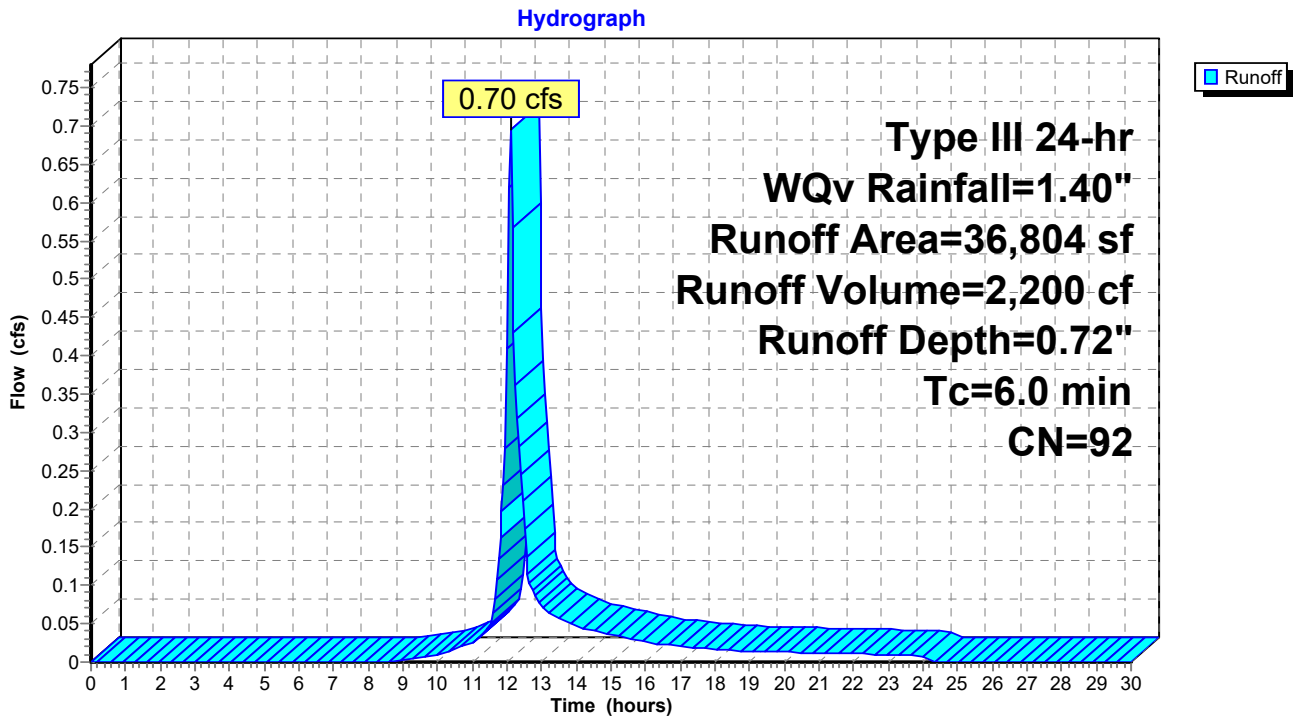
Runoff = 0.70 cfs @ 12.09 hrs, Volume= 2,200 cf, Depth= 0.72"  
Routed to Pond 1E : BIO-1E

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
25,092	98	Paved parking, HSG D
11,712	80	>75% Grass cover, Good, HSG D
36,804	92	Weighted Average
11,712		31.82% Pervious Area
25,092		68.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1E: TRAILERS**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 129

**Summary for Subcatchment PW1F: TRAILER 2**

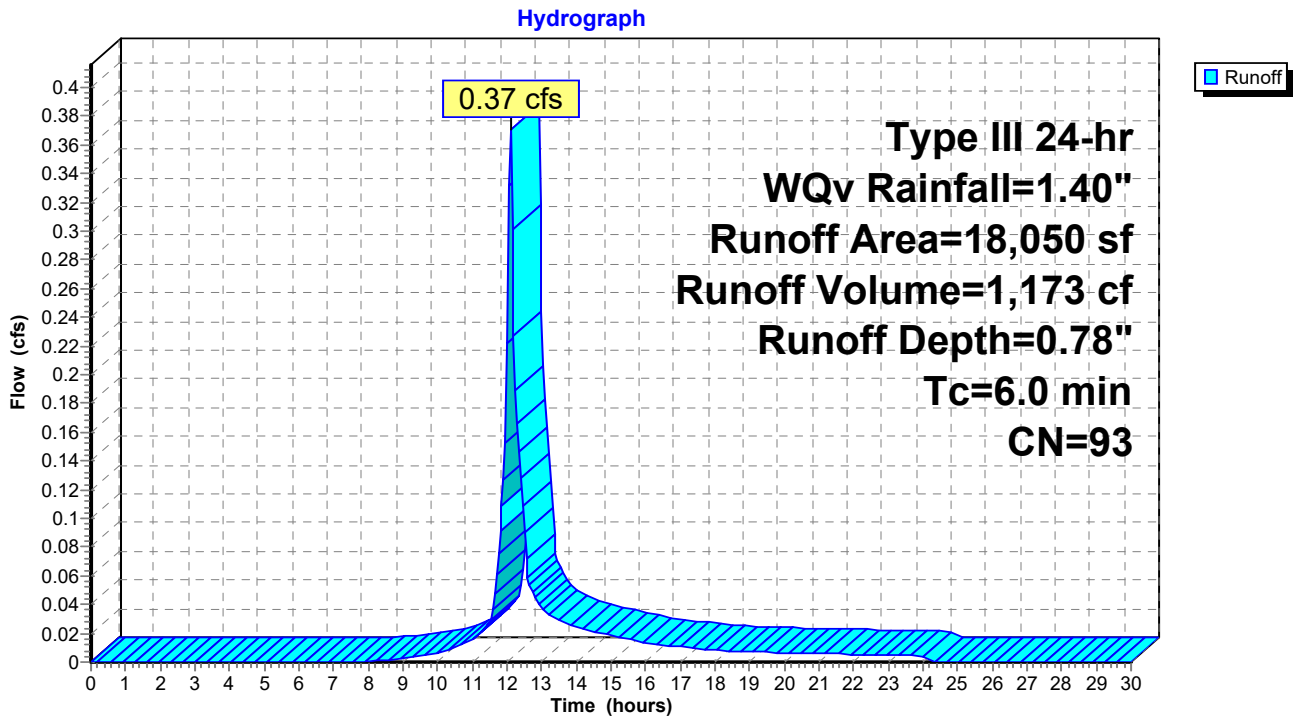
Runoff = 0.37 cfs @ 12.09 hrs, Volume= 1,173 cf, Depth= 0.78"  
 Routed to Pond 1F : BIO-1F

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
12,622	98	Paved parking, HSG D
5,428	80	>75% Grass cover, Good, HSG D
18,050	93	Weighted Average
5,428		30.07% Pervious Area
12,622		69.93% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1F: TRAILER 2**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 130

**Summary for Subcatchment PW1G: LOADING**

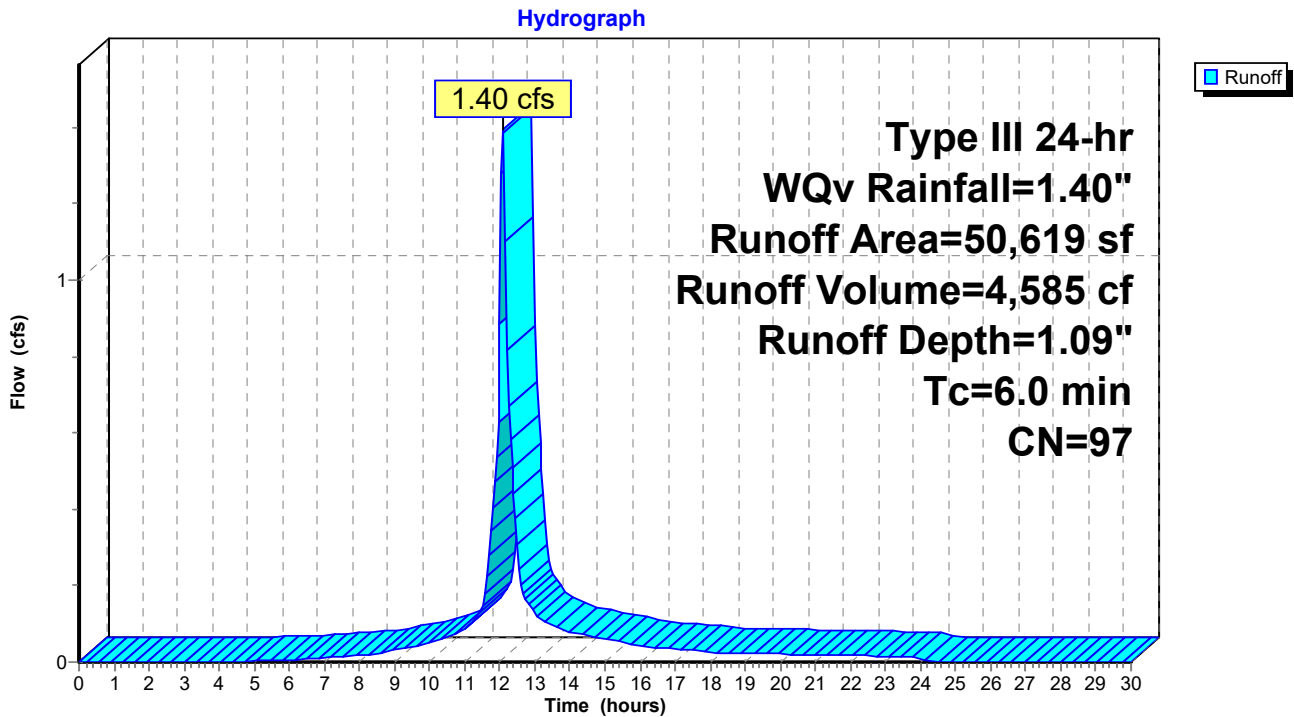
Runoff = 1.40 cfs @ 12.09 hrs, Volume= 4,585 cf, Depth= 1.09"  
 Routed to Pond SUBS : SUBS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
46,810	98	Paved parking, HSG D
3,809	80	>75% Grass cover, Good, HSG D
50,619	97	Weighted Average
3,809		7.52% Pervious Area
46,810		92.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1G: LOADING**



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 131

**Summary for Subcatchment PW1H: NW CORNER BLDG**

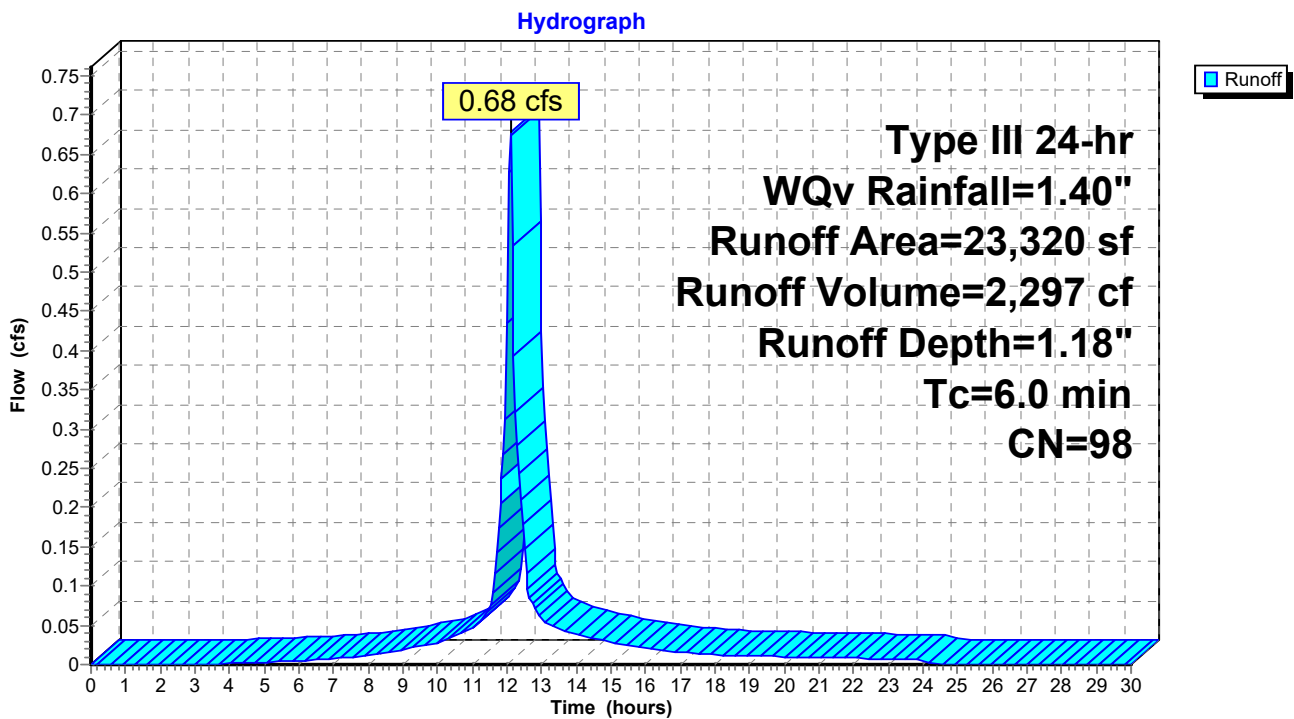
Runoff = 0.68 cfs @ 12.09 hrs, Volume= 2,297 cf, Depth= 1.18"  
 Routed to Pond 1D : BIO-1D

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Type III 24-hr WQv Rainfall=1.40"

Area (sf)	CN	Description
23,320	98	Paved parking, HSG D
0	80	>75% Grass cover, Good, HSG D
23,320	98	Weighted Average
23,320		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Subcatchment PW1H: NW CORNER BLDG**





**230119 - R1 - Dewpoint South**

Type III 24-hr WQv Rainfall=1.40"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 132

**Summary for Pond 1BN: BIO-1BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth = 0.66" for WQv event  
 Inflow = 1.19 cfs @ 12.09 hrs, Volume= 3,762 cf  
 Outflow = 0.01 cfs @ 24.09 hrs, Volume= 481 cf, Atten= 99%, Lag= 719.9 min  
 Primary = 0.01 cfs @ 24.09 hrs, Volume= 481 cf  
 Routed to Pond 2BN : BIO-2BN

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 491.79' @ 24.09 hrs Surf.Area= 2,423 sf Storage= 3,429 cf

Plug-Flow detention time= 533.5 min calculated for 481 cf (13% of inflow)  
 Center-of-Mass det. time= 378.3 min ( 1,216.0 - 837.7 )

Volume	Invert	Avail.Storage	Storage Description		
#1	490.00'	10,349 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
490.00	1,454	0	0	1,454	
492.00	2,555	3,958	3,958	2,611	
494.00	3,883	6,392	10,349	4,013	

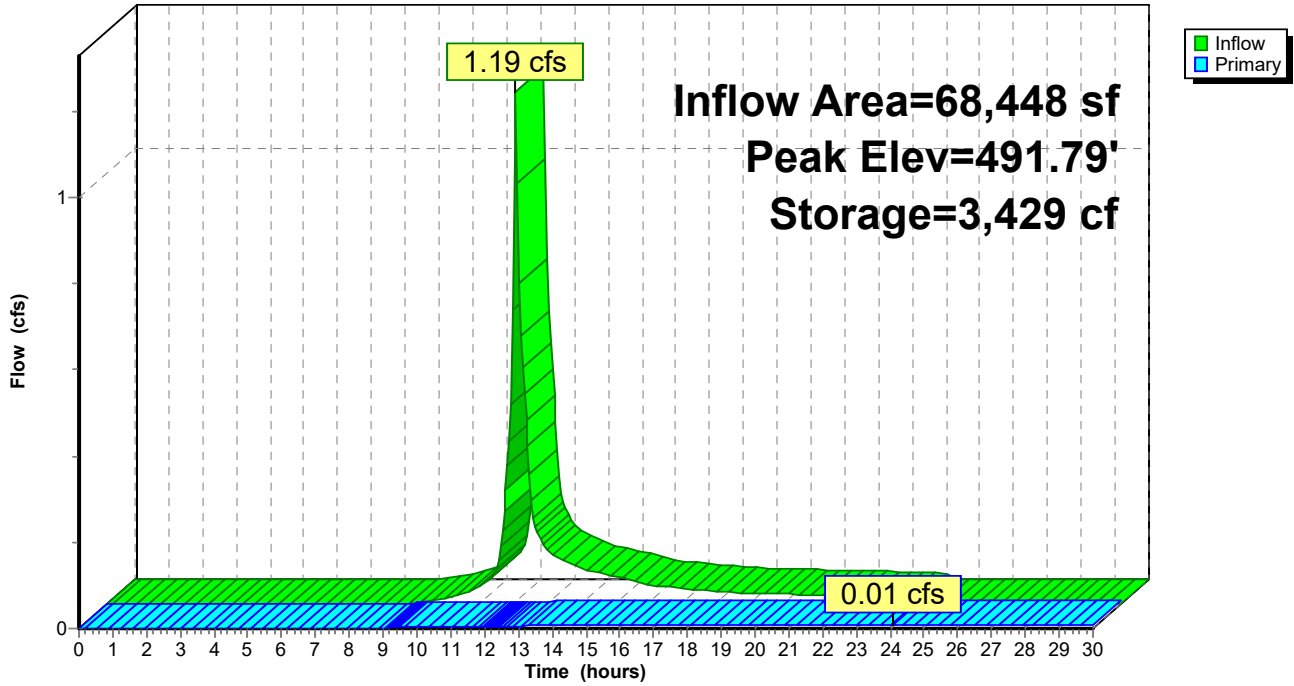
Device	Routing	Invert	Outlet Devices
#1	Primary	483.15'	<b>18.0" Round Culvert</b> L= 26.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 483.15' / 482.62' S= 0.0204 ' / Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	492.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	490.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.01 cfs @ 24.09 hrs HW=491.79' TW=484.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.01 cfs of 23.74 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 1BN: BIO-1BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 134

**Stage-Area-Storage for Pond 1BN: BIO-1BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
490.00	1,454	0	492.65	2,956	5,747
490.05	1,478	73	492.70	2,988	5,896
490.10	1,502	148	492.75	3,021	6,046
490.15	1,526	223	492.80	3,053	6,198
490.20	1,550	300	492.85	3,086	6,351
490.25	1,575	378	492.90	3,118	6,506
490.30	1,599	458	492.95	3,151	6,663
490.35	1,624	538	493.00	3,184	6,822
490.40	1,650	620	493.05	3,218	6,982
490.45	1,675	703	493.10	3,251	7,143
490.50	1,700	788	493.15	3,285	7,307
490.55	1,726	873	493.20	3,319	7,472
490.60	1,752	960	493.25	3,353	7,639
490.65	1,778	1,049	493.30	3,387	7,807
490.70	1,804	1,138	493.35	3,421	7,977
490.75	1,831	1,229	493.40	3,456	8,149
490.80	1,857	1,321	493.45	3,490	8,323
490.85	1,884	1,415	493.50	3,525	8,498
490.90	1,911	1,510	493.55	3,560	8,675
490.95	1,939	1,606	493.60	3,595	8,854
491.00	1,966	1,704	493.65	3,631	9,035
491.05	1,994	1,803	493.70	3,666	9,217
491.10	2,021	1,903	493.75	3,702	9,401
491.15	2,049	2,005	493.80	3,738	9,587
491.20	2,078	2,108	493.85	3,774	9,775
491.25	2,106	2,212	493.90	3,810	9,965
491.30	2,135	2,318	493.95	3,846	10,156
491.35	2,163	2,426	494.00	<b>3,883</b>	<b>10,349</b>
491.40	2,192	2,535			
491.45	2,221	2,645			
491.50	2,251	2,757			
491.55	2,280	2,870			
491.60	2,310	2,985			
491.65	2,340	3,101			
491.70	2,370	3,219			
491.75	2,401	3,338			
491.80	2,431	3,459			
491.85	2,462	3,581			
491.90	2,493	3,705			
491.95	2,524	3,831			
492.00	2,555	3,958			
492.05	2,585	4,086			
492.10	2,615	4,216			
492.15	2,645	4,348			
492.20	2,675	4,481			
492.25	2,706	4,615			
492.30	2,737	4,751			
492.35	2,767	4,889			
492.40	2,798	5,028			
492.45	2,830	5,169			
492.50	2,861	5,311			
492.55	2,893	5,455			
492.60	2,924	5,600			

**230119 - R1 - Dewpoint South**

Type III 24-hr WQv Rainfall=1.40"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 135

**Summary for Pond 1D: BIO-1D**

Inflow Area = 89,761 sf, 71.97% Impervious, Inflow Depth = 0.83" for WQv event  
 Inflow = 1.89 cfs @ 12.09 hrs, Volume= 6,214 cf  
 Outflow = 0.09 cfs @ 15.18 hrs, Volume= 2,517 cf, Atten= 95%, Lag= 185.4 min  
 Primary = 0.09 cfs @ 15.18 hrs, Volume= 2,517 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 468.61' @ 15.18 hrs Surf.Area= 7,278 sf Storage= 4,229 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)  
 Center-of-Mass det. time= 275.1 min ( 1,082.0 - 806.9 )

Volume	Invert	Avail.Storage	Storage Description		
#1	468.00'	15,581 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
468.00	6,529	0	0	6,529	
470.00	9,124	15,581	15,581	9,218	

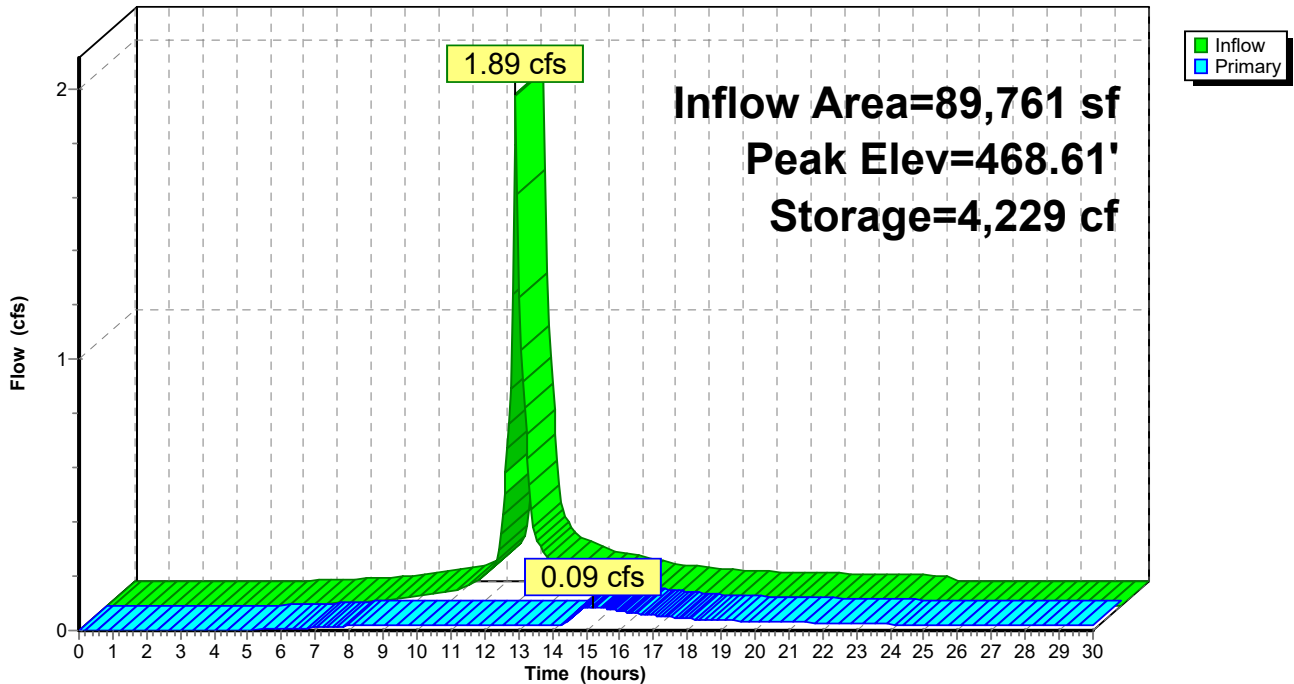
Device	Routing	Invert	Outlet Devices
#1	Primary	464.50'	<b>12.0" Round Culvert</b> L= 190.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 464.50' / 462.98' S= 0.0080 ' S= 0.0080 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.60'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	468.00'	<b>0.125 in/hr Exfiltration over Surface area</b>
#4	Primary	469.00'	<b>10.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83

**Primary OutFlow** Max=0.09 cfs @ 15.18 hrs HW=468.61' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.09 cfs of 5.29 cfs potential flow)
- 2=Broad-Crested Rectangular Weir (Weir Controls 0.07 cfs @ 0.32 fps)
- 3=Exfiltration (Exfiltration Controls 0.02 cfs)
- 4=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

Pond 1D: BIO-1D

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 137

**Stage-Area-Storage for Pond 1D: BIO-1D**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
468.00	6,529	0	469.06	7,850	7,610
468.02	6,553	131	469.08	7,876	7,768
468.04	6,577	262	469.10	7,903	7,925
468.06	6,601	394	469.12	7,929	8,084
468.08	6,624	526	469.14	7,955	8,243
468.10	6,648	659	469.16	7,981	8,402
468.12	6,672	792	469.18	8,008	8,562
468.14	6,697	926	469.20	8,034	8,722
468.16	6,721	1,060	469.22	8,060	8,883
468.18	6,745	1,195	469.24	8,087	9,045
468.20	6,769	1,330	469.26	8,113	9,207
468.22	6,793	1,465	469.28	8,140	9,369
468.24	6,818	1,601	469.30	8,166	9,532
468.26	6,842	1,738	469.32	8,193	9,696
468.28	6,866	1,875	469.34	8,220	9,860
468.30	6,891	2,013	469.36	8,246	10,025
468.32	6,915	2,151	469.38	8,273	10,190
468.34	6,940	2,289	469.40	8,300	10,356
468.36	6,964	2,428	469.42	8,327	10,522
468.38	6,989	2,568	469.44	8,354	10,689
468.40	7,013	2,708	469.46	8,381	10,856
468.42	7,038	2,848	469.48	8,408	11,024
468.44	7,063	2,989	469.50	8,435	11,192
468.46	7,087	3,131	469.52	8,462	11,361
468.48	7,112	3,273	469.54	8,489	11,531
468.50	7,137	3,415	469.56	8,516	11,701
468.52	7,162	3,558	469.58	8,543	11,871
468.54	7,187	3,702	469.60	8,570	12,043
468.56	7,212	3,846	469.62	8,598	12,214
468.58	7,237	3,990	469.64	8,625	12,386
468.60	7,262	4,135	469.66	8,652	12,559
468.62	7,287	4,281	469.68	8,680	12,733
468.64	7,312	4,427	469.70	8,707	12,906
468.66	7,337	4,573	469.72	8,735	13,081
468.68	7,363	4,720	469.74	8,762	13,256
468.70	7,388	4,868	469.76	8,790	13,431
468.72	7,413	5,016	469.78	8,817	13,607
468.74	7,439	5,164	469.80	8,845	13,784
468.76	7,464	5,313	469.82	8,873	13,961
468.78	7,490	5,463	469.84	8,900	14,139
468.80	7,515	5,613	469.86	8,928	14,317
468.82	7,541	5,764	469.88	8,956	14,496
468.84	7,566	5,915	469.90	8,984	14,675
468.86	7,592	6,066	469.92	9,012	14,855
468.88	7,617	6,218	469.94	9,040	15,036
468.90	7,643	6,371	469.96	9,068	15,217
468.92	7,669	6,524	469.98	9,096	15,399
468.94	7,695	6,678	470.00	<b>9,124</b>	<b>15,581</b>
468.96	7,721	6,832			
468.98	7,746	6,986			
469.00	7,772	7,142			
469.02	7,798	7,297			
469.04	7,824	7,454			

**230119 - R1 - Dewpoint South**

Type III 24-hr WQv Rainfall=1.40"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 138

**Summary for Pond 1E: BIO-1E**

Inflow Area = 36,804 sf, 68.18% Impervious, Inflow Depth = 0.72" for WQv event  
 Inflow = 0.70 cfs @ 12.09 hrs, Volume= 2,200 cf  
 Outflow = 0.01 cfs @ 22.88 hrs, Volume= 708 cf, Atten= 99%, Lag= 647.3 min  
 Primary = 0.01 cfs @ 22.88 hrs, Volume= 708 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 467.54' @ 22.88 hrs Surf.Area= 3,355 sf Storage= 1,701 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)  
 Center-of-Mass det. time= 356.8 min ( 1,188.3 - 831.5 )

Volume	Invert	Avail.Storage	Storage Description		
#1	467.00'	12,471 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
467.00	2,940	0	0	2,940	
468.00	3,728	3,326	3,326	3,761	
470.00	5,472	9,144	12,471	5,587	

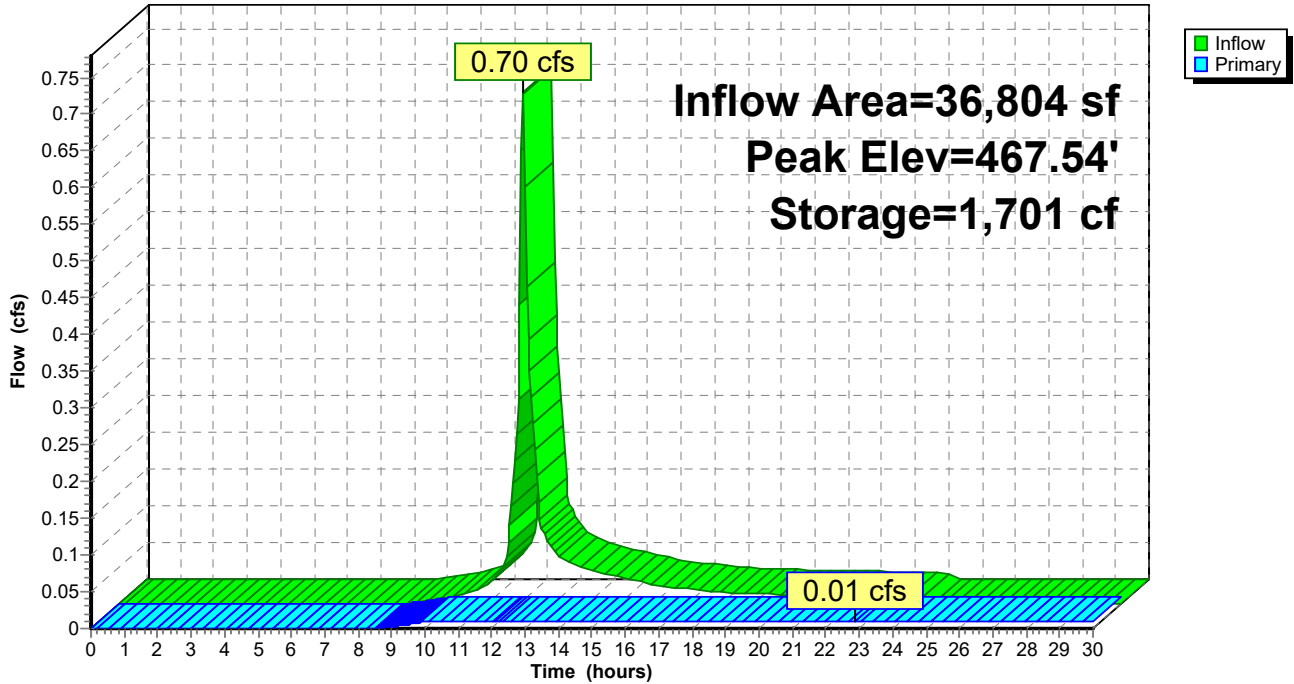
Device	Routing	Invert	Outlet Devices
#1	Primary	463.50'	<b>12.0" Round Culvert</b> L= 23.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 463.50' / 462.93' S= 0.0248 ' S= 0.0248 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	468.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	467.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.01 cfs @ 22.88 hrs HW=467.54' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.01 cfs of 7.12 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Exfiltration (Exfiltration Controls 0.01 cfs)

### Pond 1E: BIO-1E

Hydrograph





**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

*Type III 24-hr WQv Rainfall=1.40"*

Printed 2/2/2023

Page 140

**Stage-Area-Storage for Pond 1E: BIO-1E**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
467.00	2,940	0	469.65	5,143	10,613
467.05	2,977	148	469.70	5,189	10,872
467.10	3,015	298	469.75	5,236	11,132
467.15	3,052	449	469.80	5,283	11,395
467.20	3,090	603	469.85	5,330	11,661
467.25	3,128	758	469.90	5,377	11,928
467.30	3,167	916	469.95	5,424	12,198
467.35	3,205	1,075	470.00	<b>5,472</b>	<b>12,471</b>
467.40	3,244	1,236			
467.45	3,283	1,399			
467.50	3,322	1,565			
467.55	3,362	1,732			
467.60	3,402	1,901			
467.65	3,442	2,072			
467.70	3,482	2,245			
467.75	3,522	2,420			
467.80	3,563	2,597			
467.85	3,604	2,776			
467.90	3,645	2,958			
467.95	3,686	3,141			
468.00	3,728	3,326			
468.05	3,768	3,514			
468.10	3,807	3,703			
468.15	3,847	3,894			
468.20	3,887	4,088			
468.25	3,928	4,283			
468.30	3,968	4,480			
468.35	4,009	4,680			
468.40	4,050	4,881			
468.45	4,091	5,085			
468.50	4,133	5,291			
468.55	4,174	5,498			
468.60	4,216	5,708			
468.65	4,258	5,920			
468.70	4,300	6,134			
468.75	4,343	6,350			
468.80	4,386	6,568			
468.85	4,428	6,788			
468.90	4,472	7,011			
468.95	4,515	7,236			
469.00	4,558	7,462			
469.05	4,602	7,691			
469.10	4,646	7,923			
469.15	4,690	8,156			
469.20	4,734	8,392			
469.25	4,779	8,629			
469.30	4,824	8,870			
469.35	4,869	9,112			
469.40	4,914	9,356			
469.45	4,959	9,603			
469.50	5,005	9,852			
469.55	5,051	10,104			
469.60	5,097	10,357			

**230119 - R1 - Dewpoint South**

Type III 24-hr WQv Rainfall=1.40"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 141

**Summary for Pond 1F: BIO-1F**

Inflow Area = 18,050 sf, 69.93% Impervious, Inflow Depth = 0.78" for WQv event  
 Inflow = 0.37 cfs @ 12.09 hrs, Volume= 1,173 cf  
 Outflow = 0.00 cfs @ 23.01 hrs, Volume= 357 cf, Atten= 99%, Lag= 655.1 min  
 Primary = 0.00 cfs @ 23.01 hrs, Volume= 357 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 477.61' @ 23.01 hrs Surf.Area= 1,683 sf Storage= 920 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)  
 Center-of-Mass det. time= 356.5 min ( 1,181.5 - 825.0 )

Volume	Invert	Avail.Storage	Storage Description		
#1	477.00'	6,744 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
477.00	1,347	0	0	1,347	
478.00	1,919	1,625	1,625	1,941	
480.00	3,259	5,119	6,744	3,341	

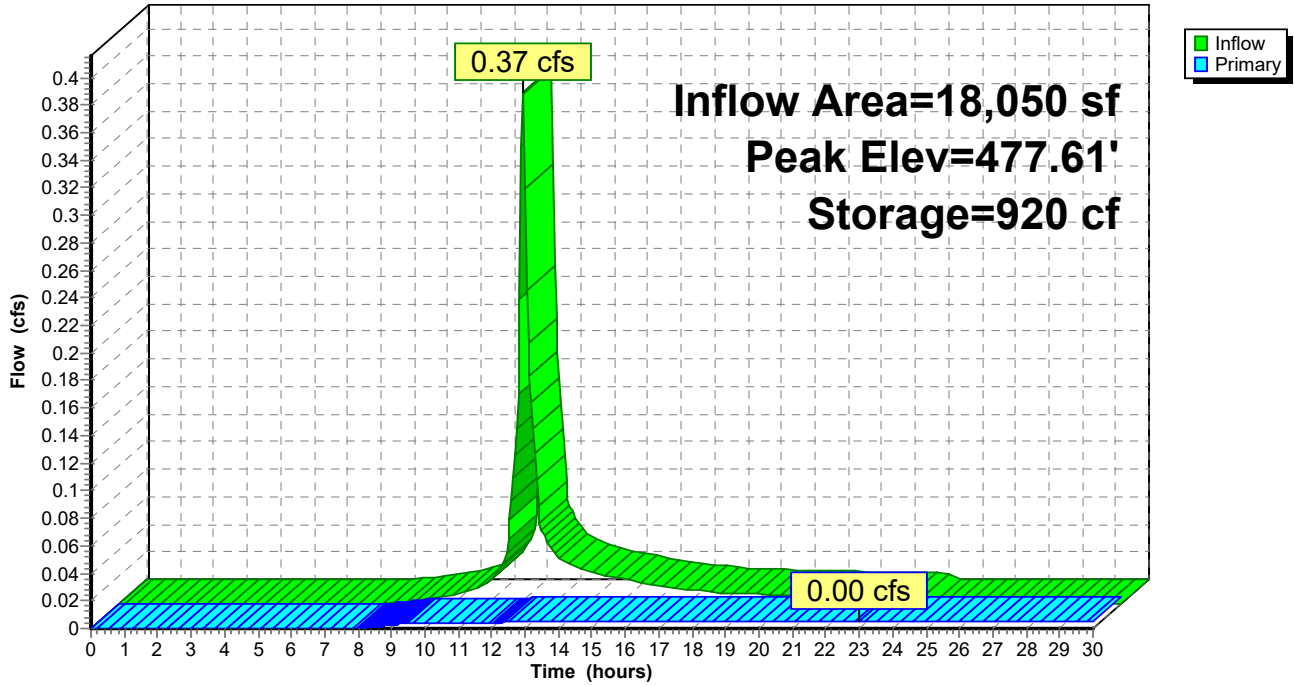
Device	Routing	Invert	Outlet Devices
#1	Primary	473.50'	<b>12.0" Round Culvert</b> L= 115.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 473.50' / 471.21' S= 0.0199 ' S= 0.0199 ' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	478.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	477.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.00 cfs @ 23.01 hrs HW=477.61' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.00 cfs of 6.85 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Exfiltration (Exfiltration Controls 0.00 cfs)

Pond 1F: BIO-1F

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 143

**Stage-Area-Storage for Pond 1F: BIO-1F**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
477.00	1,347	0	479.65	2,999	5,649
477.05	1,373	68	479.70	3,036	5,800
477.10	1,400	137	479.75	3,072	5,953
477.15	1,426	208	479.80	3,109	6,107
477.20	1,453	280	479.85	3,146	6,263
477.25	1,481	353	479.90	3,184	6,422
477.30	1,508	428	479.95	3,221	6,582
477.35	1,536	504	480.00	<b>3,259</b>	<b>6,744</b>
477.40	1,564	582			
477.45	1,592	660			
477.50	1,620	741			
477.55	1,649	823			
477.60	1,678	906			
477.65	1,707	990			
477.70	1,737	1,076			
477.75	1,767	1,164			
477.80	1,797	1,253			
477.85	1,827	1,344			
477.90	1,857	1,436			
477.95	1,888	1,529			
478.00	1,919	1,625			
478.05	1,948	1,721			
478.10	1,978	1,819			
478.15	2,007	1,919			
478.20	2,037	2,020			
478.25	2,067	2,123			
478.30	2,098	2,227			
478.35	2,128	2,333			
478.40	2,159	2,440			
478.45	2,190	2,548			
478.50	2,221	2,659			
478.55	2,252	2,770			
478.60	2,284	2,884			
478.65	2,316	2,999			
478.70	2,348	3,115			
478.75	2,380	3,234			
478.80	2,413	3,353			
478.85	2,445	3,475			
478.90	2,478	3,598			
478.95	2,512	3,723			
479.00	2,545	3,849			
479.05	2,579	3,977			
479.10	2,612	4,107			
479.15	2,646	4,239			
479.20	2,681	4,372			
479.25	2,715	4,507			
479.30	2,750	4,643			
479.35	2,785	4,782			
479.40	2,820	4,922			
479.45	2,855	5,064			
479.50	2,891	5,207			
479.55	2,927	5,353			
479.60	2,963	5,500			

**230119 - R1 - Dewpoint South**

Type III 24-hr WQv Rainfall=1.40"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 144

**Summary for Pond 2BN: BIO-2BN**

Inflow Area = 68,448 sf, 59.10% Impervious, Inflow Depth > 0.08" for WQv event  
 Inflow = 0.01 cfs @ 24.09 hrs, Volume= 481 cf  
 Outflow = 0.01 cfs @ 24.09 hrs, Volume= 481 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 0.01 cfs @ 24.09 hrs, Volume= 481 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 484.00' @ 24.09 hrs Surf.Area= 2,843 sf Storage= 0 cf

Plug-Flow detention time= 0.0 min calculated for 480 cf (100% of inflow)  
 Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume	Invert	Avail.Storage	Storage Description		
#1	484.00'	17,309 cf	<b>Custom Stage Data (Pyramidal)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
484.00	2,843	0	0	2,843	
486.00	4,295	7,088	7,088	4,371	
488.00	5,972	10,221	17,309	6,142	

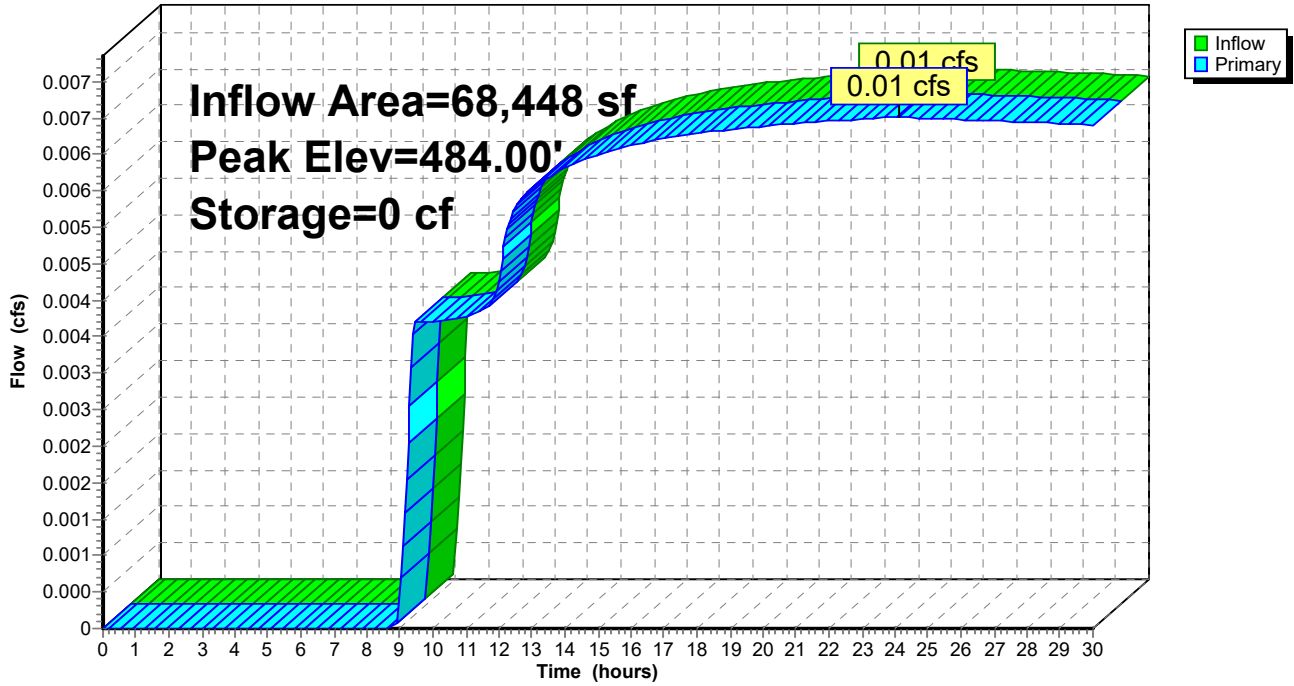
Device	Routing	Invert	Outlet Devices
#1	Primary	480.50'	<b>18.0" Round Culvert</b> L= 52.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 480.50' / 478.00' S= 0.0481 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Device 1	486.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	484.50'	<b>12.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	484.00'	<b>0.125 in/hr Exfiltration over Surface area</b>

**Primary OutFlow** Max=0.01 cfs @ 24.09 hrs HW=484.00' TW=0.00' (Dynamic Tailwater)

- 1=Culvert (Passes 0.01 cfs of 14.11 cfs potential flow)
- 2=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 3=Orifice/Grate ( Controls 0.00 cfs)
- 4=Exfiltration (Exfiltration Controls 0.01 cfs)

Pond 2BN: BIO-2BN

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 146

**Stage-Area-Storage for Pond 2BN: BIO-2BN**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
484.00	2,843	0	486.65	4,810	10,046
484.05	2,876	143	486.70	4,851	10,287
484.10	2,909	288	486.75	4,892	10,531
484.15	2,942	434	486.80	4,933	10,776
484.20	2,975	582	486.85	4,974	11,024
484.25	3,008	731	486.90	5,016	11,274
484.30	3,042	883	486.95	5,057	11,526
484.35	3,076	1,035	487.00	5,099	11,780
484.40	3,110	1,190	487.05	5,141	12,036
484.45	3,144	1,346	487.10	5,183	12,294
484.50	3,178	1,504	487.15	5,226	12,554
484.55	3,213	1,664	487.20	5,268	12,816
484.60	3,247	1,826	487.25	5,311	13,081
484.65	3,282	1,989	487.30	5,354	13,347
484.70	3,317	2,154	487.35	5,397	13,616
484.75	3,353	2,321	487.40	5,440	13,887
484.80	3,388	2,489	487.45	5,483	14,160
484.85	3,424	2,659	487.50	5,527	14,435
484.90	3,459	2,832	487.55	5,571	14,713
484.95	3,495	3,005	487.60	5,615	14,992
485.00	3,532	3,181	487.65	5,659	15,274
485.05	3,568	3,359	487.70	5,703	15,558
485.10	3,605	3,538	487.75	5,747	15,844
485.15	3,641	3,719	487.80	5,792	16,133
485.20	3,678	3,902	487.85	5,837	16,424
485.25	3,716	4,087	487.90	5,882	16,717
485.30	3,753	4,274	487.95	5,927	17,012
485.35	3,790	4,462	488.00	<b>5,972</b>	<b>17,309</b>
485.40	3,828	4,653			
485.45	3,866	4,845			
485.50	3,904	5,039			
485.55	3,942	5,235			
485.60	3,981	5,434			
485.65	4,019	5,634			
485.70	4,058	5,835			
485.75	4,097	6,039			
485.80	4,136	6,245			
485.85	4,176	6,453			
485.90	4,215	6,663			
485.95	4,255	6,875			
486.00	4,295	7,088			
486.05	4,334	7,304			
486.10	4,372	7,522			
486.15	4,411	7,741			
486.20	4,450	7,963			
486.25	4,490	8,186			
486.30	4,529	8,412			
486.35	4,569	8,639			
486.40	4,608	8,869			
486.45	4,648	9,100			
486.50	4,688	9,333			
486.55	4,729	9,569			
486.60	4,769	9,806			

**230119 - R1 - Dewpoint South**

Type III 24-hr WQv Rainfall=1.40"

Prepared by Maser Consulting

Printed 2/2/2023

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Page 147

**Summary for Pond SUBS: SUBS**

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth = 1.14" for WQv event  
 Inflow = 3.22 cfs @ 12.09 hrs, Volume= 10,743 cf  
 Outflow = 0.40 cfs @ 12.68 hrs, Volume= 10,592 cf, Atten= 88%, Lag= 35.3 min  
 Primary = 0.40 cfs @ 12.68 hrs, Volume= 10,592 cf  
 Routed to Link JF : JELLY FISH  
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf  
 Routed to Link PROP : PROPOSED

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs  
 Peak Elev= 476.06' @ 12.68 hrs Surf.Area= 8,608 sf Storage= 4,892 cf

Plug-Flow detention time= 156.4 min calculated for 10,575 cf (98% of inflow)  
 Center-of-Mass det. time= 148.0 min ( 931.0 - 783.0 )

Volume	Invert	Avail.Storage	Storage Description
#1A	475.00'	13,785 cf	<b>83.00'W x 103.72'L x 6.75'H Field A</b> 58,107 cf Overall - 23,645 cf Embedded = 34,463 cf x 40.0% Voids
#2A	475.75'	23,645 cf	<b>ADS_StormTech MC-4500 +Cap x 216 Inside #1</b> Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 216 Chambers in 9 Rows Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf
		37,430 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	472.00'	<b>12.0" Round Culvert</b> L= 30.9' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 472.00' / 471.69' S= 0.0100 '/ Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
#2	Device 1	475.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Device 1	480.25'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Secondary	479.00'	<b>18.0" Round Culvert</b> L= 46.5' Box, headwall w/3 rounded edges, Ke= 0.200 Inlet / Outlet Invert= 479.00' / 477.56' S= 0.0310 '/ Cc= 0.900 n= 0.012, Flow Area= 1.77 sf

**Primary OutFlow** Max=0.40 cfs @ 12.68 hrs HW=476.06' TW=0.00' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 0.40 cfs of 8.13 cfs potential flow)
- ↑ 2=Orifice/Grate (Orifice Controls 0.40 cfs @ 4.55 fps)
- ↑ 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=475.00' TW=0.00' (Dynamic Tailwater)

- ↑ 4=Culvert ( Controls 0.00 cfs)



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 148

**Pond SUBS: SUBS - Chamber Wizard Field A**

**Chamber Model = ADS\_StormTech MC-4500 +Cap (ADS StormTech® MC-4500 with cap, use MC-4500 b for new designs)**

Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf

Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap

Cap Storage= 35.7 cf x 2 x 9 rows = 642.6 cf

100.0" Wide + 9.0" Spacing = 109.0" C-C Row Spacing

24 Chambers/Row x 4.02' Long +2.56' Cap Length x 2 = 101.72' Row Length +12.0" End Stone x 2 = 103.72' Base Length

9 Rows x 100.0" Wide + 9.0" Spacing x 8 + 12.0" Side Stone x 2 = 83.00' Base Width

9.0" Stone Base + 60.0" Chamber Height + 12.0" Stone Cover = 6.75' Field Height

216 Chambers x 106.5 cf + 35.7 cf Cap Volume x 2 x 9 Rows = 23,644.5 cf Chamber Storage

58,107.3 cf Field - 23,644.5 cf Chambers = 34,462.7 cf Stone x 40.0% Voids = 13,785.1 cf Stone Storage

Chamber Storage + Stone Storage = 37,429.6 cf = 0.859 af

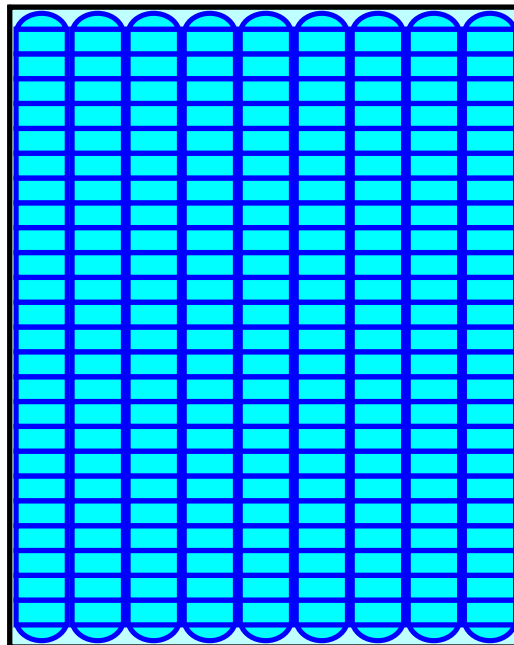
Overall Storage Efficiency = 64.4%

Overall System Size = 103.72' x 83.00' x 6.75'

216 Chambers

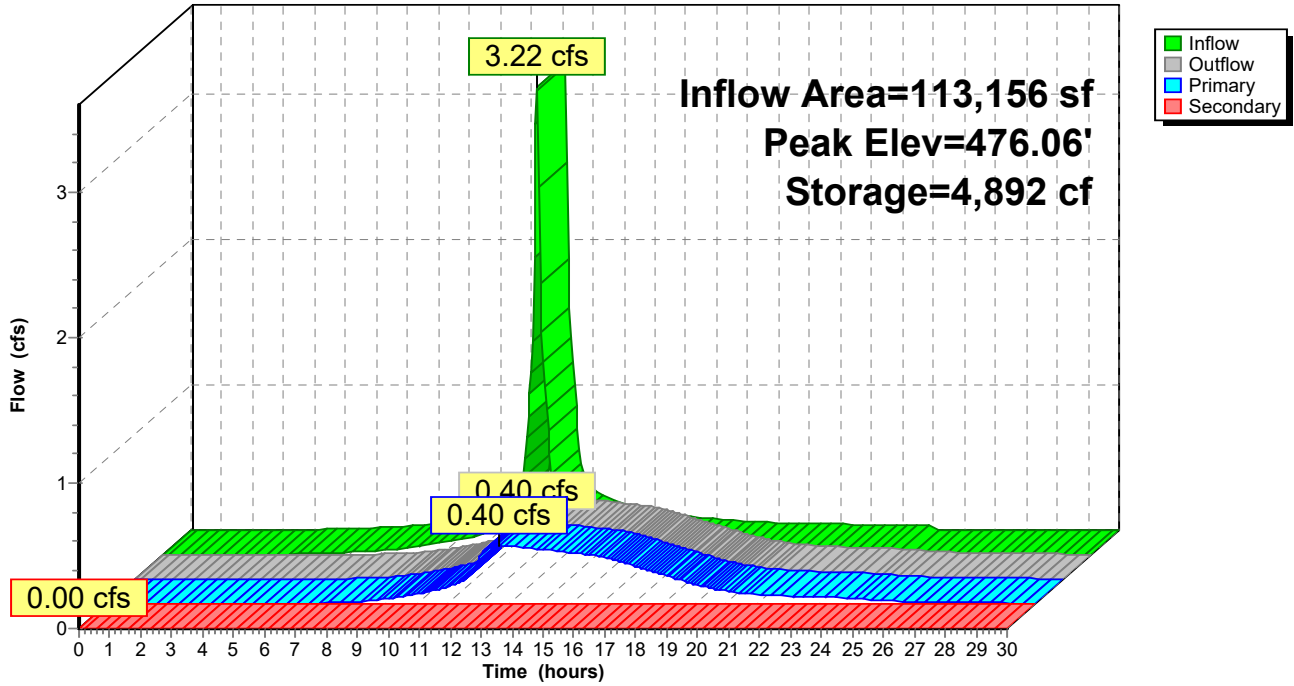
2,152.1 cy Field

1,276.4 cy Stone



### Pond SUBS: SUBS

Hydrograph



**230119 - R1 - Dewpoint South**

Prepared by Maser Consulting

HydroCAD® 10.10-6a s/n 08816 © 2020 HydroCAD Software Solutions LLC

Type III 24-hr WQv Rainfall=1.40"

Printed 2/2/2023

Page 150

**Stage-Area-Storage for Pond SUBS: SUBS**

Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
475.00	0	477.65	16,390	480.30	32,305
475.05	172	477.70	16,738	480.35	32,508
475.10	344	477.75	17,084	480.40	32,704
475.15	517	477.80	17,429	480.45	32,895
475.20	689	477.85	17,773	480.50	33,084
475.25	861	477.90	18,115	480.55	33,270
475.30	1,033	477.95	18,457	480.60	33,453
475.35	1,205	478.00	18,797	480.65	33,634
475.40	1,377	478.05	19,136	480.70	33,812
475.45	1,550	478.10	19,474	480.75	33,986
475.50	1,722	478.15	19,810	480.80	34,158
475.55	1,894	478.20	20,145	480.85	34,331
475.60	2,066	478.25	20,478	480.90	34,503
475.65	2,238	478.30	20,811	480.95	34,675
475.70	2,410	478.35	21,141	481.00	34,847
475.75	2,583	478.40	21,470	481.05	35,019
475.80	2,957	478.45	21,798	481.10	35,191
475.85	3,330	478.50	22,124	481.15	35,364
475.90	3,704	478.55	22,449	481.20	35,536
475.95	4,077	478.60	22,771	481.25	35,708
476.00	4,449	478.65	23,093	481.30	35,880
476.05	4,821	478.70	23,412	481.35	36,052
476.10	5,193	478.75	23,730	481.40	36,224
476.15	5,564	478.80	24,045	481.45	36,397
476.20	5,934	478.85	24,360	481.50	36,569
476.25	6,304	478.90	24,672	481.55	36,741
476.30	6,674	478.95	24,982	481.60	36,913
476.35	7,043	479.00	25,290	481.65	37,085
476.40	7,411	479.05	25,596	481.70	37,257
476.45	7,779	479.10	25,900	481.75	<b>37,430</b>
476.50	8,147	479.15	26,202		
476.55	8,513	479.20	26,501		
476.60	8,879	479.25	26,798		
476.65	9,245	479.30	27,093		
476.70	9,610	479.35	27,386		
476.75	9,974	479.40	27,675		
476.80	10,338	479.45	27,963		
476.85	10,700	479.50	28,247		
476.90	11,062	479.55	28,529		
476.95	11,424	479.60	28,808		
477.00	11,784	479.65	29,084		
477.05	12,144	479.70	29,357		
477.10	12,503	479.75	29,627		
477.15	12,861	479.80	29,893		
477.20	13,218	479.85	30,156		
477.25	13,574	479.90	30,414		
477.30	13,930	479.95	30,669		
477.35	14,284	480.00	30,920		
477.40	14,638	480.05	31,166		
477.45	14,990	480.10	31,407		
477.50	15,342	480.15	31,643		
477.55	15,692	480.20	31,872		
477.60	16,042	480.25	32,093		

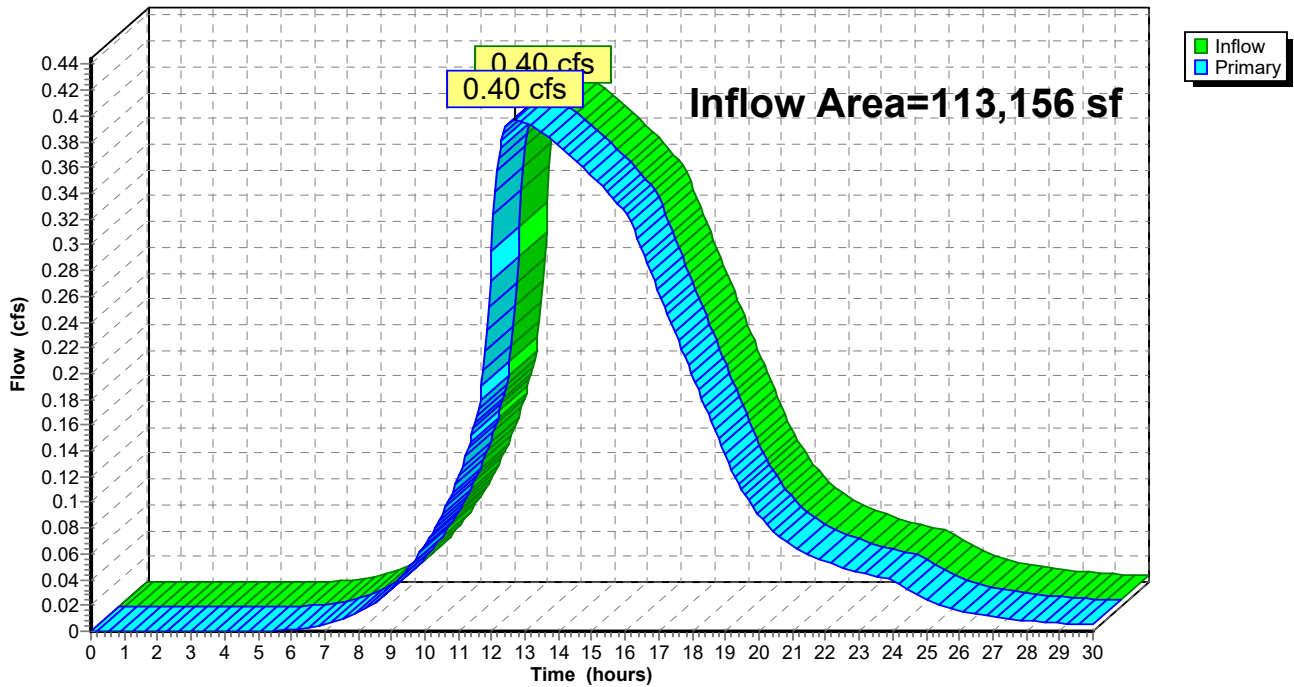
### Summary for Link JF: JELLY FISH

Inflow Area = 113,156 sf, 96.63% Impervious, Inflow Depth > 1.12" for WQv event  
Inflow = 0.40 cfs @ 12.68 hrs, Volume= 10,592 cf  
Primary = 0.40 cfs @ 12.68 hrs, Volume= 10,592 cf, Atten= 0%, Lag= 0.0 min  
Routed to Link PROP : PROPOSED

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link JF: JELLY FISH

Hydrograph

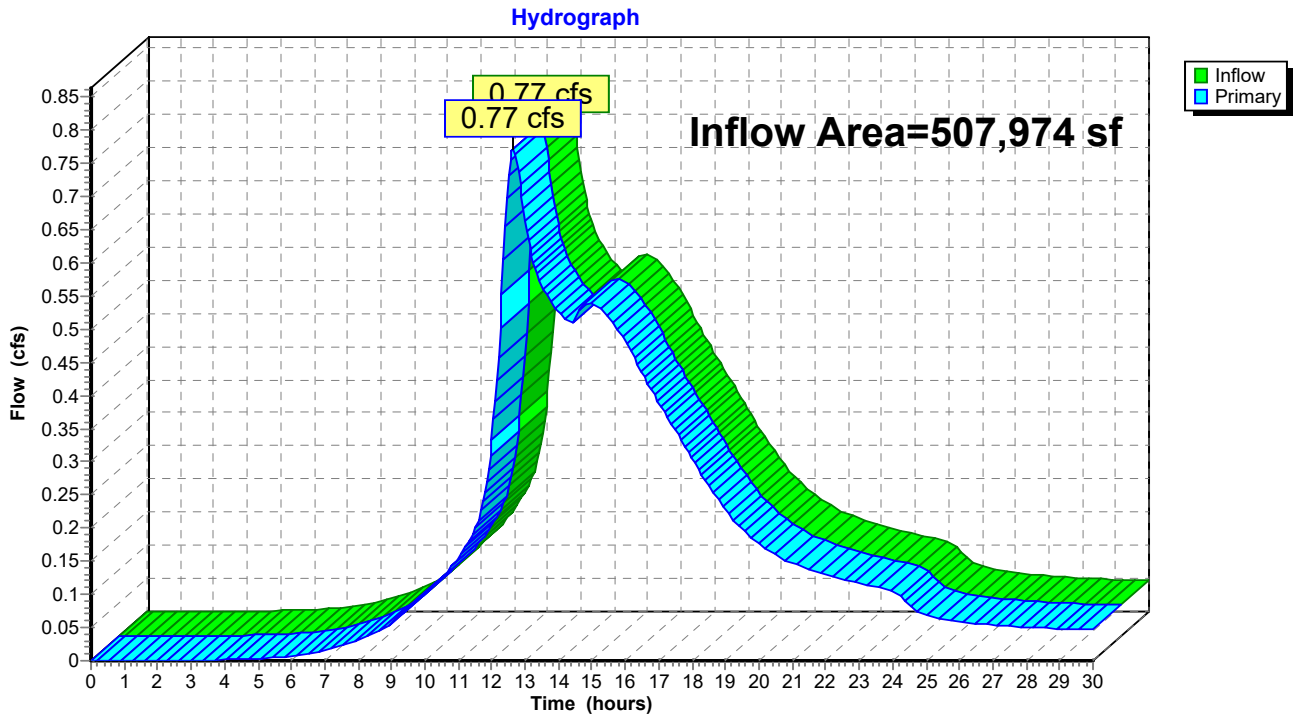


### Summary for Link PROP: PROPOSED

Inflow Area = 507,974 sf, 50.18% Impervious, Inflow Depth > 0.41" for WQv event  
Inflow = 0.77 cfs @ 12.64 hrs, Volume= 17,550 cf  
Primary = 0.77 cfs @ 12.64 hrs, Volume= 17,550 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

### Link PROP: PROPOSED



# Appendix 3 | NYSDEC Green Infrastructure Worksheets

Is this project subject to Chapter 10 of the NYS Design Manual (i.e. WQv is equal to post-development 1 year runoff volume)?..... **No**

Design Point: **1**  
 P= **1.40** *inch* *Manually enter P, Total Area and Impervious Cover.*

**Breakdown of Subcatchments**

Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft <sup>3</sup> )	Description
1	1.57	0.93	59%	0.58	4,649	BIO-1BN & BIO-2BN
2	2.06	1.48	72%	0.70	7,293	BIO-1D
3	0.85	0.58	68%	0.66	2,849	BIO-1E
4	0.42	0.29	70%	0.68	1,432	BIO-1F
5	2.60	2.51	97%	0.92	12,140	SUBS
6						
7						
8						
9						
10						
Subtotal (1-30)	7.49	5.79	77%	0.75	<b>28,362</b>	<b>Subtotal 1</b>
<b>Total</b>	7.49	5.79	77%	0.75	<b>28,362</b>	<b>Initial WQv</b>

**0.65 af**

**Identify Runoff Reduction Techniques By Area**

Technique	Total Contributing Area	Contributing Impervious Area	Notes
	(Acre)	(Acre)	
Conservation of Natural Areas	0.00	0.00	<i>minimum 10,000 sf</i>
Riparian Buffers	0.00	0.00	<i>maximum contributing length 75 feet to 150 feet</i>
Filter Strips	0.00	0.00	
Tree Planting	0.00	0.00	<i>Up to 100 sf directly connected impervious area may be subtracted per tree</i>
<b>Total</b>	<b>0.00</b>	<b>0.00</b>	

**Recalculate WQv after application of Area Reduction Techniques**

	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Runoff Coefficient Rv	WQv (ft <sup>3</sup> )
"<<Initial WQv"	7.49	5.79	77%	0.75	28,362
Subtract Area	0.00	0.00			
WQv adjusted after Area Reductions	<b>7.49</b>	<b>5.79</b>	77%	0.75	28,362
Disconnection of Rooftops		0.00			
Adjusted WQv after Area Reduction and Rooftop Disconnect	7.49	5.79	77%	0.75	<b>28,362</b>
WQv reduced by Area Reduction techniques					0

**0.65 af**  
**0.00 af**

**(For use on HSG C or D Soils with underdrains)**

**$Af = WQv * (df) / [k * (hf + df)(tf)]$**

- Af* Required Surface Area (ft<sup>2</sup>)
  - WQv* Water Quality Volume (ft<sup>3</sup>)
  - df* Depth of the Soil Medium (feet)
  - hf* Average height of water above the planter bed
  - tf* Volume Through the Filter Media (days)
- k* The hydraulic conductivity [ft/day], can be varied depending on the properties of the soil media. Some reported conductivity values are: **Sand** - 3.5 ft/day (City of Austin 1988); **Peat** - 2.0 ft/day (Galli 1990); **Leaf Compost** - 8.7 ft/day (Claytor and Schueler, 1996); **Bioretention Soil** (0.5 ft/day (Claytor & Schueler, 1996))

<b>Design Point:</b>	<b>1</b>						
<b>Enter Site Data For Drainage Area to be Treated by Practice</b>							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft <sup>3</sup> )	Precipitation (in)	Description
1	1.57	0.93	0.59	0.58	4648.51	1.40	BIO-1BN & BIO-2BN
Enter Impervious Area Reduced by Disconnection of Rooftops		0.00	59%	0.58	4,649	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.					0	ft <sup>3</sup>	
<b>Soil Information</b>							
Soil Group		D					
Soil Infiltration Rate		0.00	<i>in/hour</i>	<i>Okay</i>			
Using Underdrains?		Yes	<i>Okay</i>				
<b>Calculate the Minimum Filter Area</b>							
				Value	Units	Notes	
WQv				4,649	ft <sup>3</sup>		
Enter Depth of Soil Media			<i>df</i>	2.5	ft	2.5-4 ft	
Enter Hydraulic Conductivity			<i>k</i>	0.5	ft/day		
Enter Average Height of Ponding			<i>hf</i>	0.25	ft	6 inches max.	
Enter Filter Time			<i>tf</i>	2	days		
<b>Required Filter Area</b>			<b><i>Af</i></b>	<b>4226</b>	<b>ft<sup>2</sup></b>		
<b>Determine Actual Bio-Retention Area</b>							
Filter Width		1	ft				
Filter Length		4297	ft				
Filter Area		4297	ft <sup>2</sup>				
Actual Volume Provided		4727	ft <sup>3</sup>				
<b>Determine Runoff Reduction</b>							
Is the Bioretention contributing flow to another practice?			No	Select Practice			
RRv		1,891					
<b>RRv applied</b>		<b>1,891</b>	<b>ft<sup>3</sup></b>	<b><i>This is 40% of the storage provided or WQv whichever is less.</i></b>			
Volume Treated		2,758	ft <sup>3</sup>	<i>This is the portion of the WQv that is not reduced in the practice.</i>			
Volume Directed		0	ft <sup>3</sup>	<i>This volume is directed another practice</i>			



Sizing v	OK	Check to be sure Area provided $\geq Af$
----------	----	--

**(For use on HSG C or D Soils with underdrains)**

$$Af = WQv * (df) / [k * (hf + df)(tf)]$$

- Af* Required Surface Area (ft<sup>2</sup>)
  - WQv* Water Quality Volume (ft<sup>3</sup>)
  - df* Depth of the Soil Medium (feet)
  - hf* Average height of water above the planter bed
  - tf* Volume Through the Filter Media (days)
- k* The hydraulic conductivity [ft/day], can be varied depending on the properties of the soil media. Some reported conductivity values are: **Sand** - 3.5 ft/day (City of Austin 1988); **Peat** - 2.0 ft/day (Galli 1990); **Leaf Compost** - 8.7 ft/day (Claytor and Schueler, 1996); **Bioretention Soil** (0.5 ft/day (Claytor & Schueler, 1996)

<b>Design Point:</b>	1						
<b>Enter Site Data For Drainage Area to be Treated by Practice</b>							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft <sup>3</sup> )	Precipitation (in)	Description
2	2.06	1.48	0.72	0.70	7292.67	1.40	BIO-1D
Enter Impervious Area Reduced by Disconnection of Rooftops		0.00	72%	0.70	7,293	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.					0	ft <sup>3</sup>	
<b>Soil Information</b>							
Soil Group	A						
Soil Infiltration Rate	0.00	in/hour	Okay				
Using Underdrains?	Yes		Okay				
<b>Calculate the Minimum Filter Area</b>							
				Value	Units	Notes	
WQv				7,293	ft <sup>3</sup>		
Enter Depth of Soil Media			<i>df</i>	2.5	ft	2.5-4 ft	
Enter Hydraulic Conductivity			<i>k</i>	0.5	ft/day		
Enter Average Height of Ponding			<i>hf</i>	0.3	ft	6 inches max.	
Enter Filter Time			<i>tf</i>	2	days		
<b>Required Filter Area</b>				<b>Af</b>	<b>6511</b>	ft <sup>2</sup>	
<b>Determine Actual Bio-Retention Area</b>							
Filter Width	1	ft					
Filter Length	6529	ft					
Filter Area	6529	ft <sup>2</sup>					
Actual Volume Provided	7312	ft <sup>3</sup>					
<b>Determine Runoff Reduction</b>							
Is the Bioretention contributing flow to another practice?			No	Select Practice			
RRv	2,925						
<b>RRv applied</b>	<b>2,925</b>	ft <sup>3</sup>	<b>This is 40% of the storage provided or WQv whichever is less.</b>				
Volume Treated	4,368	ft <sup>3</sup>	This is the portion of the WQv that is not reduced in the practice.				

Volume Directed	0	ft <sup>3</sup>	This volume is directed another practice
Sizing v	OK		Check to be sure Area provided ≥ Af

**(For use on HSG C or D Soils with underdrains)**

$$Af = WQv * (df) / [k * (hf + df)(tf)]$$

- Af* Required Surface Area (ft<sup>2</sup>)
  - WQv* Water Quality Volume (ft<sup>3</sup>)
  - df* Depth of the Soil Medium (feet)
  - hf* Average height of water above the planter bed
  - tf* Volume Through the Filter Media (days)
- k* The hydraulic conductivity [ft/day], can be varied depending on the properties of the soil media. Some reported conductivity values are: **Sand** - 3.5 ft/day (City of Austin 1988); **Peat** - 2.0 ft/day (Galli 1990); **Leaf Compost** - 8.7 ft/day (Claytor and Schueler, 1996); **Bioretention Soil** (0.5 ft/day (Claytor & Schueler, 1999))

<b>Design Point:</b>	<b>1</b>						
<b>Enter Site Data For Drainage Area to be Treated by Practice</b>							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft <sup>3</sup> )	Precipitation (in)	Description
3	0.85	0.58	0.68	0.66	2849.22	1.40	BIO-1E
Enter Impervious Area Reduced by Disconnection of Rooftops		0.00	68%	0.66	2,849	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.					0	ft <sup>3</sup>	
<b>Soil Information</b>							
Soil Group	D						
Soil Infiltration Rate	0.00	in/hour	Okay				
Using Underdrains?	Yes		Okay				
<b>Calculate the Minimum Filter Area</b>							
				Value	Units	Notes	
WQv				2,849	ft <sup>3</sup>		
Enter Depth of Soil Media				<i>df</i>	2.5	ft	2.5-4 ft
Enter Hydraulic Conductivity				<i>k</i>	0.5	ft/day	
Enter Average Height of Ponding				<i>hf</i>	0.25	ft	6 inches max.
Enter Filter Time				<i>tf</i>	2	days	
<b>Required Filter Area</b>				<b>Af</b>	<b>2590</b>	ft <sup>2</sup>	
<b>Determine Actual Bio-Retention Area</b>							
Filter Width	1	ft					
Filter Length	2940	ft					
Filter Area	2940	ft <sup>2</sup>					
Actual Volume Provided	3234	ft <sup>3</sup>					
<b>Determine Runoff Reduction</b>							
Is the Bioretention contributing flow to another practice?			No	Select Practice			
RRv	1,294						
<b>RRv applied</b>	<b>1,294</b>	<b>ft<sup>3</sup></b>	<b>This is 40% of the storage provided or WQv whichever is less.</b>				

Volume Treated	1,556	ft <sup>3</sup>	This is the portion of the WQv that is not reduced in the practice.
Volume Directed	0	ft <sup>3</sup>	This volume is directed another practice
Sizing v	OK		Check to be sure Area provided ≥ Af

**(For use on HSG C or D Soils with underdrains)**

$$Af = WQv * (df) / [k * (hf + df)(tf)]$$

- Af Required Surface Area (ft<sup>2</sup>)
  - WQv Water Quality Volume (ft<sup>3</sup>)
  - df Depth of the Soil Medium (feet)
  - hf Average height of water above the planter bed
  - tf Volume Through the Filter Media (days)
- k The hydraulic conductivity [ft/day], can be varied depending on the properties of the soil media. Some reported conductivity values are: **Sand** - 3.5 ft/day (City of Austin 1988); **Peat** - 2.0 ft/day (Galli 1990); **Leaf Compost** - 8.7 ft/day (Claytor and Schueler, 1996); **Bioretention Soil** (0.5 ft/day (Claytor & Schueler, 1996))

<b>Design Point:</b>	1						
<b>Enter Site Data For Drainage Area to be Treated by Practice</b>							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft <sup>3</sup> )	Precipitation (in)	Description
4	0.42	0.29	0.70	0.68	1431.85	1.40	BIO-1F
Enter Impervious Area Reduced by Disconnection of Rooftops		0.00	70%	0.68	1,432	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.					0	ft <sup>3</sup>	
<b>Soil Information</b>							
Soil Group		D					
Soil Infiltration Rate		0.00	in/hour	Okay			
Using Underdrains?		Yes Okay					
<b>Calculate the Minimum Filter Area</b>							
				Value	Units	Notes	
WQv				1,432	ft <sup>3</sup>		
Enter Depth of Soil Media			df	2.5	ft	2.5-4 ft	
Enter Hydraulic Conductivity			k	0.5	ft/day		
Enter Average Height of Ponding			hf	0.25	ft	6 inches max.	
Enter Filter Time			tf	2	days		
<b>Required Filter Area</b>			<b>Af</b>	<b>1302</b>	<b>ft<sup>2</sup></b>		
<b>Determine Actual Bio-Retention Area</b>							
Filter Width		1	ft				
Filter Length		1347	ft				
Filter Area		1347	ft <sup>2</sup>				
Actual Volume Provided		1482	ft <sup>3</sup>				
<b>Determine Runoff Reduction</b>							
Is the Bioretention contributing flow to another practice?				Select Practice			
RRv		593					

<b>RRv applied</b>	<b>593</b>	<b>ft<sup>3</sup></b>	<b><i>This is 40% of the storage provided or WQv whichever is less.</i></b>
Volume Treated	839	ft <sup>3</sup>	<i>This is the portion of the WQv that is not reduced in the practice.</i>
Volume Directed	0	ft <sup>3</sup>	This volume is directed another practice
Sizing v	OK		<i>Check to be sure Area provided ≥ Af</i>

Total RRv Applied 6,701.95  
 Total Area 4.89  
 Total Impervious Area 3.28  
 Total Volume Treated 9,520.30

Rooftop Disconnect Impervious Area Total 0.00

## Appendix 4 | SPDES GP-0-20-001



Department of  
Environmental  
Conservation

NEW YORK STATE  
DEPARTMENT OF ENVIRONMENTAL CONSERVATION

SPDES GENERAL PERMIT  
FOR STORMWATER DISCHARGES

From

**CONSTRUCTION ACTIVITY**

Permit No. GP- 0-20-001

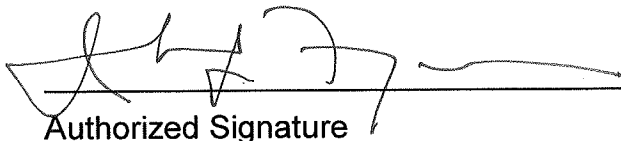
Issued Pursuant to Article 17, Titles 7, 8 and Article 70  
of the Environmental Conservation Law

Effective Date: January 29, 2020

Expiration Date: January 28, 2025

John J. Ferguson

Chief Permit Administrator



Authorized Signature

1-23-20

Date

Address: NYS DEC  
Division of Environmental Permits  
625 Broadway, 4th Floor  
Albany, N.Y. 12233-1750

## PREFACE

Pursuant to Section 402 of the Clean Water Act (“CWA”), stormwater *discharges* from certain *construction activities* are unlawful unless they are authorized by a *National Pollutant Discharge Elimination System (“NPDES”)* permit or by a state permit program. New York administers the approved State Pollutant Discharge Elimination System (SPDES) program with permits issued in accordance with the New York State Environmental Conservation Law (ECL) Article 17, Titles 7, 8 and Article 70.

An *owner or operator* of a *construction activity* that is eligible for coverage under this permit must obtain coverage prior to the *commencement of construction activity*. Activities that fit the definition of “*construction activity*”, as defined under 40 CFR 122.26(b)(14)(x), (15)(i), and (15)(ii), constitute construction of a *point source* and therefore, pursuant to ECL section 17-0505 and 17-0701, the *owner or operator* must have coverage under a SPDES permit prior to *commencing construction activity*. The *owner or operator* cannot wait until there is an actual *discharge* from the *construction site* to obtain permit coverage.

**\*Note: The italicized words/phrases within this permit are defined in Appendix A.**

**NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION  
SPDES GENERAL PERMIT FOR STORMWATER DISCHARGES FROM  
CONSTRUCTION ACTIVITIES**

**Table of Contents**

Part 1. PERMIT COVERAGE AND LIMITATIONS .....	1
A. Permit Application .....	1
B. Effluent Limitations Applicable to Discharges from Construction Activities .....	1
C. Post-construction Stormwater Management Practice Requirements .....	4
D. Maintaining Water Quality .....	8
E. Eligibility Under This General Permit.....	9
F. Activities Which Are Ineligible for Coverage Under This General Permit .....	9
Part II. PERMIT COVERAGE .....	12
A. How to Obtain Coverage .....	12
B. Notice of Intent (NOI) Submittal .....	13
C. Permit Authorization .....	13
D. General Requirements For Owners or Operators With Permit Coverage .....	15
E. Permit Coverage for Discharges Authorized Under GP-0-15-002.....	17
F. Change of Owner or Operator .....	17
Part III. STORMWATER POLLUTION PREVENTION PLAN (SWPPP).....	18
A. General SWPPP Requirements .....	18
B. Required SWPPP Contents .....	20
C. Required SWPPP Components by Project Type.....	24
Part IV. INSPECTION AND MAINTENANCE REQUIREMENTS .....	24
A. General Construction Site Inspection and Maintenance Requirements .....	24
B. Contractor Maintenance Inspection Requirements .....	24
C. Qualified Inspector Inspection Requirements .....	25
Part V. TERMINATION OF PERMIT COVERAGE .....	29
A. Termination of Permit Coverage .....	29
Part VI. REPORTING AND RETENTION RECORDS .....	31
A. Record Retention .....	31
B. Addresses .....	31
Part VII. STANDARD PERMIT CONDITIONS.....	31
A. Duty to Comply.....	31
B. Continuation of the Expired General Permit.....	32
C. Enforcement.....	32
D. Need to Halt or Reduce Activity Not a Defense.....	32
E. Duty to Mitigate .....	33
F. Duty to Provide Information.....	33
G. Other Information .....	33
H. Signatory Requirements.....	33
I. Property Rights .....	35
J. Severability.....	35



K.	Requirement to Obtain Coverage Under an Alternative Permit.....	35
L.	Proper Operation and Maintenance .....	36
M.	Inspection and Entry .....	36
N.	Permit Actions .....	37
O.	Definitions .....	37
P.	Re-Opener Clause .....	37
Q.	Penalties for Falsification of Forms and Reports .....	37
R.	Other Permits .....	38
APPENDIX A – Acronyms and Definitions .....		39
Acronyms.....		39
Definitions.....		40
APPENDIX B – Required SWPPP Components by Project Type .....		48
Table 1.....		48
Table 2.....		50
APPENDIX C – Watersheds Requiring Enhanced Phosphorus Removal.....		52
APPENDIX D – Watersheds with Lower Disturbance Threshold .....		58
APPENDIX E – 303(d) Segments Impaired by Construction Related Pollutant(s) .....		59
APPENDIX F – List of NYS DEC Regional Offices .....		65

## Part 1. PERMIT COVERAGE AND LIMITATIONS

### A. Permit Application

This permit authorizes stormwater *discharges to surface waters of the State* from the following *construction activities* identified within 40 CFR Parts 122.26(b)(14)(x), 122.26(b)(15)(i) and 122.26(b)(15)(ii), provided all of the eligibility provisions of this permit are met:

1. *Construction activities* involving soil disturbances of one (1) or more acres; including disturbances of less than one acre that are part of a *larger common plan of development or sale* that will ultimately disturb one or more acres of land; excluding *routine maintenance activity* that is performed to maintain the original line and grade, hydraulic capacity or original purpose of a facility;
2. *Construction activities* involving soil disturbances of less than one (1) acre where the Department has determined that a *SPDES* permit is required for stormwater *discharges* based on the potential for contribution to a violation of a *water quality standard* or for significant contribution of *pollutants to surface waters of the State*.
3. *Construction activities* located in the watershed(s) identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.

### B. Effluent Limitations Applicable to Discharges from Construction Activities

*Discharges* authorized by this permit must achieve, at a minimum, the effluent limitations in Part I.B.1. (a) – (f) of this permit. These limitations represent the degree of effluent reduction attainable by the application of best practicable technology currently available.

1. Erosion and Sediment Control Requirements - The *owner or operator* must select, design, install, implement and maintain control measures to *minimize the discharge of pollutants* and prevent a violation of the *water quality standards*. The selection, design, installation, implementation, and maintenance of these control measures must meet the non-numeric effluent limitations in Part I.B.1.(a) – (f) of this permit and be in accordance with the New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016, using sound engineering judgment. Where control measures are not designed in conformance with the design criteria included in the technical standard, the *owner or operator* must include in the *Stormwater Pollution Prevention Plan* (“SWPPP”) the reason(s) for the

deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.

- a. **Erosion and Sediment Controls.** Design, install and maintain effective erosion and sediment controls to *minimize* the *discharge of pollutants* and prevent a violation of the *water quality standards*. At a minimum, such controls must be designed, installed and maintained to:
- (i) *Minimize* soil erosion through application of runoff control and soil stabilization control measure to *minimize pollutant discharges*;
  - (ii) Control stormwater *discharges*, including both peak flowrates and total stormwater volume, to *minimize* channel and *streambank* erosion and scour in the immediate vicinity of the *discharge* points;
  - (iii) *Minimize* the amount of soil exposed during *construction activity*;
  - (iv) *Minimize* the disturbance of *steep slopes*;
  - (v) *Minimize* sediment *discharges* from the site;
  - (vi) Provide and maintain *natural buffers* around surface waters, direct stormwater to vegetated areas and maximize stormwater infiltration to reduce *pollutant discharges*, unless *infeasible*;
  - (vii) *Minimize* soil compaction. Minimizing soil compaction is not required where the intended function of a specific area of the site dictates that it be compacted;
  - (viii) Unless *infeasible*, preserve a sufficient amount of topsoil to complete soil restoration and establish a uniform, dense vegetative cover; and
  - (ix) *Minimize* dust. On areas of exposed soil, *minimize* dust through the appropriate application of water or other dust suppression techniques to control the generation of pollutants that could be discharged from the site.
- b. **Soil Stabilization.** In areas where soil disturbance activity has temporarily or permanently ceased, the application of soil stabilization measures must be initiated by the end of the next business day and completed within fourteen (14) days from the date the current soil disturbance activity ceased. For construction sites that *directly discharge* to one of the 303(d) segments

listed in Appendix E or is located in one of the watersheds listed in Appendix C, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days from the date the current soil disturbance activity ceased. See Appendix A for definition of *Temporarily Ceased*.

- c. **Dewatering.** *Discharges* from *dewatering* activities, including *discharges* from *dewatering* of trenches and excavations, must be managed by appropriate control measures.
  
- d. **Pollution Prevention Measures.** Design, install, implement, and maintain effective pollution prevention measures to *minimize* the *discharge* of *pollutants* and prevent a violation of the *water quality standards*. At a minimum, such measures must be designed, installed, implemented and maintained to:
  - (i) *Minimize* the *discharge* of *pollutants* from equipment and vehicle washing, wheel wash water, and other wash waters. This applies to washing operations that use clean water only. Soaps, detergents and solvents cannot be used;
  
  - (ii) *Minimize* the exposure of building materials, building products, construction wastes, trash, landscape materials, fertilizers, pesticides, herbicides, detergents, sanitary waste, hazardous and toxic waste, and other materials present on the site to precipitation and to stormwater. Minimization of exposure is not required in cases where the exposure to precipitation and to stormwater will not result in a *discharge* of *pollutants*, or where exposure of a specific material or product poses little risk of stormwater contamination (such as final products and materials intended for outdoor use) ; and
  
  - (iii) Prevent the *discharge* of *pollutants* from spills and leaks and implement chemical spill and leak prevention and response procedures.
  
- e. **Prohibited Discharges.** The following *discharges* are prohibited:
  - (i) Wastewater from washout of concrete;
  
  - (ii) Wastewater from washout and cleanout of stucco, paint, form release oils, curing compounds and other construction materials;

- (iii) Fuels, oils, or other *pollutants* used in vehicle and equipment operation and maintenance;
  - (iv) Soaps or solvents used in vehicle and equipment washing; and
  - (v) Toxic or hazardous substances from a spill or other release.
- f. Surface Outlets. When discharging from basins and impoundments, the outlets shall be designed, constructed and maintained in such a manner that sediment does not leave the basin or impoundment and that erosion at or below the outlet does not occur.

### **C. Post-construction Stormwater Management Practice Requirements**

1. The *owner or operator of a construction activity* that requires post-construction stormwater management practices pursuant to Part III.C. of this permit must select, design, install, and maintain the practices to meet the *performance criteria* in the New York State Stormwater Management Design Manual (“Design Manual”), dated January 2015, using sound engineering judgment. Where post-construction stormwater management practices (“SMPs”) are not designed in conformance with the *performance criteria* in the Design Manual, the *owner or operator* must include in the SWPPP the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.
2. The *owner or operator of a construction activity* that requires post-construction stormwater management practices pursuant to Part III.C. of this permit must design the practices to meet the applicable *sizing criteria* in Part I.C.2.a., b., c. or d. of this permit.

#### **a. Sizing Criteria for New Development**

- (i) Runoff Reduction Volume (“RRv”): Reduce the total Water Quality Volume (“WQv”) by application of RR techniques and standard SMPs with RRv capacity. The total WQv shall be calculated in accordance with the criteria in Section 4.2 of the Design Manual.
- (ii) Minimum RRv and Treatment of Remaining Total WQv: Construction activities that cannot meet the criteria in Part I.C.2.a.(i) of this permit due to site limitations shall direct runoff from all newly constructed impervious areas to a RR technique or standard SMP with RRv capacity unless infeasible. The specific site limitations that prevent the reduction of 100% of the WQv shall be documented in the SWPPP.

For each impervious area that is not directed to a RR technique or standard SMP with RRv capacity, the SWPPP must include documentation which demonstrates that all options were considered and for each option explains why it is considered infeasible.

**In no case shall the runoff reduction achieved from the newly constructed impervious areas be less than the Minimum RRv as calculated using the criteria in Section 4.3 of the Design Manual.**

The remaining portion of the total WQv that cannot be reduced shall be treated by application of standard SMPs.

- (iii) Channel Protection Volume (“Cpv”): Provide 24 hour extended detention of the post-developed 1-year, 24-hour storm event; remaining after runoff reduction. The Cpv requirement does not apply when:
  - (1) Reduction of the entire Cpv is achieved by application of runoff reduction techniques or infiltration systems, or
  - (2) The site discharges directly to tidal waters, or fifth order or larger streams.
  
- (iv) *Overbank* Flood Control Criteria (“Qp”): Requires storage to attenuate the post-development 10-year, 24-hour peak discharge rate (Qp) to predevelopment rates. The Qp requirement does not apply when:
  - (1) the site discharges directly to tidal waters or fifth order or larger streams, or
  - (2) A downstream analysis reveals that *overbank* control is not required.
  
- (v) Extreme Flood Control Criteria (“Qf”): Requires storage to attenuate the post-development 100-year, 24-hour peak discharge rate (Qf) to predevelopment rates. The Qf requirement does not apply when:
  - (1) the site discharges directly to tidal waters or fifth order or larger streams, or
  - (2) A downstream analysis reveals that *overbank* control is not required.

**b. Sizing Criteria for New Development in Enhanced Phosphorus Removal Watershed**

- (i) Runoff Reduction Volume (RRv): Reduce the total Water Quality Volume (WQv) by application of RR techniques and standard SMPs with RRv capacity. The total WQv is the runoff volume from the 1-year, 24 hour design storm over the post-developed watershed and shall be

calculated in accordance with the criteria in Section 10.3 of the Design Manual.

- (ii) Minimum RRv and Treatment of Remaining Total WQv: *Construction activities* that cannot meet the criteria in Part I.C.2.b.(i) of this permit due to *site limitations* shall direct runoff from all newly constructed *impervious areas* to a RR technique or standard SMP with RRv capacity unless *infeasible*. The specific *site limitations* that prevent the reduction of 100% of the WQv shall be documented in the SWPPP. For each *impervious area* that is not directed to a RR technique or standard SMP with RRv capacity, the SWPPP must include documentation which demonstrates that all options were considered and for each option explains why it is considered *infeasible*.

**In no case shall the runoff reduction achieved from the newly constructed *impervious areas* be less than the Minimum RRv as calculated using the criteria in Section 10.3 of the Design Manual.** The remaining portion of the total WQv that cannot be reduced shall be treated by application of standard SMPs.

- (iii) Channel Protection Volume (Cpv): Provide 24 hour extended detention of the post-developed 1-year, 24-hour storm event; remaining after runoff reduction. The Cpv requirement does not apply when:
  - (1) Reduction of the entire Cpv is achieved by application of runoff reduction techniques or infiltration systems, or
  - (2) The site *discharges* directly to tidal waters, or fifth order or larger streams.
- (iv) *Overbank* Flood Control Criteria (Qp): Requires storage to attenuate the post-development 10-year, 24-hour peak *discharge* rate (Qp) to predevelopment rates. The Qp requirement does not apply when:
  - (1) the site *discharges* directly to tidal waters or fifth order or larger streams, or
  - (2) A downstream analysis reveals that *overbank* control is not required.
- (v) Extreme Flood Control Criteria (Qf): Requires storage to attenuate the post-development 100-year, 24-hour peak *discharge* rate (Qf) to predevelopment rates. The Qf requirement does not apply when:
  - (1) the site *discharges* directly to tidal waters or fifth order or larger streams, or
  - (2) A downstream analysis reveals that *overbank* control is not required.

### c. Sizing Criteria for Redevelopment Activity

- (i) Water Quality Volume (WQv): The WQv treatment objective for *redevelopment activity* shall be addressed by one of the following options. *Redevelopment activities* located in an Enhanced Phosphorus Removal Watershed (see Part III.B.3. and Appendix C of this permit) shall calculate the WQv in accordance with Section 10.3 of the Design Manual. All other *redevelopment activities* shall calculate the WQv in accordance with Section 4.2 of the Design Manual.
- (1) Reduce the existing *impervious cover* by a minimum of 25% of the total disturbed, *impervious area*. The Soil Restoration criteria in Section 5.1.6 of the Design Manual must be applied to all newly created pervious areas, or
  - (2) Capture and treat a minimum of 25% of the WQv from the disturbed, *impervious area* by the application of standard SMPs; or reduce 25% of the WQv from the disturbed, *impervious area* by the application of RR techniques or standard SMPs with RRv capacity., or
  - (3) Capture and treat a minimum of 75% of the WQv from the disturbed, *impervious area* as well as any additional runoff from tributary areas by application of the alternative practices discussed in Sections 9.3 and 9.4 of the Design Manual., or
  - (4) Application of a combination of 1, 2 and 3 above that provide a weighted average of at least two of the above methods. Application of this method shall be in accordance with the criteria in Section 9.2.1(B) (IV) of the Design Manual.

If there is an existing post-construction stormwater management practice located on the site that captures and treats runoff from the *impervious area* that is being disturbed, the WQv treatment option selected must, at a minimum, provide treatment equal to the treatment that was being provided by the existing practice(s) if that treatment is greater than the treatment required by options 1 – 4 above.

- (ii) Channel Protection Volume (Cpv): Not required if there are no changes to hydrology that increase the *discharge* rate from the project site.
- (iii) *Overbank* Flood Control Criteria (Qp): Not required if there are no changes to hydrology that increase the *discharge* rate from the project site.
- (iv) Extreme Flood Control Criteria (Qf): Not required if there are no changes to hydrology that increase the *discharge* rate from the project site



#### **d. Sizing Criteria for Combination of Redevelopment Activity and New Development**

Construction projects that include both New Development and Redevelopment Activity shall provide post-construction stormwater management controls that meet the sizing criteria calculated as an aggregate of the Sizing Criteria in Part I.C.2.a. or b. of this permit for the New Development portion of the project and Part I.C.2.c of this permit for Redevelopment Activity portion of the project.

#### **D. Maintaining Water Quality**

The Department expects that compliance with the conditions of this permit will control *discharges* necessary to meet applicable *water quality standards*. It shall be a violation of the *ECL* for any discharge to either cause or contribute to a violation of *water quality standards* as contained in Parts 700 through 705 of Title 6 of the Official Compilation of Codes, Rules and Regulations of the State of New York, such as:

1. There shall be no increase in turbidity that will cause a substantial visible contrast to natural conditions;
2. There shall be no increase in suspended, colloidal or settleable solids that will cause deposition or impair the waters for their best usages; and
3. There shall be no residue from oil and floating substances, nor visible oil film, nor globules of grease.

If there is evidence indicating that the stormwater *discharges* authorized by this permit are causing, have the reasonable potential to cause, or are contributing to a violation of the *water quality standards*; the *owner or operator* must take appropriate corrective action in accordance with Part IV.C.5. of this general permit and document in accordance with Part IV.C.4. of this general permit. To address the *water quality standard* violation the *owner or operator* may need to provide additional information, include and implement appropriate controls in the SWPPP to correct the problem, or obtain an individual SPDES permit.

If there is evidence indicating that despite compliance with the terms and conditions of this general permit it is demonstrated that the stormwater *discharges* authorized by this permit are causing or contributing to a violation of *water quality standards*, or if the Department determines that a modification of the permit is necessary to prevent a violation of *water quality standards*, the authorized *discharges* will no longer be eligible for coverage under this permit. The Department may require the *owner or operator* to obtain an individual SPDES permit to continue discharging.

## **E. Eligibility Under This General Permit**

1. This permit may authorize all *discharges* of stormwater from *construction activity* to *surface waters of the State* and *groundwaters* except for ineligible *discharges* identified under subparagraph F. of this Part.
2. Except for non-stormwater *discharges* explicitly listed in the next paragraph, this permit only authorizes stormwater *discharges*; including stormwater runoff, snowmelt runoff, and surface runoff and drainage, from *construction activities*.
3. Notwithstanding paragraphs E.1 and E.2 above, the following non-stormwater discharges are authorized by this permit: those listed in 6 NYCRR 750-1.2(a)(29)(vi), with the following exception: “Discharges from firefighting activities are authorized only when the firefighting activities are emergencies/unplanned”; waters to which other components have not been added that are used to control dust in accordance with the SWPPP; and uncontaminated *discharges* from *construction site* de-watering operations. All non-stormwater discharges must be identified in the SWPPP. Under all circumstances, the *owner or operator* must still comply with *water quality standards* in Part I.D of this permit.
4. The *owner or operator* must maintain permit eligibility to *discharge* under this permit. Any *discharges* that are not compliant with the eligibility conditions of this permit are not authorized by the permit and the *owner or operator* must either apply for a separate permit to cover those ineligible *discharges* or take steps necessary to make the *discharge* eligible for coverage.

## **F. Activities Which Are Ineligible for Coverage Under This General Permit**

All of the following are **not** authorized by this permit:

1. *Discharges* after *construction activities* have been completed and the site has undergone *final stabilization*;
2. *Discharges* that are mixed with sources of non-stormwater other than those expressly authorized under subsection E.3. of this Part and identified in the SWPPP required by this permit;
3. *Discharges* that are required to obtain an individual SPDES permit or another SPDES general permit pursuant to Part VII.K. of this permit;
4. *Construction activities* or *discharges* from *construction activities* that may adversely affect an *endangered or threatened species* unless the *owner or*

*operator* has obtained a permit issued pursuant to 6 NYCRR Part 182 for the project or the Department has issued a letter of non-jurisdiction for the project. All documentation necessary to demonstrate eligibility shall be maintained on site in accordance with Part II.D.2 of this permit;

5. *Discharges* which either cause or contribute to a violation of *water quality standards* adopted pursuant to the *ECL* and its accompanying regulations;
6. *Construction activities* for residential, commercial and institutional projects:
  - a. Where the *discharges* from the *construction activities* are tributary to waters of the state classified as AA or AA-s; and
  - b. Which are undertaken on land with no existing *impervious cover*; and
  - c. Which disturb one (1) or more acres of land designated on the current United States Department of Agriculture (“USDA”) Soil Survey as Soil Slope Phase “D”, (provided the map unit name is inclusive of slopes greater than 25%), or Soil Slope Phase “E” or “F” (regardless of the map unit name), or a combination of the three designations.
7. *Construction activities* for linear transportation projects and linear utility projects:
  - a. Where the *discharges* from the *construction activities* are tributary to waters of the state classified as AA or AA-s; and
  - b. Which are undertaken on land with no existing *impervious cover*; and
  - c. Which disturb two (2) or more acres of land designated on the current USDA Soil Survey as Soil Slope Phase “D” (provided the map unit name is inclusive of slopes greater than 25%), or Soil Slope Phase “E” or “F” (regardless of the map unit name), or a combination of the three designations.

8. *Construction activities* that have the potential to affect an *historic property*, unless there is documentation that such impacts have been resolved. The following documentation necessary to demonstrate eligibility with this requirement shall be maintained on site in accordance with Part II.D.2 of this permit and made available to the Department in accordance with Part VII.F of this permit:
- a. Documentation that the *construction activity* is not within an archeologically sensitive area indicated on the sensitivity map, and that the *construction activity* is not located on or immediately adjacent to a property listed or determined to be eligible for listing on the National or State Registers of Historic Places, and that there is no new permanent building on the *construction site* within the following distances from a building, structure, or object that is more than 50 years old, or if there is such a new permanent building on the *construction site* within those parameters that NYS Office of Parks, Recreation and Historic Preservation (OPRHP), a Historic Preservation Commission of a Certified Local Government, or a qualified preservation professional has determined that the building, structure, or object more than 50 years old is not historically/archeologically significant.
    - 1-5 acres of disturbance - 20 feet
    - 5-20 acres of disturbance - 50 feet
    - 20+ acres of disturbance - 100 feet, or
  - b. DEC consultation form sent to OPRHP, and copied to the NYS DEC Agency Historic Preservation Officer (APO), and
    - (i) the State Environmental Quality Review (SEQR) Environmental Assessment Form (EAF) with a negative declaration or the Findings Statement, with documentation of OPRHP's agreement with the resolution; or
    - (ii) documentation from OPRHP that the *construction activity* will result in No Impact; or
    - (iii) documentation from OPRHP providing a determination of No Adverse Impact; or
    - (iv) a Letter of Resolution signed by the owner/operator, OPRHP and the DEC APO which allows for this *construction activity* to be eligible for coverage under the general permit in terms of the State Historic Preservation Act (SHPA); or
  - c. Documentation of satisfactory compliance with Section 106 of the National Historic Preservation Act for a coterminous project area:

- (i) No Affect
- (ii) No Adverse Affect
- (iii) Executed Memorandum of Agreement, or

d. Documentation that:

- (i) SHPA Section 14.09 has been completed by NYS DEC or another state agency.
9. *Discharges from construction activities* that are subject to an existing SPDES individual or general permit where a SPDES permit for *construction activity* has been terminated or denied; or where the *owner or operator* has failed to renew an expired individual permit.

## Part II. PERMIT COVERAGE

### A. How to Obtain Coverage

1. An *owner or operator* of a *construction activity* that is not subject to the requirements of a regulated, traditional land use control MS4 must first prepare a SWPPP in accordance with all applicable requirements of this permit and then submit a completed Notice of Intent (NOI) to the Department to be authorized to discharge under this permit.
2. An *owner or operator* of a *construction activity* that is subject to the requirements of a *regulated, traditional land use control MS4* must first prepare a SWPPP in accordance with all applicable requirements of this permit and then have the SWPPP reviewed and accepted by the *regulated, traditional land use control MS4* prior to submitting the NOI to the Department. The *owner or operator* shall have the “MS4 SWPPP Acceptance” form signed in accordance with Part VII.H., and then submit that form along with a completed NOI to the Department.
3. The requirement for an *owner or operator* to have its SWPPP reviewed and accepted by the *regulated, traditional land use control MS4* prior to submitting the NOI to the Department does not apply to an *owner or operator* that is obtaining permit coverage in accordance with the requirements in Part II.F. (Change of *Owner or Operator*) or where the *owner or operator* of the *construction activity* is the *regulated, traditional land use control MS4* . This exemption does not apply to *construction activities* subject to the New York City Administrative Code.

## B. Notice of Intent (NOI) Submittal

1. Prior to December 21, 2020, an owner or operator shall use either the electronic (eNOI) or paper version of the NOI that the Department prepared. Both versions of the NOI are located on the Department's website (<http://www.dec.ny.gov/>). The paper version of the NOI shall be signed in accordance with Part VII.H. of this permit and submitted to the following address:

**NOTICE OF INTENT  
NYS DEC, Bureau of Water Permits  
625 Broadway, 4<sup>th</sup> Floor  
Albany, New York 12233-3505**

2. Beginning December 21, 2020 and in accordance with EPA's 2015 NPDES Electronic Reporting Rule (40 CFR Part 127), the *owner or operator* must submit the NOI electronically using the *Department's* online NOI.
3. The *owner or operator* shall have the SWPPP preparer sign the "SWPPP Preparer Certification" statement on the NOI prior to submitting the form to the Department.
4. As of the date the NOI is submitted to the Department, the *owner or operator* shall make the NOI and SWPPP available for review and copying in accordance with the requirements in Part VII.F. of this permit.

## C. Permit Authorization

1. An *owner or operator* shall not *commence construction activity* until their authorization to *discharge* under this permit goes into effect.
2. Authorization to *discharge* under this permit will be effective when the *owner or operator* has satisfied all of the following criteria:
  - a. project review pursuant to the State Environmental Quality Review Act ("SEQRA") have been satisfied, when SEQRA is applicable. See the Department's website (<http://www.dec.ny.gov/>) for more information,
  - b. where required, all necessary Department permits subject to the *Uniform Procedures Act ("UPA")* (see 6 NYCRR Part 621), or the equivalent from another New York State agency, have been obtained, unless otherwise notified by the Department pursuant to 6 NYCRR 621.3(a)(4). *Owners or operators of construction activities* that are required to obtain *UPA* permits

must submit a preliminary SWPPP to the appropriate DEC Permit Administrator at the Regional Office listed in Appendix F at the time all other necessary *UPA* permit applications are submitted. The preliminary SWPPP must include sufficient information to demonstrate that the *construction activity* qualifies for authorization under this permit,

- c. the final SWPPP has been prepared, and
  - d. a complete NOI has been submitted to the Department in accordance with the requirements of this permit.
3. An *owner or operator* that has satisfied the requirements of Part II.C.2 above will be authorized to *discharge* stormwater from their *construction activity* in accordance with the following schedule:
- a. For *construction activities* that are not subject to the requirements of a *regulated, traditional land use control MS4*:
    - (i) Five (5) business days from the date the Department receives a complete electronic version of the NOI (eNOI) for *construction activities* with a SWPPP that has been prepared in conformance with the design criteria in the technical standard referenced in Part III.B.1 and the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C.; or
    - (ii) Sixty (60) business days from the date the Department receives a complete NOI (electronic or paper version) for *construction activities* with a SWPPP that has not been prepared in conformance with the design criteria in technical standard referenced in Part III.B.1. or, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C., the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, or;
    - (iii) Ten (10) business days from the date the Department receives a complete paper version of the NOI for *construction activities* with a SWPPP that has been prepared in conformance with the design criteria in the technical standard referenced in Part III.B.1 and the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C.

- b. For *construction activities* that are subject to the requirements of a *regulated, traditional land use control MS4*:
  - (i) Five (5) business days from the date the Department receives both a complete electronic version of the NOI (eNOI) and signed “MS4 SWPPP Acceptance” form, or
  - (ii) Ten (10) business days from the date the Department receives both a complete paper version of the NOI and signed “MS4 SWPPP Acceptance” form.
4. Coverage under this permit authorizes stormwater *discharges* from only those areas of disturbance that are identified in the NOI. If an *owner or operator* wishes to have stormwater *discharges* from future or additional areas of disturbance authorized, they must submit a new NOI that addresses that phase of the development, unless otherwise notified by the Department. The *owner or operator* shall not *commence construction activity* on the future or additional areas until their authorization to *discharge* under this permit goes into effect in accordance with Part II.C. of this permit.

#### **D. General Requirements For Owners or Operators With Permit Coverage**

1. The *owner or operator* shall ensure that the provisions of the SWPPP are implemented from the *commencement of construction activity* until all areas of disturbance have achieved *final stabilization* and the Notice of Termination (“NOT”) has been submitted to the Department in accordance with Part V. of this permit. This includes any changes made to the SWPPP pursuant to Part III.A.4. of this permit.
2. The *owner or operator* shall maintain a copy of the General Permit (GP-0-20-001), NOI, *NOI Acknowledgment Letter*, SWPPP, MS4 SWPPP Acceptance form, inspection reports, responsible contractor’s or subcontractor’s certification statement (see Part III.A.6.), and all documentation necessary to demonstrate eligibility with this permit at the *construction site* until all disturbed areas have achieved *final stabilization* and the NOT has been submitted to the Department. The documents must be maintained in a secure location, such as a job trailer, on-site construction office, or mailbox with lock. The secure location must be accessible during normal business hours to an individual performing a compliance inspection.
3. The *owner or operator of a construction activity* shall not disturb greater than five (5) acres of soil at any one time without prior written authorization from the Department or, in areas under the jurisdiction of a *regulated, traditional land*



- use control MS4, the regulated, traditional land use control MS4* (provided the *regulated, traditional land use control MS4* is not the *owner or operator* of the *construction activity*). At a minimum, the *owner or operator* must comply with the following requirements in order to be authorized to disturb greater than five (5) acres of soil at any one time:
- a. The *owner or operator* shall have a *qualified inspector* conduct **at least** two (2) site inspections in accordance with Part IV.C. of this permit every seven (7) calendar days, for as long as greater than five (5) acres of soil remain disturbed. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
  - b. In areas where soil disturbance activity has temporarily or permanently ceased, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days from the date the current soil disturbance activity ceased. The soil stabilization measures selected shall be in conformance with the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016.
  - c. The *owner or operator* shall prepare a phasing plan that defines maximum disturbed area per phase and shows required cuts and fills.
  - d. The *owner or operator* shall install any additional site-specific practices needed to protect water quality.
  - e. The *owner or operator* shall include the requirements above in their SWPPP.
4. In accordance with statute, regulations, and the terms and conditions of this permit, the Department may suspend or revoke an *owner's or operator's* coverage under this permit at any time if the Department determines that the SWPPP does not meet the permit requirements or consistent with Part VII.K..
  5. Upon a finding of significant non-compliance with the practices described in the SWPPP or violation of this permit, the Department may order an immediate stop to all activity at the site until the non-compliance is remedied. The stop work order shall be in writing, describe the non-compliance in detail, and be sent to the *owner or operator*.
  6. For *construction activities* that are subject to the requirements of a *regulated, traditional land use control MS4*, the *owner or operator* shall notify the

*regulated, traditional land use control MS4* in writing of any planned amendments or modifications to the post-construction stormwater management practice component of the SWPPP required by Part III.A. 4. and 5. of this permit. Unless otherwise notified by the *regulated, traditional land use control MS4*, the *owner or operator* shall have the SWPPP amendments or modifications reviewed and accepted by the *regulated, traditional land use control MS4* prior to commencing construction of the post-construction stormwater management practice.

#### **E. Permit Coverage for Discharges Authorized Under GP-0-15-002**

1. Upon renewal of SPDES General Permit for Stormwater Discharges from *Construction Activity* (Permit No. GP-0-15-002), an *owner or operator* of a *construction activity* with coverage under GP-0-15-002, as of the effective date of GP- 0-20-001, shall be authorized to *discharge* in accordance with GP- 0-20-001, unless otherwise notified by the Department.

An *owner or operator* may continue to implement the technical/design components of the post-construction stormwater management controls provided that such design was done in conformance with the technical standards in place at the time of initial project authorization. However, they must comply with the other, non-design provisions of GP-0-20-001.

#### **F. Change of Owner or Operator**

1. When property ownership changes or when there is a change in operational control over the construction plans and specifications, the original *owner or operator* must notify the new *owner or operator*, in writing, of the requirement to obtain permit coverage by submitting a NOI with the Department. For *construction activities* subject to the requirements of a *regulated, traditional land use control MS4*, the original *owner or operator* must also notify the MS4, in writing, of the change in ownership at least 30 calendar days prior to the change in ownership.
2. Once the new *owner or operator* obtains permit coverage, the original *owner or operator* shall then submit a completed NOT with the name and permit identification number of the new *owner or operator* to the Department at the address in Part II.B.1. of this permit. If the original *owner or operator* maintains ownership of a portion of the *construction activity* and will disturb soil, they must maintain their coverage under the permit.
3. Permit coverage for the new *owner or operator* will be effective as of the date the Department receives a complete NOI, provided the original *owner or*

*operator* was not subject to a sixty (60) business day authorization period that has not expired as of the date the Department receives the NOI from the new *owner or operator*.

### Part III. STORMWATER POLLUTION PREVENTION PLAN (SWPPP)

#### A. General SWPPP Requirements

1. A SWPPP shall be prepared and implemented by the *owner or operator* of each *construction activity* covered by this permit. The SWPPP must document the selection, design, installation, implementation and maintenance of the control measures and practices that will be used to meet the effluent limitations in Part I.B. of this permit and where applicable, the post-construction stormwater management practice requirements in Part I.C. of this permit. The SWPPP shall be prepared prior to the submittal of the NOI. The NOI shall be submitted to the Department prior to the *commencement of construction activity*. A copy of the completed, final NOI shall be included in the SWPPP.
2. The SWPPP shall describe the erosion and sediment control practices and where required, post-construction stormwater management practices that will be used and/or constructed to reduce the *pollutants* in stormwater *discharges* and to assure compliance with the terms and conditions of this permit. In addition, the SWPPP shall identify potential sources of pollution which may reasonably be expected to affect the quality of stormwater *discharges*.
3. All SWPPPs that require the post-construction stormwater management practice component shall be prepared by a *qualified professional* that is knowledgeable in the principles and practices of stormwater management and treatment.
4. The *owner or operator* must keep the SWPPP current so that it at all times accurately documents the erosion and sediment controls practices that are being used or will be used during construction, and all post-construction stormwater management practices that will be constructed on the site. At a minimum, the *owner or operator* shall amend the SWPPP, including construction drawings:
  - a. whenever the current provisions prove to be ineffective in minimizing *pollutants* in stormwater *discharges* from the site;

- b. whenever there is a change in design, construction, or operation at the *construction site* that has or could have an effect on the *discharge* of *pollutants*;
  - c. to address issues or deficiencies identified during an inspection by the *qualified inspector*, the Department or other regulatory authority; and
  - d. to document the final construction conditions.
5. The Department may notify the *owner or operator* at any time that the SWPPP does not meet one or more of the minimum requirements of this permit. The notification shall be in writing and identify the provisions of the SWPPP that require modification. Within fourteen (14) calendar days of such notification, or as otherwise indicated by the Department, the *owner or operator* shall make the required changes to the SWPPP and submit written notification to the Department that the changes have been made. If the *owner or operator* does not respond to the Department's comments in the specified time frame, the Department may suspend the *owner's or operator's* coverage under this permit or require the *owner or operator* to obtain coverage under an individual SPDES permit in accordance with Part II.D.4. of this permit.
6. Prior to the *commencement of construction activity*, the *owner or operator* must identify the contractor(s) and subcontractor(s) that will be responsible for installing, constructing, repairing, replacing, inspecting and maintaining the erosion and sediment control practices included in the SWPPP; and the contractor(s) and subcontractor(s) that will be responsible for constructing the post-construction stormwater management practices included in the SWPPP. The *owner or operator* shall have each of the contractors and subcontractors identify at least one person from their company that will be responsible for implementation of the SWPPP. This person shall be known as the *trained contractor*. The *owner or operator* shall ensure that at least one *trained contractor* is on site on a daily basis when soil disturbance activities are being performed.

The *owner or operator* shall have each of the contractors and subcontractors identified above sign a copy of the following certification statement below before they commence any *construction activity*:

"I hereby certify under penalty of law that I understand and agree to comply with the terms and conditions of the SWPPP and agree to implement any corrective actions identified by the *qualified inspector* during a site inspection. I also understand that the *owner or operator* must comply with

the terms and conditions of the most current version of the New York State Pollutant Discharge Elimination System ("SPDES") general permit for stormwater *discharges* from *construction activities* and that it is unlawful for any person to cause or contribute to a violation of *water quality standards*. Furthermore, I am aware that there are significant penalties for submitting false information, that I do not believe to be true, including the possibility of fine and imprisonment for knowing violations"

In addition to providing the certification statement above, the certification page must also identify the specific elements of the SWPPP that each contractor and subcontractor will be responsible for and include the name and title of the person providing the signature; the name and title of the *trained contractor* responsible for SWPPP implementation; the name, address and telephone number of the contracting firm; the address (or other identifying description) of the site; and the date the certification statement is signed. The *owner or operator* shall attach the certification statement(s) to the copy of the SWPPP that is maintained at the *construction site*. If new or additional contractors are hired to implement measures identified in the SWPPP after construction has commenced, they must also sign the certification statement and provide the information listed above.

7. For projects where the Department requests a copy of the SWPPP or inspection reports, the *owner or operator* shall submit the documents in both electronic (PDF only) and paper format within five (5) business days, unless otherwise notified by the Department.

## **B. Required SWPPP Contents**

1. Erosion and sediment control component - All SWPPPs prepared pursuant to this permit shall include erosion and sediment control practices designed in conformance with the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016. Where erosion and sediment control practices are not designed in conformance with the design criteria included in the technical standard, the *owner or operator* must demonstrate *equivalence* to the technical standard. At a minimum, the erosion and sediment control component of the SWPPP shall include the following:
  - a. Background information about the scope of the project, including the location, type and size of project

- b. A site map/construction drawing(s) for the project, including a general location map. At a minimum, the site map shall show the total site area; all improvements; areas of disturbance; areas that will not be disturbed; existing vegetation; on-site and adjacent off-site surface water(s); floodplain/floodway boundaries; wetlands and drainage patterns that could be affected by the *construction activity*; existing and final contours ; locations of different soil types with boundaries; material, waste, borrow or equipment storage areas located on adjacent properties; and location(s) of the stormwater *discharge(s)*;
- c. A description of the soil(s) present at the site, including an identification of the Hydrologic Soil Group (HSG);
- d. A construction phasing plan and sequence of operations describing the intended order of *construction activities*, including clearing and grubbing, excavation and grading, utility and infrastructure installation and any other activity at the site that results in soil disturbance;
- e. A description of the minimum erosion and sediment control practices to be installed or implemented for each *construction activity* that will result in soil disturbance. Include a schedule that identifies the timing of initial placement or implementation of each erosion and sediment control practice and the minimum time frames that each practice should remain in place or be implemented;
- f. A temporary and permanent soil stabilization plan that meets the requirements of this general permit and the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016, for each stage of the project, including initial land clearing and grubbing to project completion and achievement of *final stabilization*;
- g. A site map/construction drawing(s) showing the specific location(s), size(s), and length(s) of each erosion and sediment control practice;
- h. The dimensions, material specifications, installation details, and operation and maintenance requirements for all erosion and sediment control practices. Include the location and sizing of any temporary sediment basins and structural practices that will be used to divert flows from exposed soils;
- i. A maintenance inspection schedule for the contractor(s) identified in Part III.A.6. of this permit, to ensure continuous and effective operation of the erosion and sediment control practices. The maintenance inspection

schedule shall be in accordance with the requirements in the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016;

- j. A description of the pollution prevention measures that will be used to control litter, construction chemicals and construction debris from becoming a *pollutant* source in the stormwater *discharges*;
  - k. A description and location of any stormwater *discharges* associated with industrial activity other than construction at the site, including, but not limited to, stormwater *discharges* from asphalt plants and concrete plants located on the *construction site*; and
  - l. Identification of any elements of the design that are not in conformance with the design criteria in the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016. Include the reason for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.
2. Post-construction stormwater management practice component – The *owner or operator* of any construction project identified in Table 2 of Appendix B as needing post-construction stormwater management practices shall prepare a SWPPP that includes practices designed in conformance with the applicable *sizing criteria* in Part I.C.2.a., c. or d. of this permit and the *performance criteria* in the technical standard, New York State Stormwater Management Design Manual dated January 2015

Where post-construction stormwater management practices are not designed in conformance with the *performance criteria* in the technical standard, the *owner or operator* must include in the SWPPP the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.

The post-construction stormwater management practice component of the SWPPP shall include the following:

- a. Identification of all post-construction stormwater management practices to be constructed as part of the project. Include the dimensions, material specifications and installation details for each post-construction stormwater management practice;

- b. A site map/construction drawing(s) showing the specific location and size of each post-construction stormwater management practice;
- c. A Stormwater Modeling and Analysis Report that includes:
  - (i) Map(s) showing pre-development conditions, including watershed/subcatchments boundaries, flow paths/routing, and design points;
  - (ii) Map(s) showing post-development conditions, including watershed/subcatchments boundaries, flow paths/routing, design points and post-construction stormwater management practices;
  - (iii) Results of stormwater modeling (i.e. hydrology and hydraulic analysis) for the required storm events. Include supporting calculations (model runs), methodology, and a summary table that compares pre and post-development runoff rates and volumes for the different storm events;
  - (iv) Summary table, with supporting calculations, which demonstrates that each post-construction stormwater management practice has been designed in conformance with the *sizing criteria* included in the Design Manual;
  - (v) Identification of any *sizing criteria* that is not required based on the requirements included in Part I.C. of this permit; and
  - (vi) Identification of any elements of the design that are not in conformance with the *performance criteria* in the Design Manual. Include the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the Design Manual;
- d. Soil testing results and locations (test pits, borings);
- e. Infiltration test results, when required; and
- f. An operations and maintenance plan that includes inspection and maintenance schedules and actions to ensure continuous and effective operation of each post-construction stormwater management practice. The plan shall identify the entity that will be responsible for the long term operation and maintenance of each practice.



3. Enhanced Phosphorus Removal Standards - All construction projects identified in Table 2 of Appendix B that are located in the watersheds identified in Appendix C shall prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the applicable *sizing criteria* in Part I.C.2. b., c. or d. of this permit and the *performance criteria*, Enhanced Phosphorus Removal Standards included in the Design Manual. At a minimum, the post-construction stormwater management practice component of the SWPPP shall include items 2.a - 2.f. above.

### **C. Required SWPPP Components by Project Type**

Unless otherwise notified by the Department, *owners or operators of construction activities* identified in Table 1 of Appendix B are required to prepare a SWPPP that only includes erosion and sediment control practices designed in conformance with Part III.B.1 of this permit. *Owners or operators of the construction activities* identified in Table 2 of Appendix B shall prepare a SWPPP that also includes post-construction stormwater management practices designed in conformance with Part III.B.2 or 3 of this permit.

## **Part IV. INSPECTION AND MAINTENANCE REQUIREMENTS**

### **A. General Construction Site Inspection and Maintenance Requirements**

1. The *owner or operator* must ensure that all erosion and sediment control practices (including pollution prevention measures) and all post-construction stormwater management practices identified in the SWPPP are inspected and maintained in accordance with Part IV.B. and C. of this permit.
2. The terms of this permit shall not be construed to prohibit the State of New York from exercising any authority pursuant to the ECL, common law or federal law, or prohibit New York State from taking any measures, whether civil or criminal, to prevent violations of the laws of the State of New York or protect the public health and safety and/or the environment.

### **B. Contractor Maintenance Inspection Requirements**

1. The *owner or operator* of each *construction activity* identified in Tables 1 and 2 of Appendix B shall have a *trained contractor* inspect the erosion and sediment control practices and pollution prevention measures being implemented within the active work area daily to ensure that they are being maintained in effective operating condition at all times. If deficiencies are identified, the contractor shall

begin implementing corrective actions within one business day and shall complete the corrective actions in a reasonable time frame.

2. For construction sites where soil disturbance activities have been temporarily suspended (e.g. winter shutdown) and *temporary stabilization* measures have been applied to all disturbed areas, the *trained contractor* can stop conducting the maintenance inspections. The *trained contractor* shall begin conducting the maintenance inspections in accordance with Part IV.B.1. of this permit as soon as soil disturbance activities resume.
3. For construction sites where soil disturbance activities have been shut down with partial project completion, the *trained contractor* can stop conducting the maintenance inspections if all areas disturbed as of the project shutdown date have achieved *final stabilization* and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational.

### C. Qualified Inspector Inspection Requirements

The *owner or operator* shall have a *qualified inspector* conduct site inspections in conformance with the following requirements:

[Note: The *trained contractor* identified in Part III.A.6. and IV.B. of this permit **cannot** conduct the *qualified inspector* site inspections unless they meet the *qualified inspector* qualifications included in Appendix A. In order to perform these inspections, the *trained contractor* would have to be a:

- licensed Professional Engineer,
  - Certified Professional in Erosion and Sediment Control (CPESC),
  - New York State Erosion and Sediment Control Certificate Program holder
  - Registered Landscape Architect, or
  - someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided they have received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity].
1. A *qualified inspector* shall conduct site inspections for all *construction activities* identified in Tables 1 and 2 of Appendix B, with the exception of:
    - a. the construction of a single family residential subdivision with 25% or less *impervious cover* at total site build-out that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres and is not located

in one of the watersheds listed in Appendix C and not directly discharging to one of the 303(d) segments listed in Appendix E;

- b. the construction of a single family home that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres and is not located in one of the watersheds listed in Appendix C and not directly discharging to one of the 303(d) segments listed in Appendix E;
  - c. construction on agricultural property that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres; and
  - d. *construction activities* located in the watersheds identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.
2. Unless otherwise notified by the Department, the *qualified inspector* shall conduct site inspections in accordance with the following timetable:
- a. For construction sites where soil disturbance activities are on-going, the *qualified inspector* shall conduct a site inspection at least once every seven (7) calendar days.
  - b. For construction sites where soil disturbance activities are on-going and the *owner or operator* has received authorization in accordance with Part II.D.3 to disturb greater than five (5) acres of soil at any one time, the *qualified inspector* shall conduct at least two (2) site inspections every seven (7) calendar days. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
  - c. For construction sites where soil disturbance activities have been temporarily suspended (e.g. winter shutdown) and *temporary stabilization* measures have been applied to all disturbed areas, the *qualified inspector* shall conduct a site inspection at least once every thirty (30) calendar days. The *owner or operator* shall notify the DOW Water (SPDES) Program contact at the Regional Office (see contact information in Appendix F) or, in areas under the jurisdiction of a *regulated, traditional land use control MS4*, the *regulated, traditional land use control MS4* (provided the *regulated, traditional land use control MS4* is not the *owner or operator* of the *construction activity*) in writing prior to reducing the frequency of inspections.

- d. For construction sites where soil disturbance activities have been shut down with partial project completion, the *qualified inspector* can stop conducting inspections if all areas disturbed as of the project shutdown date have achieved *final stabilization* and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational. The *owner or operator* shall notify the DOW Water (SPDES) Program contact at the Regional Office (see contact information in Appendix F) or, in areas under the jurisdiction of a *regulated, traditional land use control MS4*, the *regulated, traditional land use control MS4* (provided the *regulated, traditional land use control MS4* is not the *owner or operator* of the *construction activity*) in writing prior to the shutdown. If soil disturbance activities are not resumed within 2 years from the date of shutdown, the *owner or operator* shall have the *qualified inspector* perform a final inspection and certify that all disturbed areas have achieved *final stabilization*, and all temporary, structural erosion and sediment control measures have been removed; and that all post-construction stormwater management practices have been constructed in conformance with the SWPPP by signing the “*Final Stabilization*” and “*Post-Construction Stormwater Management Practice*” certification statements on the NOT. The *owner or operator* shall then submit the completed NOT form to the address in Part II.B.1 of this permit.
  - e. For construction sites that directly *discharge* to one of the 303(d) segments listed in Appendix E or is located in one of the watersheds listed in Appendix C, the *qualified inspector* shall conduct at least two (2) site inspections every seven (7) calendar days. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
3. At a minimum, the *qualified inspector* shall inspect all erosion and sediment control practices and pollution prevention measures to ensure integrity and effectiveness, all post-construction stormwater management practices under construction to ensure that they are constructed in conformance with the SWPPP, all areas of disturbance that have not achieved *final stabilization*, all points of *discharge* to natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the *construction site*, and all points of *discharge* from the *construction site*.
  4. The *qualified inspector* shall prepare an inspection report subsequent to each and every inspection. At a minimum, the inspection report shall include and/or address the following:

- a. Date and time of inspection;
- b. Name and title of person(s) performing inspection;
- c. A description of the weather and soil conditions (e.g. dry, wet, saturated) at the time of the inspection;
- d. A description of the condition of the runoff at all points of *discharge* from the *construction site*. This shall include identification of any *discharges* of sediment from the *construction site*. Include *discharges* from conveyance systems (i.e. pipes, culverts, ditches, etc.) and overland flow;
- e. A description of the condition of all natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the *construction site* which receive runoff from disturbed areas. This shall include identification of any *discharges* of sediment to the surface waterbody;
- f. Identification of all erosion and sediment control practices and pollution prevention measures that need repair or maintenance;
- g. Identification of all erosion and sediment control practices and pollution prevention measures that were not installed properly or are not functioning as designed and need to be reinstalled or replaced;
- h. Description and sketch of areas with active soil disturbance activity, areas that have been disturbed but are inactive at the time of the inspection, and areas that have been stabilized (temporary and/or final) since the last inspection;
- i. Current phase of construction of all post-construction stormwater management practices and identification of all construction that is not in conformance with the SWPPP and technical standards;
- j. Corrective action(s) that must be taken to install, repair, replace or maintain erosion and sediment control practices and pollution prevention measures; and to correct deficiencies identified with the construction of the post-construction stormwater management practice(s);
- k. Identification and status of all corrective actions that were required by previous inspection; and

- I. Digital photographs, with date stamp, that clearly show the condition of all practices that have been identified as needing corrective actions. The *qualified inspector* shall attach paper color copies of the digital photographs to the inspection report being maintained onsite within seven (7) calendar days of the date of the inspection. The *qualified inspector* shall also take digital photographs, with date stamp, that clearly show the condition of the practice(s) after the corrective action has been completed. The *qualified inspector* shall attach paper color copies of the digital photographs to the inspection report that documents the completion of the corrective action work within seven (7) calendar days of that inspection.
5. Within one business day of the completion of an inspection, the *qualified inspector* shall notify the *owner or operator* and appropriate contractor or subcontractor identified in Part III.A.6. of this permit of any corrective actions that need to be taken. The contractor or subcontractor shall begin implementing the corrective actions within one business day of this notification and shall complete the corrective actions in a reasonable time frame.
6. All inspection reports shall be signed by the *qualified inspector*. Pursuant to Part II.D.2. of this permit, the inspection reports shall be maintained on site with the SWPPP.

## **Part V. TERMINATION OF PERMIT COVERAGE**

### **A. Termination of Permit Coverage**

1. An *owner or operator* that is eligible to terminate coverage under this permit must submit a completed NOT form to the address in Part II.B.1 of this permit. The NOT form shall be one which is associated with this permit, signed in accordance with Part VII.H of this permit.
2. An *owner or operator* may terminate coverage when one or more the following conditions have been met:
  - a. Total project completion - All *construction activity* identified in the SWPPP has been completed; and all areas of disturbance have achieved *final stabilization*; and all temporary, structural erosion and sediment control measures have been removed; and all post-construction stormwater management practices have been constructed in conformance with the SWPPP and are operational;

- b. Planned shutdown with partial project completion - All soil disturbance activities have ceased; and all areas disturbed as of the project shutdown date have achieved *final stabilization*; and all temporary, structural erosion and sediment control measures have been removed; and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational;
      - c. A new *owner or operator* has obtained coverage under this permit in accordance with Part II.F. of this permit.
      - d. The *owner or operator* obtains coverage under an alternative SPDES general permit or an individual SPDES permit.
3. For *construction activities* meeting subdivision 2a. or 2b. of this Part, the *owner or operator* shall have the *qualified inspector* perform a final site inspection prior to submitting the NOT. The *qualified inspector* shall, by signing the “*Final Stabilization*” and “Post-Construction Stormwater Management Practice certification statements on the NOT, certify that all the requirements in Part V.A.2.a. or b. of this permit have been achieved.
4. For *construction activities* that are subject to the requirements of a *regulated, traditional land use control MS4* and meet subdivision 2a. or 2b. of this Part, the *owner or operator* shall have the *regulated, traditional land use control MS4* sign the “MS4 Acceptance” statement on the NOT in accordance with the requirements in Part VII.H. of this permit. The *regulated, traditional land use control MS4* official, by signing this statement, has determined that it is acceptable for the *owner or operator* to submit the NOT in accordance with the requirements of this Part. The *regulated, traditional land use control MS4* can make this determination by performing a final site inspection themselves or by accepting the *qualified inspector’s* final site inspection certification(s) required in Part V.A.3. of this permit.
5. For *construction activities* that require post-construction stormwater management practices and meet subdivision 2a. of this Part, the *owner or operator* must, prior to submitting the NOT, ensure one of the following:
  - a. the post-construction stormwater management practice(s) and any right-of-way(s) needed to maintain such practice(s) have been deeded to the municipality in which the practice(s) is located,

- b. an executed maintenance agreement is in place with the municipality that will maintain the post-construction stormwater management practice(s),
- c. for post-construction stormwater management practices that are privately owned, the *owner or operator* has a mechanism in place that requires operation and maintenance of the practice(s) in accordance with the operation and maintenance plan, such as a deed covenant in the *owner or operator's* deed of record,
- d. for post-construction stormwater management practices that are owned by a public or private institution (e.g. school, university, hospital), government agency or authority, or public utility; the *owner or operator* has policy and procedures in place that ensures operation and maintenance of the practices in accordance with the operation and maintenance plan.

## **Part VI. REPORTING AND RETENTION RECORDS**

### **A. Record Retention**

The *owner or operator* shall retain a copy of the NOI, NOI Acknowledgment Letter, SWPPP, MS4 SWPPP Acceptance form and any inspection reports that were prepared in conjunction with this permit for a period of at least five (5) years from the date that the Department receives a complete NOT submitted in accordance with Part V. of this general permit.

### **B. Addresses**

With the exception of the NOI, NOT, and MS4 SWPPP Acceptance form (which must be submitted to the address referenced in Part II.B.1 of this permit), all written correspondence requested by the Department, including individual permit applications, shall be sent to the address of the appropriate DOW Water (SPDES) Program contact at the Regional Office listed in Appendix F.

## **Part VII. STANDARD PERMIT CONDITIONS**

### **A. Duty to Comply**

The *owner or operator* must comply with all conditions of this permit. All contractors and subcontractors associated with the project must comply with the terms of the SWPPP. Any non-compliance with this permit constitutes a violation of the Clean Water



Act (CWA) and the ECL and is grounds for an enforcement action against the *owner or operator* and/or the contractor/subcontractor; permit revocation, suspension or modification; or denial of a permit renewal application. Upon a finding of significant non-compliance with this permit or the applicable SWPPP, the Department may order an immediate stop to all *construction activity* at the site until the non-compliance is remedied. The stop work order shall be in writing, shall describe the non-compliance in detail, and shall be sent to the *owner or operator*.

If any human remains or archaeological remains are encountered during excavation, the *owner or operator* must immediately cease, or cause to cease, all *construction activity* in the area of the remains and notify the appropriate Regional Water Engineer (RWE). *Construction activity* shall not resume until written permission to do so has been received from the RWE.

#### **B. Continuation of the Expired General Permit**

This permit expires five (5) years from the effective date. If a new general permit is not issued prior to the expiration of this general permit, an *owner or operator* with coverage under this permit may continue to operate and *discharge* in accordance with the terms and conditions of this general permit, if it is extended pursuant to the State Administrative Procedure Act and 6 NYCRR Part 621, until a new general permit is issued.

#### **C. Enforcement**

Failure of the *owner or operator*, its contractors, subcontractors, agents and/or assigns to strictly adhere to any of the permit requirements contained herein shall constitute a violation of this permit. There are substantial criminal, civil, and administrative penalties associated with violating the provisions of this permit. Fines of up to \$37,500 per day for each violation and imprisonment for up to fifteen (15) years may be assessed depending upon the nature and degree of the offense.

#### **D. Need to Halt or Reduce Activity Not a Defense**

It shall not be a defense for an *owner or operator* in an enforcement action that it would have been necessary to halt or reduce the *construction activity* in order to maintain compliance with the conditions of this permit.

### **E. Duty to Mitigate**

The *owner or operator* and its contractors and subcontractors shall take all reasonable steps to *minimize* or prevent any *discharge* in violation of this permit which has a reasonable likelihood of adversely affecting human health or the environment.

### **F. Duty to Provide Information**

The *owner or operator* shall furnish to the Department, within a reasonable specified time period of a written request, all documentation necessary to demonstrate eligibility and any information to determine compliance with this permit or to determine whether cause exists for modifying or revoking this permit, or suspending or denying coverage under this permit, in accordance with the terms and conditions of this permit. The NOI, SWPPP and inspection reports required by this permit are public documents that the *owner or operator* must make available for review and copying by any person within five (5) business days of the *owner or operator* receiving a written request by any such person to review these documents. Copying of documents will be done at the requester's expense.

### **G. Other Information**

When the *owner or operator* becomes aware that they failed to submit any relevant facts, or submitted incorrect information in the NOI or in any of the documents required by this permit, or have made substantive revisions to the SWPPP (e.g. the scope of the project changes significantly, the type of post-construction stormwater management practice(s) changes, there is a reduction in the sizing of the post-construction stormwater management practice, or there is an increase in the disturbance area or *impervious area*), which were not reflected in the original NOI submitted to the Department, they shall promptly submit such facts or information to the Department using the contact information in Part II.A. of this permit. Failure of the *owner or operator* to correct or supplement any relevant facts within five (5) business days of becoming aware of the deficiency shall constitute a violation of this permit.

### **H. Signatory Requirements**

1. All NOIs and NOTs shall be signed as follows:
  - a. For a corporation these forms shall be signed by a responsible corporate officer. For the purpose of this section, a responsible corporate officer means:

- (i) a president, secretary, treasurer, or vice-president of the corporation in charge of a principal business function, or any other person who performs similar policy or decision-making functions for the corporation; or
    - (ii) the manager of one or more manufacturing, production or operating facilities, provided the manager is authorized to make management decisions which govern the operation of the regulated facility including having the explicit or implicit duty of making major capital investment recommendations, and initiating and directing other comprehensive measures to assure long term environmental compliance with environmental laws and regulations; the manager can ensure that the necessary systems are established or actions taken to gather complete and accurate information for permit application requirements; and where authority to sign documents has been assigned or delegated to the manager in accordance with corporate procedures;
  - b. For a partnership or sole proprietorship these forms shall be signed by a general partner or the proprietor, respectively; or
  - c. For a municipality, State, Federal, or other public agency these forms shall be signed by either a principal executive officer or ranking elected official. For purposes of this section, a principal executive officer of a Federal agency includes:
    - (i) the chief executive officer of the agency, or
    - (ii) a senior executive officer having responsibility for the overall operations of a principal geographic unit of the agency (e.g., Regional Administrators of EPA).
2. The SWPPP and other information requested by the Department shall be signed by a person described in Part VII.H.1. of this permit or by a duly authorized representative of that person. A person is a duly authorized representative only if:
- a. The authorization is made in writing by a person described in Part VII.H.1. of this permit;
  - b. The authorization specifies either an individual or a position having responsibility for the overall operation of the regulated facility or activity, such as the position of plant manager, operator of a well or a well field,

superintendent, position of *equivalent* responsibility, or an individual or position having overall responsibility for environmental matters for the company. (A duly authorized representative may thus be either a named individual or any individual occupying a named position) and,

- c. The written authorization shall include the name, title and signature of the authorized representative and be attached to the SWPPP.
3. All inspection reports shall be signed by the *qualified inspector* that performs the inspection.
4. The MS4 SWPPP Acceptance form shall be signed by the principal executive officer or ranking elected official from the *regulated, traditional land use control MS4*, or by a duly authorized representative of that person.

It shall constitute a permit violation if an incorrect and/or improper signatory authorizes any required forms, SWPPP and/or inspection reports.

#### **I. Property Rights**

The issuance of this permit does not convey any property rights of any sort, nor any exclusive privileges, nor does it authorize any injury to private property nor any invasion of personal rights, nor any infringement of Federal, State or local laws or regulations. *Owners or operators* must obtain any applicable conveyances, easements, licenses and/or access to real property prior to *commencing construction activity*.

#### **J. Severability**

The provisions of this permit are severable, and if any provision of this permit, or the application of any provision of this permit to any circumstance, is held invalid, the application of such provision to other circumstances, and the remainder of this permit shall not be affected thereby.

#### **K. Requirement to Obtain Coverage Under an Alternative Permit**

1. The Department may require any owner or operator authorized by this permit to apply for and/or obtain either an individual SPDES permit or another SPDES general permit. When the Department requires any discharger authorized by a general permit to apply for an individual SPDES permit, it shall notify the discharger in writing that a permit application is required. This notice shall

include a brief statement of the reasons for this decision, an application form, a statement setting a time frame for the owner or operator to file the application for an individual SPDES permit, and a deadline, not sooner than 180 days from owner or operator receipt of the notification letter, whereby the authorization to discharge under this general permit shall be terminated. Applications must be submitted to the appropriate Permit Administrator at the Regional Office. The Department may grant additional time upon demonstration, to the satisfaction of the Department, that additional time to apply for an alternative authorization is necessary or where the Department has not provided a permit determination in accordance with Part 621 of this Title.

2. When an individual SPDES permit is issued to a discharger authorized to *discharge* under a general SPDES permit for the same *discharge(s)*, the general permit authorization for outfalls authorized under the individual SPDES permit is automatically terminated on the effective date of the individual permit unless termination is earlier in accordance with 6 NYCRR Part 750.

#### **L. Proper Operation and Maintenance**

The *owner or operator* shall at all times properly operate and maintain all facilities and systems of treatment and control (and related appurtenances) which are installed or used by the *owner or operator* to achieve compliance with the conditions of this permit and with the requirements of the SWPPP.

#### **M. Inspection and Entry**

The *owner or operator* shall allow an authorized representative of the Department, EPA, applicable county health department, or, in the case of a *construction site* which *discharges* through an *MS4*, an authorized representative of the *MS4* receiving the discharge, upon the presentation of credentials and other documents as may be required by law, to:

1. Enter upon the owner's or operator's premises where a regulated facility or activity is located or conducted or where records must be kept under the conditions of this permit;
2. Have access to and copy at reasonable times, any records that must be kept under the conditions of this permit; and

3. Inspect at reasonable times any facilities or equipment (including monitoring and control equipment), practices or operations regulated or required by this permit.
4. Sample or monitor at reasonable times, for purposes of assuring permit compliance or as otherwise authorized by the Act or ECL, any substances or parameters at any location.

#### **N. Permit Actions**

This permit may, at any time, be modified, suspended, revoked, or renewed by the Department in accordance with 6 NYCRR Part 621. The filing of a request by the *owner or operator* for a permit modification, revocation and reissuance, termination, a notification of planned changes or anticipated noncompliance does not limit, diminish and/or stay compliance with any terms of this permit.

#### **O. Definitions**

Definitions of key terms are included in Appendix A of this permit.

#### **P. Re-Opener Clause**

1. If there is evidence indicating potential or realized impacts on water quality due to any stormwater discharge associated with construction activity covered by this permit, the owner or operator of such discharge may be required to obtain an individual permit or alternative general permit in accordance with Part VII.K. of this permit or the permit may be modified to include different limitations and/or requirements.
2. Any Department initiated permit modification, suspension or revocation will be conducted in accordance with 6 NYCRR Part 621, 6 NYCRR 750-1.18, and 6 NYCRR 750-1.20.

#### **Q. Penalties for Falsification of Forms and Reports**

In accordance with 6NYCRR Part 750-2.4 and 750-2.5, any person who knowingly makes any false material statement, representation, or certification in any application, record, report or other document filed or required to be maintained under this permit, including reports of compliance or noncompliance shall, upon conviction, be punished in accordance with ECL §71-1933 and or Articles 175 and 210 of the New York State Penal Law.

**R. Other Permits**

Nothing in this permit relieves the *owner or operator* from a requirement to obtain any other permits required by law.

## **APPENDIX A – Acronyms and Definitions**

### **Acronyms**

APO – Agency Preservation Officer

BMP – Best Management Practice

CPESC – Certified Professional in Erosion and Sediment Control

Cpv – Channel Protection Volume

CWA – Clean Water Act (or the Federal Water Pollution Control Act, 33 U.S.C. §1251 et seq)

DOW – Division of Water

EAF – Environmental Assessment Form

ECL - Environmental Conservation Law

EPA – U. S. Environmental Protection Agency

HSG – Hydrologic Soil Group

MS4 – Municipal Separate Storm Sewer System

NOI – Notice of Intent

NOT – Notice of Termination

NPDES – National Pollutant Discharge Elimination System

OPRHP – Office of Parks, Recreation and Historic Places

Qf – Extreme Flood

Qp – Overbank Flood

RRv – Runoff Reduction Volume

RWE – Regional Water Engineer

SEQR – State Environmental Quality Review

SEQRA - State Environmental Quality Review Act

SHPA – State Historic Preservation Act

SPDES – State Pollutant Discharge Elimination System

SWPPP – Stormwater Pollution Prevention Plan

TMDL – Total Maximum Daily Load

UPA – Uniform Procedures Act

USDA – United States Department of Agriculture

WQv – Water Quality Volume



## Definitions

All definitions in this section are solely for the purposes of this permit.

**Agricultural Building** – a structure designed and constructed to house farm implements, hay, grain, poultry, livestock or other horticultural products; excluding any structure designed, constructed or used, in whole or in part, for human habitation, as a place of employment where agricultural products are processed, treated or packaged, or as a place used by the public.

**Agricultural Property** – means the land for construction of a barn, *agricultural building*, silo, stockyard, pen or other structural practices identified in Table II in the “Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State” prepared by the Department in cooperation with agencies of New York Nonpoint Source Coordinating Committee (dated June 2007).

**Alter Hydrology from Pre to Post-Development Conditions** - means the post-development peak flow rate(s) has increased by more than 5% of the pre-developed condition for the design storm of interest (e.g. 10 yr and 100 yr).

**Combined Sewer** - means a sewer that is designed to collect and convey both “sewage” and “stormwater”.

**Commence (Commencement of) Construction Activities** - means the initial disturbance of soils associated with clearing, grading or excavation activities; or other construction related activities that disturb or expose soils such as demolition, stockpiling of fill material, and the initial installation of erosion and sediment control practices required in the SWPPP. See definition for “*Construction Activity(ies)*” also.

**Construction Activity(ies)** - means any clearing, grading, excavation, filling, demolition or stockpiling activities that result in soil disturbance. Clearing activities can include, but are not limited to, logging equipment operation, the cutting and skidding of trees, stump removal and/or brush root removal. Construction activity does not include routine maintenance that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility.

**Construction Site** – means the land area where *construction activity(ies)* will occur. See definition for “*Commence (Commencement of) Construction Activities*” and “*Larger Common Plan of Development or Sale*” also.

**Dewatering** – means the act of draining rainwater and/or groundwater from building foundations, vaults or excavations/trenches.

**Direct Discharge (to a specific surface waterbody)** - means that runoff flows from a *construction site* by overland flow and the first point of discharge is the specific surface waterbody, or runoff flows from a *construction site* to a separate storm sewer system

and the first point of discharge from the separate storm sewer system is the specific surface waterbody.

**Discharge(s)** - means any addition of any pollutant to waters of the State through an outlet or *point source*.

**Embankment** –means an earthen or rock slope that supports a road/highway.

**Endangered or Threatened Species** – see 6 NYCRR Part 182 of the Department’s rules and regulations for definition of terms and requirements.

**Environmental Conservation Law (ECL)** - means chapter 43-B of the Consolidated Laws of the State of New York, entitled the Environmental Conservation Law.

**Equivalent (Equivalence)** – means that the practice or measure meets all the performance, longevity, maintenance, and safety objectives of the technical standard and will provide an equal or greater degree of water quality protection.

**Final Stabilization** - means that all soil disturbance activities have ceased and a uniform, perennial vegetative cover with a density of eighty (80) percent over the entire pervious surface has been established; or other equivalent stabilization measures, such as permanent landscape mulches, rock rip-rap or washed/crushed stone have been applied on all disturbed areas that are not covered by permanent structures, concrete or pavement.

**General SPDES permit** - means a SPDES permit issued pursuant to 6 NYCRR Part 750-1.21 and Section 70-0117 of the ECL authorizing a category of discharges.

**Groundwater(s)** - means waters in the saturated zone. The saturated zone is a subsurface zone in which all the interstices are filled with water under pressure greater than that of the atmosphere. Although the zone may contain gas-filled interstices or interstices filled with fluids other than water, it is still considered saturated.

**Historic Property** – means any building, structure, site, object or district that is listed on the State or National Registers of Historic Places or is determined to be eligible for listing on the State or National Registers of Historic Places.

**Impervious Area (Cover)** - means all impermeable surfaces that cannot effectively infiltrate rainfall. This includes paved, concrete and gravel surfaces (i.e. parking lots, driveways, roads, runways and sidewalks); building rooftops and miscellaneous impermeable structures such as patios, pools, and sheds.

**Infeasible** – means not technologically possible, or not economically practicable and achievable in light of best industry practices.

**Larger Common Plan of Development or Sale** - means a contiguous area where multiple separate and distinct *construction activities* are occurring, or will occur, under one plan. The term “plan” in “larger common plan of development or sale” is broadly defined as any announcement or piece of documentation (including a sign, public notice or hearing, marketing plan, advertisement, drawing, permit application, State Environmental Quality Review Act (SEQRA) environmental assessment form or other documents, zoning request, computer design, etc.) or physical demarcation (including boundary signs, lot stakes, surveyor markings, etc.) indicating that *construction activities* may occur on a specific plot.

For discrete construction projects that are located within a larger common plan of development or sale that are at least 1/4 mile apart, each project can be treated as a separate plan of development or sale provided any interconnecting road, pipeline or utility project that is part of the same “common plan” is not concurrently being disturbed.

**Minimize** – means reduce and/or eliminate to the extent achievable using control measures (including best management practices) that are technologically available and economically practicable and achievable in light of best industry practices.

**Municipal Separate Storm Sewer (MS4)** - a conveyance or system of conveyances (including roads with drainage systems, municipal streets, catch basins, curbs, gutters, ditches, man-made channels, or storm drains):

- (i) Owned or operated by a State, city, town, borough, county, parish, district, association, or other public body (created by or pursuant to State law) having jurisdiction over disposal of sewage, industrial wastes, stormwater, or other wastes, including special districts under State law such as a sewer district, flood control district or drainage district, or similar entity, or an Indian tribe or an authorized Indian tribal organization, or a designated and approved management agency under section 208 of the CWA that discharges to surface waters of the State;
- (ii) Designed or used for collecting or conveying stormwater;
- (iii) Which is not a *combined sewer*, and
- (iv) Which is not part of a Publicly Owned Treatment Works (POTW) as defined at 40 CFR 122.2.

**National Pollutant Discharge Elimination System (NPDES)** - means the national system for the issuance of wastewater and stormwater permits under the Federal Water Pollution Control Act (Clean Water Act).

**Natural Buffer** –means an undisturbed area with natural cover running along a surface water (e.g. wetland, stream, river, lake, etc.).

**New Development** – means any land disturbance that does not meet the definition of Redevelopment Activity included in this appendix.

**New York State Erosion and Sediment Control Certificate Program** – a certificate program that establishes and maintains a process to identify and recognize individuals who are capable of developing, designing, inspecting and maintaining erosion and sediment control plans on projects that disturb soils in New York State. The certificate program is administered by the New York State Conservation District Employees Association.

**NOI Acknowledgment Letter** - means the letter that the Department sends to an owner or operator to acknowledge the Department's receipt and acceptance of a complete Notice of Intent. This letter documents the owner's or operator's authorization to discharge in accordance with the general permit for stormwater discharges from *construction activity*.

**Nonpoint Source** - means any source of water pollution or pollutants which is not a discrete conveyance or *point source* permitted pursuant to Title 7 or 8 of Article 17 of the Environmental Conservation Law (see ECL Section 17-1403).

**Overbank** –means flow events that exceed the capacity of the stream channel and spill out into the adjacent floodplain.

**Owner or Operator** - means the person, persons or legal entity which owns or leases the property on which the *construction activity* is occurring; an entity that has operational control over the construction plans and specifications, including the ability to make modifications to the plans and specifications; and/or an entity that has day-to-day operational control of those activities at a project that are necessary to ensure compliance with the permit conditions.

**Performance Criteria** – means the design criteria listed under the “Required Elements” sections in Chapters 5, 6 and 10 of the technical standard, New York State Stormwater Management Design Manual, dated January 2015. It does not include the Sizing Criteria (i.e. WQv, RRv, Cpv, Qp and Qf ) in Part I.C.2. of the permit.

**Point Source** - means any discernible, confined and discrete conveyance, including but not limited to any pipe, ditch, channel, tunnel, conduit, well, discrete fissure, container, rolling stock, concentrated animal feeding operation, vessel or other floating craft, or landfill leachate collection system from which *pollutants* are or may be discharged.

**Pollutant** - means dredged spoil, filter backwash, solid waste, incinerator residue, sewage, garbage, sewage sludge, munitions, chemical wastes, biological materials, radioactive materials, heat, wrecked or discarded equipment, rock, sand and industrial, municipal, agricultural waste and ballast discharged into water; which may cause or might reasonably be expected to cause pollution of the waters of the state in contravention of the standards or guidance values adopted as provided in 6 NYCRR Parts 700 et seq .

**Qualified Inspector** - means a person that is knowledgeable in the principles and practices of erosion and sediment control, such as a licensed Professional Engineer, Certified Professional in Erosion and Sediment Control (CPESC), Registered Landscape Architect, New York State Erosion and Sediment Control Certificate Program holder or other Department endorsed individual(s).

It can also mean someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided that person has training in the principles and practices of erosion and sediment control. Training in the principles and practices of erosion and sediment control means that the individual working under the direct supervision of the licensed Professional Engineer or Registered Landscape Architect has received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity. After receiving the initial training, the individual working under the direct supervision of the licensed Professional Engineer or Registered Landscape Architect shall receive four (4) hours of training every three (3) years.

It can also mean a person that meets the *Qualified Professional* qualifications in addition to the *Qualified Inspector* qualifications.

Note: Inspections of any post-construction stormwater management practices that include structural components, such as a dam for an impoundment, shall be performed by a licensed Professional Engineer.

**Qualified Professional** - means a person that is knowledgeable in the principles and practices of stormwater management and treatment, such as a licensed Professional Engineer, Registered Landscape Architect or other Department endorsed individual(s). Individuals preparing SWPPPs that require the post-construction stormwater management practice component must have an understanding of the principles of hydrology, water quality management practice design, water quantity control design, and, in many cases, the principles of hydraulics. All components of the SWPPP that involve the practice of engineering, as defined by the NYS Education Law (see Article 145), shall be prepared by, or under the direct supervision of, a professional engineer licensed to practice in the State of New York.

**Redevelopment Activity(ies)** – means the disturbance and reconstruction of existing impervious area, including impervious areas that were removed from a project site within five (5) years of preliminary project plan submission to the local government (i.e. site plan, subdivision, etc.).

**Regulated, Traditional Land Use Control MS4** - means a city, town or village with land use control authority that is authorized to discharge under New York State DEC's

SPDES General Permit For Stormwater Discharges from Municipal Separate Stormwater Sewer Systems (MS4s) or the City of New York's Individual SPDES Permit for their Municipal Separate Storm Sewer Systems (NY-0287890).

**Routine Maintenance Activity** - means *construction activity* that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility, including, but not limited to:

- Re-grading of gravel roads or parking lots,
- Cleaning and shaping of existing roadside ditches and culverts that maintains the approximate original line and grade, and hydraulic capacity of the ditch,
- Cleaning and shaping of existing roadside ditches that does not maintain the approximate original grade, hydraulic capacity and purpose of the ditch if the changes to the line and grade, hydraulic capacity or purpose of the ditch are installed to improve water quality and quantity controls (e.g. installing grass lined ditch),
- Placement of aggregate shoulder backing that stabilizes the transition between the road shoulder and the ditch or *embankment*,
- Full depth milling and filling of existing asphalt pavements, replacement of concrete pavement slabs, and similar work that does not expose soil or disturb the bottom six (6) inches of subbase material,
- Long-term use of equipment storage areas at or near highway maintenance facilities,
- Removal of sediment from the edge of the highway to restore a previously existing sheet-flow drainage connection from the highway surface to the highway ditch or *embankment*,
- Existing use of Canal Corp owned upland disposal sites for the canal, and
- Replacement of curbs, gutters, sidewalks and guide rail posts.

**Site limitations** – means site conditions that prevent the use of an infiltration technique and or infiltration of the total WQv. Typical site limitations include: seasonal high groundwater, shallow depth to bedrock, and soils with an infiltration rate less than 0.5 inches/hour. The existence of site limitations shall be confirmed and documented using actual field testing (i.e. test pits, soil borings, and infiltration test) or using information from the most current United States Department of Agriculture (USDA) Soil Survey for the County where the project is located.

**Sizing Criteria** – means the criteria included in Part I.C.2 of the permit that are used to size post-construction stormwater management control practices. The criteria include; Water Quality Volume (WQv), Runoff Reduction Volume (RRv), Channel Protection Volume (Cpv), *Overbank Flood* (Qp), and *Extreme Flood* (Qf).

**State Pollutant Discharge Elimination System (SPDES)** - means the system established pursuant to Article 17 of the ECL and 6 NYCRR Part 750 for issuance of permits authorizing discharges to the waters of the state.

**Steep Slope** – means land area designated on the current United States Department of Agriculture (“USDA”) Soil Survey as Soil Slope Phase “D”, (provided the map unit name is inclusive of slopes greater than 25%) , or Soil Slope Phase E or F, (regardless of the map unit name), or a combination of the three designations.

**Streambank** – as used in this permit, means the terrain alongside the bed of a creek or stream. The bank consists of the sides of the channel, between which the flow is confined.

**Stormwater Pollution Prevention Plan (SWPPP)** – means a project specific report, including construction drawings, that among other things: describes the construction activity(ies), identifies the potential sources of pollution at the *construction site*; describes and shows the stormwater controls that will be used to control the pollutants (i.e. erosion and sediment controls; for many projects, includes post-construction stormwater management controls); and identifies procedures the *owner or operator* will implement to comply with the terms and conditions of the permit. See Part III of the permit for a complete description of the information that must be included in the SWPPP.

**Surface Waters of the State** - shall be construed to include lakes, bays, sounds, ponds, impounding reservoirs, springs, rivers, streams, creeks, estuaries, marshes, inlets, canals, the Atlantic ocean within the territorial seas of the state of New York and all other bodies of surface water, natural or artificial, inland or coastal, fresh or salt, public or private (except those private waters that do not combine or effect a junction with natural surface waters), which are wholly or partially within or bordering the state or within its jurisdiction. Waters of the state are further defined in 6 NYCRR Parts 800 to 941.

**Temporarily Ceased** – means that an existing disturbed area will not be disturbed again within 14 calendar days of the previous soil disturbance.

**Temporary Stabilization** - means that exposed soil has been covered with material(s) as set forth in the technical standard, New York Standards and Specifications for Erosion and Sediment Control, to prevent the exposed soil from eroding. The materials can include, but are not limited to, mulch, seed and mulch, and erosion control mats (e.g. jute twisted yarn, excelsior wood fiber mats).

**Total Maximum Daily Loads (TMDLs)** - A TMDL is the sum of the allowable loads of a single pollutant from all contributing point and *nonpoint sources*. It is a calculation of the maximum amount of a pollutant that a waterbody can receive on a daily basis and still meet *water quality standards*, and an allocation of that amount to the pollutant's sources. A TMDL stipulates wasteload allocations (WLAs) for *point source* discharges, load allocations (LAs) for *nonpoint sources*, and a margin of safety (MOS).

**Trained Contractor** - means an employee from the contracting (construction) company, identified in Part III.A.6., that has received four (4) hours of Department endorsed

training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity. After receiving the initial training, the *trained contractor* shall receive four (4) hours of training every three (3) years.

It can also mean an employee from the contracting (construction) company, identified in Part III.A.6., that meets the *qualified inspector* qualifications (e.g. licensed Professional Engineer, Certified Professional in Erosion and Sediment Control (CPESC), Registered Landscape Architect, New York State Erosion and Sediment Control Certificate Program holder, or someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided they have received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity).

The *trained contractor* is responsible for the day to day implementation of the SWPPP.

**Uniform Procedures Act (UPA) Permit** - means a permit required under 6 NYCRR Part 621 of the Environmental Conservation Law (ECL), Article 70.

**Water Quality Standard** - means such measures of purity or quality for any waters in relation to their reasonable and necessary use as promulgated in 6 NYCRR Part 700 et seq.



## APPENDIX B – Required SWPPP Components by Project Type

**Table 1**  
**Construction Activities that Require the Preparation of a SWPPP That Only Includes Erosion and Sediment Controls**

<p><b>The following construction activities that involve soil disturbances of one (1) or more acres of land, but less than five (5) acres:</b></p> <ul style="list-style-type: none"><li>• Single family home <u>not</u> located in one of the watersheds listed in Appendix C or <u>not directly discharging</u> to one of the 303(d) segments listed in Appendix E</li><li>• Single family residential subdivisions with 25% or less impervious cover at total site build-out and <u>not</u> located in one of the watersheds listed in Appendix C and <u>not</u> directly discharging to one of the 303(d) segments listed in Appendix E</li><li>• Construction of a barn or other <i>agricultural building</i>, silo, stock yard or pen.</li></ul>
<p><b>The following construction activities that involve soil disturbances between five thousand (5000) square feet and one (1) acre of land:</b></p> <p>All construction activities located in the watersheds identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.</p>
<p><b>The following construction activities that involve soil disturbances of one (1) or more acres of land:</b></p> <ul style="list-style-type: none"><li>• Installation of underground, linear utilities; such as gas lines, fiber-optic cable, cable TV, electric, telephone, sewer mains, and water mains</li><li>• Environmental enhancement projects, such as wetland mitigation projects, stormwater retrofits and stream restoration projects</li><li>• Pond construction</li><li>• Linear bike paths running through areas with vegetative cover, including bike paths surfaced with an impervious cover</li><li>• Cross-country ski trails and walking/hiking trails</li><li>• Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are not part of residential, commercial or institutional development;</li><li>• Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that include incidental shoulder or curb work along an existing highway to support construction of the sidewalk, bike path or walking path.</li><li>• Slope stabilization projects</li><li>• Slope flattening that changes the grade of the site, but does not significantly change the runoff characteristics</li></ul>

**Table 1 (Continued) CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT ONLY INCLUDES EROSION AND SEDIMENT CONTROLS**

**The following construction activities that involve soil disturbances of one (1) or more acres of land:**

- Spoil areas that will be covered with vegetation
- Vegetated open space projects (i.e. recreational parks, lawns, meadows, fields, downhill ski trails) excluding projects that *alter hydrology from pre to post development* conditions,
- Athletic fields (natural grass) that do not include the construction or reconstruction of *impervious area* and do not *alter hydrology from pre to post development* conditions
- Demolition project where vegetation will be established, and no redevelopment is planned
- Overhead electric transmission line project that does not include the construction of permanent access roads or parking areas surfaced with *impervious cover*
- Structural practices as identified in Table II in the “Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State”, excluding projects that involve soil disturbances of greater than five acres and construction activities that include the construction or reconstruction of impervious area
- Temporary access roads, median crossovers, detour roads, lanes, or other temporary impervious areas that will be restored to pre-construction conditions once the construction activity is complete

**Table 2**  
**CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT INCLUDES**  
**POST-CONSTRUCTION STORMWATER MANAGEMENT PRACTICES**

**The following construction activities that involve soil disturbances of one (1) or more acres of land:**

- Single family home located in one of the watersheds listed in Appendix C or *directly discharging* to one of the 303(d) segments listed in Appendix E
- Single family home that disturbs five (5) or more acres of land
- Single family residential subdivisions located in one of the watersheds listed in Appendix C or *directly discharging* to one of the 303(d) segments listed in Appendix E
- Single family residential subdivisions that involve soil disturbances of between one (1) and five (5) acres of land with greater than 25% impervious cover at total site build-out
- Single family residential subdivisions that involve soil disturbances of five (5) or more acres of land, and single family residential subdivisions that involve soil disturbances of less than five (5) acres that are part of a larger common plan of development or sale that will ultimately disturb five or more acres of land
- Multi-family residential developments; includes duplexes, townhomes, condominiums, senior housing complexes, apartment complexes, and mobile home parks
- Airports
- Amusement parks
- Breweries, cideries, and wineries, including establishments constructed on agricultural land
- Campgrounds
- Cemeteries that include the construction or reconstruction of impervious area (>5% of disturbed area) or *alter the hydrology from pre to post development* conditions
- Commercial developments
- Churches and other places of worship
- Construction of a barn or other *agricultural building* (e.g. silo) and structural practices as identified in Table II in the "Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State" that include the construction or reconstruction of *impervious area*, excluding projects that involve soil disturbances of less than five acres.
- Golf courses
- Institutional development; includes hospitals, prisons, schools and colleges
- Industrial facilities; includes industrial parks
- Landfills
- Municipal facilities; includes highway garages, transfer stations, office buildings, POTW's, water treatment plants, and water storage tanks
- Office complexes
- Playgrounds that include the construction or reconstruction of impervious area
- Sports complexes
- Racetracks; includes racetracks with earthen (dirt) surface
- Road construction or reconstruction, including roads constructed as part of the construction activities listed in Table 1

Table 2 (Continued)

**CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT INCLUDES POST-CONSTRUCTION STORMWATER MANAGEMENT PRACTICES**

The following construction activities that involve soil disturbances of one (1) or more acres of land:

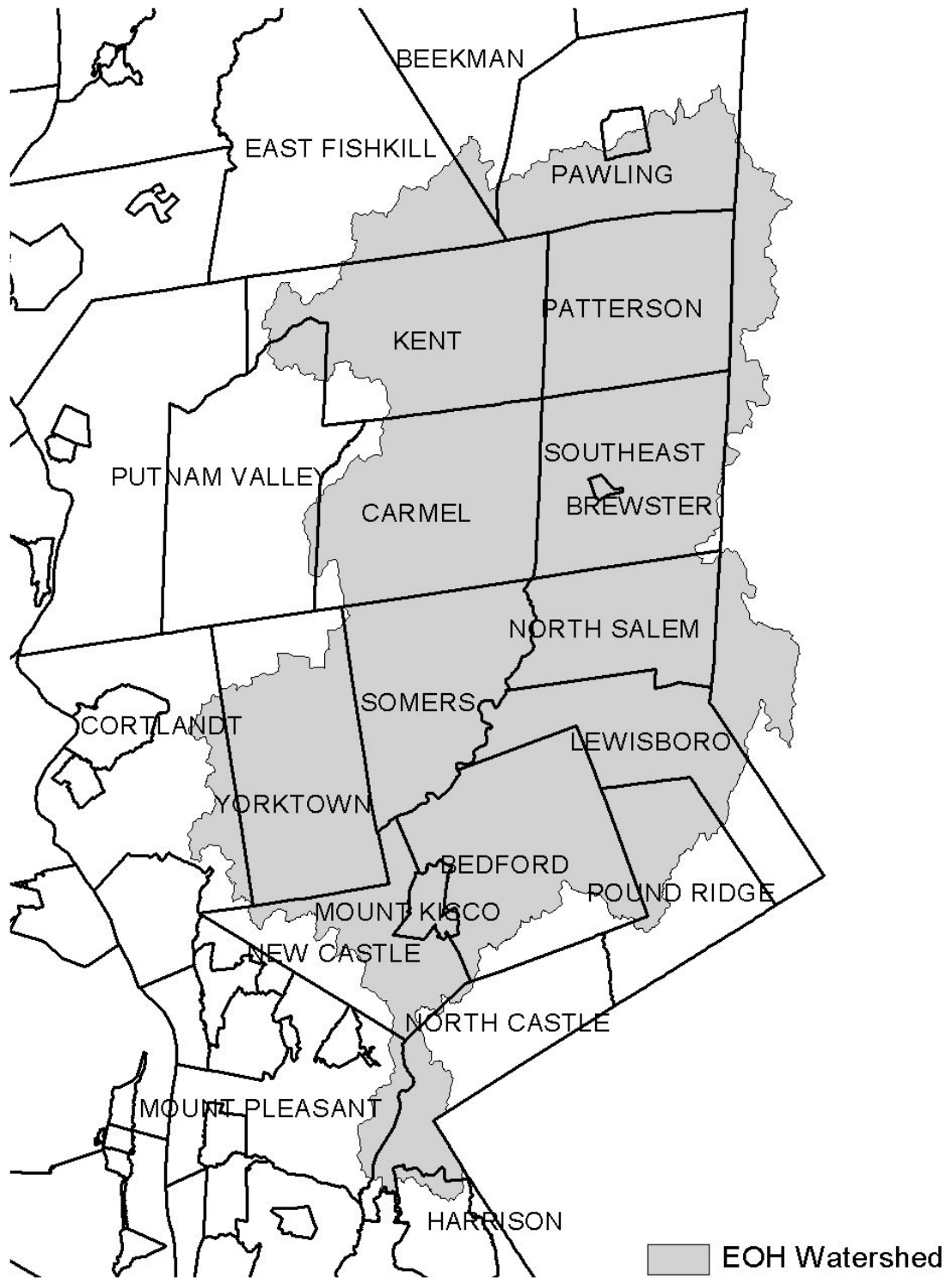
- Parking lot construction or reconstruction, including parking lots constructed as part of the construction activities listed in Table 1
- Athletic fields (natural grass) that include the construction or reconstruction of impervious area (>5% of disturbed area) or *alter the hydrology from pre to post development* conditions
- Athletic fields with artificial turf
- Permanent access roads, parking areas, substations, compressor stations and well drilling pads, surfaced with *impervious cover*, and constructed as part of an over-head electric transmission line project, wind-power project, cell tower project, oil or gas well drilling project, sewer or water main project or other linear utility project
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are part of a residential, commercial or institutional development
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are part of a highway construction or reconstruction project
- All other construction activities that include the construction or reconstruction of *impervious area* or *alter the hydrology from pre to post development* conditions, and are not listed in Table 1

## APPENDIX C – Watersheds Requiring Enhanced Phosphorus Removal

**Watersheds where *owners or operators* of construction activities identified in Table 2 of Appendix B must prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the Enhanced Phosphorus Removal Standards included in the technical standard, New York State Stormwater Management Design Manual (“Design Manual”).**

- Entire New York City Watershed located east of the Hudson River - Figure 1
- Onondaga Lake Watershed - Figure 2
- Greenwood Lake Watershed -Figure 3
- Oscawana Lake Watershed – Figure 4
- Kinderhook Lake Watershed – Figure 5

**Figure 1 - New York City Watershed East of the Hudson**



**Figure 2 - Onondaga Lake Watershed**

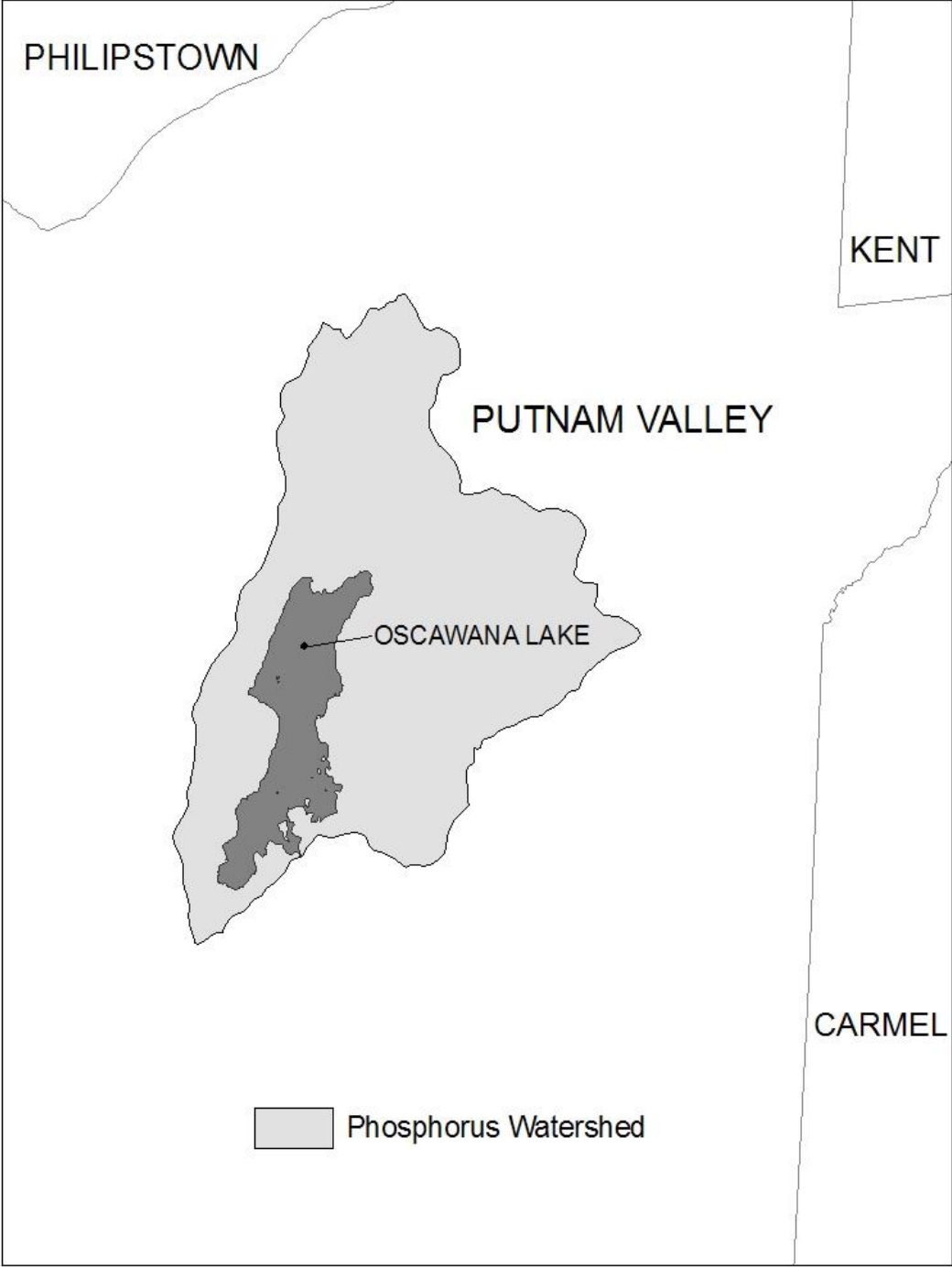


**Figure 3 - Greenwood Lake Watershed**

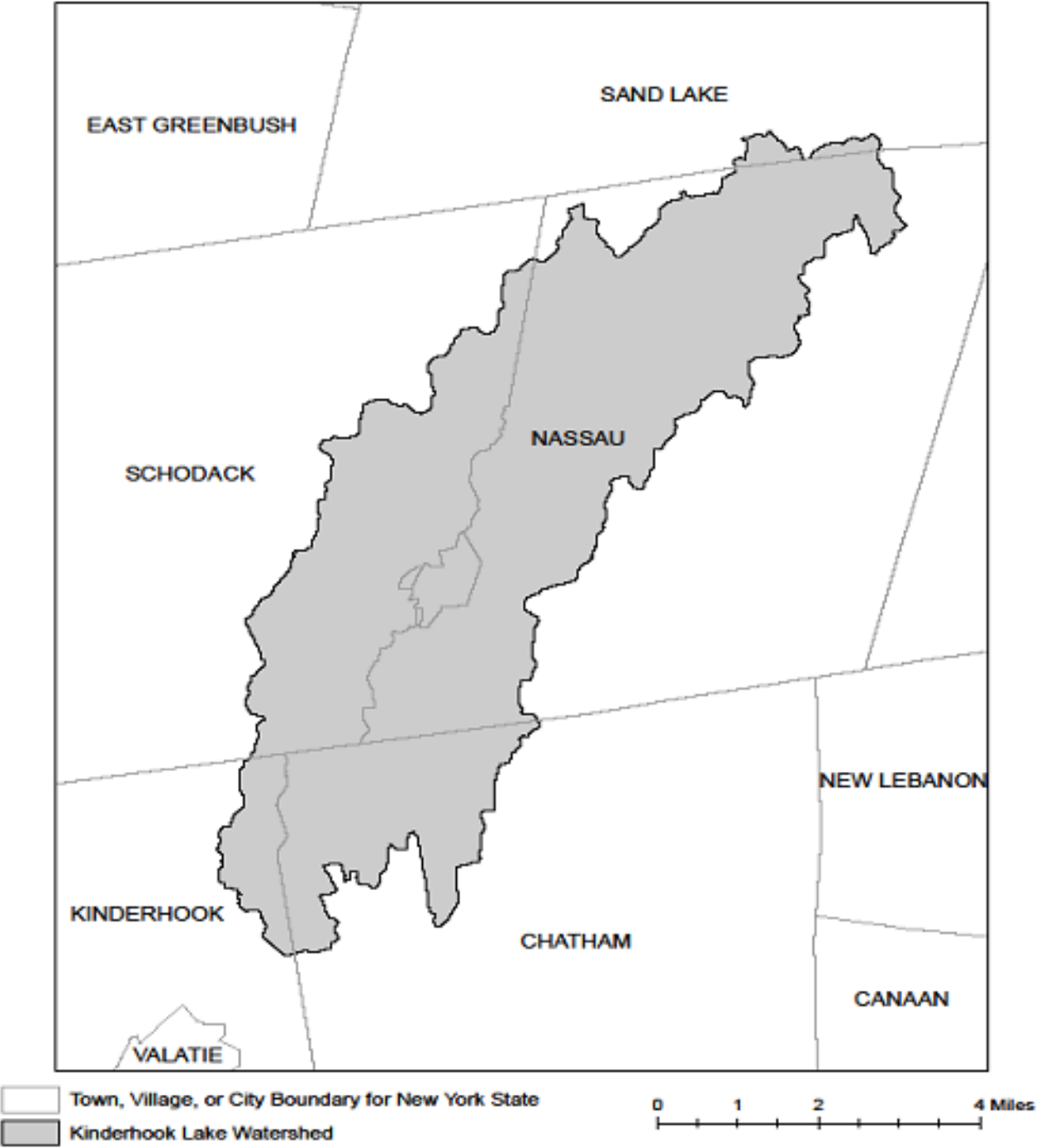




**Figure 4 - Oscawana Lake Watershed**



**Figure 5 - Kinderhook Lake Watershed**



## APPENDIX D – Watersheds with Lower Disturbance Threshold

**Watersheds where *owners or operators* of construction activities that involve soil disturbances between five thousand (5000) square feet and one (1) acre of land must obtain coverage under this permit.**

Entire New York City Watershed that is located east of the Hudson River - See Figure 1 in Appendix C

## APPENDIX E – 303(d) Segments Impaired by Construction Related Pollutant(s)

List of 303(d) segments impaired by pollutants related to *construction activity* (e.g. silt, sediment or nutrients). The list was developed using "The Final New York State 2016 Section 303(d) List of Impaired Waters Requiring a TMDL/Other Strategy" dated November 2016. *Owners or operators* of single family home and single family residential subdivisions with 25% or less total impervious cover at total site build-out that involve soil disturbances of one or more acres of land, but less than 5 acres, and *directly discharge* to one of the listed segments below shall prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the New York State Stormwater Management Design Manual ("Design Manual"), dated January 2015.

COUNTY	WATERBODY	POLLUTANT
Albany	Ann Lee (Shakers) Pond, Stump Pond	Nutrients
Albany	Basic Creek Reservoir	Nutrients
Allegany	Amity Lake, Saunders Pond	Nutrients
Bronx	Long Island Sound, Bronx	Nutrients
Bronx	Van Cortlandt Lake	Nutrients
Broome	Fly Pond, Deer Lake, Sky Lake	Nutrients
Broome	Minor Tribs to Lower Susquehanna (north)	Nutrients
Broome	Whitney Point Lake/Reservoir	Nutrients
Cattaraugus	Allegheny River/Reservoir	Nutrients
Cattaraugus	Beaver (Alma) Lake	Nutrients
Cattaraugus	Case Lake	Nutrients
Cattaraugus	Linlyco/Club Pond	Nutrients
Cayuga	Duck Lake	Nutrients
Cayuga	Little Sodus Bay	Nutrients
Chautauqua	Bear Lake	Nutrients
Chautauqua	Chadakoin River and tribs	Nutrients
Chautauqua	Chautauqua Lake, North	Nutrients
Chautauqua	Chautauqua Lake, South	Nutrients
Chautauqua	Findley Lake	Nutrients
Chautauqua	Hulburt/Clymer Pond	Nutrients
Clinton	Great Chazy River, Lower, Main Stem	Silt/Sediment
Clinton	Lake Champlain, Main Lake, Middle	Nutrients
Clinton	Lake Champlain, Main Lake, North	Nutrients
Columbia	Kinderhook Lake	Nutrients
Columbia	Robinson Pond	Nutrients
Cortland	Dean Pond	Nutrients

### 303(d) Segments Impaired by Construction Related Pollutant(s)

Dutchess	Fall Kill and tribs	Nutrients
Dutchess	Hillside Lake	Nutrients
Dutchess	Wappingers Lake	Nutrients
Dutchess	Wappingers Lake	Silt/Sediment
Erie	Beeman Creek and tribs	Nutrients
Erie	Ellicott Creek, Lower, and tribs	Silt/Sediment
Erie	Ellicott Creek, Lower, and tribs	Nutrients
Erie	Green Lake	Nutrients
Erie	Little Sister Creek, Lower, and tribs	Nutrients
Erie	Murder Creek, Lower, and tribs	Nutrients
Erie	Rush Creek and tribs	Nutrients
Erie	Scajaquada Creek, Lower, and tribs	Nutrients
Erie	Scajaquada Creek, Middle, and tribs	Nutrients
Erie	Scajaquada Creek, Upper, and tribs	Nutrients
Erie	South Branch Smoke Cr, Lower, and tribs	Silt/Sediment
Erie	South Branch Smoke Cr, Lower, and tribs	Nutrients
Essex	Lake Champlain, Main Lake, South	Nutrients
Essex	Lake Champlain, South Lake	Nutrients
Essex	Willsboro Bay	Nutrients
Genesee	Bigelow Creek and tribs	Nutrients
Genesee	Black Creek, Middle, and minor tribs	Nutrients
Genesee	Black Creek, Upper, and minor tribs	Nutrients
Genesee	Bowen Brook and tribs	Nutrients
Genesee	LeRoy Reservoir	Nutrients
Genesee	Oak Orchard Cr, Upper, and tribs	Nutrients
Genesee	Tonawanda Creek, Middle, Main Stem	Nutrients
Greene	Schoharie Reservoir	Silt/Sediment
Greene	Sleepy Hollow Lake	Silt/Sediment
Herkimer	Steele Creek tribs	Silt/Sediment
Herkimer	Steele Creek tribs	Nutrients
Jefferson	Moon Lake	Nutrients
Kings	Hendrix Creek	Nutrients
Kings	Prospect Park Lake	Nutrients
Lewis	Mill Creek/South Branch, and tribs	Nutrients
Livingston	Christie Creek and tribs	Nutrients
Livingston	Conesus Lake	Nutrients
Livingston	Mill Creek and minor tribs	Silt/Sediment
Monroe	Black Creek, Lower, and minor tribs	Nutrients
Monroe	Buck Pond	Nutrients
Monroe	Cranberry Pond	Nutrients

### 303(d) Segments Impaired by Construction Related Pollutant(s)

Monroe	Lake Ontario Shoreline, Western	Nutrients
Monroe	Long Pond	Nutrients
Monroe	Mill Creek and tribs	Nutrients
Monroe	Mill Creek/Blue Pond Outlet and tribs	Nutrients
Monroe	Minor Tribs to Irondequoit Bay	Nutrients
Monroe	Rochester Embayment - East	Nutrients
Monroe	Rochester Embayment - West	Nutrients
Monroe	Shipbuilders Creek and tribs	Nutrients
Monroe	Thomas Creek/White Brook and tribs	Nutrients
Nassau	Beaver Lake	Nutrients
Nassau	Camaans Pond	Nutrients
Nassau	East Meadow Brook, Upper, and tribs	Silt/Sediment
Nassau	East Rockaway Channel	Nutrients
Nassau	Grant Park Pond	Nutrients
Nassau	Hempstead Bay	Nutrients
Nassau	Hempstead Lake	Nutrients
Nassau	Hewlett Bay	Nutrients
Nassau	Hog Island Channel	Nutrients
Nassau	Long Island Sound, Nassau County Waters	Nutrients
Nassau	Massapequa Creek and tribs	Nutrients
Nassau	Milburn/Parsonage Creeks, Upp, and tribs	Nutrients
Nassau	Reynolds Channel, west	Nutrients
Nassau	Tidal Tribs to Hempstead Bay	Nutrients
Nassau	Tribs (fresh) to East Bay	Nutrients
Nassau	Tribs (fresh) to East Bay	Silt/Sediment
Nassau	Tribs to Smith/Halls Ponds	Nutrients
Nassau	Woodmere Channel	Nutrients
New York	Harlem Meer	Nutrients
New York	The Lake in Central Park	Nutrients
Niagara	Bergholtz Creek and tribs	Nutrients
Niagara	Hyde Park Lake	Nutrients
Niagara	Lake Ontario Shoreline, Western	Nutrients
Niagara	Lake Ontario Shoreline, Western	Nutrients
Oneida	Ballou, Nail Creeks and tribs	Nutrients
Onondaga	Harbor Brook, Lower, and tribs	Nutrients
Onondaga	Ley Creek and tribs	Nutrients
Onondaga	Minor Tribs to Onondaga Lake	Nutrients
Onondaga	Ninemile Creek, Lower, and tribs	Nutrients
Onondaga	Onondaga Creek, Lower, and tribs	Nutrients
Onondaga	Onondaga Creek, Middle, and tribs	Nutrients

### 303(d) Segments Impaired by Construction Related Pollutant(s)

Onondaga	Onondaga Lake, northern end	Nutrients
Onondaga	Onondaga Lake, southern end	Nutrients
Ontario	Great Brook and minor tribs	Silt/Sediment
Ontario	Great Brook and minor tribs	Nutrients
Ontario	Hemlock Lake Outlet and minor tribs	Nutrients
Ontario	Honeoye Lake	Nutrients
Orange	Greenwood Lake	Nutrients
Orange	Monhagen Brook and tribs	Nutrients
Orange	Orange Lake	Nutrients
Orleans	Lake Ontario Shoreline, Western	Nutrients
Orleans	Lake Ontario Shoreline, Western	Nutrients
Oswego	Lake Neatahwanta	Nutrients
Oswego	Pleasant Lake	Nutrients
Putnam	Bog Brook Reservoir	Nutrients
Putnam	Boyd Corners Reservoir	Nutrients
Putnam	Croton Falls Reservoir	Nutrients
Putnam	Diverting Reservoir	Nutrients
Putnam	East Branch Reservoir	Nutrients
Putnam	Lake Carmel	Nutrients
Putnam	Middle Branch Reservoir	Nutrients
Putnam	Oscawana Lake	Nutrients
Putnam	Palmer Lake	Nutrients
Putnam	West Branch Reservoir	Nutrients
Queens	Bergen Basin	Nutrients
Queens	Flushing Creek/Bay	Nutrients
Queens	Jamaica Bay, Eastern, and tribs (Queens)	Nutrients
Queens	Kissena Lake	Nutrients
Queens	Meadow Lake	Nutrients
Queens	Willow Lake	Nutrients
Rensselaer	Nassau Lake	Nutrients
Rensselaer	Snyders Lake	Nutrients
Richmond	Grasmere Lake/Bradys Pond	Nutrients
Rockland	Congers Lake, Swartout Lake	Nutrients
Rockland	Rockland Lake	Nutrients
Saratoga	Ballston Lake	Nutrients
Saratoga	Dwaas Kill and tribs	Silt/Sediment
Saratoga	Dwaas Kill and tribs	Nutrients
Saratoga	Lake Lonely	Nutrients
Saratoga	Round Lake	Nutrients
Saratoga	Tribs to Lake Lonely	Nutrients

### 303(d) Segments Impaired by Construction Related Pollutant(s)

Schenectady	Collins Lake	Nutrients
Schenectady	Duane Lake	Nutrients
Schenectady	Mariaville Lake	Nutrients
Schoharie	Engleville Pond	Nutrients
Schoharie	Summit Lake	Nutrients
Seneca	Reeder Creek and tribs	Nutrients
St.Lawrence	Black Lake Outlet/Black Lake	Nutrients
St.Lawrence	Fish Creek and minor tribs	Nutrients
Steuben	Smith Pond	Nutrients
Suffolk	Agawam Lake	Nutrients
Suffolk	Big/Little Fresh Ponds	Nutrients
Suffolk	Canaan Lake	Silt/Sediment
Suffolk	Canaan Lake	Nutrients
Suffolk	Flanders Bay, West/Lower Sawmill Creek	Nutrients
Suffolk	Fresh Pond	Nutrients
Suffolk	Great South Bay, East	Nutrients
Suffolk	Great South Bay, Middle	Nutrients
Suffolk	Great South Bay, West	Nutrients
Suffolk	Lake Ronkonkoma	Nutrients
Suffolk	Long Island Sound, Suffolk County, West	Nutrients
Suffolk	Mattituck (Marratooka) Pond	Nutrients
Suffolk	Meetinghouse/Terrys Creeks and tribs	Nutrients
Suffolk	Mill and Seven Ponds	Nutrients
Suffolk	Millers Pond	Nutrients
Suffolk	Moriches Bay, East	Nutrients
Suffolk	Moriches Bay, West	Nutrients
Suffolk	Peconic River, Lower, and tidal tribs	Nutrients
Suffolk	Quantuck Bay	Nutrients
Suffolk	Shinnecock Bay and Inlet	Nutrients
Suffolk	Tidal tribs to West Moriches Bay	Nutrients
Sullivan	Bodine, Montgomery Lakes	Nutrients
Sullivan	Davies Lake	Nutrients
Sullivan	Evens Lake	Nutrients
Sullivan	Pleasure Lake	Nutrients
Tompkins	Cayuga Lake, Southern End	Nutrients
Tompkins	Cayuga Lake, Southern End	Silt/Sediment
Tompkins	Owasco Inlet, Upper, and tribs	Nutrients
Ulster	Ashokan Reservoir	Silt/Sediment
Ulster	Esopus Creek, Upper, and minor tribs	Silt/Sediment
Warren	Hague Brook and tribs	Silt/Sediment



### 303(d) Segments Impaired by Construction Related Pollutant(s)

Warren	Huddle/Finkle Brooks and tribs	Silt/Sediment
Warren	Indian Brook and tribs	Silt/Sediment
Warren	Lake George	Silt/Sediment
Warren	Tribs to L.George, Village of L George	Silt/Sediment
Washington	Cossayuna Lake	Nutrients
Washington	Lake Champlain, South Bay	Nutrients
Washington	Tribs to L.George, East Shore	Silt/Sediment
Washington	Wood Cr/Champlain Canal and minor tribs	Nutrients
Wayne	Port Bay	Nutrients
Westchester	Amawalk Reservoir	Nutrients
Westchester	Blind Brook, Upper, and tribs	Silt/Sediment
Westchester	Cross River Reservoir	Nutrients
Westchester	Lake Katonah	Nutrients
Westchester	Lake Lincolndale	Nutrients
Westchester	Lake Meahagh	Nutrients
Westchester	Lake Mohegan	Nutrients
Westchester	Lake Shenorock	Nutrients
Westchester	Long Island Sound, Westchester (East)	Nutrients
Westchester	Mamaroneck River, Lower	Silt/Sediment
Westchester	Mamaroneck River, Upper, and minor tribs	Silt/Sediment
Westchester	Muscoot/Upper New Croton Reservoir	Nutrients
Westchester	New Croton Reservoir	Nutrients
Westchester	Peach Lake	Nutrients
Westchester	Reservoir No.1 (Lake Isle)	Nutrients
Westchester	Saw Mill River, Lower, and tribs	Nutrients
Westchester	Saw Mill River, Middle, and tribs	Nutrients
Westchester	Sheldrake River and tribs	Silt/Sediment
Westchester	Sheldrake River and tribs	Nutrients
Westchester	Silver Lake	Nutrients
Westchester	Teatown Lake	Nutrients
Westchester	Titicus Reservoir	Nutrients
Westchester	Truesdale Lake	Nutrients
Westchester	Wallace Pond	Nutrients
Wyoming	Java Lake	Nutrients
Wyoming	Silver Lake	Nutrients

## APPENDIX F – List of NYS DEC Regional Offices

<u>Region</u>	<u>COVERING THE FOLLOWING COUNTIES:</u>	<u>DIVISION OF ENVIRONMENTAL PERMITS (DEP) PERMIT ADMINISTRATORS</u>	<u>DIVISION OF WATER (DOW) WATER (SPDES) PROGRAM</u>
1	NASSAU AND SUFFOLK	50 CIRCLE ROAD STONY BROOK, NY 11790 TEL. (631) 444-0365	50 CIRCLE ROAD STONY BROOK, NY 11790-3409 TEL. (631) 444-0405
2	BRONX, KINGS, NEW YORK, QUEENS AND RICHMOND	1 HUNTERS POINT PLAZA, 47-40 21ST ST. LONG ISLAND CITY, NY 11101-5407 TEL. (718) 482-4997	1 HUNTERS POINT PLAZA, 47-40 21ST ST. LONG ISLAND CITY, NY 11101-5407 TEL. (718) 482-4933
3	DUTCHESS, ORANGE, PUTNAM, ROCKLAND, SULLIVAN, ULSTER AND WESTCHESTER	21 SOUTH PUTT CORNERS ROAD NEW PALTZ, NY 12561-1696 TEL. (845) 256-3059	100 HILLSIDE AVENUE, SUITE 1W WHITE PLAINS, NY 10603 TEL. (914) 428 - 2505
4	ALBANY, COLUMBIA, DELAWARE, GREENE, MONTGOMERY, OTSEGO, RENSSELAER, SCHENECTADY AND SCHOHARIE	1150 NORTH WESTCOTT ROAD SCHENECTADY, NY 12306-2014 TEL. (518) 357-2069	1130 NORTH WESTCOTT ROAD SCHENECTADY, NY 12306-2014 TEL. (518) 357-2045
5	CLINTON, ESSEX, FRANKLIN, FULTON, HAMILTON, SARATOGA, WARREN AND WASHINGTON	1115 STATE ROUTE 86, Po Box 296 RAY BROOK, NY 12977-0296 TEL. (518) 897-1234	232 GOLF COURSE ROAD WARRENSBURG, NY 12885-1172 TEL. (518) 623-1200
6	HERKIMER, JEFFERSON, LEWIS, ONEIDA AND ST. LAWRENCE	STATE OFFICE BUILDING 317 WASHINGTON STREET WATERTOWN, NY 13601-3787 TEL. (315) 785-2245	STATE OFFICE BUILDING 207 GENESEE STREET UTICA, NY 13501-2885 TEL. (315) 793-2554
7	BROOME, CAYUGA, CHENANGO, CORTLAND, MADISON, ONONDAGA, OSWEGO, TIOGA AND TOMPKINS	615 ERIE BLVD. WEST SYRACUSE, NY 13204-2400 TEL. (315) 426-7438	615 ERIE BLVD. WEST SYRACUSE, NY 13204-2400 TEL. (315) 426-7500
8	CHEMUNG, GENESEE, LIVINGSTON, MONROE, ONTARIO, ORLEANS, SCHUYLER, SENECA, STEUBEN, WAYNE AND YATES	6274 EAST AVON-LIMA ROADAVON, NY 14414-9519 TEL. (585) 226-2466	6274 EAST AVON-LIMA RD. AVON, NY 14414-9519 TEL. (585) 226-2466
9	ALLEGANY, CATTARAUGUS, CHAUTAUQUA, ERIE, NIAGARA AND WYOMING	270 MICHIGAN AVENUE BUFFALO, NY 14203-2999 TEL. (716) 851-7165	270 MICHIGAN AVENUE BUFFALO, NY 14203-2999 TEL. (716) 851-7070

## Appendix 5 | Draft Notice of Intent (N.O.I.)

# NOI for coverage under Stormwater General Permit for Construction Activity

version 1.35

(Submission #: HPR-5ZK1-V190G, version 1)

## Details

---

**Submission Alias** Dewpoint South  
**Originally Started By** CORY ROBINSON  
**Alternate Identifier** DEWPOINT SOUTH  
**Submission ID** HPR-5ZK1-V190G  
**Submission Reason** New  
**Status** Draft

## Form Input

---

### Owner/Operator Information

**Owner/Operator Name (Company/Private Owner/Municipality/Agency/Institution, etc.)**

Dewpoint Development LLC

**Owner/Operator Contact Person Last Name (NOT CONSULTANT)**

NEUMAN

**Owner/Operator Contact Person First Name**

ISAAC

**Owner/Operator Mailing Address**

1 International Boulevard, Suite 410

**City**

MAHWAH

**State**

NJ

**Zip**

07430

**Phone**

8452024900

**Email**

ISAAC@RDMGP.COM

**Federal Tax ID**

NONE PROVIDED

**Project Location**

**Project/Site Name**

DEWPOINT SOUTH

**Street Address (Not P.O. Box)**

Dolstontown Road & Caskey Lane

**Side of Street**

South

**City/Town/Village (THAT ISSUES BUILDING PERMIT)**

TOWN OF WAWAYANDA

**State**

NY

**Zip**

10973

**DEC Region**

3

**County**

ORANGE

**Name of Nearest Cross Street**

CASKEY LN

**Distance to Nearest Cross Street (Feet)**

0

**Project In Relation to Cross Street**

West

**Tax Map Numbers Section-Block-Parcel**

4-1-50.32

**Tax Map Numbers**

NONE PROVIDED

**1. Coordinates**

---

Provide the Geographic Coordinates for the project site. The two methods are:

- Navigate to the project location on the map (below) and click to place a marker and obtain the XY coordinates.

- The "Find Me" button will provide the lat/long for the person filling out this form. Then pan the map to the correct location and click the map to place a marker and obtain the XY coordinates.

**Navigate to your location and click on the map to get the X,Y coordinates**

41.422785536027035,-74.42419174133911

**Project Details****2. What is the nature of this project?**

New Construction

**3. Select the predominant land use for both pre and post development conditions.****Pre-Development Existing Landuse**

Forest

**Post-Development Future Land Use**

Commercial

**3a. If Single Family Subdivision was selected in question 3, enter the number of subdivision lots.**

NONE PROVIDED

---

4. In accordance with the larger common plan of development or sale, enter the total project site acreage, the acreage to be disturbed and the future impervious area (acreage)within the disturbed area.

\*\*\* ROUND TO THE NEAREST TENTH OF AN ACRE. \*\*\*

**Total Site Area (acres)**

11.66

**Total Area to be Disturbed (acres)**

8.6

**Existing Impervious Area to be Disturbed (acres)**

0.25

**Future Impervious Area Within Disturbed Area (acres)**

5.85

**5. Do you plan to disturb more than 5 acres of soil at any one time?**

Yes

**6. Indicate the percentage (%) of each Hydrologic Soil Group(HSG) at the site.**

**A (%)**

0

**B (%)**

0

**C (%)**

0

**D (%)**

100

**7. Is this a phased project?**

No

**8. Enter the planned start and end dates of the disturbance activities.**

**Start Date**

07/01/2023

**End Date**

12/31/2024

**9. Identify the nearest surface waterbody(ies) to which construction site runoff will discharge.**

ON SITE FEDERAL WETLAND

**9a. Type of waterbody identified in question 9?**

Wetland/Federal Jurisdiction On Site (Answer 9b)

**Other Waterbody Type Off Site Description**

NONE PROVIDED

**9b. If "wetland" was selected in 9A, how was the wetland identified?**

Delineated by Consultant

**10. Has the surface waterbody(ies in question 9 been identified as a 303(d) segment in Appendix E of GP-0-20-001?**

Yes

**11. Is this project located in one of the Watersheds identified in Appendix C of GP-0-20-001?**

No

**12. Is the project located in one of the watershed areas associated with AA and AA-S classified waters?**

No

**If No, skip question 13.**

**13. Does this construction activity disturb land with no existing impervious cover and where the Soil Slope Phase is identified as D (provided the map unit name is inclusive of slopes greater than 25%), E or F on the USDA Soil Survey?**

NONE PROVIDED

**If Yes, what is the acreage to be disturbed?**

NONE PROVIDED

**14. Will the project disturb soils within a State regulated wetland or the protected 100 foot adjacent area?**

No

**15. Does the site runoff enter a separate storm sewer system (including roadside drains, swales, ditches, culverts, etc)?**

No

**16. What is the name of the municipality/entity that owns the separate storm sewer system?**

NONE PROVIDED

**17. Does any runoff from the site enter a sewer classified as a Combined Sewer?**

No

**18. Will future use of this site be an agricultural property as defined by the NYS Agriculture and Markets Law?**

No

**19. Is this property owned by a state authority, state agency, federal government or local government?**

No

**20. Is this a remediation project being done under a Department approved work plan? (i.e. CERCLA, RCRA, Voluntary Cleanup Agreement, etc.)**

No



## **Required SWPPP Components**

**21. Has the required Erosion and Sediment Control component of the SWPPP been developed in conformance with the current NYS Standards and Specifications for Erosion and Sediment Control (aka Blue Book)?**

Yes

**22. Does this construction activity require the development of a SWPPP that includes the post-construction stormwater management practice component (i.e. Runoff Reduction, Water Quality and Quantity Control practices/techniques)?**

Yes

**If you answered No in question 22, skip question 23 and the Post-construction Criteria and Post-construction SMP Identification sections.**

**23. Has the post-construction stormwater management practice component of the SWPPP been developed in conformance with the current NYS Stormwater Management Design Manual?**

Yes

**24. The Stormwater Pollution Prevention Plan (SWPPP) was prepared by:**  
Professional Engineer (P.E.)

**SWPPP Preparer**

Colliers Engineering & Design CT, PC

**Contact Name (Last, Space, First)**

Cory Robinson

**Mailing Address**

555 Hudson Valley Ave Ste 101

**City**

New Windsor

**State**

NY

**Zip**

12553

**Phone**

8455644495

**Email**

cory.robinson@collierseng.com

**Download SWPPP Preparer Certification Form**

Please take the following steps to prepare and upload your preparer certification form:

- 1) Click on the link below to download a blank certification form

- 2) The certified SWPPP preparer should sign this form
- 3) Scan the signed form
- 4) Upload the scanned document

[Download SWPPP Preparer Certification Form](#)

**Please upload the SWPPP Preparer Certification**

NONE PROVIDED  
**Comment**  
 NONE PROVIDED

**Erosion & Sediment Control Criteria**

**25. Has a construction sequence schedule for the planned management practices been prepared?**

Yes

**26. Select all of the erosion and sediment control practices that will be employed on the project site:**

**Temporary Structural**

- Check Dams
- Dust Control
- Sediment Basin
- Sediment Traps
- Silt Fence
- Stabilized Construction Entrance
- Temporary Swale

**Biotechnical**

- Brush Matting

**Vegetative Measures**

- Brush Matting
- Mulching
- Seeding
- Temporary Swale
- Topsoiling

**Permanent Structural**

- Land Grading
- Retaining Wall
- Rock Outlet Protection

**Other**

NONE PROVIDED

**Post-Construction Criteria**

**\* IMPORTANT: Completion of Questions 27-39 is not required if response to Question 22 is No.**

**27. Identify all site planning practices that were used to prepare the final site plan/layout for the project.**

NONE PROVIDED

**27a. Indicate which of the following soil restoration criteria was used to address the requirements in Section 5.1.6("Soil Restoration") of the Design Manual (2010 version).**

All disturbed areas will be restored in accordance with the Soil Restoration requirements in Table 5.3 of the Design Manual (see page 5-22).

**28. Provide the total Water Quality Volume (WQv) required for this project (based on final site plan/layout). (Acre-feet)**

0.65

**29. Post-construction SMP Identification**

Use the Post-construction SMP Identification section to identify the RR techniques (Area Reduction), RR techniques(Volume Reduction) and Standard SMPs with RRv Capacity that were used to reduce the Total WQv Required (#28).

Identify the SMPs to be used by providing the total impervious area that contributes runoff to each technique/practice selected. For the Area Reduction Techniques, provide the total contributing area (includes pervious area) and, if applicable, the total impervious area that contributes runoff to the technique/practice.

Note: Redevelopment projects shall use the Post-Construction SMP Identification section to identify the SMPs used to treat and/or reduce the WQv required. If runoff reduction techniques will not be used to reduce the required WQv, skip to question 33a after identifying the SMPs.

**30. Indicate the Total RRv provided by the RR techniques (Area/Volume Reduction) and Standard SMPs with RRv capacity identified in question 29. (acre-feet)**

0.15

**31. Is the Total RRv provided (#30) greater than or equal to the total WQv required (#28)?**

No

**If Yes, go to question 36. If No, go to question 32.**

**32. Provide the Minimum RRv required based on HSG. [Minimum RRv Required = (P) (0.95) (Ai) / 12, Ai=(s) (Aic)] (acre-feet)**

0.124

**32a. Is the Total RRv provided (#30) greater than or equal to the Minimum RRv Required (#32)?**

Yes

**If Yes, go to question 33.**

Note: Use the space provided in question #39 to summarize the specific site limitations and justification for not reducing 100% of WQv required (#28). A detailed evaluation of the specific site limitations and justification for not reducing 100% of the WQv required (#28) must also be included in the SWPPP.

If No, sizing criteria has not been met; therefore, NOI can not be processed. SWPPP preparer must modify design to meet sizing criteria.

### 33. SMPs

Use the Post-construction SMP Identification section to identify the Standard SMPs and, if applicable, the Alternative SMPs to be used to treat the remaining total WQv (=Total WQv Required in #28 - Total RRv Provided in #30).

Also, provide the total impervious area that contributes runoff to each practice selected.

NOTE: Use the Post-construction SMP Identification section to identify the SMPs used on Redevelopment projects.

**33a. Indicate the Total WQv provided (i.e. WQv treated) by the SMPs identified in question #33 and Standard SMPs with RRv Capacity identified in question #29. (acre-feet)**

0.65

Note: For the standard SMPs with RRv capacity, the WQv provided by each practice = the WQv calculated using the contributing drainage area to the practice - provided by the practice. (See Table 3.5 in Design Manual)

**34. Provide the sum of the Total RRv provided (#30) and the WQv provided (#33a).**

0.80

**35. Is the sum of the RRv provided (#30) and the WQv provided (#33a) greater than or equal to the total WQv required (#28)?**

Yes

If Yes, go to question 36.

If No, sizing criteria has not been met; therefore, NOI can not be processed. SWPPP preparer must modify design to meet sizing criteria.

**36. Provide the total Channel Protection Storage Volume (CPv required and provided or select waiver (#36a), if applicable.**

**CPv Required (acre-feet)**

NONE PROVIDED

**CPv Provided (acre-feet)**

NONE PROVIDED

**36a. The need to provide channel protection has been waived because:**

Reduction of the total CPv is achieved on site through runoff reduction techniques or infiltration systems.

**37. Provide the Overbank Flood (Qp) and Extreme Flood (Qf) control criteria or select waiver (#37a), if applicable.**

**Overbank Flood Control Criteria (Qp)**

**Pre-Development (CFS)**

17.57

**Post-Development (CFS)**

15.77

**Total Extreme Flood Control Criteria (Qf)**

**Pre-Development (CFS)**

40.06

**Post-Development (CFS)**

39.68

**37a. The need to meet the Qp and Qf criteria has been waived because:**

NONE PROVIDED

**38. Has a long term Operation and Maintenance Plan for the post-construction stormwater management practice(s) been developed?**

Yes

**If Yes, Identify the entity responsible for the long term Operation and Maintenance**

Dewpoint North LLC

**39. Use this space to summarize the specific site limitations and justification for not reducing 100% of WQv required (#28). (See question #32a) This space can also be used for other pertinent project information.**

-preservation of wetland areas limited available area for development and stormwater ponds

-challenging topography requires significant earthwork further limiting areas available for stormwater infiltration ponds due to fill conditions

-shallow groundwater and unfavorable soils for infiltration prohibit infiltration practices around the site

## **Post-Construction SMP Identification**

### **Runoff Reduction (RR) Techniques, Standard Stormwater Management Practices (SMPs) and Alternative SMPs**

Identify the Post-construction SMPs to be used by providing the total impervious area that contributes runoff to each technique/practice selected. For the Area Reduction Techniques, provide the total contributing area (includes pervious area) and, if applicable, the total impervious area that contributes runoff to the technique/practice.

### **RR Techniques (Area Reduction)**

---

Round to the nearest tenth

**Total Contributing Acres for Conservation of Natural Area (RR-1)**

NONE PROVIDED

**Total Contributing Impervious Acres for Conservation of Natural Area (RR-1)**

NONE PROVIDED

**Total Contributing Acres for Sheetflow to Riparian Buffers/Filter Strips (RR-2)**

NONE PROVIDED

**Total Contributing Impervious Acres for Sheetflow to Riparian Buffers/Filter Strips (RR-2)**

NONE PROVIDED

**Total Contributing Acres for Tree Planting/Tree Pit (RR-3)**

NONE PROVIDED

**Total Contributing Impervious Acres for Tree Planting/Tree Pit (RR-3)**

NONE PROVIDED

**Total Contributing Acres for Disconnection of Rooftop Runoff (RR-4)**

NONE PROVIDED

**RR Techniques (Volume Reduction)**

---

**Total Contributing Impervious Acres for Disconnection of Rooftop Runoff (RR-4)**

NONE PROVIDED

**Total Contributing Impervious Acres for Vegetated Swale (RR-5)**

NONE PROVIDED

**Total Contributing Impervious Acres for Rain Garden (RR-6)**

NONE PROVIDED

**Total Contributing Impervious Acres for Stormwater Planter (RR-7)**

NONE PROVIDED

**Total Contributing Impervious Acres for Rain Barrel/Cistern (RR-8)**

NONE PROVIDED

**Total Contributing Impervious Acres for Porous Pavement (RR-9)**

NONE PROVIDED

**Total Contributing Impervious Acres for Green Roof (RR-10)**

NONE PROVIDED

**Standard SMPs with RRv Capacity**

---

**Total Contributing Impervious Acres for Infiltration Trench (I-1)**

NONE PROVIDED

**Total Contributing Impervious Acres for Infiltration Basin (I-2)**

NONE PROVIDED

**Total Contributing Impervious Acres for Dry Well (I-3)**

NONE PROVIDED

**Total Contributing Impervious Acres for Underground Infiltration System (I-4)**

NONE PROVIDED

**Total Contributing Impervious Acres for Bioretention (F-5)**

3.28

**Total Contributing Impervious Acres for Dry Swale (O-1)**

NONE PROVIDED

**Standard SMPs**

---

**Total Contributing Impervious Acres for Micropool Extended Detention (P-1)**

NONE PROVIDED

**Total Contributing Impervious Acres for Wet Pond (P-2)**

NONE PROVIDED

**Total Contributing Impervious Acres for Wet Extended Detention (P-3)**

NONE PROVIDED

**Total Contributing Impervious Acres for Multiple Pond System (P-4)**

NONE PROVIDED

**Total Contributing Impervious Acres for Pocket Pond (P-5)**

NONE PROVIDED

**Total Contributing Impervious Acres for Surface Sand Filter (F-1)**

NONE PROVIDED

**Total Contributing Impervious Acres for Underground Sand Filter (F-2)**

NONE PROVIDED

**Total Contributing Impervious Acres for Perimeter Sand Filter (F-3)**

NONE PROVIDED

**Total Contributing Impervious Acres for Organic Filter (F-4)**

NONE PROVIDED

**Total Contributing Impervious Acres for Shallow Wetland (W-1)**

NONE PROVIDED

**Total Contributing Impervious Acres for Extended Detention Wetland (W-2)**

NONE PROVIDED

**Total Contributing Impervious Acres for Pond/Wetland System (W-3)**

NONE PROVIDED

**Total Contributing Impervious Acres for Pocket Wetland (W-4)**

NONE PROVIDED

**Total Contributing Impervious Acres for Wet Swale (O-2)**

NONE PROVIDED

**Alternative SMPs (DO NOT INCLUDE PRACTICES BEING USED FOR PRETREATMENT ONLY)**

---

**Total Contributing Impervious Area for Hydrodynamic**

NONE PROVIDED

**Total Contributing Impervious Area for Wet Vault**

NONE PROVIDED

**Total Contributing Impervious Area for Media Filter**

2.51

**"Other" Alternative SMP?**

NONE PROVIDED

**Total Contributing Impervious Area for "Other"**

NONE PROVIDED

**Provide the name and manufacturer of the alternative SMPs (i.e. proprietary practice(s)) being used for WQv treatment.**

**Note: Redevelopment projects which do not use RR techniques, shall use questions 28, 29, 33 and 33a to provide SMPs used, total WQv required and total WQv provided for the project.**

**Manufacturer of Alternative SMP**

Contech Engineered Solutions LLC

**Name of Alternative SMP**

JELLYFISH FILTER

**Other Permits**



**40. Identify other DEC permits, existing and new, that are required for this project/facility.**

None

**If SPDES Multi-Sector GP, then give permit ID**

NONE PROVIDED

**If Other, then identify**

NONE PROVIDED

**41. Does this project require a US Army Corps of Engineers Wetland Permit?**

No

**If "Yes," then indicate Size of Impact, in acres, to the nearest tenth**

NONE PROVIDED

**42. If this NOI is being submitted for the purpose of continuing or transferring coverage under a general permit for stormwater runoff from construction activities, please indicate the former SPDES number assigned.**

NONE PROVIDED

### **MS4 SWPPP Acceptance**

**43. Is this project subject to the requirements of a regulated, traditional land use control MS4?**

Yes - Please attach the MS4 Acceptance form below

**If No, skip question 44**

**44. Has the "MS4 SWPPP Acceptance" form been signed by the principal executive officer or ranking elected official and submitted along with this NOI?**

No

#### **MS4 SWPPP Acceptance Form Download**

Download form from the link below. Complete, sign, and upload.

[MS4 SWPPP Acceptance Form](#)

#### **MS4 Acceptance Form Upload**

NONE PROVIDED

**Comment**

NONE PROVIDED

### **Owner/Operator Certification**

#### **Owner/Operator Certification Form Download**

Download the certification form by clicking the link below. Complete, sign, scan, and upload the form.

[Owner/Operator Certification Form \(PDF, 45KB\)](#)

**Upload Owner/Operator Certification Form**

NONE PROVIDED
<b>Comment</b>
NONE PROVIDED

## Appendix 6 | Draft Notice of Termination (N.O.T.)

**New York State Department of Environmental Conservation  
 Division of Water  
 625 Broadway, 4th Floor  
 Albany, New York 12233-3505**

\*(NOTE: Submit completed form to address above)\*

**NOTICE OF TERMINATION for Storm Water Discharges Authorized  
 under the SPDES General Permit for Construction Activity**

**Please indicate your permit identification number:** NYR \_\_\_\_\_

**I. Owner or Operator Information**

1. Owner/Operator Name:

2. Street Address:

3. City/State/Zip:

4. Contact Person:

4a. Telephone:

4b. Contact Person E-Mail:

**II. Project Site Information**

5. Project/Site Name:

6. Street Address:

7. City/Zip:

8. County:

**III. Reason for Termination**

9a.  All disturbed areas have achieved final stabilization in accordance with the general permit and SWPPP. \*Date final stabilization completed (month/year): \_\_\_\_\_

9b.  Permit coverage has been transferred to new owner/operator. Indicate new owner/operator's permit identification number: NYR \_\_\_\_\_

(Note: Permit coverage can not be terminated by owner identified in I.1. above until new owner/operator obtains coverage under the general permit)

9c.  Other (Explain on Page 2)

**IV. Final Site Information:**

10a. Did this construction activity require the development of a SWPPP that includes post-construction stormwater management practices?  yes  no (If no, go to question 10f.)

10b. Have all post-construction stormwater management practices included in the final SWPPP been constructed?  yes  no (If no, explain on Page 2)

10c. Identify the entity responsible for long-term operation and maintenance of practice(s)?

\_\_\_\_\_

**NOTICE OF TERMINATION for Storm Water Discharges Authorized under the  
SPDES General Permit for Construction Activity - continued**

10d. Has the entity responsible for long-term operation and maintenance been given a copy of the operation and maintenance plan required by the general permit?     yes     no

10e. Indicate the method used to ensure long-term operation and maintenance of the post-construction stormwater management practice(s):

- Post-construction stormwater management practice(s) and any right-of-way(s) needed to maintain practice(s) have been deeded to the municipality.
- Executed maintenance agreement is in place with the municipality that will maintain the post-construction stormwater management practice(s).
- For post-construction stormwater management practices that are privately owned, a mechanism is in place that requires operation and maintenance of the practice(s) in accordance with the operation and maintenance plan, such as a deed covenant in the owner or operator's deed of record.
- For post-construction stormwater management practices that are owned by a public or private institution (e.g. school, university or hospital), government agency or authority, or public utility; policy and procedures are in place that ensures operation and maintenance of the practice(s) in accordance with the operation and maintenance plan.

10f. Provide the total area of impervious surface (i.e. roof, pavement, concrete, gravel, etc.) constructed within the disturbance area? \_\_\_\_\_  
(acres)

11. Is this project subject to the requirements of a regulated, traditional land use control MS4?     yes  
 no  
(If Yes, complete section VI - "MS4 Acceptance" statement)

**V. Additional Information/Explanation:**  
(Use this section to answer questions 9c. and 10b., if applicable)

**VI. MS4 Acceptance - MS4 Official (principal executive officer or ranking elected official) or Duly Authorized Representative** (Note: Not required when 9b. is checked -transfer of coverage)

I have determined that it is acceptable for the owner or operator of the construction project identified in question 5 to submit the Notice of Termination at this time.

Printed Name:

Title/Position:

Signature:

Date:

**NOTICE OF TERMINATION** for Storm Water Discharges Authorized under the  
**SPDES General Permit for Construction Activity - continued**

**VII. Qualified Inspector Certification - Final Stabilization:**

I hereby certify that all disturbed areas have achieved final stabilization as defined in the current version of the general permit, and that all temporary, structural erosion and sediment control measures have been removed. Furthermore, I understand that certifying false, incorrect or inaccurate information is a violation of the referenced permit and the laws of the State of New York and could subject me to criminal, civil and/or administrative proceedings.

Printed Name:

Title/Position:

Signature:

Date:

**VIII. Qualified Inspector Certification - Post-construction Stormwater Management Practice(s):**

I hereby certify that all post-construction stormwater management practices have been constructed in conformance with the SWPPP. Furthermore, I understand that certifying false, incorrect or inaccurate information is a violation of the referenced permit and the laws of the State of New York and could subject me to criminal, civil and/or administrative proceedings.

Printed Name:

Title/Position:

Signature:

Date:

**IX. Owner or Operator Certification**

I hereby certify that this document was prepared by me or under my direction or supervision. My determination, based upon my inquiry of the person(s) who managed the construction activity, or those persons directly responsible for gathering the information, is that the information provided in this document is true, accurate and complete. Furthermore, I understand that certifying false, incorrect or inaccurate information is a violation of the referenced permit and the laws of the State of New York and could subject me to criminal, civil and/or administrative proceedings.

Printed Name:

Title/Position:

Signature:

Date:

# Appendix 7 | Draft MS4 Acceptance Form



Department of  
Environmental  
Conservation

NYS Department of Environmental Conservation  
Division of Water  
625 Broadway, 4th Floor  
Albany, New York 12233-3505

**MS4 Stormwater Pollution Prevention Plan (SWPPP) Acceptance  
Form**

for

**Construction Activities Seeking Authorization Under SPDES General Permit**  
\*(NOTE: Attach Completed Form to Notice Of Intent and Submit to Address Above)

**I. Project Owner/Operator Information**

1. Owner/Operator Name:

2. Contact Person:

3. Street Address:

4. City/State/Zip:

**II. Project Site Information**

5. Project/Site Name:

6. Street Address:

7. City/State/Zip:

**III. Stormwater Pollution Prevention Plan (SWPPP) Review and Acceptance Information**

8. SWPPP Reviewed by:

9. Title/Position:

10. Date Final SWPPP Reviewed and Accepted:

**IV. Regulated MS4 Information**

11. Name of MS4:

12. MS4 SPDES Permit Identification Number: NYR20A

13. Contact Person:

14. Street Address:

15. City/State/Zip:

16. Telephone Number:



**MS4 SWPPP Acceptance Form - continued**

**V. Certification Statement - MS4 Official (principal executive officer or ranking elected official) or Duly Authorized Representative**

I hereby certify that the final Stormwater Pollution Prevention Plan (SWPPP) for the construction project identified in question 5 has been reviewed and meets the substantive requirements in the SPDES General Permit For Stormwater Discharges from Municipal Separate Storm Sewer Systems (MS4s).  
Note: The MS4, through the acceptance of the SWPPP, assumes no responsibility for the accuracy and adequacy of the design included in the SWPPP. In addition, review and acceptance of the SWPPP by the MS4 does not relieve the owner/operator or their SWPPP preparer of responsibility or liability for errors or omissions in the plan.

Printed Name:

Title/Position:

Signature:

Date:

**VI. Additional Information**

## Appendix 8 | NRCS Hydrologic Soil Mapping



United States  
Department of  
Agriculture

**NRCS**

Natural  
Resources  
Conservation  
Service

A product of the National  
Cooperative Soil Survey,  
a joint effort of the United  
States Department of  
Agriculture and other  
Federal agencies, State  
agencies including the  
Agricultural Experiment  
Stations, and local  
participants

# Custom Soil Resource Report for Orange County, New York



# Preface

---

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist ([http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2\\_053951](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951)).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

alternative means for communication of program information (Braille, large print, audiotape, etc.) should contact USDA's TARGET Center at (202) 720-2600 (voice and TDD). To file a complaint of discrimination, write to USDA, Director, Office of Civil Rights, 1400 Independence Avenue, S.W., Washington, D.C. 20250-9410 or call (800) 795-3272 (voice) or (202) 720-6382 (TDD). USDA is an equal opportunity provider and employer.

# Contents

---

<b>Preface</b> .....	2
<b>How Soil Surveys Are Made</b> .....	5
<b>Soil Map</b> .....	8
Soil Map.....	9
Legend.....	10
Map Unit Legend.....	11
Map Unit Descriptions.....	11
Orange County, New York.....	13
ErB—Erie gravelly silt loam, 3 to 8 percent slopes.....	13
MdB—Mardin gravelly silt loam, 3 to 8 percent slopes.....	14
MdC—Mardin gravelly silt loam, 8 to 15 percent slopes.....	15
<b>References</b> .....	18

# How Soil Surveys Are Made

---

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

## Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and



## Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

---

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

# Custom Soil Resource Report Soil Map




Soil Map may not be valid at this scale.

Map Scale: 1:2,050 if printed on A landscape (11" x 8.5") sheet.  
0 30 60 120 180 Meters  
0 50 100 200 300 Feet  
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84


### MAP LEGEND

**Area of Interest (AOI)**

 Area of Interest (AOI)




















**Soils**







 Soil Map Unit Polygons

 Soil Map Unit Lines


 Soil Map Unit Points

**Special Point Features**






-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features


**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Orange County, New York  
 Survey Area Data: Version 21, Jun 11, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Data not available.

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
ErB	Erie gravelly silt loam, 3 to 8 percent slopes	6.1	46.4%
MdB	Mardin gravelly silt loam, 3 to 8 percent slopes	0.7	5.2%
MdC	Mardin gravelly silt loam, 8 to 15 percent slopes	6.4	48.4%
<b>Totals for Area of Interest</b>		<b>13.2</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

## Custom Soil Resource Report

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## Orange County, New York

### ErB—Erie gravelly silt loam, 3 to 8 percent slopes

#### Map Unit Setting

*National map unit symbol:* 9vv9

*Elevation:* 100 to 1,390 feet

*Mean annual precipitation:* 42 to 52 inches

*Mean annual air temperature:* 46 to 52 degrees F

*Frost-free period:* 135 to 215 days

*Farmland classification:* Farmland of statewide importance

#### Map Unit Composition

*Erie and similar soils:* 80 percent

*Minor components:* 20 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Erie

##### Setting

*Landform:* Till plains, drumlinoid ridges, hills

*Landform position (two-dimensional):* Footslope, summit

*Landform position (three-dimensional):* Base slope

*Down-slope shape:* Concave

*Across-slope shape:* Linear

*Parent material:* Loamy till derived from siltstone, sandstone, shale, and limestone

##### Typical profile

*H1 - 0 to 9 inches:* gravelly silt loam

*H2 - 9 to 18 inches:* channery silt loam

*H3 - 18 to 54 inches:* channery silt loam

*H4 - 54 to 70 inches:* channery silt loam

##### Properties and qualities

*Slope:* 3 to 8 percent

*Depth to restrictive feature:* 10 to 21 inches to fragipan

*Drainage class:* Somewhat poorly drained

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to moderately high (0.06 to 0.20 in/hr)

*Depth to water table:* About 6 to 18 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Calcium carbonate, maximum content:* 15 percent

*Available water capacity:* Very low (about 2.4 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 3w

*Hydrologic Soil Group:* D

*Ecological site:* F144AY037MA - Moist Dense Till Uplands

*Hydric soil rating:* No

#### Minor Components

##### Bath

*Percent of map unit:* 5 percent

## Custom Soil Resource Report

*Hydric soil rating:* No

### **Mardin**

*Percent of map unit:* 5 percent

*Hydric soil rating:* No

### **Alden**

*Percent of map unit:* 5 percent

*Landform:* Depressions

*Hydric soil rating:* Yes

### **Wurtsboro**

*Percent of map unit:* 5 percent

*Hydric soil rating:* No

## **MdB—Mardin gravelly silt loam, 3 to 8 percent slopes**

### **Map Unit Setting**

*National map unit symbol:* 2v30j

*Elevation:* 330 to 2,460 feet

*Mean annual precipitation:* 31 to 70 inches

*Mean annual air temperature:* 39 to 52 degrees F

*Frost-free period:* 105 to 180 days

*Farmland classification:* Farmland of statewide importance

### **Map Unit Composition**

*Mardin and similar soils:* 85 percent

*Minor components:* 15 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### **Description of Mardin**

#### **Setting**

*Landform:* Hills, mountains

*Landform position (two-dimensional):* Summit, shoulder

*Landform position (three-dimensional):* Interfluve, side slope

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Parent material:* Loamy till

#### **Typical profile**

*Ap - 0 to 8 inches:* gravelly silt loam

*Bw - 8 to 15 inches:* gravelly silt loam

*E - 15 to 20 inches:* gravelly silt loam

*Bx - 20 to 72 inches:* gravelly silt loam

#### **Properties and qualities**

*Slope:* 3 to 8 percent

*Surface area covered with cobbles, stones or boulders:* 0.0 percent

*Depth to restrictive feature:* 14 to 26 inches to fragipan

*Drainage class:* Moderately well drained



## Custom Soil Resource Report

*Capacity of the most limiting layer to transmit water (Ksat):* Very low to moderately low (0.00 to 0.14 in/hr)

*Depth to water table:* About 13 to 24 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Available water capacity:* Low (about 3.6 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 2w

*Hydrologic Soil Group:* D

*Ecological site:* F144AY008CT - Moist Till Uplands

*Hydric soil rating:* No

### Minor Components

#### Volusia

*Percent of map unit:* 5 percent

*Landform:* Hills, mountains

*Landform position (two-dimensional):* Footslope, summit

*Landform position (three-dimensional):* Base slope, interflue, side slope

*Down-slope shape:* Concave

*Across-slope shape:* Linear

*Hydric soil rating:* No

#### Bath

*Percent of map unit:* 5 percent

*Landform:* Hills, mountains

*Landform position (two-dimensional):* Backslope, shoulder

*Landform position (three-dimensional):* Interflue, side slope

*Down-slope shape:* Concave

*Across-slope shape:* Linear

*Hydric soil rating:* No

#### Lordstown

*Percent of map unit:* 5 percent

*Landform:* Mountains, hills

*Landform position (two-dimensional):* Summit, shoulder

*Landform position (three-dimensional):* Mountaintop, interflue, crest

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Hydric soil rating:* No

## MdC—Mardin gravelly silt loam, 8 to 15 percent slopes

### Map Unit Setting

*National map unit symbol:* 2v30l

*Elevation:* 330 to 2,460 feet

*Mean annual precipitation:* 31 to 70 inches

*Mean annual air temperature:* 39 to 52 degrees F

*Frost-free period:* 105 to 180 days

## Custom Soil Resource Report

*Farmland classification:* Farmland of statewide importance

### Map Unit Composition

*Mardin and similar soils:* 85 percent

*Minor components:* 15 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Mardin

#### Setting

*Landform:* Hills, mountains

*Landform position (two-dimensional):* Shoulder, backslope

*Landform position (three-dimensional):* Interfluve, side slope

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Parent material:* Loamy till

#### Typical profile

*Ap - 0 to 8 inches:* gravelly silt loam

*Bw - 8 to 15 inches:* gravelly silt loam

*E - 15 to 20 inches:* gravelly silt loam

*Bx - 20 to 72 inches:* gravelly silt loam

#### Properties and qualities

*Slope:* 8 to 15 percent

*Surface area covered with cobbles, stones or boulders:* 0.0 percent

*Depth to restrictive feature:* 14 to 26 inches to fragipan

*Drainage class:* Moderately well drained

*Capacity of the most limiting layer to transmit water (Ksat):* Very low to moderately low (0.00 to 0.14 in/hr)

*Depth to water table:* About 13 to 24 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Available water capacity:* Low (about 3.6 inches)

#### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 3e

*Hydrologic Soil Group:* D

*Ecological site:* F144AY008CT - Moist Till Uplands

*Hydric soil rating:* No

### Minor Components

#### Volusia

*Percent of map unit:* 5 percent

*Landform:* Hills, mountains

*Landform position (two-dimensional):* Footslope, summit

*Landform position (three-dimensional):* Base slope, interfluve, side slope

*Down-slope shape:* Concave

*Across-slope shape:* Linear

*Hydric soil rating:* No

#### Lordstown

*Percent of map unit:* 5 percent

*Landform:* Mountains, hills

*Landform position (two-dimensional):* Backslope

## Custom Soil Resource Report

*Landform position (three-dimensional):* Mountainflank, side slope, nose slope

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Hydric soil rating:* No

### **Bath**

*Percent of map unit:* 5 percent

*Landform:* Hills, mountains

*Landform position (two-dimensional):* Backslope

*Landform position (three-dimensional):* Nose slope, side slope

*Down-slope shape:* Linear

*Across-slope shape:* Linear

*Hydric soil rating:* No

# References

---

- American Association of State Highway and Transportation Officials (AASHTO). 2004. Standard specifications for transportation materials and methods of sampling and testing. 24th edition.
- American Society for Testing and Materials (ASTM). 2005. Standard classification of soils for engineering purposes. ASTM Standard D2487-00.
- Cowardin, L.M., V. Carter, F.C. Golet, and E.T. LaRoe. 1979. Classification of wetlands and deep-water habitats of the United States. U.S. Fish and Wildlife Service FWS/OBS-79/31.
- Federal Register. July 13, 1994. Changes in hydric soils of the United States.
- Federal Register. September 18, 2002. Hydric soils of the United States.
- Hurt, G.W., and L.M. Vasilas, editors. Version 6.0, 2006. Field indicators of hydric soils in the United States.
- National Research Council. 1995. Wetlands: Characteristics and boundaries.
- Soil Survey Division Staff. 1993. Soil survey manual. Soil Conservation Service. U.S. Department of Agriculture Handbook 18. [http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2\\_054262](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2_054262)
- Soil Survey Staff. 1999. Soil taxonomy: A basic system of soil classification for making and interpreting soil surveys. 2nd edition. Natural Resources Conservation Service, U.S. Department of Agriculture Handbook 436. [http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2\\_053577](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2_053577)
- Soil Survey Staff. 2010. Keys to soil taxonomy. 11th edition. U.S. Department of Agriculture, Natural Resources Conservation Service. [http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2\\_053580](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2_053580)
- Tiner, R.W., Jr. 1985. Wetlands of Delaware. U.S. Fish and Wildlife Service and Delaware Department of Natural Resources and Environmental Control, Wetlands Section.
- United States Army Corps of Engineers, Environmental Laboratory. 1987. Corps of Engineers wetlands delineation manual. Waterways Experiment Station Technical Report Y-87-1.
- United States Department of Agriculture, Natural Resources Conservation Service. National forestry manual. [http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/home/?cid=nrcs142p2\\_053374](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/home/?cid=nrcs142p2_053374)
- United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. <http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/landuse/rangepasture/?cid=stelprdb1043084>

## Custom Soil Resource Report

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. [http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2\\_054242](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2_054242)

United States Department of Agriculture, Natural Resources Conservation Service. 2006. Land resource regions and major land resource areas of the United States, the Caribbean, and the Pacific Basin. U.S. Department of Agriculture Handbook 296. [http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2\\_053624](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2_053624)

United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. [http://www.nrcs.usda.gov/Internet/FSE\\_DOCUMENTS/nrcs142p2\\_052290.pdf](http://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/nrcs142p2_052290.pdf)

# Appendix 9 | Construction Site Log Book

STATE POLLUTANT DISCHARGE ELIMINATION SYSTEM FOR CONSTRUCTION  
ACTIVITIES

CONSTRUCTION SITE LOG BOOK

Table of Contents

- I. Pre-Construction Meeting Documents
  - a. Preamble to Site Assessment and Inspections
  - b. Operator's Certification
  - c. Qualified Professional's Credentials & Certification
  - d. Pre-Construction Site Assessment Checklist
  
- II. Construction Duration Inspections
  - a. Directions
  - b. Modification to the SWPPP
  
- III. Monthly Summary Reports
  
- IV. Monitoring, Reporting, and Three-Month Status Reports
  - a. Operator's Compliance Response Form

Properly completing forms such as those contained in Appendix H meet the inspection requirement of NYS-DEC SPDES GP for Construction Activities. Completed forms shall be kept on site at all times and made available to authorities upon request.

## I. PRE-CONSTRUCTION MEETING DOCUMENTS

Project Name \_\_\_\_\_  
Permit No. \_\_\_\_\_ Date of Authorization \_\_\_\_\_  
Name of Operator \_\_\_\_\_  
Prime Contractor \_\_\_\_\_

### a. Preamble to Site Assessment and Inspections

The Following Information To Be Read By All Person's Involved in The Construction of Stormwater Related Activities:

The Operator agrees to have a qualified professional<sup>1</sup> conduct an assessment of the site prior to the commencement of construction<sup>2</sup> and certify in this inspection report that the appropriate erosion and sediment controls described in the SWPPP have been adequately installed or implemented to ensure overall preparedness of the site for the commencement of construction.

Prior to the commencement of construction, the Operator shall certify in this site logbook that the SWPPP has been prepared in accordance with the State's standards and meets all Federal, State and local erosion and sediment control requirements.

When construction starts, site inspections shall be conducted by the qualified professional at least every 7 calendar days and within 24 hours of the end of a storm event of 0.5 inches or greater (Construction Duration Inspections). The Operator shall maintain a record of all inspection reports in this site logbook. The site logbook shall be maintained on site and be made available to the permitting authorities upon request. The Operator shall post at the site, in a publicly accessible location, a summary of the site inspection activities on a monthly basis (Monthly Summary Report).

The operator shall also prepare a written summary of compliance with this general permit at a minimum frequency of every three months (Operator's Compliance Response Form), while coverage exists. The summary should address the status of achieving each component of the SWPPP.

Prior to filing the Notice of Termination or the end of permit term, the Operator shall have a qualified professional perform a final site inspection. The qualified professional shall certify that the site has undergone final stabilization<sup>3</sup> using either vegetative or structural stabilization methods and that all temporary erosion and sediment controls (such as silt fencing) not needed for long-term erosion control have been removed. In addition, the Operator must identify and certify that all permanent structures described in the SWPPP have been constructed and provide the owner(s) with an operation and maintenance plan that ensures the structure(s) continuously functions as designed.

1 "Qualified Professional means a person knowledgeable in the principles and practice of erosion and sediment controls, such as a Certified Professional in Erosion and Sediment Control (CPESC), soil scientist, licensed engineer or someone working under the direction and supervision of a licensed engineer (person must have experience in the principles and practices of erosion and sediment control).

2 "Commencement of construction" means the initial removal of vegetation and disturbance of soils associated with clearing, grading or excavating activities or other construction activities.

3 "Final stabilization" means that all soil-disturbing activities at the site have been completed and a uniform, perennial vegetative cover with a density of eighty (80) percent has been established or equivalent stabilization measures (such as the use of mulches or geotextiles) have been employed on all unpaved areas and areas not covered by permanent structures.



**b. Operators Certification**

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. Further, I hereby certify that the SWPPP meets all Federal, State, and local erosion and sediment control requirements. I am aware that false statements made herein are punishable as a class A misdemeanor pursuant to Section 210.45 of the Penal Law.

**Name (please print):** \_\_\_\_\_

**Title** \_\_\_\_\_ **Date:** \_\_\_\_\_

**Address:** \_\_\_\_\_

**Phone:** \_\_\_\_\_ **Email:** \_\_\_\_\_

**Signature:** \_\_\_\_\_

**c. Qualified Professional's Credentials & Certification**

"I hereby certify that I meet the criteria set forth in the General Permit to conduct site inspections for this project and that the appropriate erosion and sediment controls described in the SWPPP and as described in the following Pre-construction Site Assessment Checklist have been adequately installed or implemented, ensuring the overall preparedness of this site for the commencement of construction."

**Name (please print):** \_\_\_\_\_

**Title** \_\_\_\_\_ **Date:** \_\_\_\_\_

**Address:** \_\_\_\_\_

**Phone:** \_\_\_\_\_ **Email:** \_\_\_\_\_

**Signature:** \_\_\_\_\_

**d. Pre-construction Site Assessment Checklist**

**(NOTE: Provide comments below as necessary)**

**1. Notice of Intent, SWPPP, and Contractors Certification:**

**Yes No NA**

- Has a Notice of Intent been filed with the NYS Department of Conservation?
- Is the SWPPP on-site? Where? \_\_\_\_\_
- Is the Plan current? What is the latest revision date? \_\_\_\_\_
- Is a copy of the NOI (with brief description) onsite? Where? \_\_\_\_\_
- Have all contractors involved with stormwater related activities signed a contractor's certification?

**2. Resource Protection**

**Yes No NA**

- Are construction limits clearly flagged or fenced?
- Important trees and associated rooting zones, on-site septic system absorption fields, existing vegetated areas suitable for filter strips, especially in perimeter areas, have been flagged for protection.
- Creek crossings installed prior to land-disturbing activity, including clearing and blasting.

**3. Surface Water Protection**

**Yes No NA**

- Clean stormwater runoff has been diverted from areas to be disturbed.
- Bodies of water located either on site or in the vicinity of the site have been identified and protected.
- Appropriate practices to protect on-site or downstream surface water are installed.
- Are clearing and grading operations divided into areas <5 acres?

**4. Stabilized Construction Entrance**

**Yes No NA**

- A temporary construction entrance to capture mud and debris from construction vehicles before they enter the public highway has been installed.
- Other access areas (entrances, construction routes, equipment parking areas) are stabilized immediately as work takes place with gravel or other cover.
- Sediment tracked onto public streets is removed or cleaned on a regular basis.

**5. Perimeter Sediment Controls**

**Yes No NA**

- Silt fence material and installation comply with the standard drawing and specifications.
- Silt fences are installed at appropriate spacing intervals
- Sediment/detention basin was installed as first land disturbing activity.
- Sediment traps and barriers are installed.

**6. Pollution Prevention for Waste and Hazardous Materials**

**Yes No NA**

- The Operator or designated representative has been assigned to implement the spill prevention avoidance and response plan.
- The plan is contained in the SWPPP on page \_\_\_\_\_
- Appropriate materials to control spills are onsite. Where? \_\_\_\_\_

## II. CONSTRUCTION DURATION INSPECTIONS

### a. Directions:

**Inspection Forms will be filled out during the entire construction phase of the project.**

Required Elements:

- (1) On a site map, indicate the extent of all disturbed site areas and drainage pathways. Indicate site areas that are expected to undergo initial disturbance or significant site work within the next 14-day period;
- (2) Indicate on a site map all areas of the site that have undergone temporary or permanent stabilization;
- (3) Indicate all disturbed site areas that have not undergone active site work during the previous 14-day period;
- (4) Inspect all sediment control practices and record the approximate degree of sediment accumulation as a percentage of sediment storage volume (for example, 10 percent, 20 percent, 50 percent);
- (5) Inspect all erosion and sediment control practices and record all maintenance requirements such as verifying the integrity of barrier or diversion systems (earthen berms or silt fencing) and containment systems (sediment basins and sediment traps). Identify any evidence of rill or gully erosion occurring on slopes and any loss of stabilizing vegetation or seeding/mulching. Document any excessive deposition of sediment or ponding water along barrier or diversion systems. Record the depth of sediment within containment structures, any erosion near outlet and overflow structures, and verify the ability of rock filters around perforated riser pipes to pass water; and
- (6) Immediately report to the Operator any deficiencies that are identified with the implementation of the SWPPP.

**SITE PLAN/SKETCH**

\_\_\_\_\_  
**Inspector (print name)**

\_\_\_\_\_  
**Date of Inspection**

\_\_\_\_\_  
**Qualified Professional (print name)**

\_\_\_\_\_  
**Qualified Professional Signature**

The above signed acknowledges that, to the best of his/her knowledge, all information provided on the forms is accurate and complete.

**Maintaining Water Quality****Yes No NA**

- Is there an increase in turbidity causing a substantial visible contrast to natural conditions?
- Is there residue from oil and floating substances, visible oil film, or globules or grease?
- All disturbance is within the limits of the approved plans.
- Have receiving lake/bay, stream, and/or wetland been impacted by silt from project?

**Housekeeping****1. General Site Conditions****Yes No NA**

- Is construction site litter and debris appropriately managed?
- Are facilities and equipment necessary for implementation of erosion and sediment control in working order and/or properly maintained?
- Is construction impacting the adjacent property?
- Is dust adequately controlled?

**2. Temporary Stream Crossing****Yes No NA**

- Maximum diameter pipes necessary to span creek without dredging are installed.
- Installed non-woven geotextile fabric beneath approaches.
- Is fill composed of aggregate (no earth or soil)?
- Rock on approaches is clean enough to remove mud from vehicles & prevent sediment from entering stream during high flow.

**Runoff Control Practices****1. Excavation Dewatering****Yes No NA**

- Upstream and downstream berms (sandbags, inflatable dams, etc.) are installed per plan.
- Clean water from upstream pool is being pumped to the downstream pool.
- Sediment laden water from work area is being discharged to a silt-trapping device.
- Constructed upstream berm with one-foot minimum freeboard.

**2. Level Spreader****Yes No NA**

- Installed per plan.
- Constructed on undisturbed soil, not on fill, receiving only clear, non-sediment laden flow.
- Flow sheets out of level spreader without erosion on downstream edge.

**3. Interceptor Dikes and Swales****Yes No NA**

- Installed per plan with minimum side slopes 2H:1V or flatter.
- Stabilized by geotextile fabric, seed, or mulch with no erosion occurring.
- Sediment-laden runoff directed to sediment trapping structure

**Runoff Control Practices (continued)**

**4. Stone Check Dam**

**Yes No NA**

- Is channel stable? (flow is not eroding soil underneath or around the structure).
- Check is in good condition (rocks in place and no permanent pools behind the structure).
- Has accumulated sediment been removed?.

**5. Rock Outlet Protection**

**Yes No NA**

- Installed per plan.
- Installed concurrently with pipe installation.

**Soil Stabilization**

**1. Topsoil and Spoil Stockpiles**

**Yes No NA**

- Stockpiles are stabilized with vegetation and/or mulch.
- Sediment control is installed at the toe of the slope.

**2. Revegetation**

**Yes No NA**

- Temporary seedings and mulch have been applied to idle areas.
- 4 inches minimum of topsoil has been applied under permanent seedings

**Sediment Control Practices**

**1. Stabilized Construction Entrance**

**Yes No NA**

- Stone is clean enough to effectively remove mud from vehicles.
- Installed per standards and specifications?
- Does all traffic use the stabilized entrance to enter and leave site?
- Is adequate drainage provided to prevent ponding at entrance?

**2. Silt Fence**

**Yes No NA**

- Installed on Contour, 10 feet from toe of slope (not across conveyance channels).
  - Joints constructed by wrapping the two ends together for continuous support.
  - Fabric buried 6 inches minimum.
  - Posts are stable, fabric is tight and without rips or frayed areas.
- Sediment accumulation is \_\_\_\_% of design capacity.

**Sediment Control Practices (continued)****3. Storm Drain Inlet Protection (Use for Stone & Block; Filter Fabric; Curb; or, Excavated practices)****Yes No NA**

- Installed concrete blocks lengthwise so open ends face outward, not upward.
- Placed wire screen between No. 3 crushed stone and concrete blocks.
- Drainage area is 1 acre or less.
- Excavated area is 900 cubic feet.
- Excavated side slopes should be 2:1.
- 2" x 4" frame is constructed and structurally sound.
- Posts 3-foot maximum spacing between posts.
- Fabric is embedded 1 to 1.5 feet below ground and secured to frame/posts with staples at max 8-inch spacing.
- Posts are stable, fabric is tight and without rips or frayed areas.
- Sediment accumulation \_\_\_% of design capacity.

**4. Temporary Sediment Trap****Yes No NA**

- Outlet structure is constructed per the approved plan or drawing.
- Geotextile fabric has been placed beneath rock fill.
- Sediment accumulation is \_\_\_% of design capacity.

**5. Temporary Sediment Basin****Yes No NA**

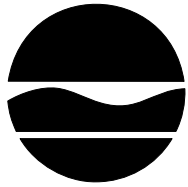
- Basin and outlet structure constructed per the approved plan.
- Basin side slopes are stabilized with seed/mulch.
- Drainage structure flushed and basin surface restored upon removal of sediment basin facility.
- Sediment accumulation is \_\_\_% of design capacity.

Note: Not all erosion and sediment control practices are included in this listing. Add additional pages to this list as required by site specific design. Construction inspection checklists for post-development stormwater management practices can be found in Appendix F of the New York Stormwater Management Design Manual.





# Appendix 10 | NYSDEC Construction Stormwater Inspection Manual



**NEW YORK STATE DEPARTMENT OF  
ENVIRONMENTAL CONSERVATION**

---

**Construction Stormwater Inspection Manual**  
**Primarily for Government Inspectors Evaluating Compliance with Construction  
Stormwater Control Requirements**

**New York State  
Department of Environmental Conservation**

# TABLE OF CONTENTS

Version 1.05 (8/27/07)

<u>Section</u>	<u>Content</u>	<u>Page</u>
<b>1.0</b>	<b>INTRODUCTION AND PURPOSE</b>	1
1.1	Compliance Inspections	1
1.2	Self-inspections	2
<b>2.0</b>	<b>PRE-INSPECTION ACTIVITIES</b>	3
2.1	Regulatory Oversight Authorities	3
2.2	Permittee's Self-inspector	5
<b>3.0</b>	<b>ON-SITE INSPECTION ACTIVITIES</b>	5
3.1	Compliance Inspections	5
3.2	Non-permitted Site Inspections	9
3.3	Self-inspections	9
<b>4.0</b>	<b>POST-INSPECTION ACTIVITIES</b>	10
4.1	Regulatory Oversight Authorities	10
4.2	Permittee's Self-inspections	11

## ATTACHMENTS

Attachment 1 - Compliance Inspection Form	12
Attachment 2 - Unpermitted Site Notice	14
Attachment 3 - Example Inspection Letter	15

## **1.0 INTRODUCTION AND PURPOSE**

The New York State Department of Environmental Conservation Division of Water (DOW) considers there to be two types of inspections germane to construction stormwater; compliance inspections and self-inspections.

This manual is for use by DOW and other regulatory oversight construction stormwater inspectors in performing compliance inspections, as well as for site operators in performing self inspections. The manual should be used in conjunction with the *New York State Standards and Specifications for Erosion and Sediment Control*, August 2005.

### **1.1 Compliance Inspections**

Regulatory compliance inspections are performed by regulatory oversight authorities such as DOW staff, or representatives of DOW and local municipal construction stormwater inspectors. These inspections are intended to determine compliance with the state or local requirements for control of construction stormwater through erosion and sediment control and post construction practices. Compliance inspections focus on determinations of compliance with legal and water quality standards. Typically, compliance inspections can be further sub-categorized to include comprehensive inspections, and follow-up or reconnaissance inspections.

Compliance inspectors will focus on determining whether:

- the project is causing water quality standard violations;
- the required Stormwater Pollution Prevention Plan (SWPPP) includes appropriate erosion and sediment controls and, to some extent, post construction controls;
- the owner/operator is complying with the SWPPP;
- where required, self-inspections are being properly performed; and
- where self-inspections are required, the owner/operator responds appropriately to the self-inspector's reports.

#### **1.1.1 Comprehensive Inspection**

Comprehensive inspections are designed to verify permittee compliance with all applicable regulatory requirements, effluent controls, and compliance schedules. This inspection involves records reviews, visual observations, and evaluations of management practices, effluents, and receiving waters.

Comprehensive inspections should be conducted according to a neutral or random inspection scheme, or in accordance with established priorities. A neutral monitoring scheme provides some objective basis for scheduling inspections and sampling visits by establishing a system (whether complex factor-based, alphabetic, or geographic) for setting priorities to ensure that a particular facility is not unfairly selected for inspection or sampling. The selection of which

facility to inspect must be made without bias to ensure that the regulatory oversight authority, if challenged for being arbitrary and capricious manner, can reasonably defend itself.

A neutral inspection scheme should set the criteria the inspector uses to choose which facilities to inspect, but the schedule for the actual inspection should remain confidential, and may be kept separate from the neutral plan.

A routine comprehensive compliance inspection is most effective when it is unannounced or conducted with very little advance warning.

### 1.1.2 Reconnaissance Inspection

A reconnaissance inspection is performed in lieu of, or following a comprehensive inspection to obtain a preliminary overview of an owner/operator's compliance program, to respond to a citizen complaint, or to assess a non-permitted site. The inspector performs a brief (generally about an hour) visual inspection of the site, discharges and receiving waters. A reconnaissance inspection uses the inspector's experience and judgement to summarize potential compliance problems, without conducting a full comprehensive inspection. The objective of a reconnaissance inspection is to expand inspection coverage without increasing inspection resource expenditures. The reconnaissance inspection is the shortest and least resource intensive of all inspections.

Reconnaissance inspections may be initiated in response to known or suspected violations, a public complaint, a violation of regulatory requirements, or as follow-up to verify that necessary actions were taken in response to a previous inspection.

## 1.2 Self-inspections

For some projects, the site owner/operator is required by their State Pollutant Discharge Elimination System (SPDES) Permit and/or local requirements to have a qualified professional<sup>1</sup> perform a "self-inspection" at the site. In self-inspections, the qualified professional determines whether the site is being managed in accordance with the SWPPP, and whether the SWPPP's recommended erosion and sediment controls are effective. If activities are not in accordance with the SWPPP, or if the SWPPP erosion and sediment controls are not effective, the qualified professional inspecting the site recommends corrections to the owner/operator.

---

<sup>1</sup> A "Qualified professional" is a person knowledgeable in the principles and practice of erosion and sediment controls, such as a licensed professional engineer, Certified Professional in Erosion and Sediment Control (CPESC), licensed landscape architect or soil scientist.

## 2.0 PRE-INSPECTION ACTIVITIES

### 2.1 Regulatory Oversight Authorities

This section is intended for inspectors with regulatory oversight authority such as agents of the DOW or a local municipality, or others acting on their behalf, such as county Soil and Water Conservation District staff. Examples of other regulatory oversight authorities include: the United States Environmental Protection Agency (EPA); New York City Department of Environmental Protection (DEP), Adirondack Park Agency (APA); the Lake George Park Commission (LGPC), and the Skaneateles Lake Watershed Authority (SLWA). Before arriving on-site to conduct the inspection, considerations concerning communication, documentation and equipment must be made.

Regulatory oversight authority is granted by state or local law to government agencies or, depending upon the particular law, an authorized representative of state or local government. SPDES rules 6 NYCRR 750-2.3 and Environmental Conservation Law 17-0303(6) and 17-0829(a) all allow for authorized representatives of the (NYSDEC) commissioner to perform all the duties of an inspector.

#### 2.1.1 Communication

##### Coordination with Other Entities

Where appropriate, prior to selecting sites for inspection, compliance inspectors should communicate with other regulatory oversight authorities to avoid unnecessary duplication or to coordinate follow-up to inspections performed by other regulatory oversight authorities.

##### Announced vs. Unannounced Inspection

Inspections may be announced or unannounced. Each method has its own advantages and disadvantages. Unannounced inspections are preferred, however many job sites are not continuously manned, or not always staffed by someone who is familiar with the SWPPP, thus necessitating an announced inspection. As an alternative, when an announced inspection is necessary, inspectors should try to give as little advanced warning as possible (24 hours is suggested).

##### Itinerary

For obvious safety reasons, inspectors should be sure to inform someone in their office which site or sites they will be visiting prior to leaving the to perform inspections.

#### 2.1.2 Documentation

##### Data Review

The inspector should review any available information such as:

- Notice of Intent
- Stormwater Pollution Prevention Plan
- Past inspection records
- Phasing plan

- Construction sequence
- Inspection and Maintenance schedules
- Site specific issues
- Consent Orders
- Access agreements

### Inspection Form

The inspector should have copies of, and be familiar with, the inspection form used by their regulatory oversight authority (example in Attachment 1) before leaving the office. Static information such as name, location and permit number can be entered onto the inspection form prior to arriving at the inspection site.

### Credentials

Inspectors should always carry proper identification to prove that they are employed by an entity with jurisdictional authority. Failure to display proper credentials may be legal grounds for denial of entry to a site.

### 2.1.3 Equipment

#### Personal Protective Equipment

DOW employees must conform to the DOW Health and Safety policy as it relates to personal protective equipment. Other regulatory oversight authorities should have their own safety policies or, if not, may wish to consult the OSHA health and safety tool at: [www.osha.gov/dep/etools/ehasp/](http://www.osha.gov/dep/etools/ehasp/) to develop a health and safety plan.

The following is a list of some of the most common health and safety gear that may be needed:

- Hard hat (Class G, Type I or better)
- Safety toe shoes
- Reflective vest
- Hearing protection (to achieve 85 dBA - 8 hr TWA)
- Safety glasses with side shields

If the construction is on an industrial site or a hazardous waste site, special training may be required prior to entering the site. The inspector should consult with OSHA or NYSDEC prior to entering such a site.

#### Monitoring Equipment

The following is a list of some equipment that may be helpful to document facts and verify compliance:

- Digital Camera
- Measuring tape or wheel
- Hand level or clinometer
- Turbidity meter (in limited circumstances)

## 2.2 Permittee's Self-inspection

This section is intended for qualified professionals who conduct site self-inspections on behalf of owner/operators. Self-inspectors are responsible for performing inspections in accordance with permit requirements and reporting to site owners and operators the results and any recommendations resulting from the inspection.

Prior to conducting inspections, qualified professionals should ensure familiarity with the Stormwater Pollution Prevention Plan and previous inspection reports.

## 3.0 ON-SITE INSPECTION PROCESS

### 3.1 Compliance Inspections

#### 3.1.1 Professionalism

*Don't Pretend to Possess Knowledge*

**Unless the inspector has experience with a particular management practice, do not pretend to possess knowledge.** Inspectors cannot be expert in all areas; their job is to collect information, not to demonstrate superior wisdom. Site operators are often willing to talk to someone who is inquisitive and interested. Within reason, asking questions to obtain new information about a management practice, construction technique or piece of equipment is one of the inspector's main roles in an inspection.

*Don't Recommend Solutions*

**The inspector should not recommend solutions or endorse products.** The solution to a compliance problem may appear obvious based on the inspector's experience. However, the responsibility should be placed on the site owner to implement a workable solution to a compliance problem that meets NYSDEC standards. The inspector should refer the site operator to the New York Standards and Specifications for Erosion and Sediment Control (the Blue Book) or the New York State Stormwater Management Design Manual (the Design Manual).

Key advice must be offered carefully. One experienced stormwater inspector suggests saying: "I can't direct you or make recommendations, but what we've seen work in other situations is ..."

The way inspectors present themselves is important to the effectiveness of the inspection. An inspector cannot be overly familiar, but will be more effective if able to establish a minimum level of communication.

#### 3.1.2 Safety

DOW employees must conform to Division health and safety policies when on a construction site. Other regulatory oversight authorities should have their own safety policies or, if not, may



wish to consult the OSHA health and safety tool at:

[www.osha.gov/dep/etools/ehasp](http://www.osha.gov/dep/etools/ehasp) to develop a health and safety plan.

Some general protections for construction sites are:

- Beware of heavy equipment, avoid operator blind spots and make sure of operator eye contact around heavy equipment.
- Avoid walking on rock rip-rap if possible. Loose rock presents a slip hazard.
- Stay out of confined spaces like tanks, trenches and foundation holes.
- Avoid lightning danger. Monitor weather conditions, get out of water, avoid open areas and high points, do not huddle in groups or near trees.
- Protect yourself from sun and heat exposure. Use sun screen or shading clothing. Remain hydrated by drinking water, watching for signs of heat cramps, exhaustion (fatigue, nausea, dizziness, headache, cool or moist skin), or stroke (high body temperature; red, hot and dry skin)
- Protect yourself from cold weather. Wear multiple layers of thin clothing. Wear a warm hat. Drink warm fluids or eat hot foods, and keep dry.
- Avoid scaffolding in excess of 4 feet above grade.
- Beware of ticks, stinging insects, snakes and poison ivy or sumac.

### 3.1.3 Legal access

DOW has general powers, set forth under ECL 17-0303, subparagraph 6, to enter premises for inspections. In addition, ECL 3-0301.2 conveys general statutory authority granting the DOW the power to access private property to fulfill DOW obligations under the law.

ECL 15-0305 gives the DOW the authority to enter at all times in or upon any property, public or private, for the purpose of inspecting or investigating conditions affecting the construction of improvements to or developments of water resources for the public health, safety or welfare.

ECL 17-0829 allows an authorized DOW representative, upon presentation of their credentials, to enter upon any premises where any effluent source is located, or in which records are required to be maintained. The representative may at reasonable times have access to, and sample discharges/pollutants to the waters or to publicly owned treatment plants where the effluent source is located. This subparagraph provides DOW representatives performing their duties authority to enter a site to pursue administrative violations. Pursuing criminal violations may require a warrant or the owner's permission to enter the site.

For sites that are permitted, DOW has authority under the permit to enter the site.

If the owner/operator's representatives onsite deny access, the inspector *should not* physically force entry. Under these circumstances the attorney representing the inspector should be immediately notified and consideration should be given to soliciting the aid of a law officer to obtain entry.

DOW staff have the right to enter at any reasonable time. If no one is available, and the site is fenced or posted, DOW staff should make all reasonable efforts to identify, contact and notify the owner that the DOW is entering the site. If the inspector has made all reasonable efforts to contact site owners, but was unable to do so, the site can then be accessed. All efforts should be taken not to cause any damage to the facility.

Other regulatory oversight authorities should seek advice on their legal authorities to enter a job site. Municipalities that have adopted Article 6 of the New York State Sample Local Law for Stormwater Management and Erosion and Sediment Control (NYSDEC, 2004, updated 2006) will have legal authority to enter sites in accordance with that chapter and any other existing municipal authority .

Agents of DOW have authority similar DOW staff authority to enter sites. However, DOW staff enjoy significant personal liability protections as state employees. That liability protection may not be the same for authorized representatives of DOW. For authorized representatives of DOW (or other regulatory oversight authorities), it is prudent to obtain permission to enter the site. If such permission is denied, the authorized representatives should inform the appropriate DOW contact, usually the regional water manager.

#### 3.1.4 Find the Legally Responsible Party (Construction Manager, Self-inspector)

The first action a compliance inspector should take upon entering a construction site is to find the construction trailer or the construction or project manager if they are available. The inspector should present appropriate identification to the site's responsible party and state the reason for the inspection; construction stormwater complaint response or neutral construction stormwater inspection. If the inspection is initiated as a response to a complaint, frequently the responsible party will ask who made the complaint. DOW keeps private individual complainants confidential. If the complainant is another regulatory oversight authority, DOW tends to make that known to the site's responsible party.

#### 3.1.5 On-site records review (NOI, SWPPP, Self-inspection Reports, Permit)

Generally, the compliance inspector should next review the on-site records. Verify that a copy of the construction stormwater permit and NOI are on-site. Verify that the acreage, site conditions, and receiving water listed on the NOI are accurate. Compare the on-site documentation with documentation already submitted to, or obtained by the compliance inspector.

If the SWPPP has not been reviewed in the office, verify that it exists and contains the minimum required components (16 for a basic plan and 22 for a full plan). On-site review of the SWPPP should determine if: there is an appropriate phasing plan; the acreage disturbed in each phase, construction sequence for each phase; proposed implementation of erosion and sediment control measures; and, where required, post construction controls. For each of the erosion and sediment control practices, the SWPPP must show design details in accordance with the NYS Standards for Erosion and Sediment Controls. The SWPPP must also include provisions for maintenance of practices during construction. On-site review of post construction controls is generally limited to verification that the proposed stormwater management practices are shown on the site plan.

Where self-inspections are required, self-inspection reports are a significant tool for the compliance inspector to determine the performance history of the site. The self-inspection reports should be done with the required frequency. Self-inspection reports must include all the details required by the permit. Generally, it is desirable for permit information to be shown on a site plan. The compliance inspector should become familiar with the report and use that familiarity to judge whether the self-inspections are being performed correctly and that the site operator is correcting deficiencies noted in the report.

### 3.1.6 Walk the Site

During wet weather conditions, it may be advantageous to observe the receiving waters prior to walking the rest of the site. At some point during the inspection, the receiving water conditions must be observed and noted. It is critical to note if there is a substantial visible contrast to natural conditions, or evidence of deposition, streambank erosion, construction debris or waste materials (e.g. concrete washdown) in the receiving stream.

Each inspector should evaluate actual implementation and maintenance of practices on-site compared to how implementation and maintenance is detailed in the SWPPP. At a minimum, the compliance inspector should observe all areas of active construction. Observing equipment or materials storage, recently stabilized areas, or stockpile areas is also appropriate to evaluate the effectiveness of management practices.

### 3.1.7 Taking Photographs

Evidence of poor receiving water conditions and poor or ineffective practices should be documented with digital photographs. Those photographs should be logged date stamped and stored on media that cannot be edited (e.g. write only CDs). Photos should also be appended to the site inspector's report.

It is also beneficial to take photographs of good practices for educational and technology transfer reasons.

### 3.1.8 Exit Interview

Clearly communicate expectations and consequences. If it is clear from the inspection that the owner/operator must modify the SWPPP, or modify management practices within an assigned period (e.g. 24 hours, 48 hours, one week, two weeks), then that finding should be communicated at the time of the exit interview. The inspector should assign the period based on factors such as how long it would reasonably take to complete such modifications and the level of risk to water quality associated with failure to make such modifications.

The inspector should make clear that NYSDEC reserves rights to future enforcement actions. If the inspector's supervisor or enforcement coordinator determines additional enforcement actions are necessary, the inspector *should not* reassure the owner/operator that the current situation is acceptable.

### **3.2 Non-permitted Site Inspections**

For sites not authorized in accordance with state or local laws, the process will be abbreviated. First verify the need for authorization and observe receiving waters to detect water quality standard violations. If there is a violation, notify the owner of the violation or other compliance actions in response to their illicit activity. For DOW staff, Attachment 2 or a similar notice can be used to notify the site owner/operator that stormwater authorization is required.

### **3.3 Self-inspections**

The role of the self-inspector is to verify that the site is complying with stormwater requirements. In particular, the self-inspector verifies that the SWPPP is being properly implemented. The self-inspector also documents SWPPP implementation so regulatory agencies can review implementation activities.

**It is not the role of the self-inspector to report directly to regulatory authorities.**

Appendix H of *The New York Standards and Specifications for Erosion and Sediment Control* - August 2005 (the Blue Book) includes a Construction Duration Inspection checklist that can be used by the owner/operators qualified professional for self-inspections. The Blue Book is available on the NYSDEC website.

#### **3.3.1 Purpose**

The self inspector should ensure that the project's SWPPP is being properly implemented. This includes ensuring that the erosion and sediment control practices are properly installed and being maintained in accordance with the SWPPP/Blue Book.

The project must be properly phased to limit the disturbance to less than five acres, and the construction sequence for each phase must be followed. The SWPPP must also be modified to address evolving circumstances. Finally, and most importantly, receiving waters must be protected.

If a soil disturbance will be greater than five acres at any given time, the site operator must obtain written permission from the DOW regional office.

#### **3.3.2 Pre-construction Conference**

The parties responsible for various aspects of stormwater compliance should be identified at the pre-construction conference. Responsible parties may include, but are not limited to, owner's engineer, owner/operator/permittee, contractors, and subcontractors.

Typical responsibilities include: installation of erosion and sediment control (E & SC) practices; maintenance of E & SC practices, inspection of E&SC practices, installation of post construction stormwater management practices (SMPs), inspection of post construction SMPs, SWPPP revisions, and contractor direction.

All parties should clearly know what is expected of them. Responsible parties should complete the Pre-construction Site Assessment Checklist provided in Appendix H of the Blue Book.

### 3.3.3 Inspection Preparation

The inspector should review the project's SWPPP (including the phasing plan, construction sequence and site specific issues) and the last few inspection reports (if the inspector has them available).

### 3.3.4 Self-inspection Components

#### Inspect installation, performance and maintenance of all E&SC practices

The self inspector should inspect all areas that are under active construction or disturbance and areas that are vulnerable to erosion. The self-inspector should also inspect areas that will be disturbed prior to the next inspection for measures required prior to construction (e.g. silt barriers, stabilized construction entrance, diversions). Finally, self-inspectors should inspect post-construction controls during and after installation.

#### Identify site deficiencies and corrective measures

The self-inspector's reports must be maintained in a log book on site and the log book must be made available to the regulatory authorities. Although the legal responsibility for filing a Notice of Termination lies with the owner/operator, the self-inspector may also be called upon to perform a final site inspection, including post construction SMPs, prior to filing the Notice of Termination.

## **4.0 POST-INSPECTION ACTIVITIES**

### **4.1 Regulatory Oversight Authorities**

This section is intended for inspectors with regulatory oversight authority such as agents of the DOW or a local municipality, or others acting on their behalf (such as County Soil and Water Conservation District staff.) Upon completion of an inspection, inspection results should be documented for the record.

#### 4.1.1 Written Notification

The inspector should inform the permittee or the on-site representative of their inspection results in writing by sending the permittee a complete, signed copy of the inspection report. The inspection report should be transmitted under a cover letter which elaborates on any deficiencies noted in the inspection report. It is not a good idea to commend exceptional efforts by the owner/operator in a letter, because such letters tend to undermine enforcement efforts when compliance status at a site degrades.

The inspector should consider providing a copy of the cover letter and inspection report to other parties with including:

- Permittee
- Contractor(s)
- Other regulatory oversight authorities
- Other parties present during the inspection (e.g. SWPPP preparer, permittee's self-inspector, etc.)

For DOW staff, an example of the inspection cover letter is included as Attachment 3.

#### 4.1.2 Inspection Tracking

DOW staff must enter their inspection results into the electronic *Water Compliance System*.

Local municipalities and other regulatory oversight authorities are encouraged to develop an electronic tracking system in which to record their inspections.

### 4.2 Permittee's Self-inspections

This section is intended for qualified professionals who conduct site inspections for permittees in accordance with a SPDES permit or local requirements.

#### 4.2.1 Written Records

##### Inspection Reports

The inspector shall prepare a written report summarizing inspection results. The inspection report is then provided to the permittee, or the permittee's duly authorized representative, and to the contractor responsible for implementing stormwater controls on-site in order to correct deficiencies noted in the inspection report. Finally, the inspection report must be added to the site log book that is required to be maintained on-site, and be available to regulatory oversight authorities for review.

#### 4.2.2 Stormwater Pollution Prevention Plan Revisions

The inspector must inform the permittee of his/her duty to amend the Stormwater Pollution Prevention Plan (SWPPP) whenever an inspection proves the SWPPP to be ineffective in:

- Eliminating or significantly minimizing pollutants from on-site sources
- Achieving the general objectives of controlling pollutants in stormwater discharges from permitted construction activity
- Eliminating discharges that cause a substantial visible contrast to natural conditions



**Water Quality Observations**

Describe the discharge(s) [source(s), impact on receiving water(s), etc.] \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Describe the quality of the receiving water(s) both upstream and downstream of the discharge \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Describe any other water quality standards or permit violations \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Additional Comments: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

Photographs attached



## ATTACHMENT 2

### \*\*\*\* NOTICE \*\*\*\*

On March 10, 2003, provisions of the Federal Clean Water Act went into effect that apply to many construction operations.

If your construction operations result in the disturbance of one acre or greater and stormwater runoff from your site reaches surface waters (i.e., lake, stream, road side ditch, swale, storm sewer system, etc.), the stormwater runoff from your site must be covered by a State Pollutant Discharge Elimination System (SPDES) Permit issued by the New York State Department of Environmental Conservation (NYSDEC).

To facilitate your compliance with the law, NYSDEC has issued a General Permit which may be applicable to your project. To obtain coverage under this General Permit, you need to prepare a Stormwater Pollution Prevention Plan (SWPPP) and then file a Notice of Intent (NOI) to the NYSDEC headquarters in Albany. The NOI form is available on the DEC website. You may also obtain a copy of the NOI form at the nearest NYSDEC regional offices.

When you file your NOI you are certifying that you have developed a SWPPP and that it will be implemented prior to commencing construction. When you submit the NOI you need to indicate if your SWPPP is in conformance with published NYSDEC technical standards; if it is, your SPDES permit coverage will be effective in as few as five business days. If your SWPPP does not conform to the DEC technical standards, coverage will not be available for at least 60 business days.

#### **Failure to have the required permit can result in legal actions which include Stop Work Orders and/or monetary penalties of up to \$37,500/day**

If your construction operations are already in progress and you are not covered by an appropriate NYSDEC permit contact the NYSDEC Regional Water Engineer as soon as possible. If your construction field operations have not yet commenced, review the NOI and the General Permit on the DEC's website or at the DEC regional office for your area. When you are comfortable that you understand and comply with the requirements, file your NOI.

The requirement to file an NOI does not replace any local requirements. Developers/Contractors are directed to contact the Local Code Enforcement Officer or Stormwater Management Officer for local requirements.

## ATTACHMENT 3

<< Date >>

Mr. John Smith  
123 Main Street  
Ferracane, NY 12345

**Re: Stormwater Inspection  
SPDES Permit Identification No. NYR10Z000 (through SPDES No. GP-02-01)  
Blowing Leaves Subdivision  
Gasper (T), Eaton (Co.)**

Dear Mr. Smith:

On the afternoon of << date >> I conducted an inspection of the construction activities associated with the Blowing Leaves Subdivision located on County Route 1 in the town of Gasper, Eaton County. The inspection was conducted in the presence of you and Mr. Samuel Siltfence of Acme Excavating Co., Inc. The purpose of the inspection was to verify compliance with the *State Pollutant Discharge Elimination System (SPDES) General Permit for Storm Water Discharges from Construction Activity* ("the general permit").

The overall rating for the project at the time of the inspection was *unsatisfactory*. A copy of my inspection report is attached for your information. In addition to the report, I would like to elaborate on the following:

### SPDES Authority

- In accordance with subdivision 750-2.1 (a) of Title 6 of the Official Compilation of Codes, Rules, and Regulations of the State of New York (6 NYCRR), a copy of your permit must be retained at the construction site. You did not have a copy of the general permit at the site. **Your failure to retain a copy of the general permit at the construction site is a violation of 6 NYCRR Part 750-2.1 (a).** Please retain a copy of the general permit at the site from this point forward.

### SWPPP Content

- In accordance with Part III.E.2. of the general permit, contractors and subcontractors must certify that they understand the terms and conditions of the general permit and the SWPPP before undertaking any construction activity at the site. Your SWPPP does not include a certification statement from Acme Excavating Co., Inc. **The failure of your contractor to sign this certification before undertaking construction activity at the site is a violation of Part III.E.2. of the general permit.** Please obtain copies of all necessary certifications and provide copies of them to each party who holds a copy of your SWPPP.
- In accordance with Part V.H.2. of the general permit, SWPPP's must be certified by the permittee. Your SWPPP was not certified by you. **Your failure to certify your SWPPP is a**

Mr. John Smith  
Re: SPDES Inspection  
Blowing Leaves Subdivision  
Gasper (T), Eaton (Co.)

<< Date >>

**violation of Part V.H.2. of the general permit.** Please certify your SWPPP.

### **Recordkeeping**

- In accordance with Parts III.D.3.a. and III.D.3.b. of the general permit, permittees must have a qualified professional conduct site inspections within 24 hours of the end of 0.5" or greater rain events and at least once per week. A review of your records revealed that your "self-inspections" are only being conducted about two or three times per month. **Your failure to have a qualified professional conduct inspections at the required frequency is a violation of Part III.D.3.b. of the general permit.** Please immediately direct your qualified professional to conduct your site inspections at the required frequency.
- Although the frequency of self-inspections does not meet requirements, the quality of them is very good. Your qualified professional has accurately noted the same SWPPP deficiencies and necessary maintenance activities that I also observed, and prepared thorough sketches on the self-inspection site maps.
- In accordance with Part V.H.2. of the general permit, the permittee must certify all reports required by the permit. A review of your records showed that your self-inspection reports were not certified. **Your failure to certify your self-inspection reports is a violation of Part V.H.2. of the general permit.** Please sign and certify any and all existing and future self-inspection reports.

### **Visual Observations**

- In accordance with Parts III.A.2. and III.A.3. of the general permit, all erosion and sediment controls (E&SC) measures must be installed (as detailed in the SWPPP) prior to the initiation of construction. During the inspection, I noted all of your E&SC measures have been correctly installed at the right times and locations.
- In accordance with Part V.L. of the general permit, all of the E&SC measures at your site must be maintained properly. While on site I observed that, among other things, the section of silt fence in place parallel to County Route 1 is in various stages of disrepair. **The failure of your contractor to adequately maintain the E&SC measures currently in place at your site is a violation of Part V.L of the general permit.** Please direct your contractor to repair this silt fence immediately and to diligently maintain all of the other required E&SC measures as they are brought to his attention by your qualified professional.
- This inspection was conducted during a rain event which resulted in a stormwater discharge to the municipal separate storm sewer system (MS4) being operated by the Eaton County Department of Public Works. Your discharge was visibly turbid whereas upstream water MS4 was clear. As a result, the discharge from the MS4 outfall into Karimipour Creek was causing

Mr. John Smith

<< Date >>

Re: SPDES Inspection  
Blowing Leaves Subdivision  
Gasper (T), Eaton (Co.)

slight turbidity. Please be advised that the narrative water quality standard for turbidity in Karimipour Creek is “no increase that will cause a substantial visible contrast to natural conditions.” I attribute the lack of maintenance of your E&SC measures to be the primary cause of the turbid discharge. Please be reminded that the general permit does not authorize you cause or contribute to a condition in contravention of any water quality standards.

If you have any questions or comments, please feel free to contact me at (999) 456-5432.

Sincerely,

Hector D. Inspector, CPESC  
Environmental Program Specialist 2

HDI:ms  
Attachment

cc w/att.: Chester Checkdam, (T) Gasper Code Enforcement Officer  
Samuel Siltfence, Acme Excavating Co., Inc.

# Appendix 11 | Contractor Certification Form



# Appendix 12 | NYSDEC Deep-Ripping & Decompaction Manual



New York State  
**DEPARTMENT OF ENVIRONMENTAL CONSERVATION**

Division of Water

---

# **Deep-Ripping and Decompaction**

---

**April 2008**

New York State  
**Department of Environmental Conservation**



Document Prepared by:

John E. Lacey,  
Land Resource Consultant and Environmental Compliance Monitor  
(Formerly with the Division of Agricultural Protection and Development Services,  
NYS Dept. of Agriculture & Markets)

## Alternative Stormwater Management Deep-Ripping and Decompaction

### Description

The two-phase practice of 1) “Deep Ripping;” and 2) “Decompaction” (deep subsoiling), of the soil material as a step in the cleanup and restoration/landscaping of a construction site, helps mitigate the physically induced impacts of soil compression; i.e.: soil compaction or the substantial increase in the bulk density of the soil material.

Deep Ripping and Decompaction are key factors which help in restoring soil pore space and permeability for water infiltration. Conversely, the physical actions of cut-and-fill work, land grading, the ongoing movement of construction equipment and the transport of building materials throughout a site alter the architecture and structure of the soil, resulting in: the mixing of layers (horizons) of soil materials, compression of those materials and diminished soil porosity which, if left unchecked, severely impairs the soil’s water holding capacity and vertical drainage (rainfall infiltration), from the surface downward.

In a humid climate region, compaction damage on a site is virtually guaranteed over the duration of a project. Soil in very moist to wet condition when compacted, will have severely reduced permeability. Figure 1 displays the early stage of the deep-ripping phase (Note that all topsoil was stripped prior to construction access, and it remains stockpiled until the next phase – decompaction – is complete). A heavy-duty tractor is pulling a three-shank ripper on the first of several series of incrementally deepening passes through the construction access corridor’s densely compressed subsoil material. Figure 2 illustrates the approximate volumetric composition of a loam surface soil when conditions are good for plant growth, with adequate natural pore space for fluctuating moisture conditions.



Fig. 1. A typical deep ripping phase of this practice, during the first in a series of progressively deeper “rips” through severely compressed subsoil.

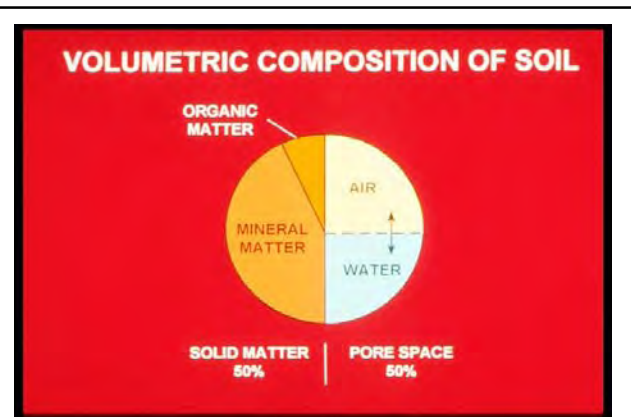


Fig. 2. About 50% of the volume of undisturbed loam surface soil is pore space, when soil is in good condition for plant growth. Brady, 2002.

## Recommended Application of Practice

The objective of Deep Ripping and Decompaction is to effectively fracture (vertically and laterally) through the thickness of the physically compressed subsoil material (see Figure 3), restoring soil porosity and permeability and aiding infiltration to help reduce runoff. Together with topsoil stripping, the “two-phase” practice of Deep Ripping and Decompaction first became established as a “best management practice” through ongoing success on commercial farmlands affected by heavy utility construction right-of-way projects (transmission pipelines and large power lines).



Fig. 3. Construction site with significant compaction of the deep basal till subsoil extends 24 inches below this exposed cut-and-fill work surface.

Soil permeability, soil drainage and cropland productivity were restored. For broader construction application, the two-phase practice of Deep Ripping and Decompaction is best adapted to areas impacted with significant soil compaction, on contiguous open portions of large construction sites and inside long, open construction corridors used as temporary access over the duration of construction. Each mitigation area should have minimal above-and-below-ground obstructions for the easy avoidance and maneuvering of a large tractor and ripping/decompacting implements. Conversely, the complete two-phase practice is not recommended in congested or obstructed areas due to the limitations on tractor and implement movement.

## Benefits

Aggressive “deep ripping” through the compressed thickness of exposed subsoil before the replacement/respreading of the topsoil layer, followed by “decompaction,” i.e.: “sub-soiling,” through the restored topsoil layer down into the subsoil, offers the following benefits:

- Increases the project (larger size) area’s direct surface infiltration of rainfall by providing the open site’s mitigated soil condition and lowers the demand on concentrated runoff control structures
- Enhances direct groundwater recharge through greater dispersion across and through a broader surface than afforded by some runoff-control structural measures
- Decreases runoff volume generated and provides hydrologic source control
- May be planned for application in feasible open locations either alone or in

conjunction with plans for structural practices (e.g., subsurface drain line or infiltration basin) serving the same or contiguous areas

- Promotes successful long-term revegetation by restoring soil permeability, drainage and water holding capacity for healthy (rather than restricted) root-system development of trees, shrubs and deep rooted ground cover, minimizing plant drowning during wet periods and burnout during dry periods.

## Feasibility/Limitations

The effectiveness of Deep Ripping and Decompaction is governed mostly by site factors such as: the original (undisturbed) soil's hydrologic characteristics; the general slope; local weather/timing (soil moisture) for implementation; the space-related freedom of equipment/implement maneuverability (noted above in **Recommended Application of Practice**), and by the proper selection and operation of tractor and implements (explained below in **Design Guidance**). The more notable site-related factors include:

### Soil

In the undisturbed condition, each identified soil type comprising a site is grouped into one of four categories of soil hydrology, Hydrologic Soil Group A, B, C or D, determined primarily by a range of characteristics including soil texture, drainage capability when thoroughly wet, and depth to water table. The natural rates of infiltration and transmission of soil-water through the undisturbed soil layers for Group A is "high" with a low runoff potential while soils in Group B are moderate in infiltration and the transmission of soil-water with a moderate runoff potential, depending somewhat on slope. Soils in Group C have slow rates of infiltration and transmission of soil-water and a moderately high runoff potential influenced by soil texture and slope; while soils in Group D have exceptionally slow rates of infiltration and transmission of soil-water, and high runoff potential.

In Figure 4, the profile displays the undisturbed horizons of a soil in Hydrologic Soil Group C and the naturally slow rate of infiltration through the subsoil. The slow rate of infiltration begins immediately below the topsoil horizon (30 cm), due to the limited amount of macro pores, e.g.: natural subsoil fractures, worm holes and root channels. Infiltration after the construction-induced mixing and compression of such subsoil material is virtually absent; but can be restored back to this natural level with the two-phase practice of deep ripping and decompaction, followed by the permanent establishment of an appropriate, deep taproot

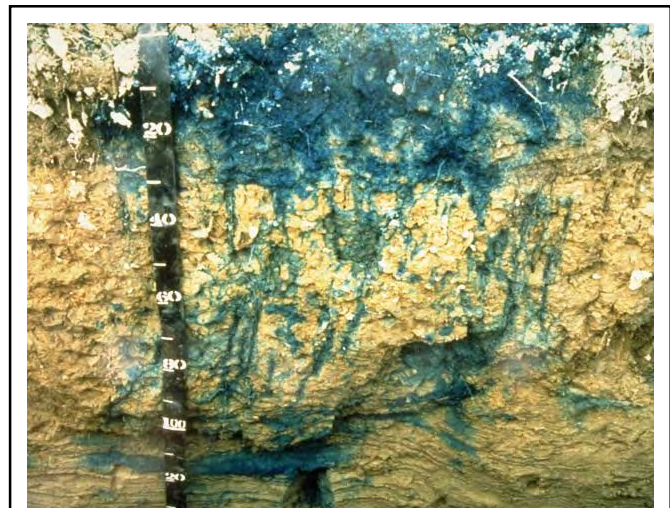


Fig. 4. Profile (in centimeters) displaying the infiltration test result of the natural undisturbed horizons of a soil in Hydrologic Soil Group C.

lawn/ground cover to help maintain the restored subsoil structure. Infiltration after construction-induced mixing and compression of such subsoil material can be notably rehabilitated with the Deep Ripping and Decomposition practice, which prepares the site for the appropriate long-term lawn/ground cover mix including deep taproot plants such as clover, fescue or trefoil, etc. needed for all rehabilitated soils.

Generally, soils in Hydrologic Soil Groups A and B, which respectively may include deep, well-drained, sandy-gravelly materials or deep, moderately well-drained basal till materials, are among the easier ones to restore permeability and infiltration, by deep ripping and decomposition. Among the many different soils in Hydrologic Soil Group C are those unique glacial tills having a natural fragipan zone, beginning about 12 to 18 inches (30 – 45cm), below surface. Although soils in Hydrologic Soil Group C do require a somewhat more carefully applied level of the Deep Ripping and Decomposition practice, it can greatly benefit such affected areas by reducing the runoff and fostering infiltration to a level equal to that of pre-disturbance.

Soils in Hydrologic Soil Group D typically have a permanent high water table close to the surface, influenced by a clay or other highly impervious layer of material. In many locations with clay subsoil material, the bulk density is so naturally high that heavy trafficking has little or no added impact on infiltration; and structural runoff control practices rather than Deep Ripping and Decomposition should be considered.

The information about Hydrologic Soil Groups is merely a general guideline. Site-specific data such as limited depths of cut-and-fill grading with minimal removal or translocation of the inherent subsoil materials (as analyzed in the county soil survey) or, conversely, the excavation and translocation of deeper, unconsolidated substratum or consolidated bedrock materials (unlike the analyzed subsoil horizons' materials referred to in the county soil survey) should always be taken into account.

Sites made up with significant quantities of large rocks, or having a very shallow depth to bedrock, are not conducive to deep ripping and decomposition (subsoiling); and other measures may be more practical.

### **Slope**

The two-phase application of 1) deep ripping and 2) decomposition (deep subsoiling), is most practical on flat, gentle and moderate slopes. In some situations, such as but not limited to temporary construction access corridors, inclusion areas that are moderately steep along a project's otherwise gentle or moderate slope may also be deep ripped and decomposed. For limited instances of moderate steepness on other projects, however, the post-construction land use and the relative alignment of the potential ripping and decomposition work in relation to the lay of the slope should be reviewed for safety and practicality. In broad construction areas predominated by moderately steep or steep slopes, the practice is generally not used.

### **Local Weather/Timing/Soil Moisture**

Effective fracturing of compressed subsoil material from the exposed work surface, laterally and vertically down through the affected zone is achieved only when the soil material is moderately dry to moderately moist. Neither one of the two-phases, deep ripping nor decomposition (deep



subsoiling), can be effectively conducted when the soil material (subsoil or replaced topsoil) is in either a “plastic” or “liquid” state of soil consistency. Pulling the respective implements legs through the soil when it is overly moist only results in the “slicing and smearing” of the material or added “squeezing and compression” instead of the necessary fracturing. Ample drying time is needed for a “rippable” soil condition not merely in the material close to the surface, but throughout the material located down to the bottom of the physically compressed zone of the subsoil.

The “poor man’s Atterberg field test” for soil plasticity is a simple “hand-roll” method used for quick, on-site determination of whether or not the moisture level of the affected soil material is low enough for: effective deep ripping of subsoil; respreading of topsoil in a friable state; and final decompaction (deep subsoiling). Using a sample of soil material obtained from the planned bottom depth of ripping, e.g.: 20 - 24 inches below exposed subsoil surface, the sample is hand rolled between the palms down to a 1/8-inch diameter thread. (Use the same test for stored topsoil material before respreading on the site.) If the respective soil sample crumbles apart in segments no greater than 3/8 of an inch long, by the time it is rolled down to 1/8 inch diameter, it is low enough in moisture for deep ripping (or topsoil replacement), and decompaction. Conversely, as shown in Figure 5, if the rolled sample stretches out in increments greater than 3/8 of an inch long before crumbling, it is in a “plastic” state of soil consistency and is too wet for subsoil ripping (as well as topsoil replacement) and final decompaction.



Fig. 5. Augered from a depth of 19 inches below the surface of the replaced topsoil, this subsoil sample was hand rolled to a 1/8-inch diameter. The test shows the soil at this site stretches out too far without crumbling; it indicates the material is in a plastic state of consistence, too wet for final decompaction (deep subsoiling) at this time.

## Design Guidance

Beyond the above-noted site factors, a vital requirement for the effective Deep Ripping and Decompaction (deep subsoiling), is implementing the practice in its distinct, two-phase process:

- 1) Deep rip the affected thickness of exposed subsoil material (see Figure 10 and 11), aggressively fracturing it before the protected topsoil is reapplied on the site (see Figure 12); and
- 2) Decompact (deep subsoil), simultaneously through the restored topsoil layer and the upper half of the affected subsoil (Figure 13). The second phase, “decompaction,” mitigates the partial recompaction which occurs during the heavy process of topsoil spreading/grading. Prior to deep ripping and decompacting the site, all construction activity, including construction equipment and material storage, site cleanup and trafficking (Figure 14), should be finished; and the site closed off to further disturbance. Likewise, once the practice is underway and the area’s soil permeability and

rainfall infiltration are being restored, a policy limiting all further traffic to permanent travel lanes is maintained.

The other critical elements, outlined below, are: using the proper implements (deep, heavy-duty rippers and subsoilers), and ample pulling-power equipment (tractors); and conducting the practice at the appropriate speed, depth and pattern(s) of movement.

Note that an appropriate plan for the separate practice of establishing a healthy perennial ground cover, with deep rooting to help maintain the restored soil structure, should be developed in advance. This may require the assistance of an agronomist or landscape horticulturist.

### Implements

Avoid the use of all undersize implements. The small-to-medium, light-duty tool will, at best, only “scarify” the uppermost surface portion of the mass of compacted subsoil material. The term “chisel plow” is commonly but incorrectly applied to a broad range of implements. While a few may be adapted for the moderate subsoiling of non-impacted soils, the majority are less durable and used for only lighter land-fitting (see Figure 6).



Fig. 6. A light duty chisel implement, not adequate for either the deep ripping or decompaction (deep subsoiling) phase.



Fig. 7. One of several variations of an agricultural ripper. This unit has long, rugged shanks mounted on a steel V-frame for deep, aggressive fracturing through Phase 1.

Use a “heavy duty” agricultural-grade, deep ripper (see Figures 7,9,10 and 11) for the first phase: the lateral and vertical fracturing of the mass of exposed and compressed subsoil, down and through, to the bottom of impact, prior to the replacement of the topsoil layer. (Any oversize rocks which are uplifted to the subsoil surface during the deep ripping phase are picked and removed.) Like the heavy-duty class of implement for the first phase, the decompaction (deep subsoiling) of Phase 2 is conducted with the heavy-duty version of the deep subsoiler. More preferable is the angled-leg variety of deep subsoiler (shown in Figures 8 and 13). It minimizes the inversion of the subsoil and topsoil layers while laterally and vertically fracturing the upper half of the previously ripped subsoil layer and all of the topsoil layer by delivering a momentary, wave-like “lifting and shattering” action up through the soil layers as it is pulled.

### **Pulling-Power of Equipment**

Use the following rule of thumb for tractor horsepower (hp) whenever deep ripping and decompacting a significantly impacted site: For both types of implement, have at least 40 hp of tractor pull available for each mounted shank/ leg.

Using the examples of a 3-shank and a 5-shank implement, the respective tractors should have 120 and 200 hp available for fracturing down to the final depth of 20-to-24 inches per phase. Final depth for the deep ripping in Phase 1 is achieved incrementally by a progressive series of passes (see Depth and Patterns of Movement, below); while for Phase 2, the full operating depth of the deep subsoiler is applied from the beginning.

The operating speed for pulling both types of implement should not exceed 2 to 3 mph. At this slow and managed rate of operating speed, maximum functional performance is sustained by the tractor and the implement performing the soil fracturing. Referring to Figure 8, the implement is the 6-leg version of the deep angled-leg subsoiler. Its two outside legs are “chained up” so that only four legs will be engaged (at the maximum depth), requiring no less than 160 hp, (rather than 240 hp) of pull. The 4-wheel drive, articulated-frame tractor in Figure 8 is 174 hp. It will be decompacting this unobstructed, former construction access area simultaneously through 11 inches of replaced topsoil and the upper 12 inches of the previously deep-ripped subsoil. In constricted areas of Phase 1) Deep Ripping, a medium-size tractor with adequate hp, such as the one in Figure 9 pulling a 3-shank deep ripper, may be more maneuverable.

Some industrial-grade variations of ripping implements are attached to power graders and bulldozers. Although highly durable, they are generally not recommended. Typically, the shanks or “teeth” of these rippers are too short and stout; and they are mounted too far apart to achieve the well-distributed type of lateral and vertical fracturing of the soil materials necessary to restore soil permeability and infiltration. In addition, the power graders and bulldozers, as pullers, are far less maneuverable for turns and patterns than the tractor.



Fig. 8. A deep, angled-leg subsoiler, ideal for Phase 2 decompaction of after the topsoil layer is graded on top of the ripped subsoil.



Fig. 9. This medium tractor is pulling a 3-shank deep ripper. The severely compacted construction access corridor is narrow, and the 120 hp tractor is more maneuverable for Phase 1 deep ripping (subsoil fracturing), here.



## Depth and Patterns of Movement

As previously noted both Phase 1 Deep Ripping through significantly compressed, exposed subsoil and Phase 2 Decompaction (deep subsoiling) through the replaced topsoil and upper subsoil need to be performed at maximum capable depth of each implement. With an implement's guide wheels attached, some have a "normal" maximum operating depth of 18 inches, while others may go deeper. In many situations, however, the tractor/implement operator must first remove the guide wheels and other non essential elements from the implement. This adapts the ripper or the deep subsoiler for skillful pulling with its frame only a few inches above surface, while the shanks or legs, fracture the soil material 20-to-24 inches deep.

There may be construction sites where the depth of the exposed subsoil's compression is moderate, e.g.: 12 inches, rather than deep. This can be verified by using a  $\frac{3}{4}$  inch cone penetrometer and a shovel to test the subsoil for its level of compaction, incrementally, every three inches of increasing depth. Once the full thickness of the subsoil's compacted zone is finally "pieced" and there is a significant drop in the psi measurements of the soil penetrometer, the depth/thickness of compaction is determined. This is repeated at several representative locations of the construction site. If the thickness of the site's subsoil compaction is verified as, for example, ten inches, then the Phase 1 Deep Ripping can be correspondingly reduced to the implement's minimum operable depth of 12 inches. However, the Phase 2 simultaneous Decompaction (subsoiling) of an 11 inch thick layer of replaced topsoil and the upper subsoil should run at the subsoiling implements full operating depth.



Fig. 10. An early pass with a 3-shank deep ripper penetrating only 8 inches into this worksite's severely compressed subsoil.



Fig. 11. A repeat run of the 3-shank ripper along the same patterned pass area as Fig. 9; here, incrementally reaching 18 of the needed 22 inches of subsoil fracture.

Typically, three separate series (patterns) are used for both the Phase 1 Deep Ripping and the Phase 2 Decompaction on significantly compacted sites. For Phase 1, each series begins with a moderate depth of rip and, by repeat-pass, continues until full depth is reached. Phase 2 applies the full depth of Decompaction (subsoiling), from the beginning.

Every separate series (pattern) consists of parallel, forward-and-return runs, with each progressive

pass of the implement's legs or shanks evenly staggered between those from the previous pass. This compensates for the shank or leg-spacing on the implement, e.g., with 24-to-30 inches between each shank or leg. The staggered return pass ensures lateral and vertical fracturing actuated every 12 to 15 inches across the densely compressed soil mass.

### Large, Unobstructed Areas

For larger easy areas, use the standard patterns of movement:

- The first series (pattern) of passes is applied lengthwise, parallel with the longest spread of the site; gradually progressing across the site's width, with each successive pass.
- The second series runs obliquely, crossing the first series at an angle of about 45 degrees.
- The third series runs at right angle (or 90 degrees), to the first series to complete the fracturing and shattering on severely compacted sites, and avoid leaving large unbroken blocks of compressed soil material. (In certain instances, the third series may be optional, depending on how thoroughly the first two series loosen the material and eliminate large chunks/blocks of material as verified by tests with a 3/4-inch cone penetrometer.)



Fig. 12. Moderately dry topsoil is being replaced on the affected site now that Phase 1 deep ripping of the compressed subsoil is complete.



Fig. 13. The same deep, angled-leg subsoiler shown in Fig. 7 is engaged at maximum depth for Phase 2, decompaction (deep soiling), of the replaced topsoil and the upper subsoil materials.

### Corridors

In long corridors of limited width and less maneuverability than larger sites, e.g.: along compacted areas used as temporary construction access, a modified series of pattern passes are used.

- First, apply the same initial lengthwise, parallel series of passes described above.

- A second series of passes makes a broad “S” shaped pattern of rips, continually and gradually alternating the “S” curves between opposite edges inside the compacted corridor.
- The third and final series again uses the broad, alternating S pattern, but it is “flip-flopped” to continually cross the previous S pattern along the corridor’s centerline. This final series of the S pattern curves back along the edge areas skipped by the second series.

## Maintenance and Cost

Once the two-phase practice of Deep Ripping and Decompanation is completed, two items are essential for maintaining a site’s soil porosity and permeability for infiltration. They are: planting and maintaining the appropriate ground cover with deep roots to maintain the soil structure (see Figure 15); and keeping the site free of traffic or other weight loads.

Note that site-specific choice of an appropriate vegetative ground-cover seed mix, including the proper seeding ratio of one or more perennial species with a deep taproot system and the proper amount of lime and soil nutrients (fertilizer mix) adapted to the soil-needs, are basic to the final practice of landscaping, i.e: surface tillage, seeding/planting/fertilizing and culti-packing or mulching is applied. The "maintenance" of an effectively deep-ripped and decompacted area is generally limited to the successful perennial (long-term) landscape ground cover; as long as no weight-bearing force of soil compaction is applied.



Fig. 14. The severely compacted soil of a temporary construction yard used daily by heavy equipment for four months; shown before deep ripping, topsoil replacement, and decompaction.



Fig. 15. The same site as Fig. 14 after deep ripping of the exposed subsoil, topsoil replacement, decompaction through the topsoil and upper subsoil and final surface tillage and revegetation to maintain soil permeability and infiltration.

The Deep Ripping and Decompaction practice is, by necessity, more extensive than periodic subsoiling of farmland. The cost of deep ripping and decompacting (deep subsoiling), will vary according to the depth and severity of soil-material compression and the relative amount of tractor and implement time that is required. In some instances, depending on open maneuverability, two-to-three acres of compacted project area may be deep-ripped in one day. In other situations of more severe compaction and - or less maneuverability, as little as one acre may be fully ripped in a day. Generally, if the Phase 1) Deep Ripping is fully effective, the Phase 2) Decompaction should be completed in  $2/3$  to  $3/4$  of the time required for Phase 1.

Using the example of two acres of Phase 1) Deep Ripping in one day, at \$1800 per day, the net cost is \$900 per acre. If the Phase 2) Decompacting or deep subsoiling takes  $3/4$  the time as Phase 1, it costs \$675 per acre for a combined total of \$1575 per acre to complete the practice (these figures do not include the cost of the separate practice of topsoil stripping and replacement). Due to the many variables, it must be recognized that cost will be determined by the specific conditions or constraints of the site and the availability of proper equipment.

## Resources

### Publications:

- American Society of Agricultural Engineers. 1971. *Compaction of Agricultural Soils*. ASAE.
- Brady, N.C., and R.R. Weil. 2002. *The Nature and Properties of Soils*. 13<sup>th</sup> ed. Pearson Education, Inc.
- Baver, L.D. 1948. *Soil Physics*. John Wiley & Sons.
- Carpachi, N. 1987 (1995 fifth printing). *Excavation and Grading Handbook, Revised*. 2<sup>nd</sup> ed. Craftsman Book Company
- Ellis, B. (Editor). 1997. *Safe & Easy Lawn Care: The Complete Guide to Organic Low Maintenance Lawn*. Houghton Mifflin.
- Harpstead, M.I., T.J. Sauer, and W.F. Bennett. 2001. *Soil Science Simplified*. 4<sup>th</sup> ed. Iowa State University Press.
- Magdoff, F., and H. van Es. 2000. *Building Soils for Better Crops*. 2<sup>nd</sup> ed. Sustainable Agricultural Networks
- McCarthy, D.F. 1993. *Essentials of Soil Mechanics and Foundations, Basic Geotechnics* 4<sup>th</sup> ed. Regents/Prentice Hall.
- Plaster, E.J. 1992. *Soil Science & Management*. 3<sup>rd</sup> ed. Delmar Publishers.
- Union Gas Limited, Ontario, Canada. 1984. *Rehabilitation of Agricultural Lands, Dawn-Kerwood Loop Pipeline; Technical Report*. Ecological Services for Planning, Ltd.; Robinson, Merritt & Devries, Ltd. and Smith, Hoffman Associates, Ltd.
- US Department of Agriculture in cooperation with Cornell University Agricultural Experiment Station. Various years. *Soil Survey of (various names) County, New York*. USDA.

### Internet Access:

- Examples of implements:  
V-Rippers. Access by internet search of *John Deere Ag -New Equipment for 915* (larger-frame model) *V-Rippe*; and, *for 913* (smaller-frame model) *V-Ripper*. Deep, angled-leg subsoiler. Access by internet search of: *Bigham Brothers Shear Bolt Paratill-Subsoiler*.  
[http://salesmanual.deere.com/sales/salesmanual/en\\_NA/primary\\_tillage/2008/feature/rippers/915v\\_pattern\\_frame.html?sbu=ag&link=prodcats](http://salesmanual.deere.com/sales/salesmanual/en_NA/primary_tillage/2008/feature/rippers/915v_pattern_frame.html?sbu=ag&link=prodcats) Last visited March 08.
- Soils data of USDA Natural Resources Conservation Service. *NRCS Web Soil Survey*. <http://websoilsurvey.nrcs.usda.gov/app/> and *USDA-NRCS Official Soil Series Descriptions; View by Name*. <http://ortho.ftw.nrcs.usda.gov/cgi-bin/osd/osdname.cgi> . Last visited Jan. 08.
- Soil penetrometer information. Access by internet searches of: *Diagnosing Soil Compaction using a Penetrometer (soil compaction tester)*, *PSU Extension*; as well as *Dickey-john Soil Compaction Tester*.  
<http://www.dickey-johnproducts.com/pdf/SoilCompactionTest.pdf> and <http://cropsoil.psu.edu/Extension/Facts/uc178pdf> Last visited Sept. 07

## Appendix 13 | NRCC Precipitation Tables



# Extreme Precipitation Tables

## Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

<b>Smoothing</b>	Yes
<b>State</b>	New York
<b>Location</b>	
<b>Longitude</b>	74.425 degrees West
<b>Latitude</b>	41.423 degrees North
<b>Elevation</b>	0 feet
<b>Date/Time</b>	Wed, 04 Aug 2021 09:08:26 -0400

### Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
<b>1yr</b>	0.33	0.50	0.62	0.82	1.02	1.26	<b>1yr</b>	0.88	1.18	1.45	1.77	2.17	2.64	3.07	<b>1yr</b>	2.33	2.95	3.38	4.08	4.71	<b>1yr</b>
<b>2yr</b>	0.39	0.60	0.75	0.98	1.24	1.54	<b>2yr</b>	1.07	1.43	1.76	2.15	2.62	3.17	3.63	<b>2yr</b>	2.80	3.49	4.00	4.71	5.37	<b>2yr</b>
<b>5yr</b>	0.46	0.71	0.89	1.19	1.53	1.92	<b>5yr</b>	1.32	1.77	2.20	2.70	3.28	3.96	4.57	<b>5yr</b>	3.50	4.40	5.01	5.80	6.57	<b>5yr</b>
<b>10yr</b>	0.51	0.81	1.02	1.38	1.80	2.27	<b>10yr</b>	1.55	2.08	2.62	3.21	3.89	4.68	5.45	<b>10yr</b>	4.14	5.24	5.96	6.79	7.66	<b>10yr</b>
<b>25yr</b>	0.60	0.95	1.21	1.67	2.23	2.85	<b>25yr</b>	1.92	2.57	3.29	4.05	4.90	5.85	6.87	<b>25yr</b>	5.18	6.61	7.49	8.38	9.40	<b>25yr</b>
<b>50yr</b>	0.68	1.09	1.39	1.95	2.62	3.38	<b>50yr</b>	2.26	3.01	3.91	4.81	5.81	6.94	8.20	<b>50yr</b>	6.14	7.89	8.90	9.82	10.98	<b>50yr</b>
<b>100yr</b>	0.77	1.24	1.60	2.27	3.09	4.01	<b>100yr</b>	2.67	3.54	4.66	5.73	6.91	8.22	9.79	<b>100yr</b>	7.28	9.42	10.59	11.52	12.82	<b>100yr</b>
<b>200yr</b>	0.87	1.42	1.84	2.64	3.65	4.76	<b>200yr</b>	3.15	4.17	5.54	6.82	8.22	9.75	11.70	<b>200yr</b>	8.63	11.25	12.61	13.52	14.99	<b>200yr</b>
<b>500yr</b>	1.04	1.71	2.24	3.25	4.55	5.97	<b>500yr</b>	3.93	5.17	6.96	8.57	10.32	12.23	14.81	<b>500yr</b>	10.82	14.24	15.90	16.72	18.44	<b>500yr</b>

### Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
<b>1yr</b>	0.29	0.44	0.54	0.73	0.89	1.11	<b>1yr</b>	0.77	1.09	1.26	1.61	1.98	2.41	2.61	<b>1yr</b>	2.14	2.51	2.86	3.36	3.93	<b>1yr</b>
<b>2yr</b>	0.37	0.58	0.71	0.96	1.19	1.43	<b>2yr</b>	1.03	1.40	1.62	2.07	2.56	3.09	3.52	<b>2yr</b>	2.73	3.39	3.90	4.58	5.23	<b>2yr</b>
<b>5yr</b>	0.42	0.65	0.81	1.11	1.41	1.66	<b>5yr</b>	1.22	1.62	1.88	2.42	3.01	3.69	4.26	<b>5yr</b>	3.27	4.10	4.70	5.40	6.16	<b>5yr</b>
<b>10yr</b>	0.46	0.71	0.88	1.24	1.60	1.86	<b>10yr</b>	1.38	1.82	2.10	2.66	3.38	4.23	4.92	<b>10yr</b>	3.74	4.73	5.39	6.05	6.87	<b>10yr</b>
<b>25yr</b>	0.53	0.80	1.00	1.42	1.87	2.13	<b>25yr</b>	1.62	2.09	2.47	3.19	3.91	5.06	5.96	<b>25yr</b>	4.48	5.73	6.49	6.93	7.93	<b>25yr</b>
<b>50yr</b>	0.58	0.88	1.10	1.58	2.12	2.40	<b>50yr</b>	1.83	2.35	2.77	3.61	4.38	5.82	6.90	<b>50yr</b>	5.15	6.63	7.48	7.68	8.85	<b>50yr</b>
<b>100yr</b>	0.64	0.97	1.21	1.75	2.40	2.69	<b>100yr</b>	2.07	2.63	3.12	4.09	4.92	6.72	8.02	<b>100yr</b>	5.95	7.71	8.62	9.08	9.84	<b>100yr</b>
<b>200yr</b>	0.71	1.07	1.36	1.97	2.74	3.01	<b>200yr</b>	2.37	2.94	3.51	4.66	5.53	7.77	9.32	<b>200yr</b>	6.88	8.96	9.97	10.26	10.93	<b>200yr</b>
<b>500yr</b>	0.83	1.23	1.58	2.30	3.27	3.50	<b>500yr</b>	2.82	3.42	4.11	5.55	6.50	9.44	11.40	<b>500yr</b>	8.36	10.96	12.11	12.05	12.57	<b>500yr</b>

### Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
<b>1yr</b>	0.36	0.55	0.68	0.91	1.12	1.35	<b>1yr</b>	0.97	1.32	1.53	1.95	2.40	2.83	3.31	<b>1yr</b>	2.50	3.18	3.65	4.37	5.11	<b>1yr</b>
<b>2yr</b>	0.41	0.63	0.78	1.05	1.30	1.54	<b>2yr</b>	1.12	1.51	1.76	2.23	2.78	3.29	3.75	<b>2yr</b>	2.91	3.61	4.17	4.96	5.61	<b>2yr</b>
<b>5yr</b>	0.50	0.77	0.95	1.31	1.66	1.98	<b>5yr</b>	1.43	1.93	2.25	2.88	3.58	4.27	4.88	<b>5yr</b>	3.78	4.69	5.32	6.20	6.95	<b>5yr</b>
<b>10yr</b>	0.59	0.91	1.13	1.58	2.04	2.44	<b>10yr</b>	1.76	2.39	2.74	3.54	4.38	5.22	5.99	<b>10yr</b>	4.62	5.76	6.44	7.45	8.40	<b>10yr</b>
<b>25yr</b>	0.75	1.14	1.41	2.02	2.66	3.25	<b>25yr</b>	2.29	3.18	3.64	4.64	5.73	6.79	7.82	<b>25yr</b>	6.01	7.52	8.31	9.50	10.69	<b>25yr</b>
<b>50yr</b>	0.89	1.35	1.68	2.42	3.26	3.73	<b>50yr</b>	2.81	3.64	4.46	5.68	7.00	8.27	9.57	<b>50yr</b>	7.32	9.20	10.09	11.44	12.85	<b>50yr</b>
<b>100yr</b>	1.06	1.60	2.01	2.90	3.98	4.54	<b>100yr</b>	3.44	4.43	5.47	6.94	8.57	10.08	11.73	<b>100yr</b>	8.92	11.28	12.23	13.99	15.46	<b>100yr</b>
<b>200yr</b>	1.27	1.91	2.42	3.50	4.88	5.53	<b>200yr</b>	4.21	5.40	6.72	8.50	10.49	12.29	14.38	<b>200yr</b>	10.88	13.82	14.84	16.89	18.61	<b>200yr</b>
<b>500yr</b>	1.61	2.40	3.08	4.48	6.37	7.16	<b>500yr</b>	5.49	7.00	8.83	11.11	13.70	15.94	18.78	<b>500yr</b>	14.11	18.06	19.15	21.67	23.82	<b>500yr</b>



# Appendix 14 | Operation and Maintenance Plan



## Site Drainage

A State Pollutant Discharge Elimination System Permit (SPDES GP 0-20-001) is required from the New York State Department of Environmental Conservation (NYSDEC) and a Storm Water Pollution Prevention Plan (SWPPP) has been prepared for review/approval by the Town of New Paltz (an MS4 community). The site improvements made to the parcel are new construction and will increase the impervious area on the site. The study provides the proposed improvements and provides measures that will be used to control potential impacts due to stormwater runoff.

## Constructed Stormwater Control Practices

### **Catch Basins:**

Catch basins on-site are utilized to collect stormwater run-off and melting snow from the paved parking areas, driveway and sidewalks. These are located along the centerline of roadside swales.

### **Roof leaders:**

Roof leaders are utilized to collect stormwater run-off from the roof and discharge it into the subsurface chamber system.

### **Swirl chamber units:**

The swirl chamber unit a compact, below grade stormwater treatment system that provides water quality mitigation. These systems receive overland flow through grated inlets as well as piped inlets from the various catch basins and drain/yard inlets located throughout the site.

### **Subsurface Arch Chamber System:**

A subsurface chamber system is proposed to provide water quality and quantity mitigation in keeping with the requirements in the New York State Storm Water Management Design Manual (NYSSMDM). The system also has an outlet control structure which regulates the out-flow of stormwater.

### **Bioretention Areas:**

These are shallow stormwater depressions which capture run-off from a surrounding drainage area (six inch deep surface ponding area) and then utilize an engineered soil strata and vegetation for treatment.

See Design Plans and Details for these improvements.

## Typical Maintenance for Stormwater Practices

As a consequence of its function, the stormwater conveyance system collects and transports runoff that may contain certain pollutants. Maintaining catch basins, stormwater inlets, and the basins on a regular basis will remove pollutants, prevent clogging of the downstream conveyance system, restore catch basins' sediment trapping capacity, and ensure the system functions properly to avoid flooding.

### **Catch Basins:**

Catch basins should be inspected monthly and after heavy rain fall to ensure they are functioning properly. Typical maintenance of catch basins includes removal of debris from the grate and sump. This can be done manually or using a vehicle equipped with a vacuum pump. Catch basins should be cleaned out at least one (1) time per year. A good time to clean out catch basins is in the spring to remove the build-up of leaves, sand used for traction, dirt, and other debris that accumulates during winter months.

#### **Roof leaders:**

Roof leaders, similar to the catch basins, require typical maintenance which includes removal of debris manually. Inspections of the leaders should occur monthly and after heavy rain fall to ensure they are still functioning properly. These should be cleaned out at least one (1) time per year.

#### **Swirl Chamber Systems:**

The swirl chamber systems should be inspected at regular intervals and maintained when necessary to ensure optimum performance. The rate at which the system collects pollutants will depend more heavily on site activities than the size of the unit, i.e., unstable soils or heavy winter sanding will cause the treatment chamber to fill more quickly, but regular street sweeping will slow accumulation of said sediment and pollutants.

At a minimum, inspections should be performed twice per year (i.e. spring and fall) however more frequent inspections may be necessary in equipment wash down areas and in climates where winter sanding operations may lead to rapid accumulations of a large volume of sediment. The swirl chamber systems should be cleaned when the level of sediment has reached 75% of the capacity in the isolated sump or when significant level of hydrocarbons or trash has accumulated.

Cleaning of the swirl chamber systems should be done during dry weather conditions when no flow is entering the system. Cleanout of the swirl chamber system with a vacuum truck is generally the most effective and convenient method of excavating pollutants from the system. Disposal of all material removed from the swirl chamber systems should be done in accordance with local regulations. In many locations, disposal of evacuated sediments may be handled in the same manner as disposal of sediments removed from catch basins or deep sump manholes.

The Manufacturer's Operation and Maintenance Manual can be found in the appendix of the SWPPP. The minimum requirements to maintain intended operation are set forth by the manufacturer and should be strictly adhered to.

#### **Subsurface Arch Chamber System:**

The Subsurface Arch Chamber System should be inspected monthly (pipes, outlet control structure, etc.) and after heavy rain fall to ensure proper functionality. Refer to Appendix for Manufacturers recommended Operation & Maintenance of the Stormtech Chambers.

#### **Bioretention Areas:**

These areas should be inspected monthly and after heavy rain fall to ensure they are functioning properly. Typical maintenance of the bio-retention areas include removal of debris, weeding

(especially in the first couple of years while the plants are establishing their root systems) and mulching. Any areas devoid of mulch shall be re-mulched on an annual basis. Dead or diseased plant material shall be replaced immediately.

Silt/Sediment removal from the filter bed shall be conducted when the accumulation exceeds one inch or every five to six years. If the filter bed ponds water at the surface for more than 48 hours, the top 4-6 inches (below the mulch) of material shall be removed and replaced with fresh material. Any plant material removed during clean-out shall be replaced in-kind.

See Design Plans and Details for the components of the soil mixture for the filter bed.

### **Stormwater Basins:**

These basins should be inspected monthly (this includes the inlets pipes, rip-rap, embankments, outlet control structure, emergency spillway and fencing) and after heavy rain fall to ensure proper functionality.

Long-term Stormwater Basin maintenance requires the following:

- Mowing grass, at least twice yearly. Grass clippings and other debris must be removed from the basin area after each cutting. Removal of woody brush and trees. Reestablish good grass cover in areas where woody material has been removed.
- Leaves shall be removed as needed from the basin and outlet control structure.
- Restore and reseed eroded any areas and gullies along embankment areas. Reoccurring erosion should be inspected by a licensed professional engineer to determine probable cause and remedial action that may be necessary.
- General maintenance and repairs of the stormwater outlet and inlet structures.
- Sediment removal from forebay and micropool every five to six years or when 50% full.
- The emergency spillway must remain free of debris and maintain the design elevation in order to convey stormwater during a catastrophic storm event.

In general, any deficiencies identified during the regular inspections or otherwise for all the stormwater management facilities should be corrected immediately. See appendices for forms to record inspection and maintenance work for the stormwater facilities.

r:\projects\2020\20006912a\reports\drainage\dewpoint north\dec 2021\report\appendix\appendix 16 - o & m plan\stormwater operation & maintenance plan appendix.docx



# Isolator<sup>®</sup> Row O&M Manual





## THE ISOLATOR<sup>®</sup> ROW

### INTRODUCTION

An important component of any Stormwater Pollution Prevention Plan is inspection and maintenance. The StormTech Isolator Row is a technique to inexpensively enhance Total Suspended Solids (TSS) removal and provide easy access for inspection and maintenance.

### THE ISOLATOR ROW

The Isolator Row is a row of StormTech chambers, either SC-160LP, SC-310, SC-310-3, SC-740, DC-780, MC-3500 or MC-4500 models, that is surrounded with filter fabric and connected to a closely located manhole for easy access. The fabric-wrapped chambers provide for settling and filtration of sediment as storm water rises in the Isolator Row and ultimately passes through the filter fabric. The open bottom chambers and perforated sidewalls (SC-310, SC-310-3 and SC-740 models) allow storm water to flow both vertically and horizontally out of the chambers. Sediments are captured in the Isolator Row protecting the storage areas of the adjacent stone and chambers from sediment accumulation.

Two different fabrics are used for the Isolator Row. A woven geotextile fabric is placed between the stone and the Isolator Row chambers. The tough geotextile provides a media for storm water filtration and provides a durable surface for maintenance operations. It is also designed to prevent scour of the underlying stone and remain intact during high pressure jetting. A non-woven fabric is placed over the chambers to provide a filter media for flows passing through the perforations in the sidewall of the chamber. The non-woven fabric is not required over the SC-160LP, DC-780, MC-3500 or MC-4500 models as these chambers do not have perforated side walls.

The Isolator Row is typically designed to capture the “first flush” and offers the versatility to be sized on a volume basis or flow rate basis. An upstream manhole not only provides access to the Isolator Row but typically includes a high flow weir such that storm water flowrates or volumes that exceed the capacity of the Isolator Row overtop the overflow weir and discharge through a manifold to the other chambers.

The Isolator Row may also be part of a treatment train. By treating storm water prior to entry into the chamber system, the service life can be extended and pollutants such as hydrocarbons can be captured. Pre-treatment best management practices can be as simple as deep sump catch basins, oil-water separators or can be innovative storm water treatment devices. The design of the treatment train and selection of pretreatment devices by the design engineer is often driven by regulatory requirements. Whether pretreatment is used or not, the Isolator Row is recommended by StormTech as an effective means to minimize maintenance requirements and maintenance costs.

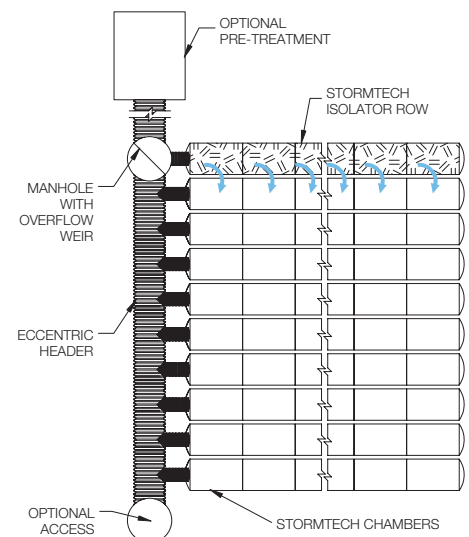
*Note: See the StormTech Design Manual for detailed information on designing inlets for a StormTech system, including the Isolator Row.*



Looking down the Isolator Row from the manhole opening, woven geotextile is shown between the chamber and stone base.



StormTech Isolator Row with Overflow Spillway (not to scale)





## ISOLATOR ROW INSPECTION/MAINTENANCE

### INSPECTION

The frequency of inspection and maintenance varies by location. A routine inspection schedule needs to be established for each individual location based upon site specific variables. The type of land use (i.e. industrial, commercial, residential), anticipated pollutant load, percent imperviousness, climate, etc. all play a critical role in determining the actual frequency of inspection and maintenance practices.

At a minimum, StormTech recommends annual inspections. Initially, the Isolator Row should be inspected every 6 months for the first year of operation. For subsequent years, the inspection should be adjusted based upon previous observation of sediment deposition.

The Isolator Row incorporates a combination of standard manhole(s) and strategically located inspection ports (as needed). The inspection ports allow for easy access to the system from the surface, eliminating the need to perform a confined space entry for inspection purposes.

If upon visual inspection it is found that sediment has accumulated, a stadia rod should be inserted to determine the depth of sediment. When the average depth of sediment exceeds 3 inches throughout the length of the Isolator Row, clean-out should be performed.

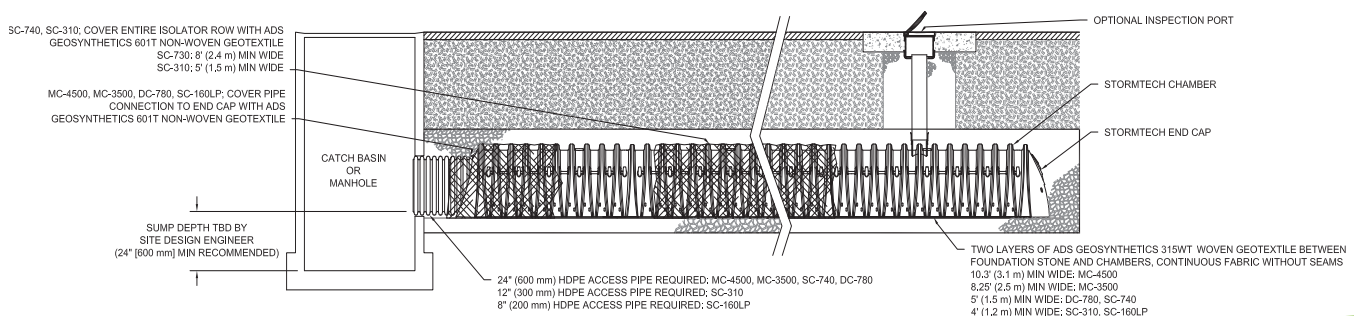
### MAINTENANCE

The Isolator Row was designed to reduce the cost of periodic maintenance. By “isolating” sediments to just one row, costs are dramatically reduced by eliminating the need to clean out each row of the entire storage bed. If inspection indicates the potential need for maintenance, access is provided via a manhole(s) located on the end(s) of the row for cleanout. If entry into the manhole is required, please follow local and OSHA rules for a confined space entries.

Maintenance is accomplished with the JetVac process. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row while scouring and suspending sediments. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles. Selection of an appropriate JetVac nozzle will improve maintenance efficiency. Fixed nozzles designed for culverts or large diameter pipe cleaning are preferable. Rear facing jets with an effective spread of at least 45” are best. Most JetVac reels have 400 feet of hose allowing maintenance of an Isolator Row up to 50 chambers long. **The JetVac process shall only be performed on StormTech Isolator Rows that have AASHTO class 1 woven geotextile (as specified by StormTech) over their angular base stone.**

### StormTech Isolator Row (not to scale)

*Note: Non-woven fabric is only required over the inlet pipe connection into the end cap for SC-160LP, DC-780, MC-3500 and MC-4500 chamber models and is not required over the entire Isolator Row.*



# ISOLATOR ROW STEP BY STEP MAINTENANCE PROCEDURES

## STEP 1

Inspect Isolator Row for sediment.

- A) Inspection ports (if present)
  - i. Remove lid from floor box frame
  - ii. Remove cap from inspection riser
  - iii. Using a flashlight and stadia rod, measure depth of sediment and record results on maintenance log.
  - iv. If sediment is at or above 3 inch depth, proceed to Step 2. If not, proceed to Step 3.
- B) All Isolator Rows
  - i. Remove cover from manhole at upstream end of Isolator Row
  - ii. Using a flashlight, inspect down Isolator Row through outlet pipe
    - 1. Mirrors on poles or cameras may be used to avoid a confined space entry
    - 2. Follow OSHA regulations for confined space entry if entering manhole
  - iii. If sediment is at or above the lower row of sidewall holes (approximately 3 inches), proceed to Step 2. If not, proceed to Step 3.

## STEP 2

Clean out Isolator Row using the JetVac process.

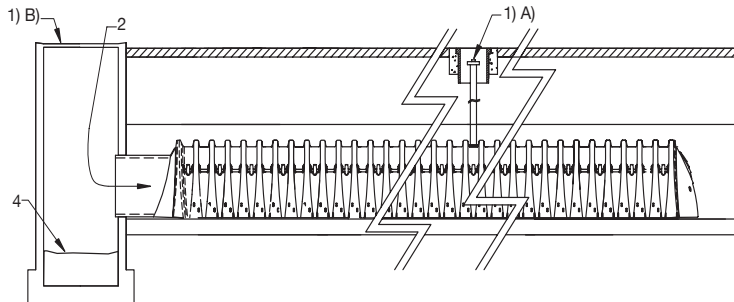
- A) A fixed floor cleaning nozzle with rear facing nozzle spread of 45 inches or more is preferable
- B) Apply multiple passes of JetVac until backflush water is clean
- C) Vacuum manhole sump as required

## STEP 3

Replace all caps, lids and covers, record observations and actions.

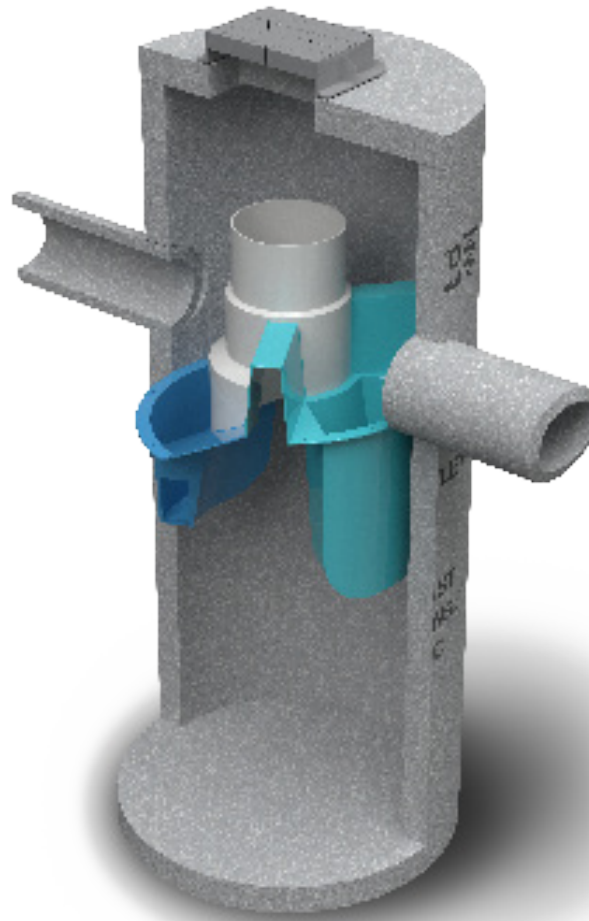
## STEP 4

Inspect & clean catch basins and manholes upstream of the StormTech system.



## SAMPLE MAINTENANCE LOG

Date	Stadia Rod Readings		Sediment Depth (1)-(2)	Observations/Actions	Inspector
	Fixed point to chamber bottom (1)	Fixed point to top of sediment (2)			
3/15/11	6.3 ft	none		New installation. Fixed point is CI frame at grade	DJM
9/24/11		6.2	0.1 ft	Some grit felt	SM
6/20/13		5.8	0.5 ft	Mucky feel, debris visible in manhole and in Isolator Row, maintenance due	NV
7/7/13	6.3 ft		0	System jetted and vacuumed	DJM



## Operation and Maintenance Manual

**First Defense<sup>®</sup> High Capacity and First Defense<sup>®</sup> Optimum**

---

Vortex Separator for Stormwater Treatment



## Table of Contents

<b>3</b>	<b>FIRST DEFENSE® BY HYDRO INTERNATIONAL</b> <ul style="list-style-type: none"><li>- INTRODUCTION</li><li>- OPERATION</li><li>- POLLUTANT CAPTURE AND RETENTION</li></ul>
<b>4</b>	<b>MODEL SIZES &amp; CONFIGURATIONS</b> <ul style="list-style-type: none"><li>- FIRST DEFENSE® COMPONENTS</li></ul>
<b>5</b>	<b>MAINTENANCE</b> <ul style="list-style-type: none"><li>- OVERVIEW</li><li>- MAINTENANCE EQUIPMENT CONSIDERATIONS</li><li>- DETERMINING YOUR MAINTENANCE SCHEDULE</li></ul>
<b>6</b>	<b>MAINTENANCE PROCEDURES</b> <ul style="list-style-type: none"><li>- INSPECTION</li><li>- FLOATABLES AND SEDIMENT CLEAN OUT</li></ul>
<b>8</b>	<b>FIRST DEFENSE® INSTALLATION LOG</b>
<b>9</b>	<b>FIRST DEFENSE® INSPECTION AND MAINTENANCE LOG</b>

---

**COPYRIGHT STATEMENT:** The contents of this manual, including the graphics contained herein, are intended for the use of the recipient to whom the document and all associated information are directed. Hydro International plc owns the copyright of this document, which is supplied in confidence. It must not be used for any purpose other than that for which it is supplied and must not be reproduced, in whole or in part stored in a retrieval system or transmitted in any form or by any means without prior permission in writing from Hydro International plc. First Defense® is a trademarked hydrodynamic vortex separation device of Hydro International plc. A patent covering the First Defense® has been granted.

**DISCLAIMER:** Information and data contained in this manual is exclusively for the purpose of assisting in the operation and maintenance of Hydro International plc's First Defense®. No warranty is given nor can liability be accepted for use of this information for any other purpose. Hydro International plc has a policy of continuous product development and reserves the right to amend specifications without notice.

# I. First Defense® by Hydro International

## Introduction

The First Defense® is an enhanced vortex separator that combines an effective and economical stormwater treatment chamber with an integral peak flow bypass. It efficiently removes total suspended solids (TSS), trash and hydrocarbons from stormwater runoff without washing out previously captured pollutants. The First Defense® is available in several model configurations to accommodate a wide range of pipe sizes, peak flows and depth constraints.

The two product models described in this guide are the First Defense® High Capacity and the First Defense® Optimum; they are inspected and maintained identically.

## Operation

The First Defense® operates on simple fluid hydraulics. It is self-activating, has no moving parts, no external power requirement and is fabricated with durable non-corrosive components. No manual procedures are required to operate the unit and maintenance is limited to monitoring accumulations of stored pollutants and periodic clean-outs. The First Defense® has been designed to allow for easy and safe access for inspection, monitoring and clean-out procedures. Neither entry into the unit nor removal of the internal components is necessary for maintenance, thus safety concerns related to confined-space-entry are avoided.

## Pollutant Capture and Retention

The internal components of the First Defense® have been designed to optimize pollutant capture. Sediment is captured and retained in the base of the unit, while oil and floatables are stored on the water surface in the inner volume (Fig.1).

The pollutant storage volumes are isolated from the built-in bypass chamber to prevent washout during high-flow storm events. The sump of the First Defense® retains a standing water level between storm events. This ensures a quiescent flow regime at the onset of a storm, preventing resuspension and washout of pollutants captured during previous events.

Accessories such as oil absorbent pads are available for enhanced oil removal and storage. Due to the separation of the oil and floatable storage volume from the outlet, the potential for washout of stored pollutants between clean-outs is minimized.

## Applications

- Stormwater treatment at the point of entry into the drainage line
- Sites constrained by space, topography or drainage profiles with limited slope and depth of cover
- Retrofit installations where stormwater treatment is placed on or tied into an existing storm drain line
- Pretreatment for filters, infiltration and storage

## Advantages

- Inlet options include surface grate or multiple inlet pipes
- Integral high capacity bypass conveys large peak flows without the need for “offline” arrangements using separate junction manholes
- Long flow path through the device ensures a long residence time within the treatment chamber, enhancing pollutant settling
- Delivered to site pre-assembled and ready for installation

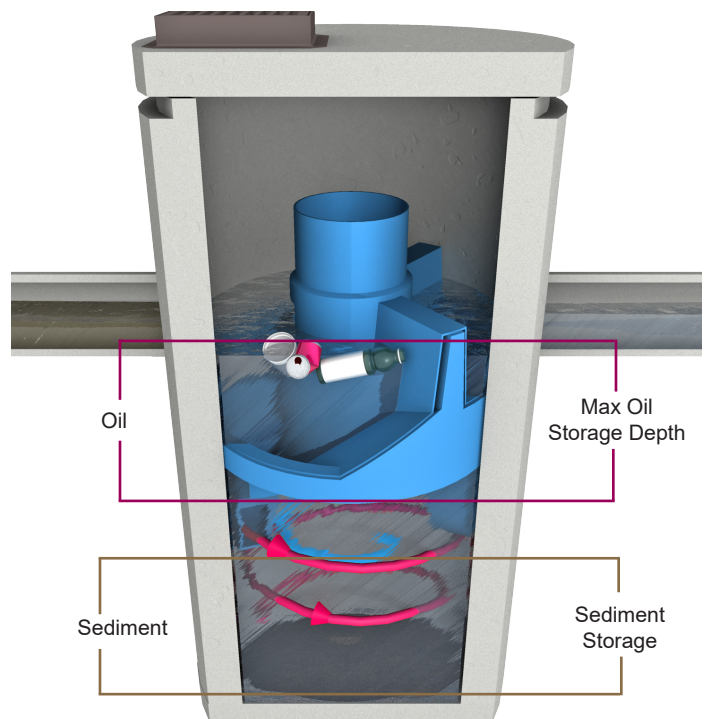


Fig.1 Pollutant storage volumes in the First Defense®.

## II. Model Sizes & Configurations

The First Defense® inlet and internal bypass arrangements are available in several model sizes and configurations. The components have modified geometries allowing greater design flexibility to accommodate various site constraints.

All First Defense® models include the internal components that are designed to remove and retain total suspended solids (TSS), gross solids, floatable trash and hydrocarbons (Fig.2). First Defense® model sizes (diameter) are shown in Table 1.

## III. Maintenance

### First Defense® Components

- |                    |                             |                         |
|--------------------|-----------------------------|-------------------------|
| 1. Built-In Bypass | 4. Floatables Draw-off Port | 7. Sediment Storage     |
| 2. Inlet Pipe      | 5. Outlet Pipe              | 8. Inlet Grate or Cover |
| 3. Inlet Chute     | 6. Floatables Storage       |                         |

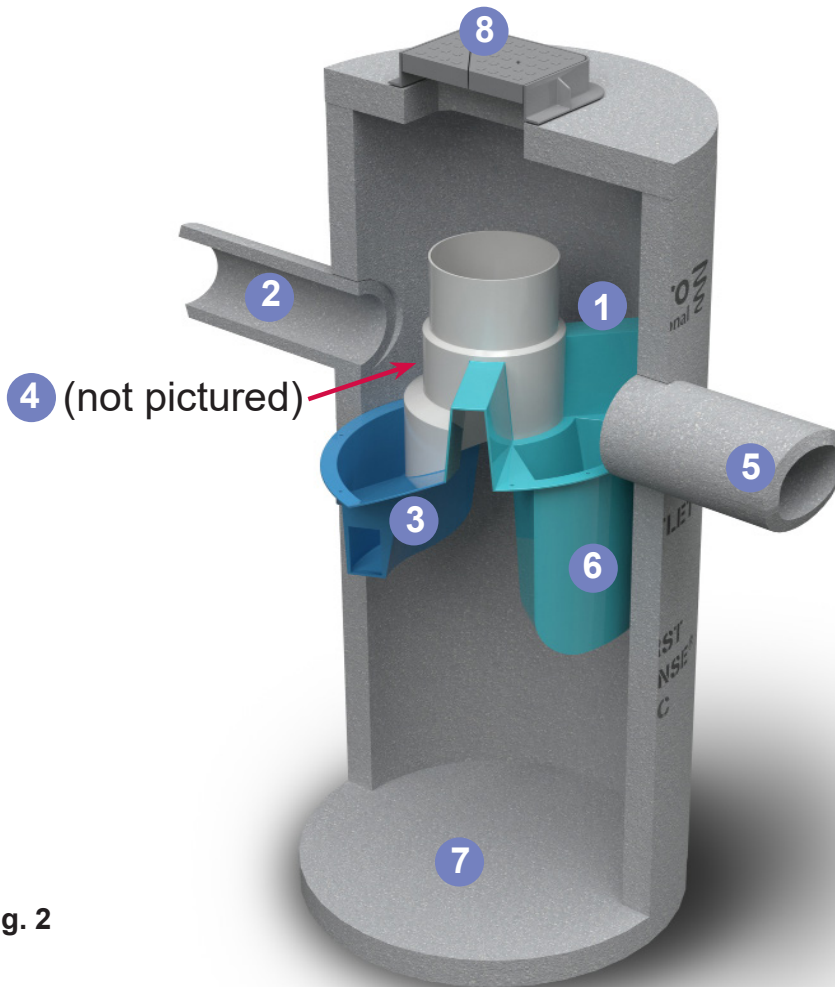


Fig. 2

Table 1

First Defense® Model Sizes
(ft / m) diameter
3 / 0.9
4 / 1.2
5 / 1.5
6 / 1.8
7 / 2.1
8 / 2.4
10 / 3.0

## Overview

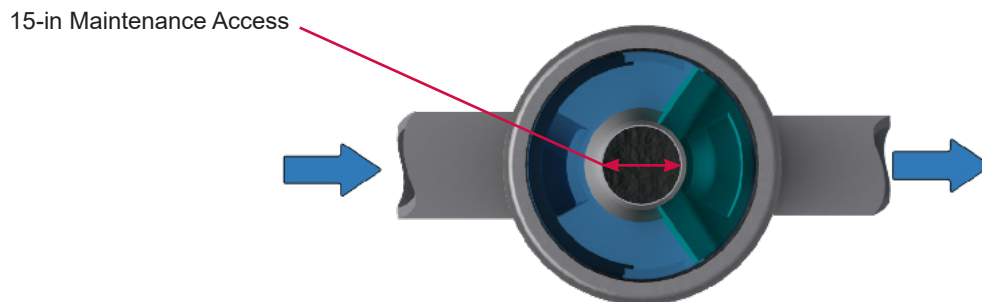
The First Defense® protects the environment by removing a wide range of pollutants from stormwater runoff. Periodic removal of these captured pollutants is essential to the continuous, long-term functioning of the First Defense®. The First Defense® will capture and retain sediment and oil until the sediment and oil storage volumes are full to capacity. When sediment and oil storage capacities are reached, the First Defense® will no longer be able to store removed sediment and oil.

The First Defense® allows for easy and safe inspection, monitoring and clean-out procedures. A commercially or municipally owned sump-vac is used to remove captured sediment and floatables. Access ports are located in the top of the manhole.

Maintenance events may include Inspection, Oil & Floatables Removal, and Sediment Removal. Maintenance events do not require entry into the First Defense®, nor do they require the internal components of the First Defense® to be removed. In the case of inspection and floatables removal, a vactor truck is not required. However, a vactor truck is required if the maintenance event is to include oil removal and/or sediment removal.

## Maintenance Equipment Considerations

The internal components of the First Defense® have a centrally located circular shaft through which the sediment storage sump can be accessed with a sump vac hose. The open diameter of this access shaft is 15 inches in diameter (Fig.3). Therefore, the nozzle fitting of any vactor hose used for maintenance should be less than 15 inches in diameter.



*Fig.3 The central opening to the sump of the First Defense® is 15 inches in diameter.*

## Determining Your Maintenance Schedule

The frequency of clean out is determined in the field after installation. During the first year of operation, the unit should be inspected every six months to determine the rate of sediment and floatables accumulation. A simple probe such as a Sludge-Judge® can be used to determine the level of accumulated solids stored in the sump. This information can be recorded in the maintenance log (see page 9) to establish a routine maintenance schedule.

The vactor procedure, including both sediment and oil / floatables removal, for First Defense® typically takes less than 30 minutes and removes a combined water/oil volume of about 765 gallons.

### Inspection Procedures

1. Set up any necessary safety equipment around the access port or grate of the First Defense® as stipulated by local ordinances. Safety equipment should notify passing pedestrian and road traffic that work is being done.
2. Remove the grate or lid to the manhole.
3. Without entering the vessel, look down into the chamber to inspect the inside. Make note of any irregularities. Fig.4 shows the standing water level that should be observed.
4. Without entering the vessel, use the pole with the skimmer net to remove floatables and loose debris from the components and water surface.
5. Using a sediment probe such as a Sludge Judge®, measure the depth of sediment that has collected in the sump of the vessel.
6. On the Maintenance Log (see page 9), record the date, unit location, estimated volume of floatables and gross debris removed, and the depth of sediment measured. Also note any apparent irregularities such as damaged components or blockages.
7. Securely replace the grate or lid.
8. Take down safety equipment.
9. Notify Hydro International of any irregularities noted during inspection.

### Floatables and Sediment Clean Out

Floatables clean out is typically done in conjunction with sediment removal. A commercially or municipally owned sump-vac is used to remove captured sediment and floatables (Fig.4).

Floatables and loose debris can also be netted with a skimmer and pole. The access port located at the top of the manhole provides unobstructed access for a vactor hose to be lowered to the base of the sump.

### Scheduling

- Floatables and sump clean out are typically conducted once a year during any season.
- Floatables and sump clean out should occur as soon as possible following a spill in the contributing drainage area.



Fig.4 Floatables are removed with a vactor hose

### Recommended Equipment

- Safety Equipment (traffic cones, etc)
- Crow bar or other tool to remove grate or lid
- Pole with skimmer or net (if only floatables are being removed)
- Sediment probe (such as a Sludge Judge®)
- Vactor truck (flexible hose recommended)
- First Defense® Maintenance Log



### *Floatables and Sediment Clean Out Procedures*

1. Set up any necessary safety equipment around the access port or grate of the First Defense® as stipulated by local ordinances. Safety equipment should notify passing pedestrian and road traffic that work is being done.
2. Remove the grate or lid to the manhole.
3. Without entering the vessel, look down into the chamber to inspect the inside. Make note of any irregularities.
4. Remove oil and floatables stored on the surface of the water with the vacator hose or with the skimmer or net
5. Using a sediment probe such as a Sludge Judge®, measure the depth of sediment that has collected in the sump of the vessel and record it in the Maintenance Log (page 9).
6. Once all floatables have been removed, drop the vacator hose to the base of the sump. Vacator out the sediment and gross debris off the sump floor
7. Retract the vacator hose from the vessel.
8. On the Maintenance Log provided by Hydro International, record the date, unit location, estimated volume of floatables and gross debris removed, and the depth of sediment measured. Also note any apparent irregularities such as damaged components, blockages, or irregularly high or low water levels.
9. Securely replace the grate or lid.

## Maintenance at a Glance

Inspection	<ul style="list-style-type: none"> <li>- Regularly during first year of installation</li> <li>- Every 6 months after the first year of installation</li> </ul>
Oil and Floatables Removal	<ul style="list-style-type: none"> <li>- Once per year, with sediment removal</li> <li>- Following a spill in the drainage area</li> </ul>
Sediment Removal	<ul style="list-style-type: none"> <li>- Once per year or as needed</li> <li>- Following a spill in the drainage area</li> </ul>

NOTE: For most clean outs the entire volume of liquid does not need to be removed from the manhole. Only remove the first few inches of oils and floatables from the water surface to reduce the total volume of liquid removed during a clean out.



## First Defense® Installation Log

HYDRO INTERNATIONAL REFERENCE NUMBER:	
SITE NAME:	
SITE LOCATION:	
OWNER:	CONTRACTOR:
CONTACT NAME:	CONTACT NAME:
COMPANY NAME:	COMPANY NAME:
ADDRESS:	ADDRESS:
TELEPHONE:	TELEPHONE:
FAX:	FAX:

INSTALLATION DATE:    /    /

MODEL SIZE (CIRCLE ONE):    [3-FT]    [4-FT]    [5-FT]    [6-FT]    [7-FT]    [8-FT]    [10-FT]

INLET (CIRCLE ALL THAT APPLY):    GRATED INLET (CATCH BASIN)    INLET PIPE (FLOW THROUGH)



## First Defense<sup>®</sup> Inspection and Maintenance Log

Date	Initials	Depth of Floatables and Oils	Sediment Depth Measured	Volume of Sediment Removed	Site Activity and Comments









## Stormwater Solutions

94 Hutchins Drive  
Portland, ME 04102

Tel: (207) 756-6200

Fax: (207) 756-6212

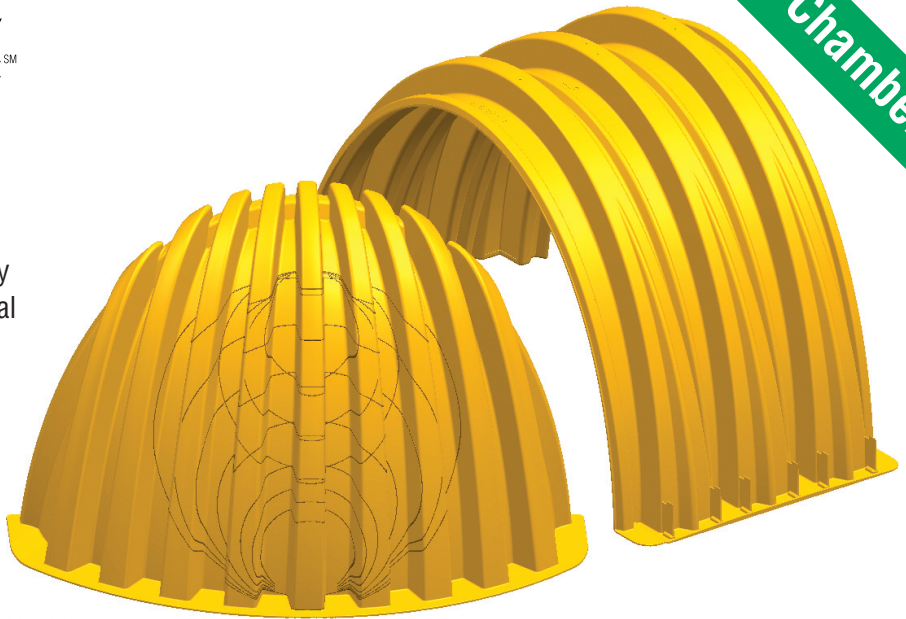
[stormwaterinquiry@hydro-int.com](mailto:stormwaterinquiry@hydro-int.com)

[www.hydro-int.com](http://www.hydro-int.com)

## Appendix 15 | ADS Stormtech

## StormTech™ MC-4500 Chamber

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots thus maximizing land usage for commercial and municipal applications.



### StormTech MC-4500 Chamber (not to scale)

#### Nominal Chamber Specifications

Size (L x W x H)	52" (1321 mm) x 100" (2540 mm) x 60" (1524 mm)
Chamber Storage	106.5 ft <sup>3</sup> (3.01 m <sup>3</sup> )
Min. Installed Storage*	162.6 ft <sup>3</sup> (4.60 m <sup>3</sup> )
Nominal Weight	120 lbs (54.4 kg)

\* This assumes a minimum of 12" (305 mm) of stone above, 9" (229 mm) of stone below chambers, 9" (229 mm) of stone between chambers/end caps and 40% stone porosity.

### StormTech MC-4500 End Cap (not to scale)

#### Nominal End Cap Specifications

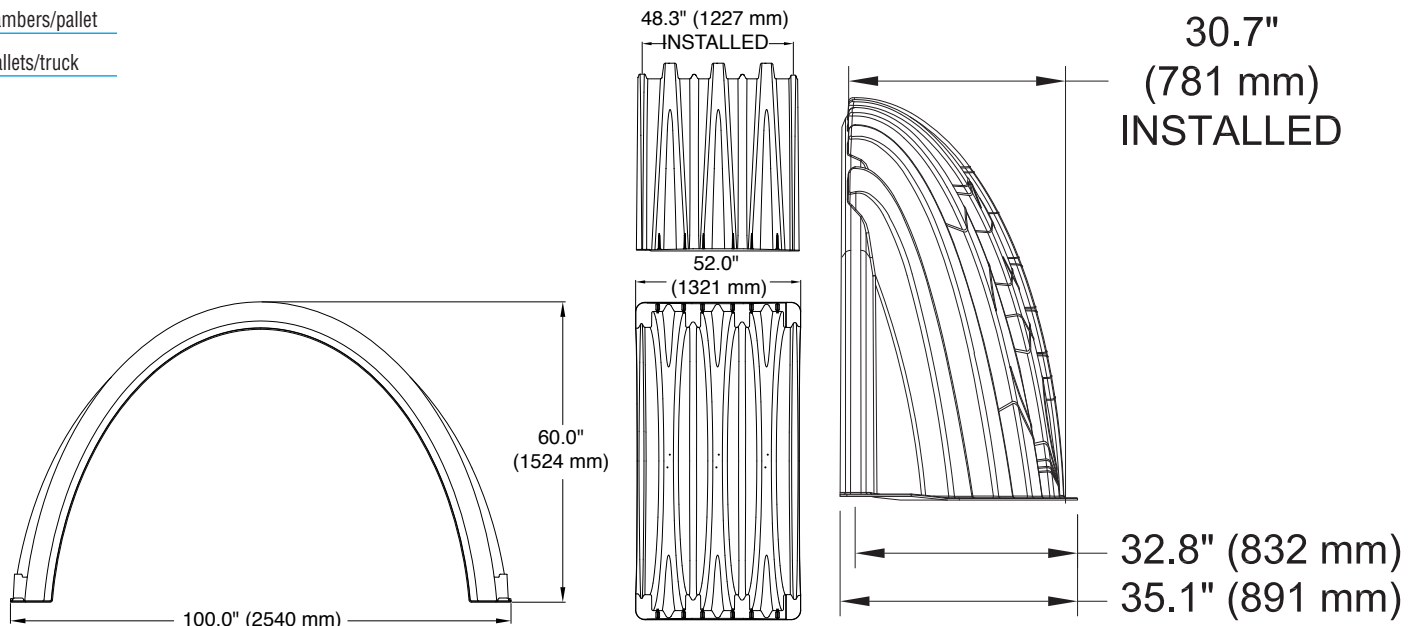
Size (L x W x H)	35.1" (891 mm) x 90.2" (2291 mm) x 59.4" (1509 mm)
End Cap Storage	35.7 ft <sup>3</sup> (1.01 m <sup>3</sup> )
Min. Installed Storage*	108.7 ft <sup>3</sup> (3.08 m <sup>3</sup> )
Nominal Weight	120 lbs (54.4 kg)

\* This assumes a minimum of 12" (305 mm) of stone above, 9" (229 mm) of stone below, 12" (305 mm) of stone perimeter, 9" (229 mm) of stone between chambers/end caps and 40% stone porosity.

### Shipping

8 chambers/pallet

11 pallets/truck



### Storage Volume Per Chamber/End Cap ft<sup>3</sup> (m<sup>3</sup>)

	Bare Unit Storage ft <sup>3</sup> (m <sup>3</sup> )	Chamber/End Cap and Stone Volume — Stone Foundation Depth in. (mm)			
		9" (229 mm)	12" (305 mm)	15" (381 mm)	18" (457 mm)
<b>Chamber</b>	106.5 (3.02)	162.6 (4.60)	166.3 (4.71)	169.9 (4.81)	173.6 (4.91)
<b>End Cap</b>	35.7 (1.01)	108.7 (3.08)	111.9 (3.17)	115.2 (3.26)	118.4 (3.35)

NOTE: Assumes 9" (229 mm) min. row spacing, 12" (305 mm) min. of stone above, 40% stone porosity and includes the bare chamber/end cap volume. End cap volume assumes 12" (305 mm) min. stone perimeter.

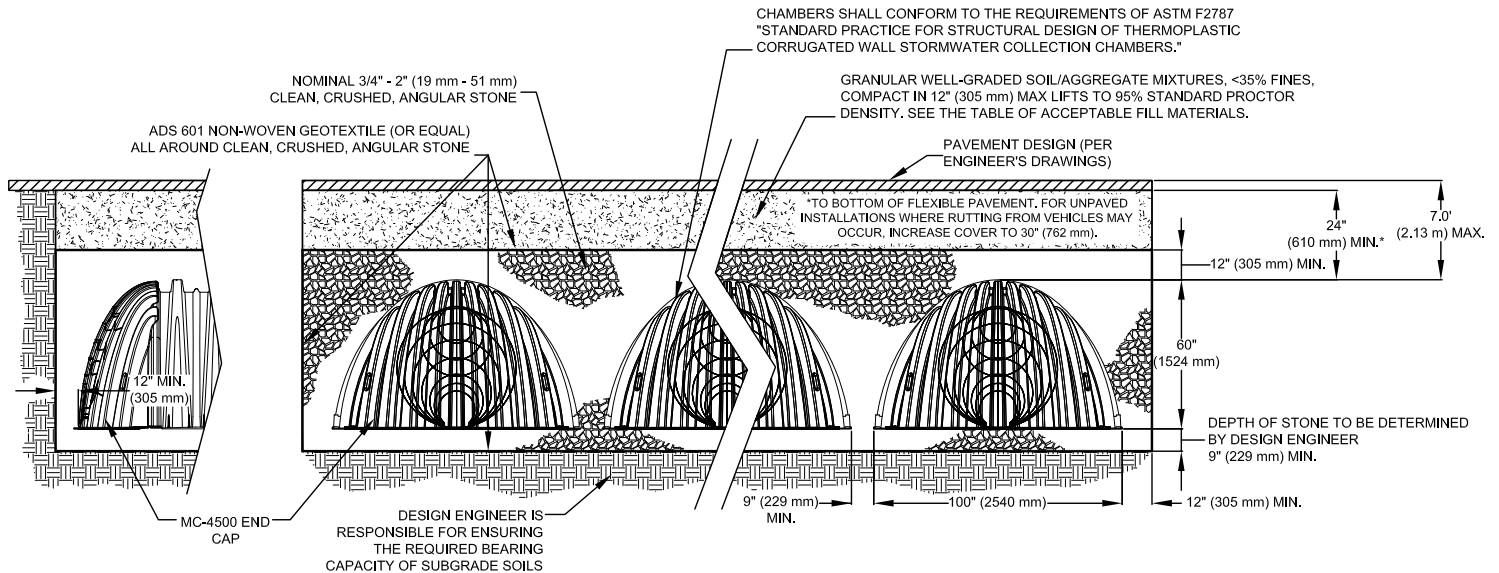
### Volume of Excavation Per Chamber/End Cap in yd<sup>3</sup> (m<sup>3</sup>)

	Stone Foundation Depth			
	9" (229 mm)	12" (305 mm)	15" (381 mm)	18" (457 mm)
<b>Chamber</b>	10.5 (8.0)	10.8 (8.3)	11.2 (8.5)	11.5 (8.8)
<b>End Cap</b>	9.3 (7.1)	9.6 (7.3)	9.9 (7.6)	10.2 (7.8)

NOTE: Assumes 9" (229 mm) min. of separation between chamber rows, 12" (305 mm) min. of perimeter in front of end caps, and 24" (610 mm) of cover. The volume of excavation will vary as the depth of cover increases.

### General Cross Section

\*\*Contact your local StormTech representative or visit [www.stormtech.com](http://www.stormtech.com) for a copy of the latest installation instructions.



THE INSTALLED CHAMBER SYSTEM SHALL PROVIDE THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS SECTION 12.12 FOR EARTH AND LIVE LOADS, WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.

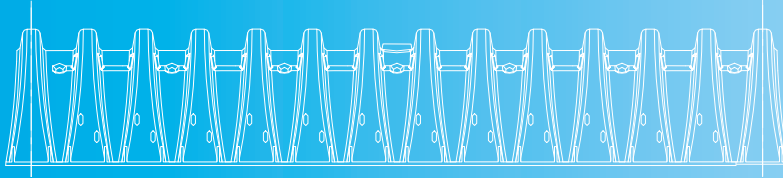


20 Beaver Road, Suite 104 | Wethersfield | Connecticut | 06109  
860.529.8188 | 888.892.2694 | fax 866.328.8401 | fax 860-529-8040 | [www.stormtech.com](http://www.stormtech.com)

\*Advanced Drainage Systems, the ADS logo, the green stripe, are registered trademarks of Advanced Drainage Systems. StormTech and MC-4500 are registered trademarks of StormTech, Inc. Green Building Council Member logo is a registered trademark of the U.S. Green Building Council. ADS "Terms and Conditions of Sale" are available on the ADS website, [www.ads-pipe.com](http://www.ads-pipe.com)



# Tech Sheet



## ASTM & AASHTO Standards for Buried Thermoplastic Structures

Tech Sheet # 6  
November 2012

### Design Requirements for Thermoplastic Structures:

1. The structural design must evaluate short term live loads, intermediate term loads and long term soil loads.
2. The materials used in production must provide necessary short, intermediate and long term properties.
3. The structural design must be completed by experts in the field of soil-structure interaction.
4. The product must be designed and manufactured to meet meaningful standards.
5. The structural design of the subsurface stormwater system must be up to the standards that a professional engineer expects.

### General:

This summarizes key components of structural design and national standards for subsurface thermoplastic structures. Although the focus of this guidance is on chamber systems, the principles apply to the wider category of buried products of various structural shapes and material properties.

### Structural Design of a Subsurface Thermoplastic System:

The objective of *structural* design is to ensure a proper safety factor over the intended **service life** of the buried system. Typically the intended service life of a subsurface storm drainage system ranges from 20 to 100 years. Since the polypropylene and polyethylene, thermoplastic materials now used for subsurface structures are very stable in the stormwater environment; the limiting criterion for service life is generally long-term structural stability.

The primary benefit of subsurface systems is to facilitate additional paved surfaces for the purpose of parking or traffic flow. For such applications, where public safety is of paramount importance, “structural survival”, i.e. lack of failure, is not sufficient. For a design to be safe, structural **safety factors** must be demonstrated for the entire service life of the project to account for uncertainties in loading, installation, and material performance. AASHTO design procedures mandate load factors of 1.75 for live loads to account for impact effects and the presence of multiple or overweight loads and 1.95 for earth loads on buried culverts.

There are two components to ensuring long term performance of any structural product: 1) the product must be designed, tested and manufactured to meet meaningful **product standards** and 2) the system must be designed to meet meaningful **design standards**. ASTM and AASHTO, the most respected, dependable standards available, have developed standards for buried structures.

### Short Term Properties, Intermediate Term Properties, Long Term Properties, Strain and Deflection:

Buried thermoplastic products must be designed for three conditions: 1) short duration live loads under shallow cover, 2) minimum 1-week sustained loads and 3) permanent earth loads. **Load duration** is a key criterion for the design of thermoplastic structures since the “apparent strength” and stiffness decrease with increasing load duration. For live load design, the thermoplastic product must be able to withstand the dynamic load from moving vehicles. *Live load design is based on short duration loads and short term material properties.* Intermediate load design requires the thermoplastic product to withstand 1-week sustained loads from parked oversized loads. *Intermediate load design is based on 1-week duration loads and 1-week material properties.*

1 AASHTO is the American Association of State Highway and Transportation Officials

2 ASTM / ASTM International is the American Society of Testing Materials



Earth (dead) loads are permanent in duration and magnitude. For dead load design, the thermoplastic product must be able to withstand the continuous dead load and remain stable after 75 years or more under sustained load. For thermoplastic systems using structural aggregate (stone) support, the performance of the structure is a function of the ability of the thermoplastic structure to shed significant portion of the load to the surrounding stone (arching). *Earth load design is based on permanent loads and long term material properties.* The material properties that govern long-term design are tensile creep rupture and creep modulus.

**Strain limits** are the maximum strains that can occur before the structure fails. Long, slender shapes are inherently unstable and fail at lower loads by buckling. Wide, flat shapes may also buckle under continuous load. Design for long-term service life must be based on long duration loads, long term creep modulus and strain limits. ***Without proper soil support, thermoplastic structures may reach a strain limit and fail.***

**Deflection** is generally not a failure limit or a service limit for soil supported chamber systems. When deflection is not limited by soil support, excessive deflection of thermoplastic structures has been found to cause pavement distress. ***Without proper soil support, deflection is a service limit for thermoplastic structures.***

**Specifying industry standards, not just products, establishes objective, meaningful performance criteria and a defensible basis of design.**

#### **AASHTO Standards:**

The AASHTO LRFD Bridge Design Specification is the primary source of design standards for soil-structure interaction under traffic loads. Section 3 of this specification provides for calculation of loads and Section 12.12 provides for structural design of buried thermoplastic structures.

##### **The AASHTO standard:**

- **Assures design safety factors for live loads and long-term loads**
- **Provides the design method for soil-structure interaction**
- **Assures a long-term service life by designing for creep and strain limits**
- **Provides consulting engineers with a defensible basis of design**

#### **ASTM Standards:**

ASTM is an internationally recognized source for a variety of standards including; testing methods, standard practices and product specifications. ASTM has developed two product standards for Stormwater chambers, designations ASTM F2418 (polypropylene chambers) and ASTM F2922 (polyethylene chambers).

##### **The ASTM F 2418 and F2922 Standards:**

- **Assure consistent product quality in a non-proprietary specification**
- **Establish physical and mechanical requirements for the finished product**
- **Establish long and short-term material properties for design**
- **Require AASHTO safety factors and full scale validation testing**

ASTM has developed a design standard for Stormwater chambers, designation: ASTM F 2787, entitled "Standard Practice for Structural Design of Thermoplastic Corrugated Wall Stormwater Collection Chambers".

##### **The ASTM F 2787 Standard:**

- **Applies the AASHTO Section 12.12 thermoplastic pipe design criteria and applies it directly to chambers**
- **Includes an additional design load for a minimum 1-week sustained vehicle load to account for parked vehicles**
- **Provides design criteria that can be applied to different thermoplastic resins.**

#### **Product Design:**

Stone support is a key component of the soil-structure interaction system. Stone columns between thermoplastic components provide the load paths from the load above to the foundation below. For stone-structure designs, the stone reduces the load that the thermoplastic components must carry and limits the deflection and strain of the thermoplastic components. Designs of subsurface thermoplastic structures that purport to require no structural stone or are not designed in accordance with AASHTO requirements may result in excessive deflections or complete failure.

**StormTech chambers are designed and rigorously tested in accordance with national standards to provide the most reliable subsurface system available.**

ADS "Terms and Conditions of Sale" are available on the ADS website, [www.ads-pipe.com](http://www.ads-pipe.com)  
StormTech is a registered trademark of StormTech, Inc.

©2012 Advanced Drainage Systems, Inc. ST TS6 11/12





# MC-3500 & MC-4500 Design Manual

*StormTech® Chamber Systems for Stormwater Management*



THE MOST **ADVANCED** NAME IN WATER MANAGEMENT SOLUTIONS®



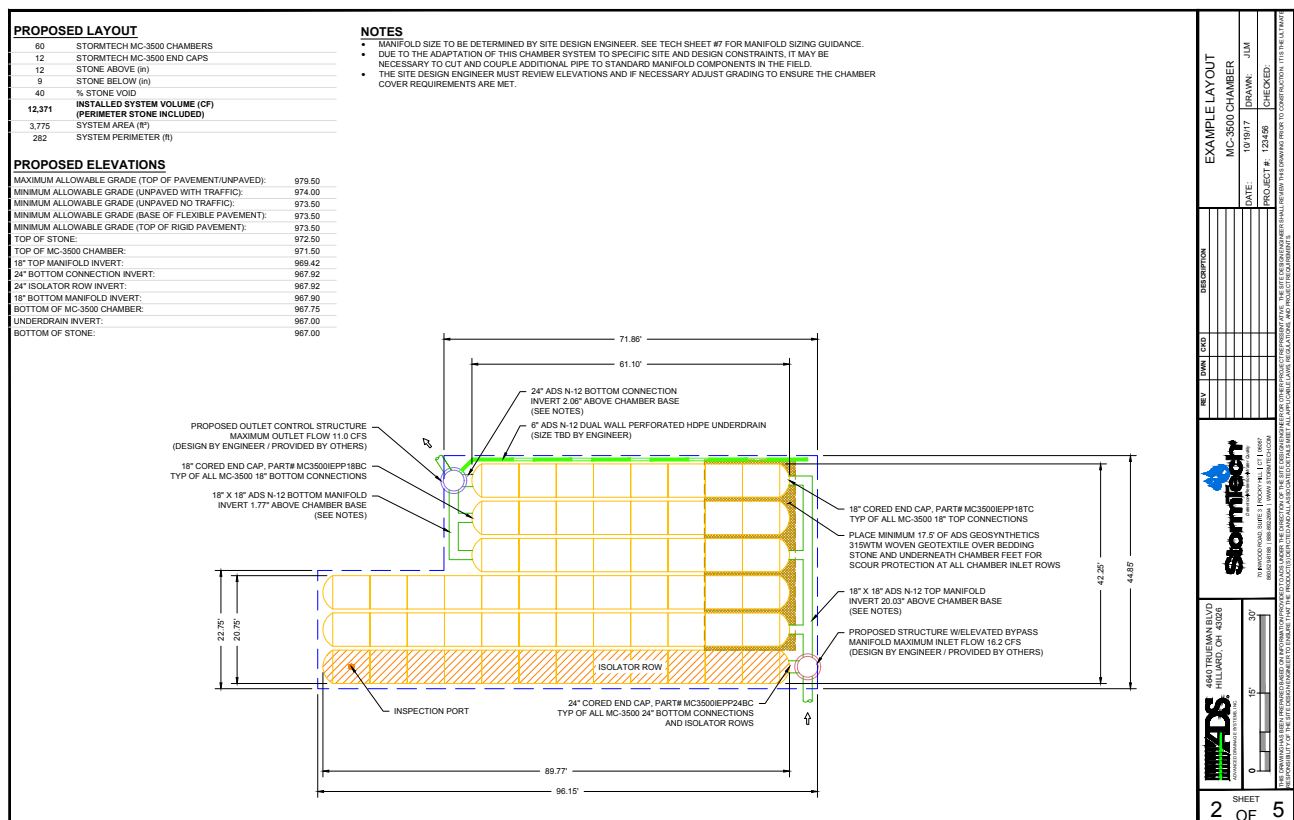


# Table of Contents

1.0	Product Information . . . . .	2
2.0	Foundation for Chambers. . . . .	8
3.0	Required Materials/Row Separation . . . . .	11
4.0	Hydraulics. . . . .	13
5.0	Cumulative Storage Volume . . . . .	15
6.0	System Sizing. . . . .	20
7.0	Structural Cross Sections and Specifications . . . . .	22
8.0	General Notes. . . . .	24
9.0	Inspection and Maintenance . . . . .	25

\*For SC-160LP, SC-310, SC-740 & DC-780 designs, please refer to the SC-160LP/SC-310/SC-740/DC-780 Design Manual.

StormTech Engineering Services assists design professionals in specifying StormTech stormwater systems. This assistance includes the layout of chambers to meet the engineer's volume requirements and the connections to and from the chambers. They can also assist converting and cost engineering projects currently specified with ponds, pipe, concrete vaults and other manufactured stormwater detention/retention products. Please note that it is the responsibility of the site design engineer to ensure that the chamber bed layout meets all design requirements and is in compliance with applicable laws and regulations governing a project.



This manual is exclusively intended to assist engineers in the design of subsurface stormwater systems using StormTech chambers.

Call StormTech at 860.529.8188 or 888.892.2694 or visit our website at [www.stormtech.com](http://www.stormtech.com) for technical and product information.

# StormTech MC-3500 Chamber

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots, thus maximizing land usage for private (commercial) and public applications. StormTech chambers can also be used in conjunction with Green Infrastructure, thus enhancing the performance and extending the service life of these practices.



## Stormtech MC-3500 Chamber (not to scale) Nominal Chamber Specifications

**Size (L x W x H)**  
90" x 77" x 45"  
2,286 mm x 1,956 mm x 1,143 mm

**Chamber Storage**  
109.9 ft<sup>3</sup> (3.11 m<sup>3</sup>)

**Min. Installed Storage\***  
175.0 ft<sup>3</sup> (4.96 m<sup>3</sup>)

**Weight**  
134 lbs (60.8 kg)

**Shipping**  
15 chambers/pallet  
7 end caps/pallet  
7 pallets/truck

\*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below chambers, 6" (150 mm) of stone between chambers/end caps and 40% stone porosity.

## Stormtech MC-3500 END CAP (not to scale) Nominal End Cap Specifications

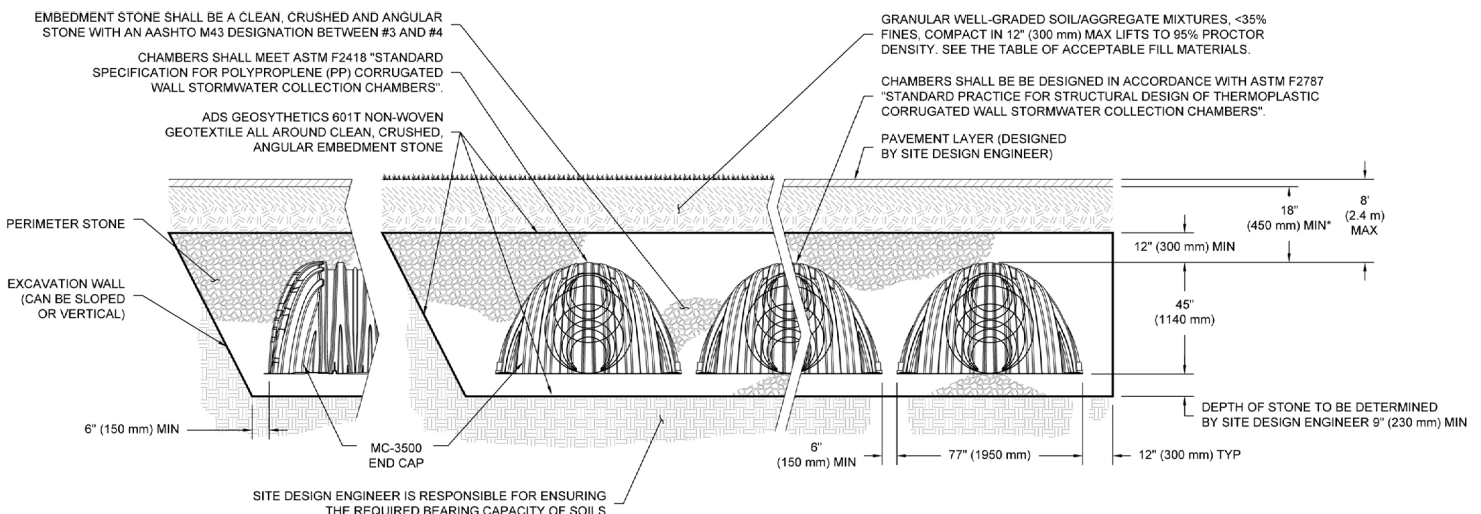
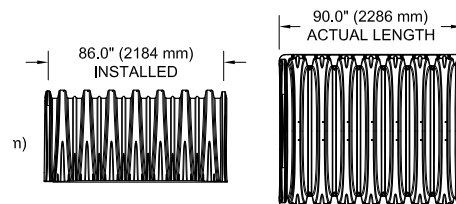
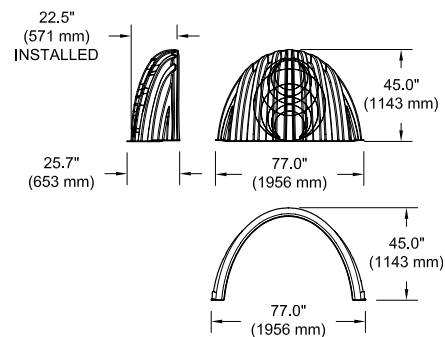
**Size (L x W x H)**  
26.5" x 71" x 45.1"  
673 mm x 1,803 mm x 1,145 mm

**End Cap Storage**  
14.9 ft<sup>3</sup> (0.42 m<sup>3</sup>)

**Min. Installed Storage\***  
45.1ft<sup>3</sup> (1.28 m<sup>3</sup>)

**Weight**  
49 lbs (22.2 kg)

\*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below, 6" (150 mm) of stone perimeter, 6" (150 mm) of stone between chambers/end caps and 40% stone porosity.



\*MINIMUM COVER TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 24" (600 mm).



# StormTech MC-3500 Chamber

## Storage Volume Per Chamber/End Cap ft<sup>3</sup> (m<sup>3</sup>)

	Bare Unit Storage ft <sup>3</sup> (m <sup>3</sup> )	Chamber/End Cap and Stone Volume — Stone Foundation Depth in. (mm)			
		9 (230)	12 (300)	15 (375)	18 (450)
<b>MC-3500 Chamber</b>	109.9 (3.11)	175.0 (4.96)	179.9 (5.09)	184.9 (5.24)	189.9 (5.38)
<b>MC-3500 End Cap</b>	14.9 (0.42)	45.1 (1.28)	46.6 (1.32)	48.3 (1.37)	49.9 (1.41)

Note: Assumes 6" (150 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume.

## Amount of Stone Per Chamber

ENGLISH tons (yd <sup>3</sup> )	Stone Foundation Depth			
	9"	12"	15"	18"
<b>Chamber</b>	8.5 (6.0)	9.1 (6.5)	9.7 (6.9)	10.4 (7.4)
<b>End Cap</b>	3.9 (2.8)	4.1 (2.9)	4.3 (3.1)	4.5 (3.2)
METRIC kg (m <sup>3</sup> )	230 mm	300 mm	375 mm	450 mm
<b>Chamber</b>	7711 (4.6)	8255 (5.0)	8800 (5.3)	9435 (5.7)
<b>End Cap</b>	3538 (2.1)	3719 (2.2)	3901 (2.4)	4082 (2.5)

Note: Assumes 12" (300 mm) of stone above and 6" (150 mm) row spacing and 6" (150 mm) of perimeter stone in front of end caps.

## Volume of Excavation Per Chamber/End Cap yd<sup>3</sup> (m<sup>3</sup>)

	Stone Foundation Depth			
	9" (230 mm)	12" (300 mm)	15" (375 mm)	18" (450 mm)
<b>Chamber</b>	11.9 (9.1)	12.4 (9.5)	12.8 (9.8)	13.3 (10.2)
<b>End Cap</b>	4.0 (3.1)	4.1 (3.2)	4.3 (3.3)	4.4 (3.4)

Note: Assumes 6" (150 mm) of separation between chamber rows and 24" (600 mm) of cover. The volume of excavation will vary as depth of cover increases.

Special applications will be considered on a project by project basis. Please contact our application department should you have a unique application for our team to evaluate.



# StormTech MC-4500 Chamber

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots, thus maximizing land usage for private (commercial) and public applications. StormTech chambers can also be used in conjunction with Green Infrastructure, thus enhancing the performance and extending the service life of these practices.



## Stormtech MC-4500 Chamber (not to scale)

### Nominal Chamber Specifications

**Size (L x W x H)**  
52" x 100" x 60"  
1321 mm x 2540 mm x 1524 mm

**Chamber Storage**  
106.5 ft<sup>3</sup> (3.01 m<sup>3</sup>)

**Min. Installed Storage\***  
162.6 ft<sup>3</sup> (4.60 m<sup>3</sup>)

**Weight**  
Nominal 125 lbs (56.7 kg)

**Shipping**  
7 chambers/pallet  
5 end caps/pallet  
11 pallets/truck

\*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below chambers, 9" (230 mm) of stone between chambers/end caps and 40% stone porosity.

## Stormtech MC-4500 end cap (not to scale)

### Nominal End Cap Specifications

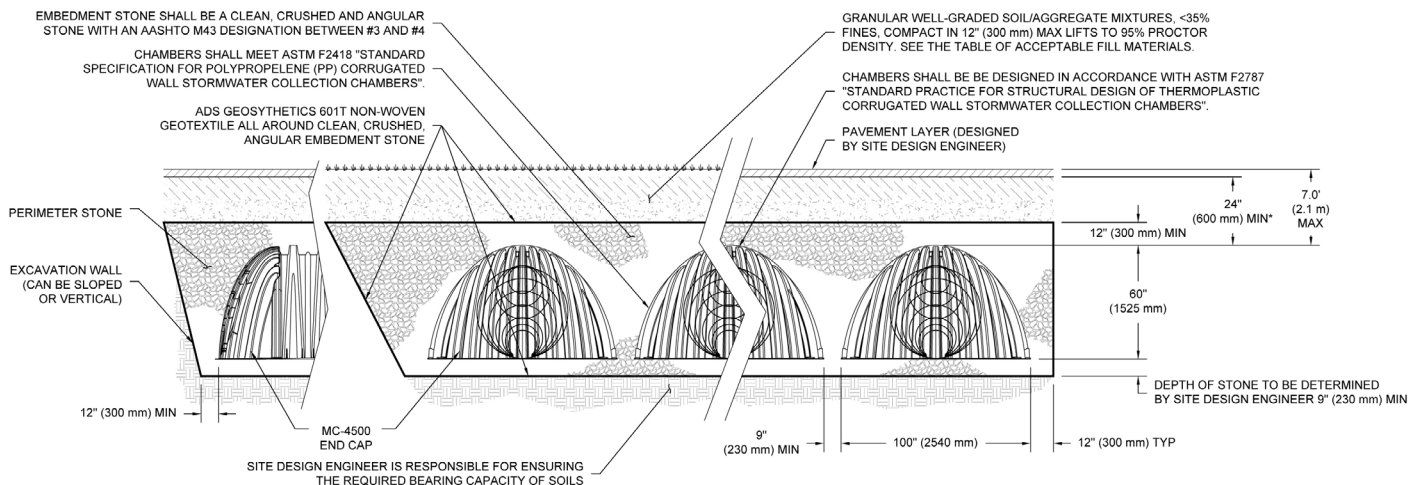
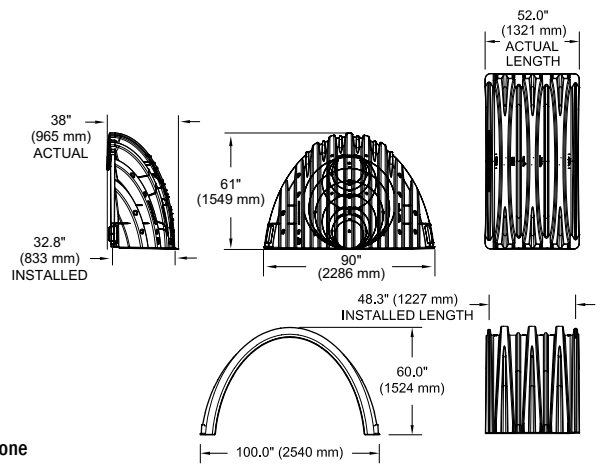
**Size (L x W x H)**  
38" x 90" x 61"  
965 mm x 2286 mm x 1549 mm

**End Cap Storage**  
39.5 ft<sup>3</sup> (1.12 m<sup>3</sup>)

**Min. Installed Storage\***  
115.3 ft<sup>3</sup> (3.26 m<sup>3</sup>)

**Weight**  
Nominal 90.0 lbs (40.8 kg)

\*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below, 12" (300 mm) of stone perimeter, 9" (230 mm) of stone between chambers/end caps and 40% stone porosity.



\*MINIMUM COVER TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 30" (750 mm).



# StormTech MC-4500 Chamber

## Storage Volume Per Chamber/End Cap ft<sup>3</sup> (m<sup>3</sup>)

	Bare Unit Storage ft <sup>3</sup> (m <sup>3</sup> )	Chamber/End Cap and Stone Volume — Stone Foundation Depth in. (mm)			
		9 (230)	12 (300)	15 (375)	18 (450)
<b>MC-4500 Chamber</b>	106.5 (3.02)	162.6 (4.60)	166.3 (4.71)	169.9 (4.71)	173.6 (4.91)
<b>MC-4500 End Cap</b>	39.5 (1.12)	115.3 (3.26)	111.9 (3.17)	121.9 (3.45)	125.2 (3.54)

Note: Assumes 9" (230 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume. End cap volume assumes 12" (300 mm) stone perimeter in front of end cap.

## Amount of Stone Per Chamber

ENGLISH tons (yd <sup>3</sup> )	Stone Foundation Depth			
	9"	12"	15"	18"
<b>Chamber</b>	7.4 (5.2)	7.8 (5.5)	8.3 (5.9)	8.8 (6.2)
<b>End Cap</b>	9.8 (7.0)	10.2 (7.3)	10.6 (7.6)	11.1 (7.9)
METRIC kg (m <sup>3</sup> )	230 mm	300 mm	375 mm	450 mm
<b>Chamber</b>	6713 (4.0)	7076 (4.2)	7529 (4.5)	7983 (4.7)
<b>End Cap</b>	8890 (5.3)	9253 (5.5)	9616 (5.8)	10069 (6.0)

Note: Assumes 12" (300 mm) of stone above and 9" (230 mm) row spacing and 12" (300 mm) of perimeter stone in front of end caps.

## Volume of Excavation Per Chamber/End Cap yd<sup>3</sup> (m<sup>3</sup>)

	Stone Foundation Depth			
	9" (230 mm)	12" (300 mm)	15"(375 mm)	18"(450 mm)
<b>Chamber</b>	10.5 (8.0)	10.8 (8.3)	11.2 (8.5)	11.5 (8.8)
<b>End Cap</b>	9.7 (7.4)	10.0 (7.6)	10.3 (7.9)	10.6 (8.1)

Note: Assumes 9" (230 mm) of separation between chamber rows, 12" (300 mm) of perimeter in front of the end caps, and 24" (600 mm) of cover. The volume of excavation will vary as depth of cover increases.

Special applications will be considered on a project by project basis. Please contact our application department should you have a unique application for our team to evaluate.



## 1.1 PRODUCT DESIGN

StormTech's commitment to thorough product testing programs, materials evaluation and adherence to national standards has resulted in two more superior products. Like other StormTech chambers, the MC-3500 and MC-4500 are designed to meet the full scope of design requirements of the American Society of Testing Materials (ASTM) International specification F2787 "Standard Practice for Structural Design of Thermoplastic Corrugated Wall Stormwater Collection Chambers" and produced to the requirements of the ASTM F 2418 "Standard Specification for Polypropylene (PP) Corrugated Stormwater Collection Chambers".

The StormTech MC-3500 and MC-4500 chambers provide the full AASHTO safety factors for live loads and permanent earth loads. The ASTM F 2787 standard provides specific guidance on how to design thermoplastic chambers in accordance with AASHTO Section 12.12. of the AASHTO LRFD Bridge Design Specifications. ASTM F 2787 requires that the safety factors included in the AASHTO guidance are achieved as a prerequisite to meeting ASTM F 2418. The three standards provide both the assurance of product quality and safe structural design.

The design of larger chambers in the same tradition of our other chambers required the collaboration of experts in soil-structure interaction, plastics and manufacturing. Years of extensive research, including laboratory testing and field verification, were required to produce chambers that are ready to meet both the rigors of installation and the longevity expected by engineers and owners.

This Design Manual provides the details and specifications necessary for consulting engineers to design stormwater management systems using the MC-3500 and MC-4500 chambers. It provides specifications for storage capacities, layout dimensions as well as requirements for design to ensure a long service life. The basic design concepts for foundation and backfill materials, subgrade bearing capacities and row spacing remain equally as pertinent for the MC-3500 and MC-4500 as the SC-740, SC-310 and DC-780 chamber systems. However, since many design values and dimensional requirements are different for these larger chambers than the SC-740, SC-310 and DC-780 chambers, design manuals and installation instructions are not interchangeable.

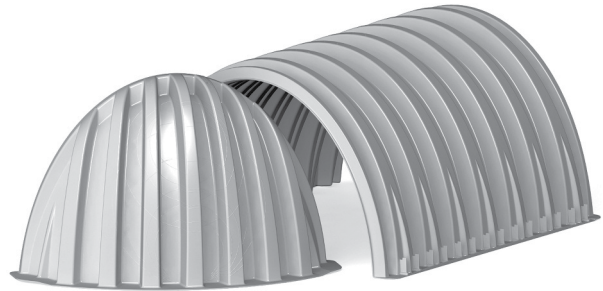
This manual includes only those details, dimensions, cover limits, etc for the MC-3500 and MC-4500 and is intended to be a stand-alone design guide for the MC-3500 and MC-4500 chambers. A Construction Guide specifically for these two chamber models has also been published.

## 1.2 TECHNICAL SUPPORT

The StormTech Technical Services Department is available to assist the engineer with the layout of MC-3500 and MC-4500 chamber systems and answer questions regarding all the StormTech chamber models. Call the Technical Services Department, email us at [info@stormtech.com](mailto:info@stormtech.com) or contact your local StormTech representative.

## 1.3 MC-3500 AND MC-4500 CHAMBERS

All StormTech chambers are designed to the full scope of AASHTO requirements without repeating end walls or other structural reinforcing. StormTech's continuously curved, elliptical arch and the surrounding angular backfill are the key components of the structural system. With the addition of patent pending integral stiffening ribs (**Figure 5**), the MC-3500 and MC-4500 are assured to provide a long, safe service life. Like other StormTech chambers, the MC-3500 and MC-4500 are produced from high quality, impact modified resins which are tested for short-term and long-term mechanical properties.



With all StormTech chambers, one chamber type is used for the start, middle and end of rows. Rows are formed by overlapping the upper joint corrugation of the next chamber over the lower joint corrugation of the previous chamber (**Figure 6**).

## 1.4 CHAMBER JOINTS

All StormTech chambers are designed with an optimized joining system. The height and width of the end corrugations have been designed to provide the required structural safety factors while providing an unobstructed flow path down each row.



To assist the contractor, StormTech chambers are molded with simple assembly instructions and arrows that indicate the direction in which to build rows. The corrugation valley immediately adjacent to the lower joint corrugation is marked “Overlap Here - Lower Joint.” The corrugation valley immediately adjacent to the upper joint corrugation is marked “Build This Direction - Upper Joint.”

Two people can safely and efficiently carry and place chambers without cumbersome connectors, special tools or heavy equipment. Each row of chambers must begin and end with a joint corrugation. Since joint corrugations are of a different size than the corrugations along the body of the chamber, chambers cannot be field cut and installed. Only whole MC-3500 and MC-4500 chambers can be used. For system layout assistance contact StormTech.

## 1.5 MC-3500 AND MC-4500 END CAPS

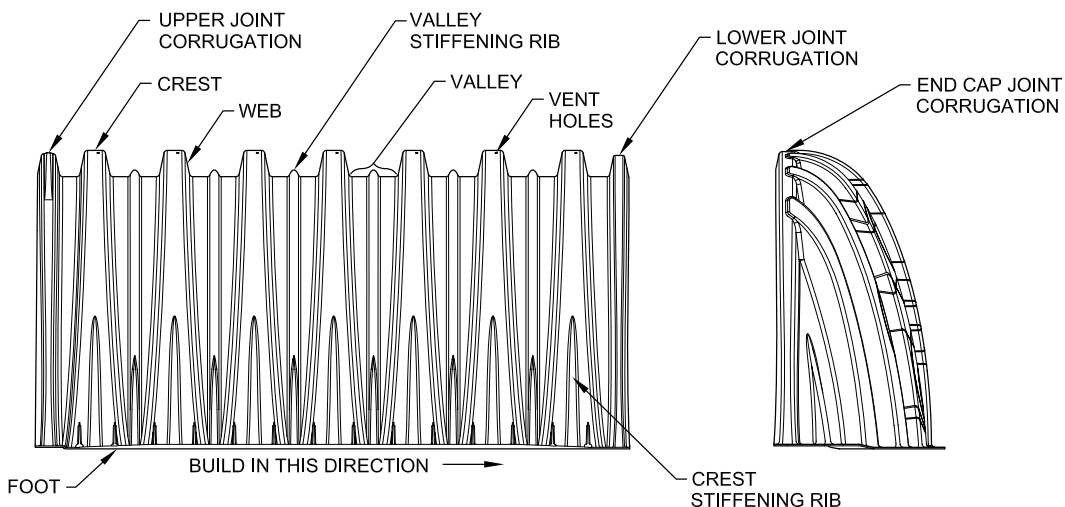
The MC-3500 and MC-4500 end caps are easy to install. These end caps are designed with a corrugation joint that fits over the top of either end of the chamber. The end cap joint is simply set over the top of either of the upper or lower chamber joint corrugations (**Figure 7**).

The MC-3500 end cap has pipe cutting guides for 12”–24” (300 mm–600 mm) top inverts (**Figure 9**).

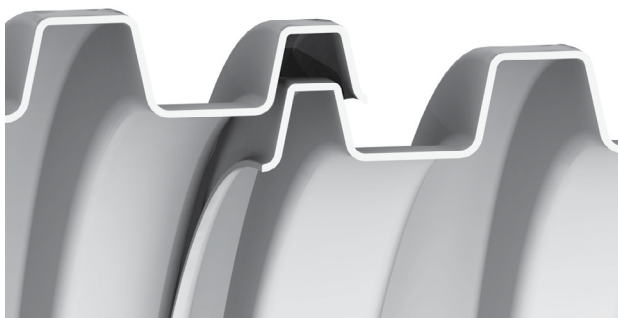
The MC-4500 end cap has pipe cutting guides for 12”–42” (300 mm–1050 mm) bottom inverts and 12”–24” (300 mm–600 mm) top inverts (**Figure 8**).

Standard and custom pre-cored end caps are available. Pre-cored end caps, 18” in diameter and larger include a welded crown plate.

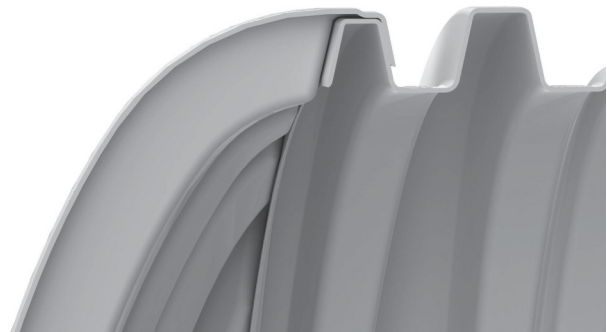
**FIGURE 5—Chamber and End Cap Components**



**FIGURE 6—Chamber Joint Overlap**

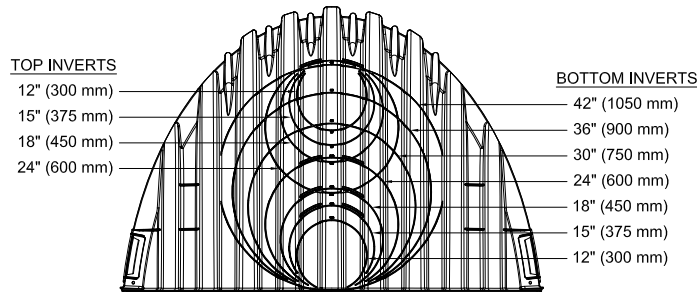


**FIGURE 7—End Cap Joint Overlap**

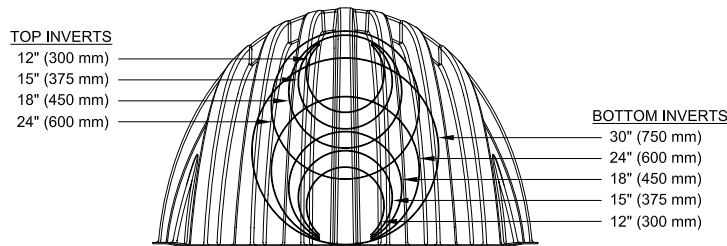




**FIGURE 8—MC-4500 End Cap Inverts**



**FIGURE 9—MC-3500 End Cap Inverts**

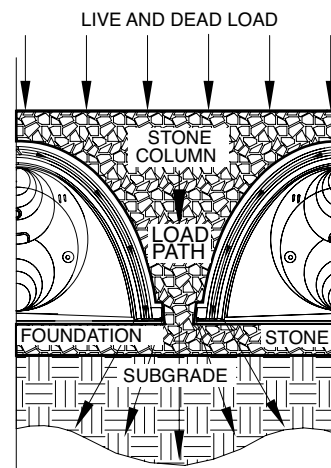


## 2.0 Foundations for Chambers

### 2.1 FOUNDATION REQUIREMENTS

StormTech chamber systems can be installed in various soil types. The subgrade bearing capacity and the cover height over the chambers determine the required depth of clean, crushed, angular foundation stone below the chambers. Foundation stone, also called bedding, is the stone between the subgrade soils and the feet of the chamber. Flexible structures are designed to transfer a significant portion of both live and dead loads through the surrounding soils. Chamber systems accomplish this by creating load paths through the columns of embedment stone between and around the rows of chambers. This creates load concentrations at the base of the columns between the rows. The foundation stone spreads out the concentrated loads to distributed loads that can be supported by the subgrade soils.

Since increasing the cover height (top of chamber to finished grade) causes increasing soil load, a greater depth of foundation stone is necessary to distribute the load to the subgrade soils. **Table 1** and **2** specify the minimum required foundation depths for varying cover heights and allowable subgrade bearing capacities. These tables are based on StormTech service loads. The minimum required foundation depth is 9" (230 mm) for both chambers.



### 2.2 WEAKER SOILS

StormTech has not provided guidance for subgrade bearing capacities less than 2000 pounds per square foot [(2.0 ksf) (96 kPa)]. These soils are often highly variable, may contain organic materials and could be more sensitive to moisture. A geotechnical engineer must be consulted if soils with bearing capacities less than 2000 psf (96 kPa) are present.

# 2.0 Foundations for Chambers

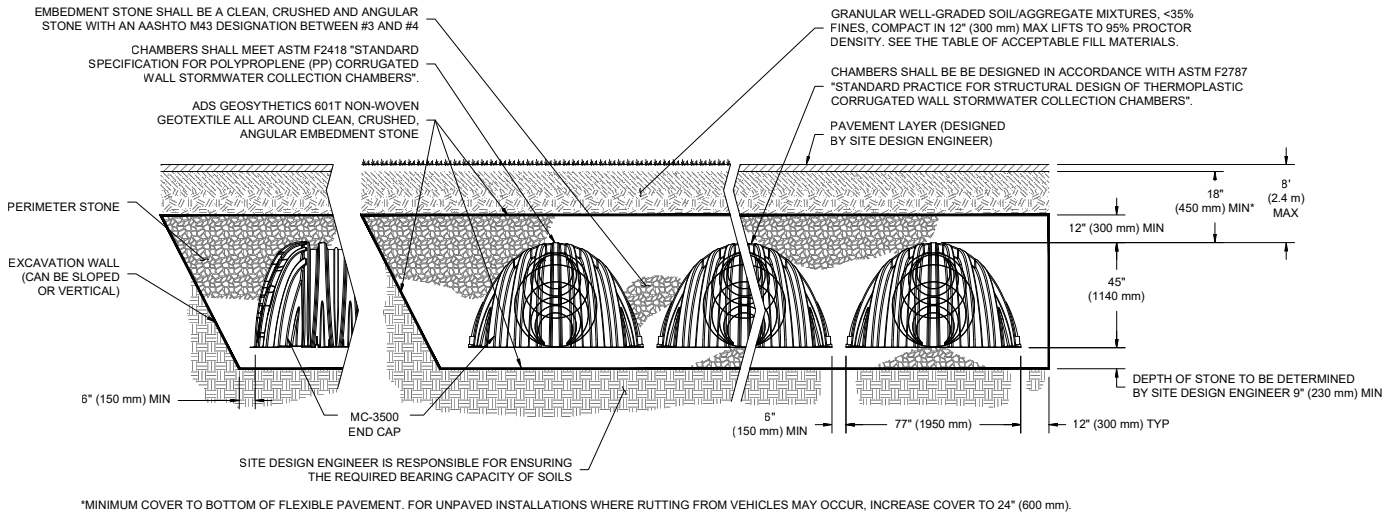
**TABLE 1—MC-3500 Minimum Required Foundation Depth in inches (millimeters)**

Assumes 6" (150 mm) row spacing.

Cover Hgt. ft. (m)	Minimum Bearing Resistance for Service Loads ksf (kPa)																								
	4.4 (211)	4.3 (206)	4.2 (201)	4.1 (196)	4.0 (192)	3.9 (187)	3.8 (182)	3.7 (177)	3.6 (172)	3.5 (168)	3.4 (163)	3.3 (158)	3.2 (153)	3.1 (148)	3.0 (144)	2.9 (139)	2.8 (134)	2.7 (129)	2.6 (124)	2.5 (120)	2.4 (115)	2.3 (110)	2.2 (105)	2.1 (101)	2.0 (96)
1.5 (0.46)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)
2.0 (0.61)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)
2.5 (0.76)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	18 (450)
3.0 (0.91)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	18 (450)	18 (450)
3.5 (1.07)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)
4.0 (1.22)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)
4.5 (1.37)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)
5.0 (1.52)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)
5.5 (1.68)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)
6.0 (1.83)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)
6.5 (1.98)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)
7.0 (2.13)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)
7.5 (2.30)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)
8.0 (2.44)	9 (230)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)	30 (750)

**NOTE:** The design engineer is solely responsible for assessing the bearing resistance (allowable bearing capacity) of the subgrade soils and determining the depth of foundation stone. Subgrade bearing resistance should be assessed with consideration for the range of soil moisture conditions expected under a stormwater system.

**FIGURE 10A—MC-3500 Structural Cross Section Detail (Not to Scale)**



Special applications will be considered on a project by project basis. Please contact our applications department should you have a unique application for our team to evaluate.

# 2.0 Foundations for Chambers

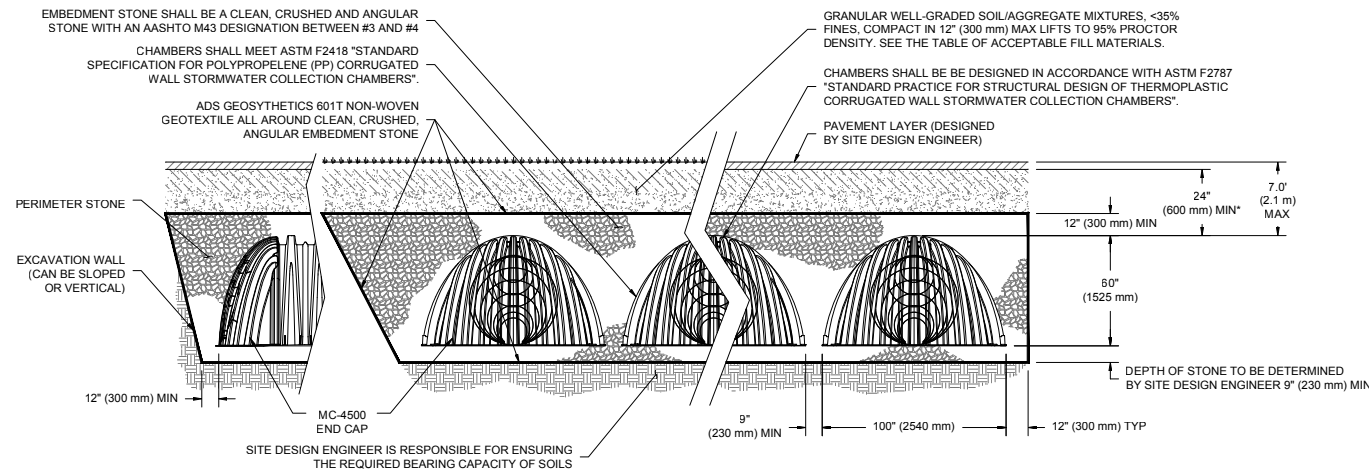
**TABLE 2—MC-4500 Minimum Required Foundation Depth in inches (millimeters)**

Assumes 9" (230 mm) row spacing.

Cover Hgt. ft. (m)	Minimum Bearing Resistance for Service Loads ksf (kPa)																								
	4.4 (211)	4.3 (206)	4.2 (201)	4.1 (196)	4.0 (192)	3.9 (187)	3.8 (182)	3.7 (177)	3.6 (172)	3.5 (168)	3.4 (163)	3.3 (158)	3.2 (153)	3.1 (148)	3.0 (144)	2.9 (139)	2.8 (134)	2.7 (129)	2.6 (124)	2.5 (120)	2.4 (115)	2.3 (110)	2.2 (105)	2.1 (101)	2.0 (96)
2.0 (0.61)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)
2.5 (0.76)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	18 (450)	24 (600)
3.0 (0.91)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)
3.5 (1.07)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)
4.0 (1.22)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)
4.5 (1.37)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)
5.0 (1.52)	9 (230)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	36 (900)
5.5 (1.68)	9 (230)	9 (230)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	36 (900)	36 (900)
6.0 (1.83)	9 (230)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	36 (900)	36 (900)	36 (900)	36 (900)
6.5 (1.98)	9 (230)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	36 (900)	36 (900)	36 (900)	42 (1050)
7.0 (2.13)	12 (300)	12 (300)	12 (300)	12 (300)	15 (375)	15 (375)	15 (375)	15 (375)	18 (450)	18 (450)	18 (450)	24 (600)	24 (600)	24 (600)	24 (600)	24 (600)	30 (750)	30 (750)	30 (750)	30 (750)	36 (900)	36 (900)	36 (900)	42 (1050)	42 (1050)

**NOTE:** The design engineer is solely responsible for assessing the bearing resistance (allowable bearing capacity) of the subgrade soils and determining the depth of foundation stone. Subgrade bearing resistance should be assessed with consideration for the range of soil moisture conditions expected under a stormwater system.

**FIGURE 10B—MC-4500 Structural Cross Section Detail (Not to Scale)**



Special applications will be considered on a project by project basis. Please contact our applications department should you have a unique application for our team to evaluate.

## 3.1 Foundation and Embedment Stone

The stone surrounding the chambers consists of the foundation stone below the chambers and embedment stone surrounding the chambers. The foundation stone and embedment stone are important components of the structural system and also provide open void space for stormwater storage. **Table 3** provides the stone specifications that achieve both structural requirements and a porosity of 40% for stormwater storage. **Figure 11** specifies the extents of each backfill stone location.

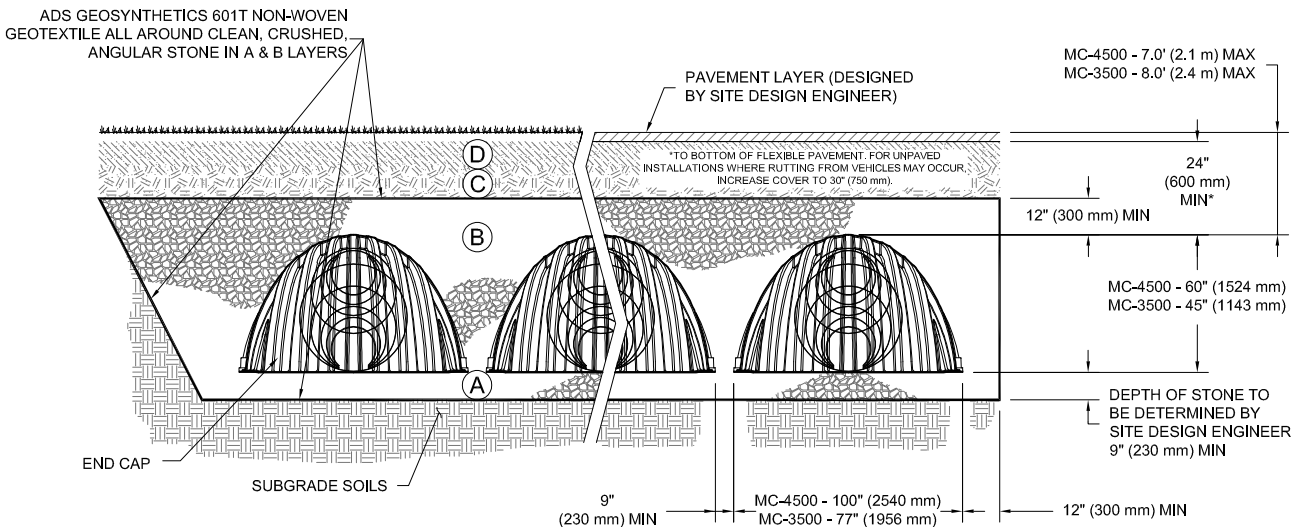
**TABLE 3—Acceptable Fill Materials**

MATERIAL LOCATION		DESCRIPTION	AASHTO DESIGNATION	COMPACTION/DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
C	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 <sup>1</sup> A-1,A-2-4,A-3 OR AASHTO M43 <sup>1</sup> 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTOINS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL-GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
B	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FORM THE FOUADATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 4	NO COMPACTION REQUIRED
A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 4	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. <sup>2,3</sup>

PLEASE NOTE:

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.

**FIGURE 11—Fill Material Locations**



Once layer 'C' is placed, any soil/material can be placed in layer 'D' up to the finished grade. Most pavement subbase soils can be used to replace the materials of layer 'C' or 'D' at the design engineer's discretion.



## 3.0 Required Materials/Row Separation

### 3.2 FILL ABOVE CHAMBERS

Refer to **Table 3** and **Figure 11** for acceptable fill material above the clean, crushed, angular stone. StormTech requires a minimum of 24" (600 mm) from the top of the chamber to the bottom of flexible pavement. For non-paved installations where rutting from vehicles may occur StormTech requires a minimum of 30" (750 mm) from top of chamber to finished grade.

### 3.3 GEOTEXTILE SEPARATION

A non-woven geotextile meeting AASHTO M288 Class 2 separation requirements must be installed to completely envelope the system and prevent soil intrusion into the crushed, angular stone. Overlap adjacent geotextile rolls per AASHTO M288 separation guidelines. Contact StormTech for a list of acceptable geotextiles.

### 3.4 PARALLEL ROW SEPARATION/ PERPENDICULAR BED SEPARATION

#### Parallel Row Separation

The minimum installed spacing between parallel rows after backfilling is 9" (230 mm) for the MC-4500 chambers and 6" (150mm) for the MC-3500 (measurement taken between the outside edges of the feet). Spacers may be used for layout convenience. Row spacing wider than the minimum spacing above may be specified.

#### Perpendicular Bed Separation

When beds are laid perpendicular to each other, a minimum installed spacing of 36" (900 mm) between beds is required.

### 3.5 Special Structural Designs

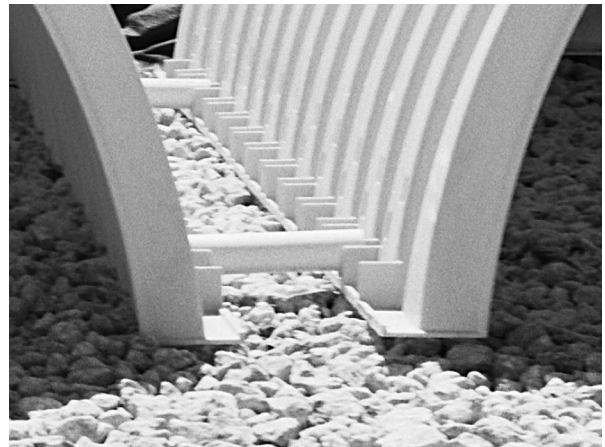
StormTech engineers may provide special structural designs to enable deeper cover depths or increase the capacity to carry higher live loads. Special designs may utilize the additional strength that can be achieved by compaction of embedment stone or by increasing the spacing between rows.

Increasing the spacing between chamber rows may also facilitate the application of StormTech chambers with either less foundation stone or with weaker subgrade soils. This may be a good option where vertical restrictions on site prevent the use of a deeper foundation.

Contact ADS Engineering Services for more information on special structural designs.



System Cross Section



Minimum Row Spacing

### 4.1 GENERAL

StormTech subsurface chamber systems offer the flexibility for a variety of inlet and outlet configurations. Contact the StormTech Technical Services Department or your local StormTech representative for assistance configuring inlet and outlet connections.

The open graded stone around and under the chambers provides a significant conveyance capacity ranging from approximately 0.8 cfs (23 l/s) to 13 cfs (368 l/s) per MC-3500 chamber and 0.54 cfs (15 l/s) to 8.5 cfs (240 l/s) for the MC-4500 chamber. The actual conveyance capacity is dependent upon stone size, depth of foundation stone and head of water. Although the high conveyance capacity of the open graded stone is an important component of the flow network, StormTech recommends that a system of inlet and outlet manifolds be designed to distribute and convey the peak flow through the chamber system.

It is the responsibility of the design engineer to provide the design flow rates and storage volumes for the stormwater system and to ensure that the final design meets all conveyance and storage requirements. However, StormTech will work with the design engineer to assist with manifold and chamber layouts that meet the design objectives.

### 4.2 THE ISOLATOR® ROW

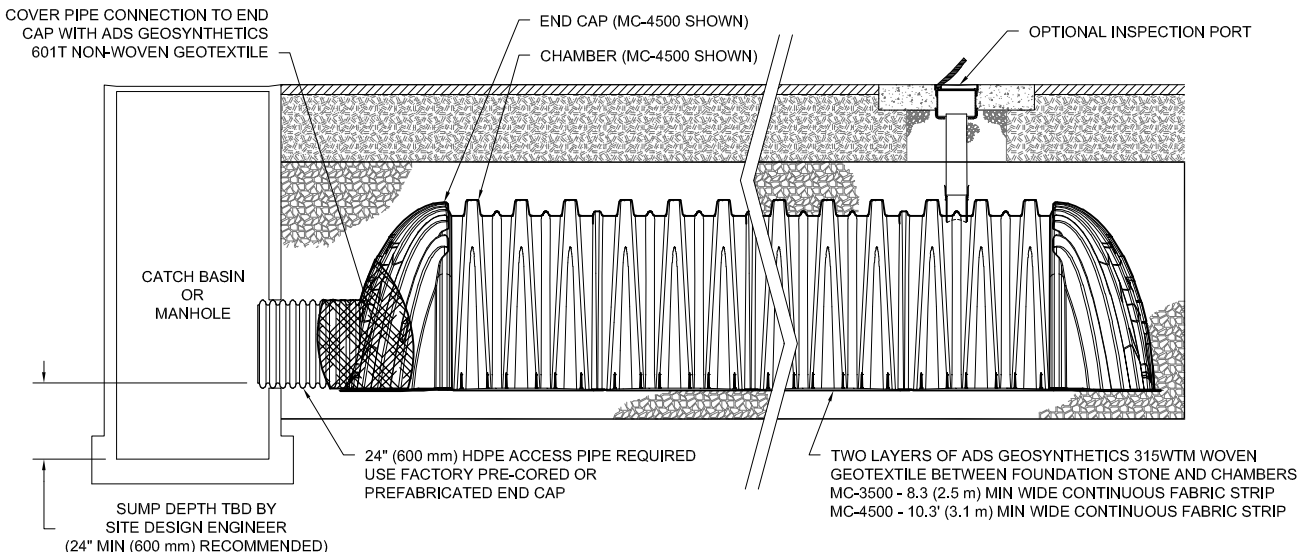
The Isolator Row is a patented system that inexpensively captures total suspended solids (TSS) and debris and provides easy access for inspection and maintenance. A double layer of woven geotextile between the bottom of the chambers and the foundation stone provides the filter media that satisfies most contaminant removal objectives. Each installed MC-3500 chamber and MC-3500 end cap provides 42.9 ft<sup>2</sup> (4.0 m<sup>2</sup>) and 7.5 ft<sup>2</sup> (0.7 m<sup>2</sup>) of bottom filter area respectively. Each installed MC-4500 chamber and MC-4500 end cap provides 30.1 ft<sup>2</sup> (2.80 m<sup>2</sup>) and 12.8 ft<sup>2</sup> (1.19 m<sup>2</sup>) of bottom filter area respectively.

The Isolator Row can be configured for maintenance objectives or, in some regulatory jurisdictions, for water quality objectives. For water quality applications, Isolator Rows can be sized based on water quality volume or flow rate.

All Isolator Rows require: 1) a manhole for maintenance access, 2) a means of diversion of flows to the Isolator Row and 3) a high flow bypass. Flow diversion can be accomplished by either a weir in the upstream access manhole or simply by feeding the Isolator Row at a lower elevation than the high flow bypass. Contact StormTech for assistance sizing Isolator Rows.

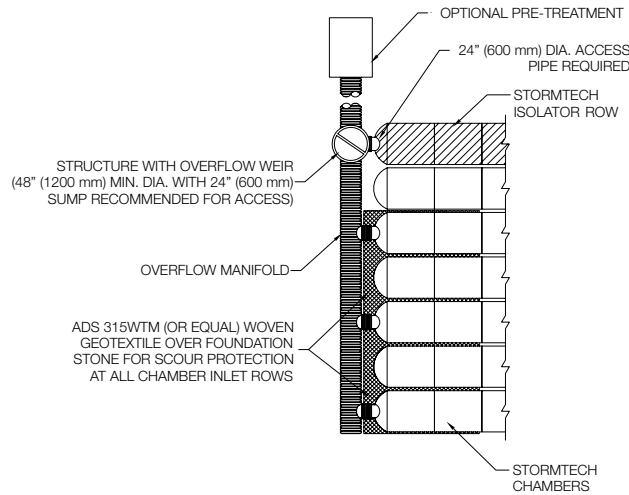
When additional stormwater treatment is required, StormTech systems can be configured using a treatment train approach where other stormwater BMPs are located in series.

**FIGURE 12—StormTech Isolator Row Detail**



# 4.0 Hydraulics

**FIGURE 13—Typical Inlet Configuration With Isolator Row and Scour Protection**



### 4.3 INLET MANIFOLDS

The primary function of the inlet manifold is to convey and distribute flows to a sufficient number of rows in the chamber bed such that there is ample conveyance capacity to pass the peak flows without creating an unacceptable backwater condition in upstream piping or scour the foundation stone under the chambers.

Manifolds are connected to the end caps either at the top or bottom of the end cap. Standard distances from the base of chamber to the invert of inlet and outlet manifolds connecting to StormTech end caps can be found in table 6. High inlet flow rates from either connection location produce a shear scour potential of the foundation stone. Inlet flows from top inlets also produce impingement scour potential. Scour potential is reduced when standing water is present over the foundation stone. However, for safe design across the wide range of applications, StormTech assumes minimal standing water at the time the design flow occurs.

To minimize scour potential, StormTech recommends the installation of woven scour protection fabric at each inlet row. This enables a protected transition zone from the concentrated flow coming out of the inlet pipe to a uniform flow across the entire width of the chamber for both top and bottom connections.

Allowable flow rates for design are dependent upon: the elevation of inlet pipe, foundation stone size and scour protection. With an appropriate scour protection geotextile installed from the end cap to at least 14.5 ft (4.42 m) in front of the inlet pipe for the MC-3500 and for the MC-4500, for both top and bottom feeds, the flow rates listed in **Table 4** can be used for all StormTech specified foundation stone gradations.

**\*See StormTech’s Tech Sheet #7 for manifold sizing guidance.**

**Table 4—Allowable Inlet Flows\***

Inlet Pipe Diameter Inches (mm)	Allowable Maximum Flow Rate cfs (l/s)
12 (300)	2.48 (70)
15 (375)	3.5 (99)
18 (450)	5.5 (156)
24 (600)	8.5 (241) [MC-3500]
24 (600)	9.5 (269) [MC-4500]

\*Assumes appropriate length of scour fabric per section 4.3

**Table 5—Maximum Outlet Flow Rate Capacities From StormTech Outlet Manifolds**

PIPE DIA.	FLOW (CFS)	FLOW (L/S)
6" (150 mm)	0.4	11.3
8" (200 mm)	0.7	19.8
10" (250 mm)	1.0	28.3
12" (300 mm)	2.0	56.6
15" (375 mm)	2.7	76.5
18" (450 mm)	4.0	113.3
24" (600 mm)	7.0	198.2
30" (750 mm)	11.0	311.5
36" (900 mm)	16.0	453.1
42" (1050 mm)	22.0	623.0
48" (1200 mm)	28.0	792.9

**Table 6—Standard Distances From Base of Chamber to Invert of Inlet and Outlet Manifolds on StormTech End Caps**

MC-3500 ENDCAPS			
	PIPE DIA.	INV. (IN)	INV. (MM)
TOP	6" (150 mm)	33.21	841
	8" (200 mm)	31.16	789
	10" (250 mm)	29.04	738
	12" (300 mm)	26.36	671
	15" (375 mm)	23.39	594
	18" (450 mm)	20.03	509
BOTTOM	24" (600 mm)	14.48	369
	12" (750 mm)	1.35	34
	15" (900 mm)	1.5	40
	18" (1050 mm)	1.77	46
24" (1200 mm)	2.06	52	
MC-4500 ENDCAPS			
	PIPE DIA.	INV. (IN)	INV. (MM)
	12" (300 mm)	35.69	907
	15" (375 mm)	32.72	831
	18" (450 mm)	29.36	746
	24" (600 mm)	23.05	585
BOTTOM	12" (750 mm)	1.55	34
	15" (900 mm)	1.7	43
	18" (1050 mm)	1.97	50
	24" (1200 mm)	2.26	57

## 4.4 OUTLET MANIFOLDS

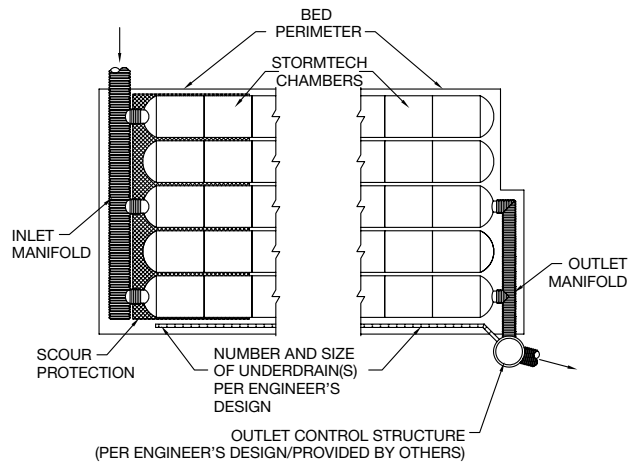
The primary function of the outlet manifold is to convey peak flows from the chamber system to the outlet control structure. Outlet manifolds are often sized for attenuated flows. They may be smaller in diameter and have fewer row connections than inlet manifolds. In some applications however, the intent of the outlet piping is to convey an unattenuated bypass flow rate and manifolds may be sized similar to inlet manifolds.

Since chambers are generally flowing at or near full at the time of the peak outlet flow rate, scour is generally not governing and outlet manifold sizing is based on pipe flow equations. In most cases, StormTech recommends that outlet manifolds connect the same rows that are connected to an inlet manifold. This provides a continuous flow path through open conduits to pass the peak flow without dependence on passing peak flows through stone.

The primary function of the underdrains is to draw down water stored in the stone below the invert of the manifold. Underdrains are generally not sized for conveyance of the peak flow.

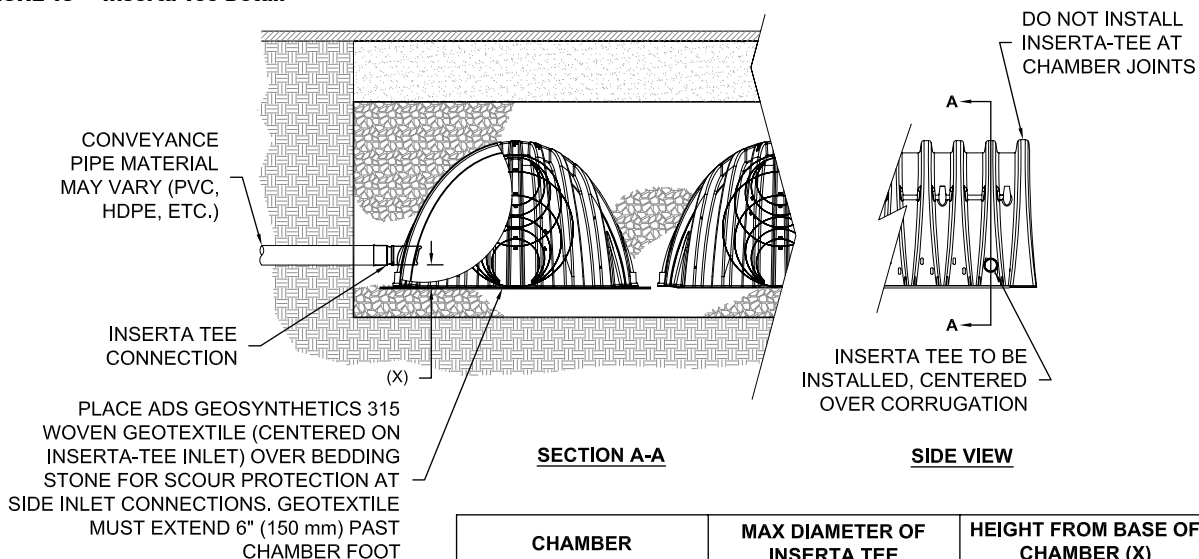
The maximum outlet flow rate capacities from StormTech outlet manifolds can be found in **Table 5**.

**FIGURE 14—Typical Inlet, Outlet and Underdrain Configuration**



## 4.5 INSERTA TEE INLET CONNECTIONS

**FIGURE 15—Inserta Tee Detail**



**NOTE:**  
PART NUMBERS WILL VARY BASED ON INLET PIPE MATERIALS. CONTACT STORMTECH FOR MORE INFORMATION.

CHAMBER	MAX DIAMETER OF INSERTA TEE	HEIGHT FROM BASE OF CHAMBER (X)
MC-3500	12" (250 mm)	6" (150 mm)
MC-4500	12" (250 mm)	8" (200 mm)

INSERTA TEE FITTINGS AVAILABLE FOR SDR 26, SDR 35, SCH 40 IPS GASKETED & SOLVENT WELD, N-12, HP STORM, C-900 OR DUCTILE IRON



# 5.0 Cumulative Storage Volumes



**Tables 7 and 8** provide cumulative storage volumes for the MC-3500 chamber and end cap. These tables can be used to calculate the stage-storage relationship for the retention or detention system. Digital spreadsheets in which the number of chambers and end caps can be input for quick

cumulative storage calculations are available at [www.stormtech.com](http://www.stormtech.com). For assistance with site-specific calculations or input into routing software, contact the StormTech Technical Services Department.

**TABLE 7 – MC-3500 Incremental Storage Volume Per Chamber**

Assumes 40% stone porosity. Calculations are based upon a 9" (230 mm) stone base under the chambers, 12" (300 mm) of stone above chambers, and 6" (150 mm) of spacing between chambers.

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
66 (1676)	0.00	175.02 (4.956)
65 (1651)	0.00	173.36 (4.909)
64 (1626)	0.00	171.71 (4.862)
63 (1600)	Stone 0.00	170.06 (4.816)
62 (1575)	Cover 0.00	168.41 (4.769)
61 (1549)	0.00	166.76 (4.722)
60 (1524)	0.00	165.10 (4.675)
59 (1499)	0.00	163.45 (4.628)
58 (1473)	0.00	161.80 (4.582)
57 (1448)	0.00	160.15 (4.535)
56 (1422)	0.00	158.49 (4.488)
55 (1397)	0.00	156.84 (4.441)
54 (1372)	109.95 (3.113)	155.19 (4.394)
53 (1346)	109.89 (3.112)	153.50 (4.347)
52 (1321)	109.69 (3.106)	151.73 (4.297)
51 (1295)	109.40 (3.098)	149.91 (4.245)
50 (1270)	109.00 (3.086)	148.01 (4.191)
49 (1245)	108.31 (3.067)	145.95 (4.133)
48 (1219)	107.28 (3.038)	143.68 (4.068)
47 (1194)	106.03 (3.003)	141.28 (4.000)
46 (1168)	104.61 (2.962)	138.77 (3.930)
45 (1143)	103.04 (2.918)	136.17 (3.856)
44 (1118)	101.33 (2.869)	133.50 (3.780)
43 (1092)	99.50 (2.818)	130.75 (3.702)
42 (1067)	97.56 (2.763)	127.93 (3.623)
41 (1041)	95.52 (2.705)	125.06 (3.541)
40 (1016)	93.39 (2.644)	122.12 (3.458)
39 (991)	91.16 (2.581)	119.14 (3.374)
38 (965)	88.86 (2.516)	116.10 (3.288)
37 (948)	86.47 (2.449)	113.02 (3.200)
36 (914)	84.01 (2.379)	109.89 (3.112)
35 (889)	81.49 (2.307)	106.72 (3.022)
34 (864)	78.89 (2.234)	103.51 (2.931)
33 (838)	76.24 (2.159)	100.27 (2.839)

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
32 (813)	73.52 (2.082)	96.98 (2.746)
31 (787)	70.75 (2.003)	93.67 (2.652)
30 (762)	67.92 (1.923)	90.32 (2.558)
29 (737)	65.05 (1.842)	86.94 (2.462)
28 (711)	62.12 (1.759)	83.54 (2.366)
27 (686)	59.15 (1.675)	80.10 (2.268)
26 (680)	56.14 (1.590)	76.64 (2.170)
25 (635)	53.09 (1.503)	73.16 (2.072)
24 (610)	49.99 (1.416)	69.65 (1.972)
23 (584)	46.86 (1.327)	66.12 (1.872)
22 (559)	43.70 (1.237)	62.57 (1.772)
21 (533)	40.50 (1.147)	59.00 (1.671)
20 (508)	37.27 (1.055)	55.41 (1.569)
19 (483)	34.01 (0.963)	51.80 (1.467)
18 (457)	30.72 (0.870)	48.17 (1.364)
17 (432)	27.40 (0.776)	44.53 (1.261)
16 (406)	24.05 (0.681)	40.87 (1.157)
15 (381)	20.69 (0.586)	37.20 (1.053)
14 (356)	17.29 (0.490)	33.51 (0.949)
13 (330)	13.88 (0.393)	29.81 (0.844)
12 (305)	10.44 (0.296)	26.09 (0.739)
11 (279)	6.98 (0.198)	22.37 (0.633)
10 (254)	3.51 (0.099)	18.63 (0.527)
9 (229)	0.00	14.87 (0.421)
8 (203)	0.00	13.22 (0.374)
7 (178)	0.00	11.57 (0.328)
6 (152)	Stone 0.00	9.91 (0.281)
5 (127)	Foundation 0.00	8.26 (0.234)
4 (102)	0.00	6.61 (0.187)
3 (76)	0.00	4.96 (0.140)
2 (51)	0.00	3.30 (0.094)
1 (25)	0.00	1.65 (0.047)

*NOTE: Add 1.65 ft<sup>3</sup> (0.047 m<sup>3</sup>) of storage for each additional inch (25 mm) of stone foundation. Contact StormTech for cumulative volume spreadsheets in digital format.*

# 5.0 Cumulative Storage Volume



**TABLE 8 – MC-3500 Incremental Storage Volume Per End Cap**

Assumes 40% stone porosity. Calculations are based upon a 9" (230 mm) stone base under the chambers, 12" (300 mm) of stone above end caps, and 6" (150 mm) of spacing between end caps and 6" (150 mm) of stone perimeter.

Depth of Water in System Inches (mm)	Cumulative End Cap Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
66 (1676)	0.00	45.10 (1.277)
65 (1651)	0.00	44.55 (1.262)
64 (1626)	0.00	44.00 (1.246)
63 (1600)	Stone 0.00	43.46 (1.231)
62 (1575)	Cover 0.00	42.91 (1.215)
61 (1549)	0.00	42.36 (1.200)
60 (1524)	0.00	41.81 (1.184)
59 (1499)	0.00	41.27 (1.169)
58 (1473)	0.00	40.72 (1.153)
57 (1448)	0.00	40.17 (1.138)
56 (1422)	0.00	39.62 (1.122)
55 (1397)	0.00	39.08 (1.107)
54 (1372)	15.64 (0.443)	38.53 (1.091)
53 (1346)	15.64 (0.443)	37.98 (1.076)
52 (1321)	15.63 (0.443)	37.42 (1.060)
51 (1295)	15.62 (0.442)	36.85 (1.043)
50 (1270)	15.60 (0.442)	36.27 (1.027)
49 (1245)	15.56 (0.441)	35.68 (1.010)
48 (1219)	15.51 (0.439)	35.08 (0.993)
47 (1194)	15.44 (0.437)	34.47 (0.976)
46 (1168)	15.35 (0.435)	33.85 (0.959)
45 (1143)	15.25 (0.432)	33.22 (0.941)
44 (1118)	15.13 (0.428)	32.57 (0.922)
43 (1092)	14.99 (0.424)	31.91 (0.904)
42 (1067)	14.83 (0.420)	31.25 (0.885)
41 (1041)	14.65 (0.415)	30.57 (0.866)
40 (1016)	14.45 (0.409)	29.88 (0.846)
39 (991)	14.24 (0.403)	29.18 (0.826)
38 (965)	14.00 (0.396)	28.48 (0.806)
37 (948)	13.74 (0.389)	27.76 (0.786)
36 (914)	13.47 (0.381)	27.04 (0.766)
35 (889)	13.18 (0.373)	26.30 (0.745)
34 (864)	12.86 (0.364)	25.56 (0.724)

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
33 (838)	12.53 (0.355)	24.82 (0.703)
32 (813)	12.18 (0.345)	24.06 (0.681)
31 (787)	11.81 (0.335)	23.30 (0.660)
30 (762)	11.42 (0.323)	22.53 (0.638)
29 (737)	11.01 (0.312)	21.75 (0.616)
28 (711)	10.58 (0.300)	20.96 (0.594)
27 (686)	10.13 (0.287)	20.17 (0.571)
26 (680)	9.67 (0.274)	19.37 (0.549)
25 (635)	9.19 (0.260)	18.57 (0.526)
24 (610)	8.70 (0.246)	17.76 (0.503)
23 (584)	8.19 (0.232)	16.94 (0.480)
22 (559)	7.67 (0.217)	16.12 (0.456)
21 (533)	7.13 (0.202)	15.29 (0.433)
20 (508)	6.59 (0.187)	14.45 (0.409)
19 (483)	6.03 (0.171)	13.61 (0.385)
18 (457)	5.46 (0.155)	12.76 (0.361)
17 (432)	4.88 (0.138)	11.91 (0.337)
16 (406)	4.30 (0.122)	11.06 (0.313)
15 (381)	3.70 (0.105)	10.20 (0.289)
14 (356)	3.10 (0.088)	9.33 (0.264)
13 (330)	2.49 (0.071)	8.46 (0.240)
12 (305)	1.88 (0.053)	7.59 (0.215)
11 (279)	1.26 (0.036)	6.71 (0.190)
10 (254)	0.63 (0.018)	5.83 (0.165)
9 (229)	0.00	4.93 (0.139)
8 (203)	0.00	4.38 (0.124)
7 (178)	0.00	3.83 (0.108)
6 (152)	Stone 0.00	3.28 (0.093)
5 (127)	Foundation 0.00	2.74 (0.077)
4 (102)	0.00	2.19 (0.062)
3 (76)	0.00	1.64 (0.046)
2 (51)	0.00	1.09 (0.031)
1 (25)	0.00	0.55 (0.015)

NOTE: Add 0.56 ft<sup>3</sup> (0.016 m<sup>3</sup>) of storage for each additional inch (25 mm) of stone foundation. Contact StormTech for cumulative volume spreadsheets in digital format.

# 5.0 Cumulative Storage Volumes



Tables 9 and 10 provide cumulative storage volumes for the MC-4500 chamber and end cap. These tables can be used to calculate the stage-storage relationship for the retention or detention system. Digital spreadsheets in which the number of chambers and end caps can be input for quick

cumulative storage calculations are available at [www.stormtech.com](http://www.stormtech.com). For assistance with site-specific calculations or input into routing software, contact the StormTech Technical Services Department.

**TABLE 9 – MC-4500 Incremental Storage Volume Per Chamber**

Assumes 40% stone porosity. Calculations are based upon a 9" (230 mm) stone base under the chambers, 12" (300 mm) of stone above chambers, and 9" (230 mm) of spacing between chambers.

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
81 (2057)	0.00	162.62 (4.065)
80 (2032)	0.00	161.40 (4.570)
79 (2007)	0.00	160.18 (4.536)
78 (1981)	Stone 0.00	158.98 (4.501)
77 (1956)	Cover 0.00	157.74 (4.467)
76 (1930)	0.00	156.62 (4.432)
75 (1905)	0.00	155.30 (4.398)
74 (1880)	0.00	154.09 (4.363)
73 (1854)	0.00	152.87 (4.329)
72 (1829)	0.00	151.65 (4.294)
71 (1803)	0.00	150.43 (4.294)
70 (1778)	0.00	149.21 (4.225)
69 (1753)	106.51 (3.016)	147.99 (4.191)
68 (1727)	106.47 (3.015)	146.75 (4.156)
67 (1702)	106.35 (3.012)	145.46 (4.119)
66 (1676)	106.18 (3.007)	144.14 (4.082)
65 (1651)	105.98 (3.001)	142.80 (4.044)
64 (1626)	105.71 (2.993)	141.42 (4.005)
63 (1600)	105.25 (2.981)	139.93 (3.962)
62 (1575)	104.59 (2.962)	138.31 (3.917)
61 (1549)	103.79 (2.939)	136.61 (3.869)
60 (1524)	102.88 (2.913)	134.85 (3.819)
59 (1499)	101.88 (2.885)	133.03 (3.767)
58 (1473)	100.79 (2.854)	131.16 (3.714)
57 (1448)	99.63 (2.821)	129.24 (3.660)
56 (1422)	98.39 (2.786)	127.28 (3.604)
55 (1397)	97.10 (2.749)	125.28 (3.548)
54 (1372)	95.73 (2.711)	123.25 (3.490)
53 (1346)	94.32 (2.671)	121.18 (3.490)
52 (1321)	92.84 (2.629)	119.08 (3.372)
51 (1295)	91.32 (2.586)	116.94 (3.311)
50 (1270)	89.74 (2.541)	114.78 (3.250)
49 (1245)	88.12 (2.495)	112.59 (3.188)
48 (1219)	86.45 (2.448)	110.37 (3.125)
47 (1194)	84.75 (2.400)	108.13 (3.062)
46 (1168)	83.00 (2.350)	105.86 (2.998)
45 (1143)	81.21 (2.300)	103.56 (2.933)
44 (1118)	79.38 (2.248)	101.25 (2.867)
43 (1092)	77.52 (2.195)	98.91 (2.801)

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
42 (1067)	75.62 (2.141)	96.55 (2.734)
41 (1041)	73.69 (2.087)	94.18 (2.667)
40 (1016)	71.72 (2.031)	91.78 (2.599)
39 (991)	69.73 (1.974)	89.36 (2.531)
38 (965)	67.70 (1.917)	86.93 (2.462)
37 (948)	65.65 (1.859)	84.48 (2.392)
36 (914)	63.57 (1.800)	82.01 (2.322)
35 (889)	61.46 (1.740)	79.53 (2.252)
34 (864)	59.32 (1.680)	77.03 (2.181)
33 (838)	57.17 (1.619)	74.52 (2.110)
32 (813)	54.98 (1.557)	71.99 (2.038)
31 (787)	52.78 (1.495)	69.45 (1.966)
30 (762)	50.55 (1.431)	66.89 (1.894)
29 (737)	48.30 (1.368)	64.32 (1.821)
28 (711)	46.03 (1.303)	61.74 (1.748)
27 (686)	43.74 (1.239)	59.19 (1.675)
26 (680)	41.43 (1.173)	56.55 (1.601)
25 (610)	39.11 (1.107)	53.93 (1.527)
24 (609)	36.77 (1.041)	51.31 (1.453)
23 (584)	34.41 (0.974)	48.67 (1.378)
22 (559)	32.03 (0.907)	46.03 (1.303)
21 (533)	29.64 (0.839)	43.38 (1.228)
20 (508)	27.23 (0.771)	40.71 (1.153)
19 (483)	24.81 (0.703)	38.04 (1.077)
18 (457)	22.38 (0.634)	35.37 (1.001)
17 (432)	19.94 (0.565)	32.68 (0.925)
16 (406)	17.48 (0.495)	29.99 (0.849)
15 (381)	15.01 (0.425)	27.29 (0.773)
14 (356)	12.53 (0.355)	24.58 (0.696)
13 (330)	10.05 (0.284)	21.87 (0.619)
12 (305)	7.55 (0.214)	19.15 (0.542)
11 (279)	5.04 (0.143)	16.43 (0.465)
10 (254)	2.53 (0.072)	13.70 (0.388)
9 (229)	0.00	10.97 (0.311)
8 (203)	0.00	9.75 (0.276)
7 (178)	0.00	8.53 (0.242)
6 (152)	Stone 0.00	7.31 (0.207)
5 (127)	Foundation 0.00	6.09 (0.173)
4 (102)	0.00	4.87 (0.138)
3 (76)	0.00	3.66 (0.104)
2 (51)	0.00	2.44 (0.069)
1 (25)	0.00	1.22 (0.035)

NOTE: Add 1.22 ft<sup>3</sup> (0.035 m<sup>3</sup>) of storage for each additional inch (25 mm) of stone foundation. Contact StormTech for cumulative volume spreadsheets in digital format.

# 5.0 Cumulative Storage Volumes



**TABLE 10 – MC-4500 Incremental Storage Volume Per End Cap**

Assumes 40% stone porosity. Calculations are based upon a 9" (230 mm) stone base under the chambers, 12" (300 mm) of stone above end caps, and 9" (230 mm) of spacing between end caps and 6" (150 mm) of stone perimeter.

Depth of Water in System Inches (mm)	Cumulative End Cap Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
81 (2057)	0.00	115.28 (3.264)
80 (2032)	0.00	114.15 (3.232)
79 (2007)	0.00	113.02 (3.200)
78 (1981)	Stone 0.00	111.89 (3.168)
77 (1956)	Cover 0.00	110.76 (3.136)
76 (1930)	0.00	109.63 (3.104)
75 (1905)	0.00	108.50 (3.072)
74 (1880)	0.00	107.37 (3.040)
73 (1854)	0.00	106.24 (3.008)
72 (1829)	0.00	105.11 (2.976)
71 (1803)	0.00	103.98 (2.944)
70 (1778)	0.00	102.85 (2.912)
69 (1753)	39.54 (1.120)	101.72 (2.880)
68 (1727)	39.53 (1.119)	100.58 (2.848)
67 (1702)	39.50 (1.118)	99.43 (2.816)
66 (1676)	39.45 (1.117)	98.27 (2.783)
65 (1651)	39.38 (1.115)	97.10 (2.750)
64 (1626)	39.30 (1.113)	95.92 (2.716)
63 (1600)	39.19 (1.110)	94.73 (2.682)
62 (1575)	39.06 (1.106)	93.52 (2.648)
61 (1549)	38.90 (1.101)	92.29 (2.613)
60 (1524)	38.71 (1.096)	91.04 (2.578)
59 (1499)	38.49 (1.090)	89.78 (2.542)
58 (1473)	38.24 (1.083)	88.50 (2.506)
57 (1448)	37.97 (1.075)	87.21 (2.469)
56 (1422)	37.67 (1.067)	85.90 (2.432)
55 (1397)	37.34 (1.057)	84.57 (2.395)
54 (1372)	36.98 (1.047)	83.23 (2.357)
53 (1346)	36.60 (1.036)	81.87 (2.318)
52 (1321)	36.19 (1.025)	80.49 (2.279)
51 (1295)	35.75 (1.012)	79.10 (2.240)
50 (1270)	35.28 (0.999)	77.69 (2.200)
49 (1245)	34.79 (0.985)	76.26 (2.159)
48 (1219)	34.27 (0.970)	74.82 (2.119)
47 (1194)	33.72 (0.955)	73.36 (2.077)
46 (1168)	33.15 (0.939)	71.89 (2.036)
45 (1143)	32.57 (0.922)	70.40 (1.994)
44 (1118)	31.96 (0.905)	68.91 (1.951)
43 (1092)	31.32 (0.887)	67.40 (1.909)

Depth of Water in System Inches (mm)	Cumulative Chamber Storage ft <sup>3</sup> (m <sup>3</sup> )	Total System Cumulative Storage ft <sup>3</sup> (m <sup>3</sup> )
42 (1067)	30.68 (0.869)	65.88 (1.866)
41 (1041)	30.00 (0.850)	64.35 (1.822)
40 (1016)	29.30 (0.830)	62.80 (1.778)
39 (991)	28.58 (0.809)	61.23 (1.734)
38 (965)	27.84 (0.788)	59.65 (1.689)
37 (948)	27.07 (0.767)	58.07 (1.644)
36 (914)	26.29 (0.744)	56.46 (1.599)
35 (889)	25.48 (0.722)	54.85 (1.553)
34 (864)	24.66 (0.698)	53.23 (1.507)
33 (838)	23.83 (0.675)	51.60 (1.461)
32 (813)	22.98 (0.651)	49.96 (1.415)
31 (787)	22.12 (0.626)	48.31 (1.368)
30 (762)	21.23 (0.601)	46.65 (1.321)
29 (737)	20.32 (0.575)	44.97 (1.273)
28 (711)	19.40 (0.549)	43.29 (1.226)
27 (686)	18.48 (0.523)	41.61 (1.178)
26 (680)	17.54 (0.497)	39.91 (1.130)
25 (610)	16.59 (0.470)	38.21 (1.082)
24 (609)	15.62 (0.442)	36.50 (1.033)
23 (584)	14.64 (0.414)	34.78 (0.985)
22 (559)	13.66 (0.387)	33.07 (0.936)
21 (533)	12.66 (0.359)	31.33 (0.887)
20 (508)	11.65 (0.330)	29.60 (0.838)
19 (483)	10.63 (0.301)	27.85 (0.789)
18 (457)	9.60 (0.272)	26.11 (0.739)
17 (432)	8.56 (0.242)	24.35 (0.690)
16 (406)	7.51 (0.213)	22.59 (0.640)
15 (381)	6.46 (0.183)	20.83 (0.590)
14 (356)	5.41 (0.153)	19.07 (0.540)
13 (330)	4.35 (0.123)	17.31 (0.490)
12 (305)	3.28 (0.093)	15.53 (0.440)
11 (279)	2.19 (0.062)	13.75 (0.389)
10 (254)	1.11 (0.031)	11.97 (0.339)
9 (229)	0.00	10.17 (0.288)
8 (203)	0.00	9.04 (0.256)
7 (178)	0.00	7.91 (0.224)
6 (152)	Stone 0.00	6.78 (0.192)
5 (127)	Foundation 0.00	5.65 (0.160)
4 (102)	0.00	4.52 (0.128)
3 (76)	0.00	3.39 (0.096)
2 (51)	0.00	2.26 (0.064)
1 (25)	0.00	1.13 (0.032)

NOTE: Add 1.08 ft<sup>3</sup> (0.031 m<sup>3</sup>) of storage for each additional inch (25 mm) of stone foundation. Contact StormTech for cumulative volume spreadsheets in digital format.

The following steps provide the calculations necessary for preliminary sizing of an MC-3500 chamber system. For custom bed configurations to fit specific sites, contact the StormTech Technical Services Department or your local StormTech representative.

**1) Determine the amount of storage volume (VS) required.** It is the design engineer's sole responsibility to determine the storage volume required.

**TABLE 11—Storage Volume Per Chamber/End Cap ft<sup>3</sup> (m<sup>3</sup>)**

	Bare Unit Storage ft <sup>3</sup> (m <sup>3</sup> )	Chamber/End Cap and Stone Volume — Stone Foundation Depth in. (mm)			
		9 (230)	12 (300)	15 (375)	18 (450)
<b>MC-3500 Chamber</b>	109.9 (3.11)	175.0 (4.96)	179.9 (5.09)	184.9 (5.24)	189.9 (5.38)
<b>MC-3500 End Cap</b>	14.9 (0.42)	45.1 (1.28)	46.6 (1.32)	48.3 (1.37)	49.9 (1.41)

*NOTE: Assumes 6" (150 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume. End cap volume assumes 6" (150 mm) stone perimeter.*

**2) Determine the number of chambers (C) required.** To calculate the number of chambers required for adequate storage, divide the storage volume (Vs) by the storage volume of the chamber (from **Table 11**), as follows: **C = Vs / Storage Volume per Chamber**

**3) Determine the number of end caps required.** The number of end caps (EC) required depends on the number of rows required by the project. Once the number of chamber rows is determined, multiply the number of chamber rows by 2 to determine the number of end caps required. **EC = No. of Chamber Rows x 2**

*NOTE: Additional end caps may be required for systems having inlet locations within the chamber bed.*

**4) Determine additional storage provided by end caps.** End Caps will provide additional storage to the project. Multiply the number of end caps (EC) by the storage volume per end cap (ECS) to determine the additional storage (As) provided by the end caps. **As = EC x ECS**

**5) Adjust number of chambers (C) to account for additional end cap storage (As).** The original number of chambers (C) can now be reduced due to the additional storage in the end caps. Divide the additional storage (As) by the storage volume per chamber to determine the number of chambers that can be removed. **Number of chambers to remove = As/ volume per chamber**

*NOTE: Additional storage exists in the stone perimeter as well as in the inlet and outlet manifold systems. Contact StormTech's Technical Services Department for assistance with determining the number of chambers and end caps required for your project.*

**6) Determine the required bed size (S).** The size of the bed will depend on the number of chambers and end caps required:

**MC-3500 area per chamber = 49.6 ft<sup>2</sup> (4.6 m<sup>2</sup>)**  
**MC-3500 area per end cap = 16.4 ft<sup>2</sup> (1.5 m<sup>2</sup>)**

$$S = (C \times \text{area per chamber}) + (EC \times \text{area per end cap})$$

*NOTE: It is necessary to add 12" (300 mm) of stone perimeter parallel to the chamber rows and 6" (150 mm) of stone perimeter from the base of all end caps. The additional area due to perimeter stone is not included in the area numbers above.*

**7) Determine the amount of stone (Vst) required.** To calculate the total amount of clean, crushed, angular stone required, multiply the number of chambers (C) and the number of end caps (EC) by the selected weight of stone from **Table 12**.

*NOTE: Clean, crushed, angular stone is also required around the perimeter of the system.*

**TABLE 12—Amount of Stone Per Chamber/End Cap**

ENGLISH tons (yd <sup>3</sup> )	Stone Foundation Depth			
	9"	12"	15"	18"
<b>MC-3500</b>	8.5 (6.0)	9.1 (6.5)	9.7 (6.9)	10.4 (7.4)
<b>End Cap</b>	3.9 (2.8)	4.1 (2.9)	4.3 (3.1)	4.5 (3.2)
METRIC kg (m <sup>3</sup> )	230 mm	300 mm	375 mm	450 mm
<b>MC-3500</b>	7711 (4.6)	8255 (5.0)	8800 (5.3)	9435 (5.7)
<b>End Cap</b>	3538 (2.1)	3719 (2.2)	3901 (2.4)	4082 (2.5)

*NOTE: Assumes 12" (300 mm) of stone above, and 6" (150 mm) row spacing, and 6" (150 mm) of perimeter stone in front of end caps.*

**8) Determine the volume of excavation (Ex) required.** Each additional foot of cover will add a volume of excavation of 1.9 yd<sup>3</sup> (1.5 m<sup>3</sup>) per MC-3500 chamber and

**TABLE 13—Volume of Excavation Per Chamber/End Cap yd<sup>3</sup> (m<sup>3</sup>)**

	Stone Foundation Depth			
	9" (230 mm)	12" (300 mm)	15" (375 mm)	18" (450 mm)
<b>MC-3500</b>	11.9 (9.1)	12.4 (9.5)	12.8 (9.8)	13.3 (10.2)
<b>End Cap</b>	4.0 (3.1)	4.1 (3.2)	4.3 (3.3)	4.4 (3.4)

*NOTE: Assumes 6" (150 mm) separation between chamber rows, 6" (150 mm) of perimeter in front of end caps, and 24" (600 mm) of cover. The volume of excavation will vary as the depth of cover increases.*

0.6 yd<sup>3</sup> (0.5 m<sup>3</sup>) per MC-3500 end cap.

**9) Determine the area of geotextile (F) required.** The bottom, top and sides of the bed must be covered with a non-woven geotextile (filter fabric) that meets AASHTO M288 Class 2 requirements. The area of the sidewalls must be calculated and a 24" (600 mm) overlap must be included for all seams. Geotextiles typically come in 15 foot (4.57 m) wide rolls.



The following steps provide the calculations necessary for preliminary sizing of an MC-4500 chamber system. For custom bed configurations to fit specific sites, contact the StormTech Technical Services Department or your local StormTech representative.

**1) Determine the amount of storage volume (VS) required.** It is the design engineer's sole responsibility to determine the storage volume required.

**TABLE 14—Storage Volume Per Chamber/End Cap ft<sup>3</sup> (m<sup>3</sup>)**

	Bare Unit Storage ft <sup>3</sup> (m <sup>3</sup> )	Chamber/End Cap and Stone Volume — Stone Foundation Depth in. (mm)			
		9 (230)	12 (300)	15 (375)	18 (450)
<b>MC-4500 Chamber</b>	106.5 (3.01)	162.6 (4.60)	166.3 (4.71)	169.9 (4.81)	173.6 (4.91)
<b>MC-4500 End Cap</b>	39.5 (1.12)	115.3 (3.26)	118.6 (3.36)	121.9 (3.45)	125.2 (3.54)

*NOTE: Assumes 9" (230 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume. End cap volume assumes 12" (300 mm) stone perimeter.*

**2) Determine the number of chambers (C) required.** To calculate the number of chambers required for adequate storage, divide the storage volume (Vs) by the storage volume of the chamber (from **Table 14**), as follows: **C = Vs / Storage Volume per Chamber**

**3) Determine the number of end caps required.** The number of end caps (EC) required depends on the number of rows required by the project. Once the number of chamber rows is determined, multiply the number of chamber rows by 2 to determine the number of end caps required. **EC = No. of Chamber Rows x 2**

*NOTE: Additional end caps may be required for systems having inlet locations within the chamber bed.*

**4) Determine additional storage provided by end caps.** End Caps will provide additional storage to the project. Multiply the number of end caps (EC) by the storage volume per end cap (ECS) to determine the additional storage (As) provided by the end caps. **As = EC x ECS**

**5) Adjust number of chambers (C) to account for additional end cap storage (As).** The original number of chambers (C) can now be reduced due to the additional storage in the end caps. Divide the additional storage (As) by the storage volume per chamber to determine the number of chambers that can be removed. **Number of chambers to remove = As/ volume per chamber**

*NOTE: Additional storage exists in the stone perimeter as well as in the inlet and outlet manifold systems. Contact StormTech's Technical Services Department for assistance with determining the number of chambers and end caps required for your project.*

**6) Determine the required bed size (S).** The size of the bed will depend on the number of chambers and end caps required:

**MC-4500 area per chamber = 36.6 ft<sup>2</sup> (3.4 m<sup>2</sup>)**  
**MC-4500 area per end cap = 23.9 ft<sup>2</sup> (2.2 m<sup>2</sup>)**

**S = (C x area per chamber) + (EC x area per end cap)**

*NOTE: It is necessary to add 12" (300 mm) of stone perimeter parallel to the chamber rows and 6" (150 mm) of stone perimeter from the base of all end caps. The additional area due to perimeter stone is not included in the area numbers above.*

**7) Determine the amount of stone (Vst) required.** To calculate the total amount of clean, crushed, angular stone required, multiply the number of chambers (C) and the number of end caps (EC) by the selected weight of stone from **Table 15**.

*NOTE: Clean, crushed, angular stone is also required around the perimeter of the system.*

**TABLE 15—Amount of Stone Per Chamber**

ENGLISH tons (yd <sup>3</sup> )	Stone Foundation Depth			
	9"	12"	15"	18"
<b>MC-4500</b>	7.4 (5.2)	7.8 (5.5)	8.3 (5.9)	8.8 (6.2)
<b>End Cap</b>	9.8 (7.0)	10.2 (7.3)	10.6 (7.6)	11.1 (7.9)
METRIC kg (m <sup>3</sup> )	230 mm	300 mm	375 mm	450 mm
<b>MC-4500</b>	6681 (4.0)	7117 (4.2)	7552 (4.5)	7987 (4.7)
<b>End Cap</b>	8890 (5.3)	9253 (5.5)	9616 (5.8)	10069 (6.0)

*NOTE: Assumes 12" (300 mm) of stone above, and 9" (230 mm) row spacing, and 12" (300 mm) of perimeter stone in front of end caps.*

**8) Determine the volume of excavation (Ex) required.** Each additional foot of cover will add a volume of excavation of 1.4 yd<sup>3</sup> (1.0 m<sup>3</sup>) per MC-4500 chamber and 1.4 yd<sup>3</sup> (0.8 m<sup>3</sup>) per MC-4500 end cap.

**TABLE 16—Volume of Excavation Per Chamber/End Cap yd<sup>3</sup> (m<sup>3</sup>)**

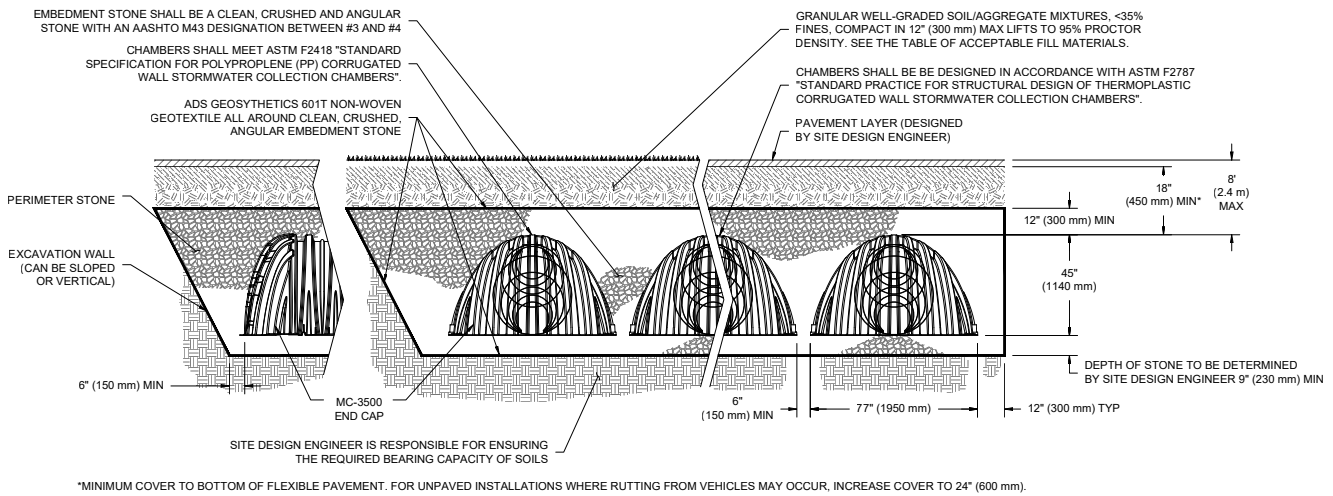
	Stone Foundation Depth			
	9" (230 mm)	12" (300 mm)	15"/(375 mm)	18"/(450 mm)
<b>MC-4500</b>	10.5 (8.0)	10.8 (8.3)	11.2 (8.5)	11.5 (8.8)
<b>End Cap</b>	9.7 (7.4)	10.0 (7.6)	10.3 (7.9)	10.6 (8.1)

*NOTE: Assumes 9" (230 mm) separation between chamber rows, 12" (300 mm) of perimeter in front of end caps, and 24" (600 mm) of cover. The volume of excavation will vary as the depth of cover increases.*

**9) Determine the area of geotextile (F) required.** The bottom, top and sides of the bed must be covered with a non-woven geotextile (filter fabric) that meets AASHTO M288 Class 2 requirements. The area of the sidewalls must be calculated and a 24" (600 mm) overlap must be included for all seams. Geotextiles typically come in 15 foot (4.57 m) wide rolls.

# 7.0 Structural Cross Sections and Specifications

**FIGURE 16—MC-3500 Structural Cross Section Detail (Not to Scale)**



*Special applications will be considered on a project by project basis. Please contact our application department should you have a unique application for our team to evaluate.*

## MC-3500 STORMWATER CHAMBER SPECIFICATIONS

1. Chambers shall be StormTech MC-3500 or approved equal.
2. Chambers shall be made from virgin, impact-modified polypropylene copolymers.
3. Chamber rows shall provide continuous, unobstructed internal space with no internal panels that would impede flow.
4. The structural design of the chambers, the structural backfill and the installation requirements shall ensure that the load factors specified in the AASHTO LRFD Bridge Design Specifications, Section 12.12 are met for: 1) long-duration dead loads and 2) short-duration live loads, based on the AASHTO Design Truck with consideration for impact and multiple vehicle presences.
5. Chambers shall meet the requirements of ASTM F 2418, "Standard Specification for Polypropylene (PP) Corrugated Wall Stormwater Collection Chambers."
6. Chambers shall conform to the requirements of ASTM F 2787, "Standard Practice for Structural Design of Thermoplastic Corrugated Wall Stormwater Collection Chambers."
7. Only chambers that are approved by the engineer will be allowed. The contractor shall submit (3 sets) of the following to the engineer for approval before delivering chambers to the project site:
  - A structural evaluation by a registered structural engineer that demonstrates that the load factors specified in the AASHTO LRFD Bridge Design Specifications, Section 12.12 are met. The 50-year creep modulus data specified in ASTM F 2418 must be used as part of the AASHTO structural evaluation to verify long-term performance.
  - Structural cross section detail on which the structural cross section is based.
8. The installation of chambers shall be in accordance with the manufacturer's latest Construction Guide.

*Detail drawings available in Cad Rev. 2000 format at [www.stormtech.com](http://www.stormtech.com)*





1. StormTech requires installing contractors to use and understand the latest **StormTech MC-3500 and MC-4500 Construction Guide** prior to beginning system installation.
2. StormTech offers installation consultations to installing contractors. Contact our Technical Service Department or local StormTech representative at least 30 days prior to system installation to arrange a pre-installation consultation. Our representatives can then answer questions or address comments on the StormTech chamber system and inform the installing contractor of the minimum installation requirements before beginning the system's construction. Call 860-529-8188 to speak to a Technical Service Representative or visit [www.stormtech.com](http://www.stormtech.com) to receive a copy of our Construction Guide.
3. StormTech requirements for systems with pavement design (asphalt, concrete pavers, etc.): Minimum cover is 18" (450mm) for the MC-3500 and 24"(600mm) for the MC-4500 not including pavement; MC-3500 maximum cover is 8.0' (1.98 m) and MC-4500 maximum cover is 7.0' (2.43 m) both including pavement. For designs with cover depths deeper than these maximums, please contact Stormtech. For installations that do not include pavement, where rutting from vehicles may occur, minimum required cover is increased to 30" (762 mm).
4. The contractor must report any discrepancies with the bearing capacity of the subgrade materials to the design engineer.
5. AASHTO M288 Class 2 non-woven geotextile (ADS601 or equal) (filter fabric) must be used as indicated in the project plans.
6. Stone placement between chamber rows and around perimeter must follow instructions as indicated in the most current version of StormTech MC-3500 / MC-4500 Construction Guide.
7. Backfilling over the chambers must follow requirements as indicated in the most current version of StormTech MC-3500 / MC-4500 Construction Guide.
8. The contractor must refer to StormTech MC-3500 / MC-4500 Construction Guide for a Table of Acceptable Vehicle Loads at various depths of cover. This information is also available at the StormTech website: [www.stormtech.com](http://www.stormtech.com). The contractor is responsible for preventing vehicles that exceed StormTech requirements from traveling across or parking over the stormwater system. Temporary fencing, warning tape and appropriately located signs are commonly used to prevent unauthorized vehicles from entering sensitive construction areas.
9. The contractor must apply erosion and sediment control measures to protect the stormwater system during all phases of site construction per local codes and design engineer's specifications.
10. STORMTECH PRODUCT WARRANTY IS LIMITED. Contact StormTech for warranty information.

## 9.1 ISOLATOR ROW INSPECTION

Regular inspection and maintenance are essential to assure a properly functioning stormwater system. Inspection is easily accomplished through the manhole or optional inspection ports of an Isolator Row. Please follow local and OSHA rules for a confined space entry.

Inspection ports can allow inspection to be accomplished completely from the surface without the need for a confined space entry. Inspection ports provide visual access to the system with the use of a flashlight. A stadia rod may be inserted to determine the depth of sediment. If upon visual inspection it is found that sediment has accumulated to an average depth exceeding 3" (76 mm), cleanout is required.

A StormTech Isolator Row should initially be inspected immediately after completion of the site's construction. While every effort should be made to prevent sediment from entering the system during construction, it is during this time that excess amounts of sediments are most likely to enter any stormwater system. Inspection and maintenance, if necessary, should be performed prior to passing responsibility over to the site's owner. Once in normal service, a StormTech Isolator Row should be inspected bi-annually until an understanding of the sites characteristics is developed. The site's maintenance manager can then revise the inspection schedule based on experience or local requirements.

## 9.2 ISOLATOR ROW MAINTENANCE

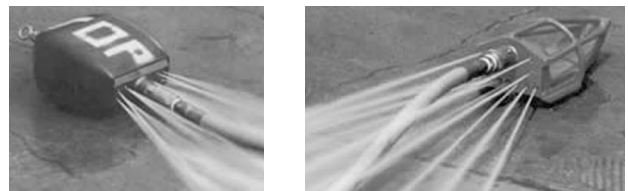
JetVac maintenance is recommended if sediment has been collected to an average depth of 3" (76 mm) inside the Isolator Row. More frequent maintenance may be required to maintain minimum flow rates through the Isolator Row. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row while scouring and suspending sediments. As the nozzle is retrieved, a wave of suspended sediments is flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/ JetVac combination vehicles. Fixed nozzles designed for culverts or large diameter pipe cleaning are preferable. Rear facing jets with an effective spread of at least 45" (1143 mm) are best. The JetVac process shall only be performed on StormTech Rows that have AASHTO class 1 woven geotextile over their foundation stone (ADS 315WTM or equal).



Looking down the Isolator Row



A typical JetVac truck (This is not a StormTech product.)



Examples of culvert cleaning nozzles appropriate for Isolator Row maintenance. (These are not StormTech products).

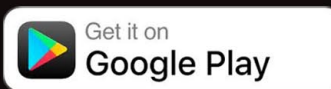
# SiteASSIST™

by StormTech®

The SiteASSIST App enables ADS to take customer service and field support to unprecedented levels. With detailed instructions on proper installation techniques for StormTech chambers and supporting video animations, this tool is designed to insure installed performance.



**DOWNLOAD THE APP TODAY**







MC-4500

MC-3500

DC-780

SC-740

SC-310

SC-160LP

## A Family of Products and Services for the Stormwater Industry:

- MC-3500 and MC-4500 Chambers and End Caps
- SC-310 and SC-740 Chambers and End Caps
- DC-780 Chambers and End Caps
- Fabricated End Caps
- Fabricated Manifold Fittings
- Patented Isolator Row for Maintenance and Water Quality
- Chamber Separation Spacers
- In-House System Layout Assistance
- On-Site Educational Seminars
- Worldwide Technical Sales Group
- Centralized Product Applications Department
- Research and Development Team
- Technical Literature, O&M Manuals and Detailed CAD drawings all downloadable via our Website

*StormTech provides state-of-the-art products and services that meet or exceed industry performance standards and expectations. We offer designers, regulators, owners and contractors the highest quality products and services for stormwater management that "Saves Valuable Land and Protects Water Resources."*



Advanced Drainage Systems, Inc.  
4640 Trueman Blvd. Hilliard, OH 43026

1-800-821-6710

[www.ads-pipe.com](http://www.ads-pipe.com)

# Appendix 16 | Subsurface Chamber Information

# First Defense® High Capacity

A Simple Solution for your Trickiest Sites

## Product Profile

The First Defense® High Capacity is an enhanced vortex separator that combines an effective stormwater treatment chamber with an integral peak flow bypass. It efficiently removes sediment total suspended solids (TSS), trash and hydrocarbons from stormwater runoff without washing out previously captured pollutants. The First Defense® High Capacity is available in several model configurations to accommodate a wide range of pipe sizes, peak flows and depth constraints (**Table 1**, next page).

## Applications

- Stormwater treatment at the point of entry into the drainage line
- Sites constrained by space, topography or drainage profiles with limited slope and depth of cover
- Retrofit installations where stormwater treatment is placed on or tied into an existing storm drain line
- Pretreatment for filters, infiltration and storage

## Advantages

- Inlet options include surface grate or multiple inlet pipes
- Integral high capacity bypass conveys large peak flows without the need for “offline” arrangements using separate junction manholes
- Proven to prevent pollutant washout at up to 450% of its treatment flow
- Long flow path through the device ensures a long residence time within the treatment chamber, enhancing pollutant settling
- Delivered to site pre-assembled and ready for installation

## How it Works

The First Defense® High Capacity has internal components designed to remove and retain gross debris, total suspended solids (TSS) and hydrocarbons (**Fig.1**).

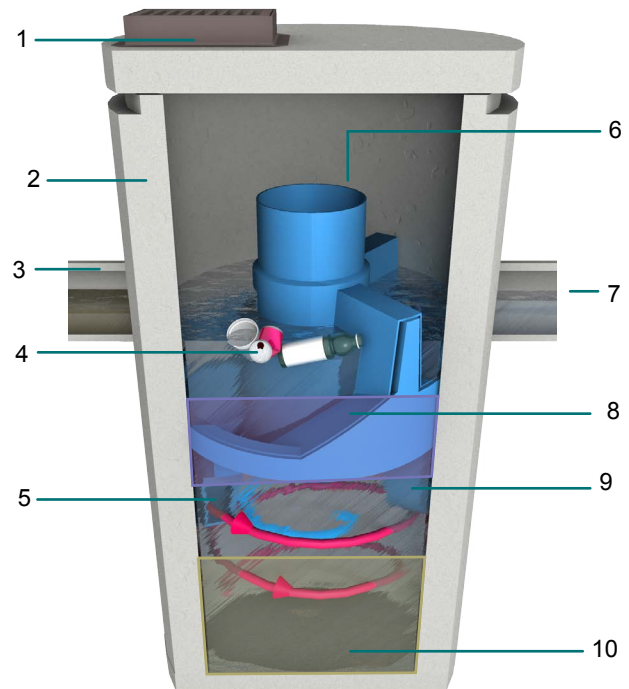
Contaminated stormwater runoff enters the inlet chute from a surface grate and/or inlet pipe. The inlet chute introduces flow into the chamber tangentially to create a low energy vortex flow regime (**magenta arrow**) that directs sediment into the sump while oils, floating trash and debris rise to the surface.

Treated stormwater exits through a submerged outlet chute located opposite to the direction of the rotating flow (**blue arrow**). Enhanced vortex separation is provided by forcing the rotating flow within the vessel to follow the longest path possible rather than directly from inlet to outlet.

Higher flows bypass the treatment chamber to prevent turbulence and washout of captured pollutants. An internal bypass conveys infrequent peak flows directly to the outlet eliminating the need for, and expense of, external bypass control structures. A floatables draw off slot functions to convey floatables into the treatment chamber prior to bypass.

## Verified by NJCAT and NJDEP

**Fig.1** The First Defense® High Capacity has internal components designed to efficiently capture pollutants and prevent washout at peak flows.



## Components

- |   |                               |
|---|-------------------------------|
| 1. Inlet Grate (optional)                     | 6. Internal Bypass            |
| 2. Precast chamber                            | 7. Outlet pipe                |
| 3. Inlet Pipe (optional)                      | 8. Oil and Floatables Storage |
| 4. Floatables Draw Off Slot<br>(not pictured) | 9. Outlet chute               |
| 5. Inlet Chute                                | 10. Sediment Storage Sump     |

# First Defense® High Capacity

## Sizing & Design

This adaptable online treatment system works easily with large pipes, multiple inlet pipes, inlet grates and now, contains a high capacity bypass for the conveyance of large peak flows. Designed with site flexibility in mind, the First Defense® High Capacity allows engineers to maximize available site space without compromising treatment level.

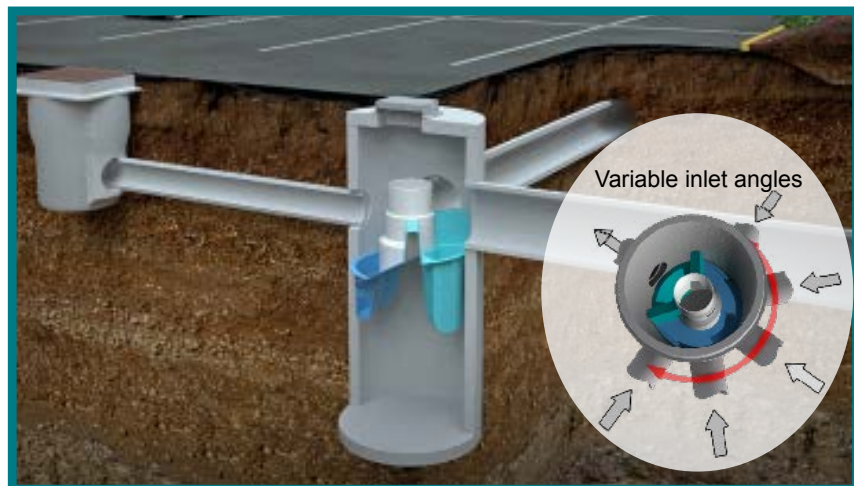


Fig 2. Works with multiple inlet pipes and grates

## Inspection and Maintenance

Nobody maintains our systems better than we do. To ensure optimal, ongoing device performance, be sure to recommend Hydro International as a preferred service and maintenance provider to your clients.

Call **1 (800) 848-2706** to schedule an inspection and cleanout or learn more at [hydro-int.com/service](http://hydro-int.com/service)

## Free Stormwater Separator Sizing Calculator for Engineers



This simple online tool will recommend the best separator, model size and online/offline arrangement based on site-specific data entered by the user.

Go to [hydro-int.com/sizing](http://hydro-int.com/sizing) to access the tool.



Fig 3. Maintenance is done with a vector truck

Table 1. First Defense® High Capacity Design Criteria.

First Defense® High Capacity Model Number	Diameter	Typical TSS Treatment Flow Rates			Peak Online Flow Rate	Maximum Pipe Diameter <sup>1</sup>	Oil Storage Capacity	Typical Sediment Storage Capacity <sup>2</sup>	Minimum Distance from Outlet Invert to Top of Rim <sup>3</sup>	Standard Distance from Outlet Invert to Sump Floor
		NJDEP Certified	106µm	230µm						
	(ft / m)	(cfs / L/s)	(cfs / L/s)	(cfs / L/s)	(cfs / L/s)	(in / mm)	(gal / L)	(yd <sup>3</sup> / m <sup>3</sup> )	(ft / m)	(ft / m)
FD-3HC	3 / 0.9	0.84 / 23.7	0.3 / 8.77	0.53 / 15.0	15 / 424	18 / 457	125 / 473	0.4 / 0.3	2.0 - 3.5 / 0.6 - 1.0	3.71 / 1.13
FD-4HC	4 / 1.2	1.50 / 42.4	0.7 / 20	1.2 / 34	18 / 510	24 / 600	191 / 723	0.7 / 0.5	2.3 - 3.9 / 0.7 - 1.2	4.97 / 1.5
FD-5HC	5 / 1.5	2.34 / 66.2	1.3 / 37.9	2.2 / 62.2	20 / 566	24 / 609	300 / 1135	1.1 / .84	2.5 - 4.5 / 0.7 - 1.3	5.19 / 1.5
FD-6HC	6 / 1.8	3.38 / 95.7	2.2 / 63	3.8 / 108	32 / 906	30 / 750	496 / 1,878	1.6 / 1.2	3.0 - 5.1 / 0.9 - 1.6	5.97 / 1.8
FD-8HC	8 / 2.4	6.00 / 169.9	5.1 / 144	8.6 / 243	50 / 1,415	48 / 1219	1120 / 4239	2.8 / 2.1	3.0 - 6.0 / 0.9 - 1.8	7.40 / 2.2

<sup>1</sup>Contact Hydro International when larger pipe sizes are required.

<sup>2</sup>Contact Hydro International when custom sediment storage capacity is required.

<sup>3</sup>Minimum distance for models depends on pipe diameter.



## State of New Jersey

DEPARTMENT OF ENVIRONMENTAL PROTECTION

Bureau of Nonpoint Pollution Control  
Division of Water Quality  
401-02B

Post Office Box 420

Trenton, New Jersey 08625-0420

609-633-7021 Fax: 609-777-0432

[http://www.state.nj.us/dep/dwq/bnpc\\_home.htm](http://www.state.nj.us/dep/dwq/bnpc_home.htm)

CHRIS CHRISTIE  
*Governor*

KIM GUADAGNO  
*Lt. Governor*

BOB MARTIN  
*Commissioner*

April 4, 2016

Lisa Lemont, CPSWQ  
Business Development Manager  
Hydro International  
94 Hutchins Drive  
Portland, ME 04102

Re: MTD Lab Certification  
First Defense® HC (FDHC) Stormwater Treatment Device by Hydro International

### **TSS Removal Rate 50%**

Dear Ms. Lemont:

The Stormwater Management rules under N.J.A.C. 7:8-5.5(b) and 5.7 (c) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Hydro International has requested an MTD Laboratory Certification for the First Defense® HC Stormwater Treatment Device.

The projects falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advance Technology" dated January 25, 2013. The applicable protocol is the "New Jersey Laboratory Testing Protocol to Assess Total Suspended Solids Removal by a Hydrodynamic Sedimentation Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated February 2016) for this device is published online at <http://www.njcat.org/verification-process/technology-verification-database.html>.

**The NJDEP certifies the use of the First Defense® HC Stormwater Treatment Device by Hydro International at a TSS removal rate of 50% when designed, operated and maintained in accordance with the information provided in the Verification Appendix and the following conditions:**

1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-5.5.



2. The First Defense® HC Stormwater Treatment Device shall be installed using the same configuration reviewed by NJCAT and shall be sized in accordance with the criteria specified in item 6 below.
3. This First Defense® HC Stormwater Treatment Device cannot be used in series with another MTD or a media filter (such as a sand filter) to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
4. Additional design criteria for MTDs can be found in Chapter 9.6 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual which can be found on-line at [www.njstormwater.org](http://www.njstormwater.org).
5. The maintenance plan for a site using the First Defense® HC Stormwater Treatment Device shall incorporate, at a minimum, the maintenance requirements noted in the attached document. However, it is recommended to review the maintenance website at [http://www.hydro-int.com/UserFiles/downloads/FD\\_O%2BM\\_F1512.pdf](http://www.hydro-int.com/UserFiles/downloads/FD_O%2BM_F1512.pdf) for any changes to the maintenance requirements.
6. Sizing Requirements:

The example below demonstrates the sizing procedure for the First Defense® HC Stormwater Treatment Device:

Example: A 0.25 acre impervious site is to be treated to 50% TSS removal using a First Defense® HC Stormwater Treatment Device. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs.

Maximum Treatment Flow Rate (MTFR) Evaluation:

The site runoff (Q) was based on the following:

time of concentration = 10 minutes

i=3.2 in/hr (page 5-8, Fig. 5-3 of the NJ Stormwater BMP Manual)

c=0.99 (curve number for impervious)

$Q=ciA=0.99 \times 3.2 \times 0.25 = 0.79$  cfs

Given the site runoff is 0.79 cfs and based on Table 1 below, the First Defense® HC Model 4-ft with a MTFR of 1.5 cfs would be the smallest model approved that could be used for this site that could remove 50% of the TSS from the impervious area without exceeding the MTFR.

The sizing table corresponding to the available system models is noted below. Additional specifications regarding each model can be found in the Verification Appendix under Table A-1 and Table A-2 of the NJCAT Verification Report.

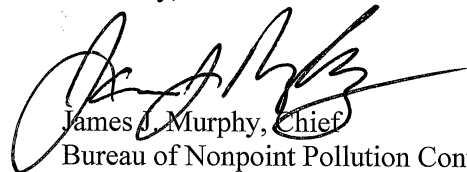
Table 1 First Defense® HC Models

First Defense® Model	Manhole Diameter (ft)	Maximum Treatment Flowrate, MTFR (cfs)
4-ft	4-ft	1.50
6-ft	6-ft	3.38
8-ft	8-ft	6.00

Be advised a detailed maintenance plan is mandatory for any project with a Stormwater BMP subject to the Stormwater Management Rules, N.J.A.C. 7:8. The plan must include all of the items identified in the Stormwater Management Rules, N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of inspection and maintenance equipment and tools, specific corrective and preventative maintenance tasks, indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance of the New Jersey Stormwater Best Management Practices Manual.

If you have any questions regarding the above information, please contact Mr. Titus Magnanao of my office at (609) 633-7021.

Sincerely,



James J. Murphy, Chief  
Bureau of Nonpoint Pollution Control

Attachment: Maintenance Plan

C: Chron File  
Richard Magee, NJCAT  
Vince Mazzei, DLUR  
Ravi Patraju, NJDEP  
Gabriel Mahon, BNPC  
Titus Magnanao, BNPC

**PART 1 - GENERAL****1.01 SCOPE**

- A. Work described in this section includes furnishing all labor, equipment, materials, tools and incidentals required for a complete and operable installation of the First Defense® stormwater treatment system as shown on the drawings and specified herein.
- B. The manufacturer shall design and supply the equipment listed herein and the Contractor shall install the equipment in accordance with the manufacturer's Handling, Storage, and Installation Instructions.

**1.02 GENERAL REQUIREMENTS**

- A. The treatment system shall use an induced vortex to separate pollutants from stormwater runoff. The system shall be self-activating with no mechanical parts or external power requirements.
- B. Upon request, independently certified performance data and references shall be made available to the Engineer of Record for use in determining that the treatment system meets the design criteria and performance requirements stated herein.

**1.03 SUBMITTALS**

- A. Submittals shall be provided and shall include the following:
  - i. Site plan showing location and orientation of proposed pipe sizes, connections and excavation limits.
  - ii. Product installation drawings showing plan and elevation views with water elevations for the flow conditions specified herein.
  - iii. Performance data as required in Part 2.
  - iv. Inspection and maintenance procedures.

**1.04 QUALITY ASSURANCE**

- A. The treatment system shall be manufactured under the direction of an ISO 9001 Certified Company.
- B. Inspection

The treatment system shall be subject to inspection by the Engineer of Record or the owner's representative at either the place of manufacture or the project site. Any and all observed defects shall be repaired to the satisfaction of the owner or owner's representative or replacement shall be made available.

### C. Warranty

The manufacturer shall guarantee the treatment system free from defects in materials and workmanship for a period of two years following installation. If during the warranty period defects in materials or workmanship are noted, then the manufacturer shall be promptly notified. The decision to repair or replace affected units shall be made at the discretion of the manufacturer.

### D. Patent Indemnity

Upon request, the manufacturer shall warrant that the treatment system does not infringe upon or violate any patent, copyright, trade secret or any other proprietary right of any third party and shall indemnify the Owner against any loss, cost, expense or liability arising out of such claim whether or not such claim is successful.

### E. Certificate of Compliance

Upon request, the manufacturer shall provide a "Letter of Certification" to certify that the treatment system adheres to the specifications required herein and complies with the project's stormwater management permit.

## 1.05 MANUFACTURER

- A. The treatment system shall be supplied by a manufacturer regularly engaged in such work who has furnished similar installations that have been in successful and continuous operation for a minimum period of five years. The manufacturer shall be a Stormwater Equipment Manufacturer Association (SWEMA) member.
- B. The treatment system shall be certified by an acceptable State agency, such as a State Department of Environmental Protection (DEP) or industry verification or assessment agency (e.g.: ETV, NJCAT, NETE, MaSTEP).

## **PART 2 – STORMWATER HVS**

### 2.01 General

- A. The treatment system shall use a tangential inlet chute to establish rotational flow within a cylindrical vortex chamber and be able to treat the Water Quality Flow Rate stated herein without re-suspending and releasing captured pollutants. The treatment system shall not release captured floating pollutants during surcharge conditions.
- B. The treatment system shall not exceed the pressure drop (headloss) for the design flow rates specified herein as determined by ASTM C1745 / C1745M – 11.
- C. The treatment system shall fit within the limits of excavation (area and depth) as shown in the project plans and will not exceed the dimensions for the design flow rates specified herein.
- D. The storage capacities for pollutants that settle (sediment) and float (oil) shall not be less than the volumes listed in Table 1. The treatment system shall operate as

intended and perform as specified herein as pollutants accumulate. The accumulation of pollutants that settle shall not reduce the volume required in the treatment system for separation and for preventing re-suspension and washout, or reduce the floatables storage volume capacity.

- E. Minimum 24-inch frame and cover shall provide access to the sediment storage volumes from the surface for inspection and maintenance. Removal of pollutants from the treatment system shall be possible without requiring confined space entry.

**2.02 Performance**

- A. Performance of the treatment system shall be based on independent full-scale laboratory testing and shall adhere to the Performance Specifications listed in Table 1. The laboratory testing used as the basis of product performance shall be undertaken in accordance with testing protocols approved or endorsed by SWEMA or acceptable State agency, such as a State Department of Environmental Protection (DEP) or recognized verification agency (e.g.: ETV, NJCAT, NETE, MaSTEP).
- B. Performance of the treatment system shall be based on treating the Water Quality Flow rate (WQF) without internally bypassing and without re-suspension and washout of captured pollutants (scour). The Maximum Treatment Flow Rate(s) (MTFR-106 and/or MTFR-230) shall be greater than or equal to the WQF. The treatment system shall remove greater than or equal to 90% of TSS based on the Target Particle Size (TPS) of 106 microns and/or 80% of TSS based on the TPS of 230 microns at MTFR-106 and MTFR-230, respectively.
- C. The treatment system shall convey the Peak On-line Flow Rates listed in Table 1 without causing upstream surcharge conditions. Full-scale independent laboratory scour testing shall demonstrate effluent control of less than or equal to 5 mg/L for all flows up to 200% of MTFR-106.
- D. The treatment system shall be capable of capturing and retaining fine silt and sand size particles. Analysis of captured sediment from full-scale field installations shall demonstrate particle sizes predominately in the 20-micron range.

Table 1.

First Defense® Model	Diameter	Maximum Treatment Flow Rates (MTFR)		Peak Online Flow Rate	Maximum Pipe Diameter	Oil Storage Capacity	Minimum Sediment Storage Capacity	Min. Cover (F/G to Invert)	Min. Depth
		106µm	230µm						
	(ft/m)	(cfs/L/s)	(cfs/L/s)	(cfs /L/s)	(in/mm)	(gal/L)	(yd³/m³)	(ft/m)	(ft/m)
FD-4	4/1.2	0.7/20	1.2/34	6.0/170	18/450	180/681	1.3/ 1.0	3.1/1.1	5.47/1.7
FD-4HC				18.0/510	24/600			2.3-3.9/0.7-1.2	
FD-6	6/1.8	2.2/63	3.8/108	18.0/510	24/600	420/1,590	3.3/ 2.5	4.0 / 1.2	6.52/2.0
FD-6HC				32/906	30/750			3.0-5.1/0.9-1.6	

**PART 3 – EQUIPMENT**

- A. The treatment system shall be manufactured with materials typically used in stormwater drainage systems that have a minimum life expectancy of 30 years.
- (i) Materials of construction shall be cross-linked polyethylene (XLPE) and/or Type 304 stainless steel or carbon steel powder coated in accordance with ASTM 775/ ASTM A775M. All components shall be designed to withstand normal loadings associated with fabrication, shipping, site installation, and normal operation of the equipment.
  - (ii) Precast shall be manufactured with concrete that has attained a compressive strength of 4,000 psi after 28 days. The structure shall be reinforced to withstand an HS20-44 loading. Shiplap joints shall be sealed with butyl rubber mastic sealant conforming to ASTM C990. Slab tops shall be suitably reinforced and provided with manhole openings and covers as required. The cast iron manhole frames and covers shall be sized as per the manufacturer's drawings and shall be in accordance with ASTM A48, CL.35B and AASHTO M105. The masonry fixing bolts shall be Type 304 stainless steel.
  - (iii) All piping connections and ancillary items not listed herein shall be provided by the Contractor.

**PART 4 - EQUIPMENT DELIVERY**

- A. The treatment components of the treatment system shall be delivered within six weeks of date of approved technical submittal.
- B. The components of the treatment system shall be preassembled and delivered to the site fully fabricated and ready for the final assembly.
- C. Off-loading, storage, and installation shall be by the Contractor.
- D. The Contractor shall inspect and provide signed acceptance of equipment prior to unloading, or notify the manufacturer of any damage to equipment to effect proper remedial action. Failure to notify the manufacturer of damage to equipment prior to unloading will void all warranties pertaining to subject equipment.

**PART 5 - EQUIPMENT INSTALLATION**

- A. The system shall be installed in strict accordance with the site plans, and the manufacturer's general arrangement drawings and Handling, Storage and Installation Instructions. The Contractor shall be responsible for installing the equipment and all necessary site connections.

- B. The Manufacturer shall be notified immediately of any equipment which is damaged during unloading, storage, or installation. The damaged equipment shall be repaired or replaced at the discretion of the manufacturer and entirely at the Contractor's expense.
- C. The precast concrete structure shall be set on a granular or compacted sand sub-base in accordance with local requirements for standard manhole installation. In no instances shall the compacted sub-base material have a thickness of less than 12 inches.
- D. The precast concrete structure shall be set level and plumb to within 0.5%.
- E. Non-shrink grout or hydraulic cement conforming to ASTM C 595 shall be used to provide a water tight seal in the lift holes, any drain holes and around the concrete knock-outs for the inlet and outlet pipes.
- F. The Contractor shall, at the discretion of the owner or owner's representative, test the concrete structure for water tightness before backfilling.

# Appendix 17 | Geotechnical Investigation Report & Infiltration Results by Kevin Patton, P.E.



**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, N.Y. 12550**  
845 275-7732 PATTONGEOTECH.COM

CLIENT:	RDM Group	PROJECT:	Dewpoint Dolsontown
	1 International Drive, Suite 410		Town of Wawayanda, N.Y.
	Mahwah, NJ 07430	PROJ. No.:	21416
		DATE:	March 25, 2022

## GEOTECHNICAL INVESTIGATION REPORT

### Table of Contents

Section		Page
1.	PROJECT DESCRIPTION	2
2.	SOIL INVESTIGATION AND TEST RESULTS	3
2.1.	Soil Boring Blow Counts and Laboratory Data	4
2.2.	Subsurface Profile and Summary of Soil Conditions	6
3.	EVALUATION	7
3.1.	Subgrade Preparation	7
3.2.	Excavation	8
3.3.	Fill Materials and CLSM	8
3.4.	Fill Placement and Compaction	9
3.5.	Compaction Requirements	11
3.6.	Testing	12
3.7.	Geosynthetic Materials	12
4.	DESIGN VALUES AND RECOMMENDATIONS	14
4.1.	Bearing Capacity and Soil Pressure	14
4.2.	Control of Groundwater and Soil Gases	15
4.3.	Seismic and Expansive Properties	15
5.	NOTES AND LIMITATIONS	16

SOIL TECHNICAL NOTES

BORING LOCATIONS

SUBSURFACE PROFILE

SOIL BORING LOGS

LABORATORY TEST REPORTS

USDA SOIL REPORT DATA

## 1. PROJECT DESCRIPTION

This geotechnical investigation report was prepared for use in the design and construction of two new warehouses on two wooded lots, one on the south side of Dolsontown Road and the other across from it on the north side, as shown on the attached plan. Both lots are wooded and appear to have had past agricultural use, but no prior development; they are situated near the west end of a roughly ninety-foot high hill which is elongated northeast-to-southwest, cresting at an elevation of about 540 feet, approximately 750 feet northeast from the project area. Monhagen Brook skirts the project area, approaching it from the north, flowing through the northwest part of the north parcel, then south and east around the south parcel; the stream channel has a very gentle slope, and is at about 460 feet elevation where it crosses the north parcel.

The proposed south building has an approximately 125,000 square foot footprint, with a length of 590 feet east-to-west, parallel to the road, and a depth of 212 feet. Existing elevations range from about 515 feet near the northeast corner to 485 feet at the southeast corner and 477 feet along the west end. The proposed floor elevation was not provided; it is estimated to be about 495 feet, resulting in a nominal twenty-foot cut at the high end and an eighteen-foot fill at the low end. With the floor at this elevation the south warehouse could be built with the slab at finished grade around its entire perimeter, with a relatively steep slope (2H:1V) down to the building from the corner of Dolsontown Road and Caskey Lane, but it may be more practical to design the east half of the north wall and the north two-thirds of the east wall as retaining walls, with the building corner cut into the slope, with little change to the adjacent grades in that area.

The north building has proposed dimensions of 150 by 200 feet (30,000 square feet), with the short end parallel to Dolsontown Road. The existing elevations in the building area range from about 517 feet at the southeast corner to 480 feet at the northwest corner; a floor elevation of 490 feet was estimated for purposes of this report, resulting in a nominal 27-foot cut at the southeast corner and ten-foot fill at the northwest building corner. A retaining wall is proposed, to the northwest of the building, to allow development of the loading docks and truck apron on the west side of the building, which would most likely be cut into the hillside on the east side and the east part of the two ends.

The USDA Soil Survey indicates that the native topsoil type in the two project areas is Mardin gravelly silt loam, changing to Erie gravelly silt loam in the lower areas. These soils typically form over deep deposits of clayey glacial till, sometimes with significant sandy to gravelly layers, and sometimes with abundant cobbles and boulders. The soils encountered in the borings were generally consistent with the Soil Survey data, tending to be clayey to silty-clayey, with occasional boulders. No significant areas of fill were encountered. Bedrock appears to be deeper than the expected depths of excavation for the buildings.

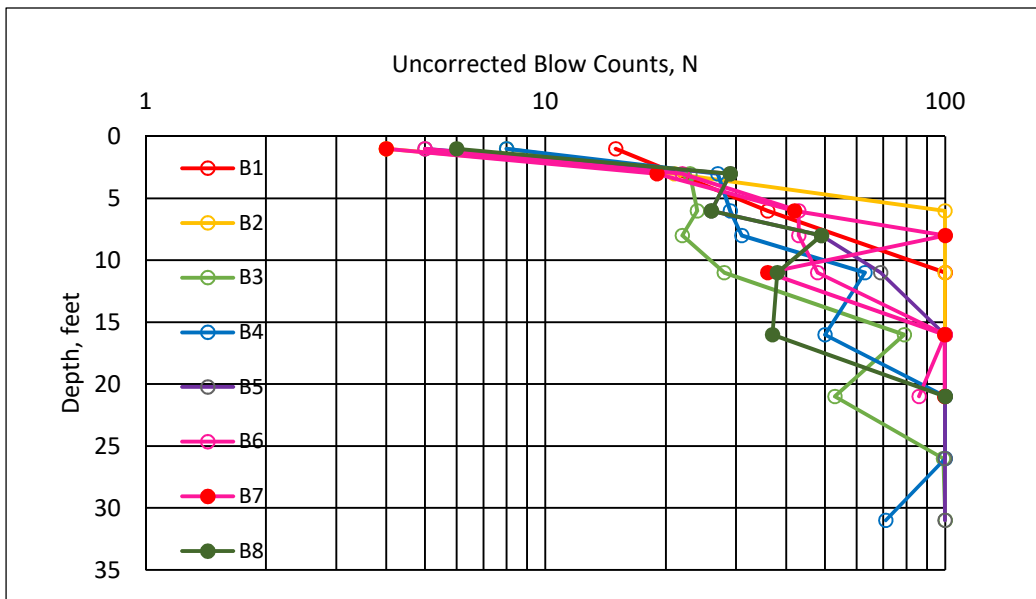
## **2. SOIL INVESTIGATION AND TEST RESULTS**

Prior to drilling the soil borings, test pits were excavated in proposed stormwater control areas downhill from both building areas; the results of that investigation were reported separately and are discussed below, in Section 2.2. Eight soil borings were drilled on April 21, 22, 25 and 26, by the hollow-stem auger method, using a track-mounted drill rig; borings B1 through B6 were drilled in the south building area, and B7 and B8 were drilled in the north building area. Drilling was performed by General Borings, Inc. of Prospect, Connecticut. The subsurface investigation was supervised and witnessed by Wyeth Patton, under the direction of Kevin Patton, P.E.

Soil sampling and testing in the borings were performed by the Standard Penetration Test (SPT,) using an Automatic Hammer, in accordance with ASTM D1586 (Standard Method for Penetration Test and Split-Barrel Sampling of Soils.) The SPT provides the Blow Count "N" Value, equal to the number of blows of the 140-pound steel hammer that were required to drive the 2-inch outside diameter split-spoon sampling tube into the soil, over a twelve-inch increment. Soil samples are also recovered by this method, and additional tests were performed in the field and lab, as noted on the soil boring log, using a hand penetrometer to test bearing capacity. Laboratory testing was performed on representative soil samples, for moisture content, particle size distribution and Atterberg Limits, and one sample was tested for unit weight (density.) USCS classifications of the soil, per ASTM D2487 and D2488, are provided on the logs and on the subsurface profile drawing.

2.1. Soil Boring Blow Count and Laboratory Data

Field Blow Count Values, N								
	B1	B2	B3	B4	B5	B6	B7	B8
Elevation±:	515	509	495	494	510	486	504	497
Depth, ft.: 1	15	4	8	8	5	5	4	6
3		21	23	27	29	22	19	29
6	36	50/1"	24	29	26	43	42	26
8			22	31	49	43	50/3"	49
11	50/3"	50/1"	28	63	69	48	36	38
16	50/2"	--	79	50	50/2"	50/4"	50/1"	37
21		50/1"	53	50/4"	50/5"	86	50/6"	50/6"
26			88/11"	50/4"	50/2"			
31			50/2"	71	50/5"			
Auger Refusal, ft	19.0	23.5					23.5	
Cored:		15-20						



Natural Moisture Content, Percent								
Depth, feet	B1	B2	B3	B4	B5	B6	B7	B8
3		11.4	12.2		8.0	11.9	11.8	8.9
6	12.5		11.8	11.6	11.2	8.8	11.8	10.3
8			14.2	11.9	11.2	10.5		
11	10.9				9.8	11.6	13.1	
16			9.0	9.9	7.8	7.6	9.3	9.2
21		9.3	8.3	13.1	8.8	9.6	3.7	
26			11.0					
31				11.8				

<b>SOIL TEXTURE</b>			
<b>Particle Size Analysis</b>			
Sample		B5-S9	B8-S4
Depth		31 feet	8 feet
Type		Gray Till	Brown Till
USCS Class		CL-ML, Sandy Silty Clay	SC, Clayey Sand with Gravel
Sieve Size	mm	Percent Passing by Weight	
¾"	19.0	100	100
#4	4.75	90	81
#10	2.00	84	73
#40	0.425	78	64
#200	0.075	68	49
Hydrometer	0.050	65	46
	0.005	26	25
	0.002	15	17
<b>Atterberg Limits</b>			
Liquid Limit		20	23
Plastic Limit		15	15
Plasticity Index		5	8

<b>Soil Density / Unit Weight</b>	
Sample	B3-S5
Depth	11 feet
Type	Brown silty clay till
Moist Density, pcf	140
Dry Density, pcf	123
Percent Moisture	13.8

The Standard Penetration Test results (blow counts) indicated loose conditions close to the surface, then medium-dense soil to about five feet depth; from five to twelve feet the soil was medium-dense to very dense, from twelve to eighteen feet it was dense to very dense, and below eighteen feet depth it was very dense.

The moisture contents of the samples were generally at the low end of the normal range for the soil types tested, despite many of the samples being in a very moist to wet condition. These moisture contents, mostly in the eight percent to fourteen percent range, reflect the very densely-consolidated nature of the soil, as indicated by the blow counts, the penetrometer measurements and the density test which was performed on a random, representative sample of the brown till. This sample's moist density was about ten pounds per cubic foot heavier than 'normal' soil and its moisture content of 13.8 percent indicates a very moist condition, although the sample did not appear to be wet.

The particle size analyses and Atterberg Limits tests were performed on representative samples of the brown and the gray till; these samples were dense to very dense, and were composed of a well-graded mix of sand, silt and clay sizes with minor gravel. The sample of gray till contained about two-thirds silt and clay, twenty percent sand and ten percent gravel; the brown till sample was composed of about one half

silt and clay, thirty percent sand and twenty percent gravel, and while technically classified as 'SC, clayey sand with gravel,' if the sample had one percent additional passing the #200 sieve it would be classified as 'CL, Sandy Clay.' Note that the split-spoon sampling method which was used to collect the samples excludes particles that are medium gravel-size or larger. The gravel fraction may be under-represented; cobbles and boulders are also present in the soil but are not represented by the tests. The samples had similar Atterberg Limits results, indicating a silty clay to lean clay composition with a low potential for expansion.

## **2.2. Subsurface Profile and Summary of Soil Conditions**

Subsurface conditions encountered in the borings are described in the boring logs and are summarized in the drawing attached to this report. The soils in both building areas consisted of layered glacial till; at the south building the till encountered in the cut portion of the building was mostly composed of silty clay and clay, with little to some sand and traces to little gravel. The borings in the fill portion of the south building also encountered these soils, inter-layered with till with a sandy silt to silty sand composition. Boulders were encountered in three of the six borings in this area. The soils were mostly moist to very moist, with wet zones of perched groundwater at varying depths, however the actual moisture content was relatively low, due to the high degree of consolidation and low porosity of the soil. The till encountered in the borings in the north building area were similar to the deeper soils in the south building area, and included layers of significantly more sandy to gravelly till with little silt. The soils at the north building were mostly in a moist condition and were wet near the surface; occasional boulders were also present.

Test Pits excavated during the stormwater investigation also encountered layered glacial till, with layers of silty, clayey, silty-sandy and clayey-sandy till downhill from both building areas. These soils were mostly in a very moist to wet condition, and the stabilized groundwater depths were determined to be less than thirty inches from the surface at most locations. Occasional small boulders were also encountered in these test pits, most of which were excavated to eight feet depth.

Bedrock appears to be sufficiently deep that it will not be encountered in the building excavations. Due to time limitations, no boring was drilled at high point in the north building (elevation 516±,) however all of the borings were drilled to depths of twenty to thirty feet without encountering bedrock, and the hill on which the project is situated is believed to be a drumlin or drumlin-like glacial deposit composed mostly of till, with bedrock at relatively great depth.

### 3. EVALUATION

#### 3.1. Subgrade Preparation

The conditions encountered in the investigation were evaluated for their impacts on construction methods, structural-geotechnical design, and long-term performance. The evaluation indicates that the subgrade conditions throughout the two proposed building areas are suitable for the use of shallow spread footing foundations and slabs-on-grade, subject to performing the required subgrade preparation operations, as described below.

Remove all existing topsoil, soft subsoil, stumps and large roots from the subgrade surface, in all building foundation areas, and to at least one foot beyond the building for each foot of fill to be placed in fill areas. Excavate to at least twelve inches below the original natural grade, and to the top of stiff, unyielding soil. Use excavation methods that minimize disturbance of the final subgrade surface. Compact the surface as needed to consolidate any soil that was loosened during excavation. Remove any pockets or small zones of unsuitable materials that are encountered, and replace them with controlled compacted fill. Contact the Engineer prior to performing any significant extra excavation. Where stumps or boulders are removed, or where other over-excavation work is performed to prepare subgrade areas, the sides of the excavation shall be trimmed back to stable soil as each lift is placed; as the backfill is compacted, extra care shall be taken to ensure thorough compaction where the edges of each lift meet the sides of the excavation. Where deficient soil is removed from below footing locations, the remediated area shall extend at least one foot out from the footing per foot of depth (1 to 1 splay.) Refer to the Fill Placement and Compaction section of this report for additional comments regarding subgrade preparation for areas of site-borrow fill placement.

If bedrock is encountered and excavation is performed by ripping, hammering and/or blasting, remove the rock to an approximately level and uniform elevation, with a slope of ten percent or less in areas below footings. If the rock subgrade surface has open fractures, level and seat the surface by tracking back-and-forth over it with a bulldozer or excavator, or spade it with the excavator bucket in tight areas, then compact the surface with several passes of a vibratory trench roller or a single-drum soil roller. A layer up to four inches thick of Structural Fill or ¾-inch to 1½-inch crushed stone may be placed over the rock surface to facilitate compaction. Remove loose rock from vertical steps in the foundation.

Footings may bear directly on the prepared soil or rock subgrade, or on controlled compacted fill placed over the subgrade. Footing bearing surfaces shall be free from frost, mud and loose soil or standing water, when concrete is placed. Rock surfaces should be thoroughly moistened prior to placing concrete. Where fine-grained native soil is present at the bearing elevation, a layer up to four inches thick of Structural Fill may be placed in the footing bottom to protect the soil surface, after properly preparing the surface to a level and stable condition. This layer shall be thoroughly compacted with a vibratory plate tamper or roller, and its surface shall not extend above the design bearing elevation.

In the slab areas, select fill material should be used for the final two feet of fill below the slab base. Structural Fill or similar granular material should be used in those areas, to protect the subgrade prior to slab placement, especially if the slab will be placed by ready-mix trucks driving over the surface.

### **3.2. Excavation**

The native soils may be excavated using conventional heavy equipment, such as tracked excavators and bulldozers. Scraper pans may be used; the pans will likely need a bulldozer pusher when cutting into the borrow area surface; moderate interference from boulders should be expected. Rollers, wheel loaders and other heavy equipment should be sized appropriately for the subgrade conditions. Traffic from dump trucks, pans and similar heavy vehicles should be minimized on the exposed surface of the subgrade and on compacted fine-grained fills. Little or no rock excavation is expected within the building areas.

The investigation indicates that the soils which will be encountered in the building excavations are likely to predominately be OSHA Type A, requiring a minimum slope of 0.75-to-1 in shallow excavations, with benching permitted. Soil types for excavation requirements must be confirmed by a qualified representative of the Contractor during construction. In most locations, shoring of excavations should not be required, as there appears to be sufficient distance from the property line to the estimated limits of the foundation work area to allow the use of conventional excavation slopes. Shoring may be required near the southeast corner of the north building, depending on the actual depth of the cut in this area. The design of any necessary shoring or other support-of-excavation is the responsibility of the Contractor and is not included in this report.

Groundwater seepage rates in the building excavations are expected to be slow, but will likely be persistent, at least during wet seasons, and occasional zones of concentrated seepage may be encountered from zones of perched water. Groundwater seepage and stormwater should be removed promptly from the excavations, and the groundwater elevation should be maintained at least one foot below the surface in foundation construction areas. When dewatering excavations, the water level should be drawn down at a controlled rate to minimize sloughing, allowing the water to drain from the soil in the sides of the excavation.

### **3.3. Fill Materials and CLSM**

Soils excavated from the site are expected to be of fair quality for re-use as fill and backfill for foundations, slabs and pavement areas. The native clayey soils can be used as fill, but are moisture-sensitive and are typically difficult to work with, especially when the weather is other than warm and dry. The investigation did indicate, however, that most of the potential borrow soils are only slightly wetter than optimum moisture, and if excavated, spread and compacted during favorable weather (drying conditions) the work can be performed relatively efficiently. Boulders and large cobbles must be removed from the borrow fill. Clumps of clayey soil larger than two-thirds the lift thickness must be broken up.

If imported fill is used below foundations and slabs, it shall be of a quality at least equal to that of the site-borrow soil, and if possible should consist of granular material, e.g. imported Structural Fill, which shall be good-quality bank-run sand and gravel or crushed stone, and should comply with the gradation limits below. Structural Fill may also be used as foundation backfill. Structural Fill HD (Heavy Duty) should be used in areas to be protected from heavy construction traffic and where subgrade stabilization and/or enhanced drainage is needed.

All fill materials shall be composed of sound, durable particles, shall be free from frost or snow, garbage, construction debris or other deleterious material, and shall be substantially free from organic matter and



roots. Recycled crushed concrete and masonry from a registered source may be acceptable for some applications, subject to approval by the Designer of Record. Fill shall not be placed over frozen or unstable soil, unless approved by the Engineer.

Sieve size		Structural Fill	Structural Fill HD
Inch	mm	Percent Passing by Weight	
4"	100	100	100
1½"	37.5	50-100	50-95
#4	4.75	20-70	20-50
#40	0.425	5-40	5-25
#200	0.075	0-30	0-10
Plasticity Index		6 max.	Non-plastic

CLSM (Controlled Low-Strength Material, aka flowable fill or k-crete,) may be used under footings and foundations when specifically approved by the Engineer, and may also be used to backfill trenches or other excavations, typically where rapid fill placement is required, fill areas are narrow, or the use of conventional compaction methods is not practical. For support of footings, a CLSM mix consisting of sand, cement and water, with a 56-day compressive strength of 75 to 200 psi, is appropriate. CLSM may produce high fluid pressures during placement, and caution must be used for placements against foundation walls, near unbraced cuts, etc. Pipes or tanks can also float if not properly restrained during placement. CLSM should not be placed against unprotected aluminum; CLSM containing flyash should not be used in contact with cast iron or ductile iron. Hardened CLSM masses may also adversely affect groundwater flow, possibly causing erosion under or along the CLSM, particularly in sloping trenches.

**Other Fill Materials:**

- Crushed stone base course for slabs-on-grade should consist of ASTM C33 #56 or #57 stone (¾- to ¾-inch size,) or as required by the slab system design.
- Crushed stone or gravel for footing drains should consist of ASTM C33 #5, #56 or #57 stone (¾-inch or ¾-¾-inch size.)
- Well-graded granular subbase material (NYSDOT Item 733-04 'Item 4' or similar) should be used under sidewalks and exterior slabs.

**3.4. Fill Placement and Compaction**

Soil surfaces, including the surfaces of previously-placed fill materials, shall be prepared to a stiff and essentially unyielding condition prior to placing each new lift of fill. Bedrock surfaces to receive fill shall be free from voids or loose areas and the rock surface shall be free from large loose pieces of stone. Use mid-size equipment to compact the site-borrow fill material. Vibratory trench rollers, and single-drum soil rollers with a nominal size of three to seven tons, are appropriate for the observed site conditions. Larger rollers may be used when compacting well-graded granular fill over essentially unyielding surfaces. In areas with limited access, vibratory plate tampers or jumping-jack tampers may be used. Avoid over-compacting the soil in landscaped areas.

Fill shall be placed in controlled lifts, with each lift compacted to the required density at a moisture content close to optimum moisture, as determined by ASTM D1557. When the moisture content of the fill is within

two percent of optimum, fill may be placed in lifts with compacted thicknesses of up to twelve inches. If the moisture content is two to three percent from optimum, reduce the maximum thickness to eight inches, and if it is more than three percent from optimum, discontinue compaction. Use a reduced lift thickness if required to obtain the specified percent compaction and when using small compaction equipment. If the fill is too dry, mix in water as the fill is spread; surface watering is typically ineffective.

Where fill will be placed against slopes, bench the fill into the slope to create a stair-step interface, for improved stability and groundwater control. Lightly scarify the surface of the existing soil prior to placing the fill, and key the fill into the subgrade at the toe of the slope. When the fill is more than five feet high against a slope of twenty percent or more, the key should be at least two feet deep and ten feet wide.

For cut slopes and fill slopes with a height of thirty feet or more, and a slope of 33 percent or greater (one in three,) terraces should be provided at vertical intervals of thirty feet or less, to control drainage and debris. The terraces should be at least six feet wide, but where more than one is required, the terrace nearest mid-height of the slope should have a width of at least twelve feet, for maintenance access. Drainage swales shall be provided on terraces. Refer to the optional Appendix J of the Building Code for additional details.

Pipe bedding in utility trenches may act as groundwater flow routes during or after construction. Use well-graded bedding, or interrupt coarse granular bedding with occasional zones of compatible lower-permeability soil to control minor seepage. Avoid the use of excessively coarse pipe bedding material that can allow fines to wash in from the surrounding soil. Contact the Engineer if excessive groundwater is encountered.

Open-graded stone base course material for slabs-on-grade should be graded level and seated with one or more compaction passes, to help resist displacement during slab area preparation and concrete placement.

It is expected that the native clayey glacial till will be used for the majority of the fill in the building areas. Careful preparation, placement and compaction methods must be employed, and the fill section must be properly designed.

- Prepare the fill by drying it to a somewhat crumbly consistency, then thoroughly break up the soil clods so that they are no larger than two-thirds of the lift thickness (e.g. smaller than eight inches for a twelve-inch thick lift.)
- Mix and spread the fill so that the larger clods are well-mixed with finer pulverized soil; remove boulders during preparation and placement. Condition the fill as needed to reach the proper compaction moisture content, mixing the fill so that the moisture is uniform throughout the lift thickness.
- Re-work any 'clod clusters,' where the fill is lacking in fines, to a well-graded condition, by crushing, mixing and/or adding fine fill material.
- Compact the clay fill with a mid-size single-drum vibratory roller, or with a dual-drum trench roller where access is limited; a heavy roller will tend to produce rutting, and a light roller will not adequately compact the soil. A roller with a sheep's-foot or tamping foot drum is preferred, both because it tends to knead and compact the soil clods, and because the compacted surface promotes the dispersed vertical drainage of water infiltration, versus the surface produced by a smooth-drum roller, which promotes lateral seepage movement, potentially causing local saturation and the creation of soft spots.

- Drainage must be provided at the bottom of any significant fill sections, to minimize water accumulation in the base of the clay, which can cause softening and settlement. A layer of granular fill, such as 'Structural Fill,' at least one foot thick, is typically sufficient, provided the granular layer is free to drain laterally and/or vertically. Where the vertical drainage into a clay subgrade is to be provided, trim the clay subgrade carefully to a suitable surface without disturbance, and do not compact the clay prior to placing the granular fill; this will promote infiltration, but the rate may still be slow.
- The top of the fill must also be provided with proper drainage, particularly below parking lots, lawns, and in other areas of surface water infiltration. The final lift of clay fill should be at least two feet below the proposed top-of-pavement elevation in paved areas, to provide sufficient depth for drainage and for protection of the clay subgrade during construction and paving. In landscaped areas, the top of the clay fill should also be at least two feet deep, to allow for a sufficient thickness of fill with a suitable moisture capacity to support vegetation.
- The top of the clay fill must be carefully graded to avoid low spots, where surface water infiltration can accumulate; it should be pitched gently toward underdrains or other outlets, and not made perfectly level.
- Installation of a layer of geotextile between the top of the clay fill and the pavement subbase and landscaping fill is recommended. The geotextile will promote the retention of water from surface infiltration in the pavement base and drainage layers and in the landscaping, and will reduce concentrated infiltration into the clay fill.
- Surface water infiltration in the shallow fill materials and in the clay fill will tend to seek curbs, utility trenches and similar discontinuities, and subsurface drainage should be provided from these features; where water concentration along utilities needs to be minimized, use well-graded bedding material.
- Embankment slopes constructed with clay fill should be built slightly wide, then trimmed back, to allow thorough compaction near the edge. The fill placed in the outer zone (six feet wide, or one third of the fill height above, whichever is greater) should be compacted at a moisture content no more than one percent above optimum, leaving the soil clods slightly crumbly and creating some initial lateral permeability.
- The surfaces of embankment slopes should be scarified prior to placing topsoil, and small benches or one- to two-foot wide steps should be provided at frequent intervals to protect against sliding of the topsoil. The topsoil should be well-graded and relatively free-draining for erosion resistance, and should be placed at the minimum required thickness when the slope is steeper than three-on-one.

### **3.5. Compaction Requirements**

Compact each lift of fill supporting slabs or foundations with at least six one-way compaction passes, even if the required compaction percentage is obtained with fewer passes. Each compaction pass shall be made at a slow walking speed (less than four feet per second,) with the equipment passing completely over all areas of the fill. Fill materials shall be compacted to at least the following percentage of the ASTM D1557 maximum dry density. For coarse-graded fill materials with more than thirty percent retained on the 3/4-inch sieve, the ASTM D4253 Maximum Index Density test may be substituted for the D1557 test.

Minimum Percent Compaction	
Location	Minimum Percent
Below footings, foundations and slabs	95
Exterior Foundation Backfill in Landscaped Areas	90

### 3.6. Testing

The prepared subgrade shall be inspected to verify that it has been prepared in conformance with the requirements of this report, prior to placing fill. Compaction testing is required by Code for each lift of fill supporting foundations, and testing shall be performed while the work is in progress. Recommended test procedures and frequencies are provided below.

**PROOF-ROLLING:** Proof-rolling of the prepared subgrade is not required, but may be performed to determine the limits of a soft area. Use an appropriately-sized vehicle, to avoid damaging wet and/or fine-grained, but otherwise acceptable soils. Observe the effects of the moving roller; if the soil exhibits excessive deflection, rutting or cracking, additional excavation or drying of the subgrade may be required.

**BEARING CAPACITY:** The prepared subgrade surface shall be free from loose material and shall be in a dense and unyielding condition; if this condition is not encountered at the design bearing elevation, testing shall be performed with a Static Cone Penetrometer or equivalent device, and the design bearing capacity shall be obtained within 3 inches of the surface in footing excavations. The soil throughout the foundation area shall be probed thoroughly to check for soft spots. If the bearing capacity tests are acceptable, the soil is undisturbed, is free from organics and is densely-consolidated, and if the observed yielding conditions are not due to the presence of loose or deficient soils, the subgrade may be accepted.

**COMPACTION TESTING:** Compaction tests of fill and backfill supporting foundations or slabs-on-grade should be performed in at least three representative locations for each lift, and in at least one location per 2500 square feet of fill surface. Compaction tests should be performed with a nuclear moisture-density gauge, per ASTM Test Method D6938, unless otherwise approved. Required percent compaction values are provided above.

**CLSM:** When flowable fill is used to support footings or foundations, at least one set of three 6x12-inch test cylinders shall be cast from each day's placement, per ASTM D4832. Test the cylinders for unit weight and for compliance with the specified strength requirements. Cast additional cylinders if early tests are needed.

### 3.7. Geosynthetic Materials

Geosynthetic materials are expected be used for reinforcement and drainage applications at the site on an as-needed basis, or where required by Code, such as for footing drains. Geosynthetic materials shall be installed over a smooth and evenly shaped subgrade, to avoid 'tenting' of the material over voids or high points. The geosynthetic shall be installed substantially free from wrinkles, and fill material shall be placed and spread in a manner which pushes the wrinkles out but which does not otherwise displace the geosynthetic material. Vehicles shall not drive on the exposed geosynthetics. The following material types are recommended, with typical examples of suitable products.

Drainage Separation: For footing drains and similar applications, a woven drainage geotextile with at least 4% open area, with an apparent opening size of 0.21mm (#70) or smaller, should be installed between the native soils and open-graded drainage zones. A suitable product is Carthage Mills "Carthage 6%." Non-woven geotextiles are not recommended for use in this application, due to the presence of fine particles in the native soil that will tend to clog the fabric. If stone drains are installed in areas of fine sand or cohesionless silt, provide a zone of clean sand at least three inches thick between the geotextile and the soil.

Subgrade Reinforcement: Typically, a woven reinforcing geotextile such as TenCate Mirafi 600X should be used where needed to improve the stability of soft subgrade soils. Geogrids may be used instead of woven geotextiles, especially if free drainage is desired. A minimum of twelve inches of granular fill cover is typically required to mobilize the strength of the reinforcing geosynthetic. Woven reinforcement geotextile will usually act as an infiltration barrier when installed in a continuous horizontal layer, and non-woven separation geotextile may also work as a barrier; this may or may not be desirable, depending on the installation location and conditions.

Subgrade Separation: Where fines from the subgrade may infiltrate into an overlying granular layer, and strengthening of the subgrade and free vertical drainage are not required, a non-woven geotextile such as Mirafi S600 or 160N should be used.

#### 4. DESIGN VALUES AND RECOMMENDATIONS

Soil engineering properties and recommendations for design are provided in this section; additional important design considerations are also discussed in the other sections of this report. The design values assume that the building will be supported by a conventional spread footing foundation with slab-on-grade floor, as described in the previous sections, and will be provided with proper drainage.

##### 4.1. Bearing Capacity and Soil Pressure

Allowable Bearing Capacity, $q_a$		
	Cut Areas	Fill Areas
Footings bearing at least 42 inches below finished grade, with a minimum width of 24 inches	4000 psf	3000 psf
Footings bearing at least 24 inches below finished grade, minimum width as noted	4000 psf 24" min.	3000 psf 60" min.
Minor Footings bearing at least 12 inches below finished grade, with a minimum width of 12 inches	2500 psf	1500 psf

Soil Properties	Native Soils
Soil Moist Density, $\gamma$ , lbs/cu ft	140
Effective Internal Angle of Friction, $\phi$	32°
Coefficient of Friction (vs. concrete)	0.40
Coefficient of Active Earth Pressure, $k_a$	0.31
Coefficient of Passive Earth Pressure, $k_p$	3.25
Coefficient of At-Rest Earth Pressure, $k_o$	0.47
Lateral Bearing Capacity (psf per ft below grade)	225
Modulus of Subgrade Reaction, $k$ , psi per inch	200

Two bearing capacity values are provided, one for the in-situ glacial till soils and one for footings bearing on fill composed of this soil. It is recommended that the footings be designed following one of three strategies:

- Method 1. Design all footings for the lower (fill area) bearing capacity.
- Method 2. Design the footings for the most of the cut area for 4000 psf bearing. Design the footings in the fill area and in the last adjacent column bays of the cut area for 3000 psf bearing capacity.
- Method 3. Design all footings for the higher (cut area) bearing capacity. In the fill area, the final 24 inches of fill below the foundation shall consist of Structural Fill; this zone of granular fill shall extend at least 24 inches beyond the edges of the footings.

Footings subject to frost shall bear at least 42 inches below finished grade, or shall be otherwise protected from frost. Bearing elevations of footings shall be established such that a line drawn between the bottoms of two adjacent footings is not steeper than 30 degrees between the closest points on the footings. (Slope of 1 vertical to 1.75 horizontal.)

Up to one inch of settlement and 3/4-inch of differential settlement should be anticipated for the new foundation during construction, due to normal elastic compression of the soils below the footings, however in cut areas the actual settlement is expected to be one quarter inch or less. Where clay fill is placed in the recommended manner, an additional one quarter inch to one half inch of settlement should be expected per five feet of fill thickness below the footings.

#### 4.2. Control of Groundwater and Soil Gases

Minor groundwater seepage should be expected in excavations and below-grade areas during and after construction. Conventional damp-proofing, including placement of slabs-on-grade over a vapor barrier and an open-graded stone base course, and installation of conventional footing drains are appropriate to control water seepage around the foundation walls of the building. The borings do not indicate that vertical drainage panels or a zone of sand or gravel outside the walls (where they will be backfilled above the slab elevation) will be necessary for seepage control, but this additional drainage is of relatively low cost and its inclusion should be considered, to protect against unexpected seepage or future changed conditions. Stormwater infiltration from the parking and landscaped area should be diverted away from the building.

Soil gases that could normally be expected to impact the structure are water vapor and radon. Thorough foundation damp-proofing, as noted above, placement of dense concrete in slabs-on-grade, (low water-to-cementitious ratio, thoroughly consolidated,) and sealing of all wall-to-slab joints, concrete cracks, pipe penetrations, drainage sumps, etc. are usually effective in controlling transmission of these gases to interior spaces. If an open-graded base course is used under the slab, a passive vapor mitigation system can be included, using small-diameter PVC pipes. The potential for these gases to adversely impact the use of the building is estimated to be low, if the above recommended practices are used, and normal interior ventilation is provided.

#### 4.3. Seismic and Expansive Properties

**Seismic Design Values:** The Seismic Site Class and Seismic Design Category for the proposed construction were determined per section 1613 of the New York State Building Code and ASCE 7-16. Seismic values for the site were obtained from the current database maintained by the Applied Technology Council, Redwood City, Cal., and are consistent with the published maps in the Building Code. Values were as follow.

Occupancy Category	I/II/III	
<b>Seismic Site Class</b>	C - Very Dense Soil and Soft Rock	
<b>IBC Seismic Design Category</b>	<b>SDC - B</b>	
Maximum Acceleration	0.2 sec $S_S$	0.212 g
	1.0 sec $S_1$	0.054 g
Maximum Spectral Response Acceleration	0.2 sec $S_{MS}$	0.275 g
	1.0 sec $S_{M1}$	0.082 g
5% Damped Spectral Response	0.2 sec $S_{DS}$	0.184 g
	1.0 sec $S_{D1}$	0.054 g



The seismic design values are based on the “risk adjusted maximum probable earthquake.” These are not the maximum values that *could* occur, they are values that are not likely to be exceeded during the service life of a typical structure.

**Liquefaction Potential:** The soils encountered in the investigation have negligible liquefaction susceptibility. The soils are dense and do not have texture/permeability combinations that are associated with loss of shear strength during anticipated seismic events. No special mitigation measures are required.


**Expansive Soils and Frost Heave:** The soils encountered in the investigation have a very low potential for expansion due to shrinking and swelling resulting from moisture changes. This behavior is typically associated with high-plasticity silt and clay soils. Physical testing and qualitative examination indicate that the soil properties do not meet the criteria for potentially expansive soils as defined in section 1803.5.3 of the Code. No mitigation measures are required. The on-site soils are moderately to highly susceptible to frost heave. Frost heave can be minimized by providing good drainage and by thoroughly compacting the soil. Well-graded granular fill should be used in areas where frost heave could result in damage.

## 5. NOTES AND LIMITATIONS

Please see the attached pages for additional information. Subsurface conditions encountered during construction shall be compared to the soil boring logs and this report; any significant variations from anticipated conditions must be evaluated for their effect on the design. This report summarizes the results of a limited investigation and does not purport to predict every variation in subsurface conditions. Elevations, slopes, contours, project layout and similar or related data provided in this report were interpreted from the drawings, from field data or from other information which was provided, unless otherwise noted.

This geotechnical investigation was conducted to evaluate the engineering properties of the soils at the site, to aid in the design of the proposed work. The investigation did not include evaluation of the potential effects of the proposed construction on other properties, nor did it include inspection of, or sampling for, items of environmental concern such as the presence of soil contaminants or of regulated wetlands, and did not include review of local zoning regulations, codes, floodplain boundaries or similar matters, unless specifically referenced in the report. This investigation was conducted solely for the use of the Client, the Client’s Project Designers and Agents and the Authorities Having Jurisdiction; this report should not be used by others, nor for any use other than its stated purpose, without contacting the Engineer. Any such use is solely at the user’s risk.

Prepared by Kevin L. Patton, P.E.



The image shows a blue circular professional seal for Kevin L. Patton, a Licensed Professional Engineer in the State of New York. The seal contains the text "LICENSED PROFESSIONAL ENGINEER", "KEVIN L. PATTON", "May 25, 2020", and "STATE OF NEW YORK" with the license number "072197". A handwritten signature in black ink is written across the seal.



The USCS (Unified Soil Classification System) was used to classify the soils in this report. The USCS is described in ASTM D2487 (laboratory test method) and D2488 (visual-manual method.) The USCS classification gives a 'Group Symbol' and 'Group Name' based on particle size distribution (gradation,) clay properties (Atterberg Limits) and basic composition (mineral or organic.)

**USCS Soil Classes**

Soils with less than 5% passing the #200 sieve:

GW, GP, SW, SP – Well-graded gravel, Poorly-graded gravel, Well-graded sand, Poorly-graded sand.

Soils with 12% to 50% passing the #200 sieve:

GC, GM, GC-GM, SC, SM, SC-SM – Clayey gravel, Silty gravel, Silty clayey gravel, Clayey sand, Silty sand, Silty clayey sand.

Soils with 5% to 12% passing the #200 sieve use a dual symbol, such as SW-SC (Clayey well-graded sand.)

Soils with more than 50% passing the #200 sieve:

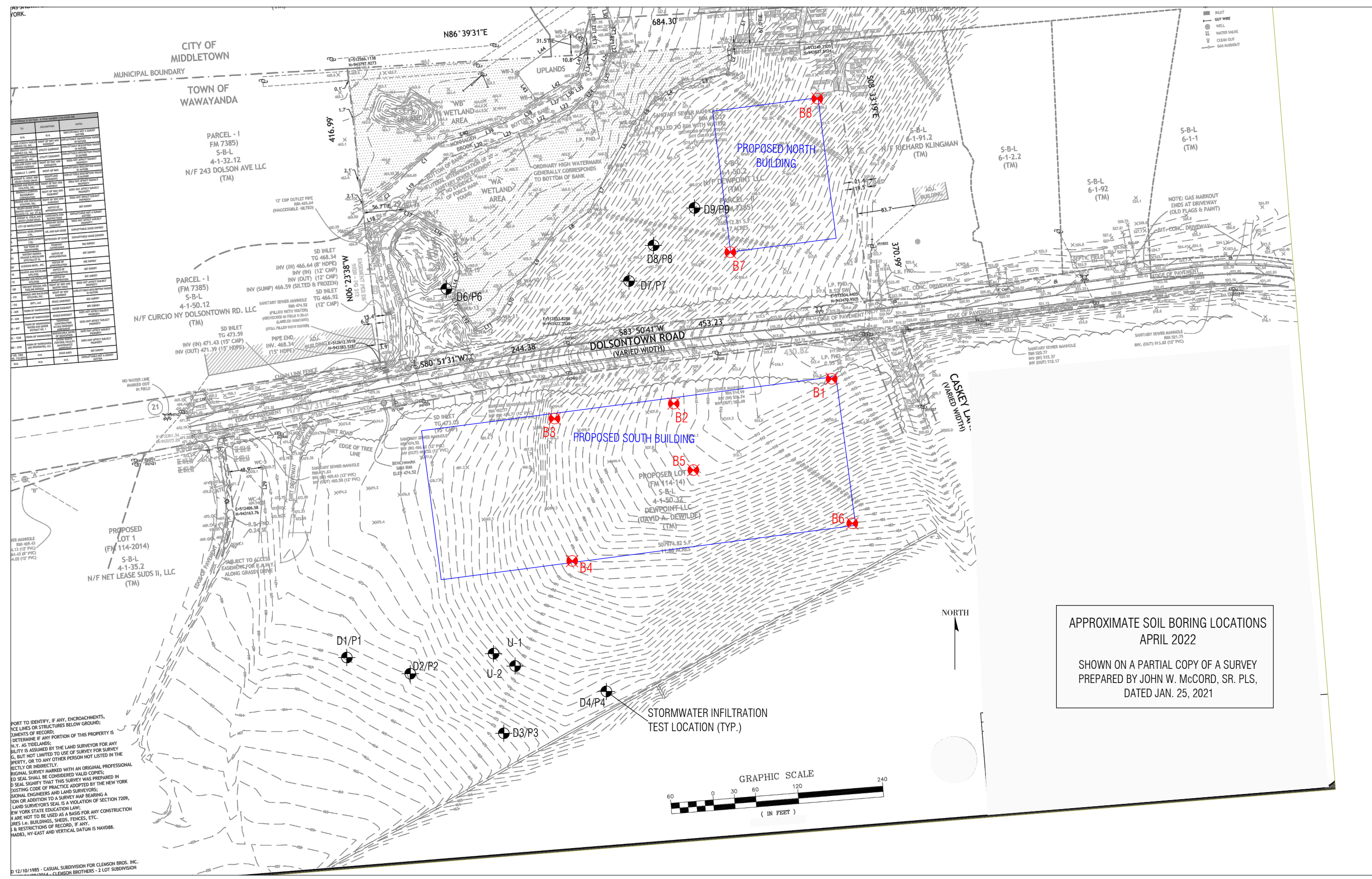
CL-ML, ML, CL, MH, CH, OL, OH – Silty clay, Silt, Lean clay, Elastic silt, Fat clay, Organic silt, Organic clay.

Highly organic soils:

PT – Peat.

The soil group name is modified with the term 'with sand' or 'with gravel' added if the soil contains more than 15% of these materials; clays and silts with 30% or more plus-#200 material are described as 'sandy' or 'gravelly' (whichever is predominate.) Examples – GM, Silty gravel with sand; CL, Gravelly lean clay.

Particle size	Fine- and Coarse-grained Soils	Atterberg Limits
>12" (300mm)      Boulders 12" to 3" (300-75mm)      Cobbles 3" to #4 (75-4.75mm)      Gravel #4 to #200 (4.75-0.075mm)      Sand <#200 (0.075mm)      Silt & Clay	The USCS classification applies to the material smaller than the 3-inch sieve.  'Fine-Grained Soils' (silts and clays) have more than 50% passing the #200 sieve and are classified by their Atterberg Limits.	Test is performed on the clay, silt and fine sand fraction of the soil: Liquid Limit (LL) – moisture content (%) at which soil becomes very soft. Plastic Limit (PL) – moisture content at which soil crumbles. Plasticity Index (PI) = LL minus PL
<b>Organic Soils</b>  Highly organic soils such as peat are visually classified. Partly organic soils, with a mix of organic and mineral matter, are classified visually and by Atterberg Limits tests.	'Coarse-Grained Soils' (sands and gravels) have less than 50% passing the #200 sieve. When more than 50% of the plus-200 material is retained on the #4 sieve the general soil type is gravel, and if more than 50% is finer than the #4 sieve, it is sand.	Higher PI values may indicate reduced permeability and increased drying shrinkage.
<b>Moisture Content</b>  Moisture is visually estimated and samples are usually tested. Soil moisture capacity varies with texture and compaction.  Typical examples: GW, moist at 3%, saturated at 9% SP, moist at 6%, saturated at 20%. CL, moist at 12%, saturated at 33%.	Clean coarse-grained soils are classified as well-graded (Classes GW, SW) or poorly-graded (GP, SP.) Well-graded soils have a wider range of sizes and are typically more stable. Poorly-graded soils are usually more permeable.	LL > 50 indicates soil with a higher potential to shrink and swell due to changing moisture content.  Silts have lower PI values, and behave like very fine sand; most silts also contain some clay. Behavior of clays is partly controlled by electrochemical forces and varies among the several clay minerals.
<b>Color</b>	<b>Relative Quantities</b>	<b>USDA Soil Classification</b>
Soil color sometimes indicates groundwater conditions, with subdued colors below the water table and mottled (mixed) colors in the zone of seasonal water table fluctuation. Color changes tend to be more prominent in fine-grained soils.	Estimated percentages in descriptions: <5% - Trace 5-10% - Traces 10-25% - Little 25-35% - Some 'And' - Approx. equal amounts 'Few' - <10% (cobbles and boulders)	USDA classifications are based on the relative amounts of sand, silt and clay in the soil fraction passing the #10 (2mm) sieve. 'Gravelly' indicates more than 15% of #10 to 3" size. 'Channery' indicates 15 to 35% thin flat pieces up to 6" long.



KEVIN L. PATTON, P.E. 36 PATTON ROAD NEWBURGH, NY 12550 845 275-7732 PATTONGEOTECH.COM		DEWPOINT DOLSONTOWN	TOWN OF WAWAYANDA, N.Y.	SOIL BORING LOCATIONS
REV.	DATE	BY		
0	5/25/2022	KLP		

PORT TO IDENTIFY, IF ANY, ENCROACHMENTS,  
ICE LINES OR STRUCTURES BELOW GROUND;  
DUMENTS OF RECORD;  
DETERMINE IF ANY PORTION OF THIS PROPERTY IS  
N.Y. AS TIDELANDS;  
ABILITY IS ASSUMED BY THE LAND SURVEYOR FOR ANY  
S, BUT NOT LIMITED TO USE OF SURVEY FOR SURVEY  
PROPERTY, OR TO ANY OTHER PERSON NOT LISTED IN THE  
RECTLY OR INDIRECTLY.  
ORIGINAL SURVEY MARKED WITH AN ORIGINAL PROFESSIONAL  
ED SEAL SHALL BE CONSIDERED VALID COPIES.  
D SEAL SIGNIFY THAT THIS SURVEY WAS PREPARED IN  
EXISTING CODE OF PRACTICE ADOPTED BY THE NEW YORK  
SIONAL ENGINEERS AND LAND SURVEYORS.  
ION OR ADDITION TO A SURVEY MAP BEARING A  
LAND SURVEYOR'S SEAL IS A VIOLATION OF SECTION 7209,  
EN YORK STATE EDUCATION LAW;  
ARE NOT TO BE USED AS A BASIS FOR ANY CONSTRUCTION  
URES I.e. BUILDINGS, SHEDS, FENCES, ETC.  
S & RESTRICTIONS OF RECORD, IF ANY.  
NADS, NY-EAST AND VERTICAL DATUM IS HAYD88.

D 12/10/1985 - CASUAL SUBDIVISION FOR CLEMON BROS., INC.  
S-2014 - CLEMON BROTHERS - 2 LOT SUBDIVISION



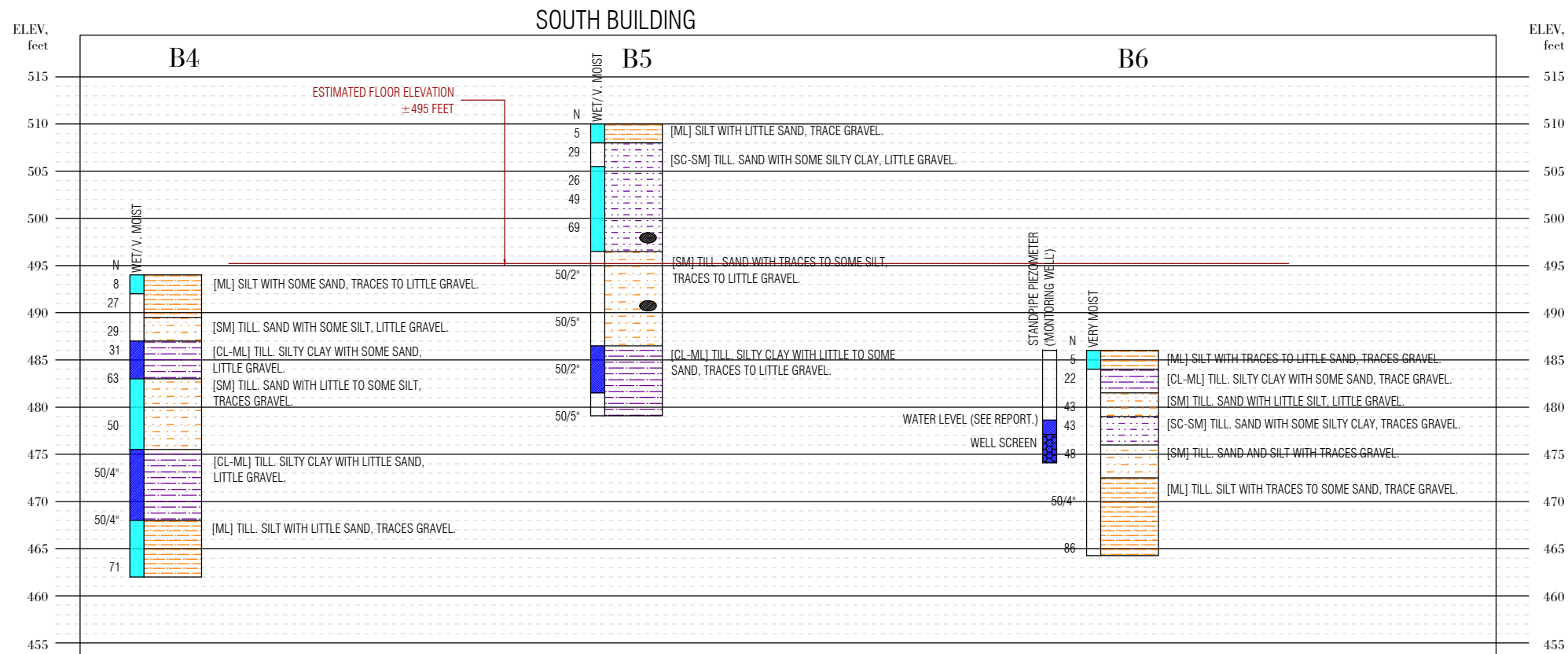
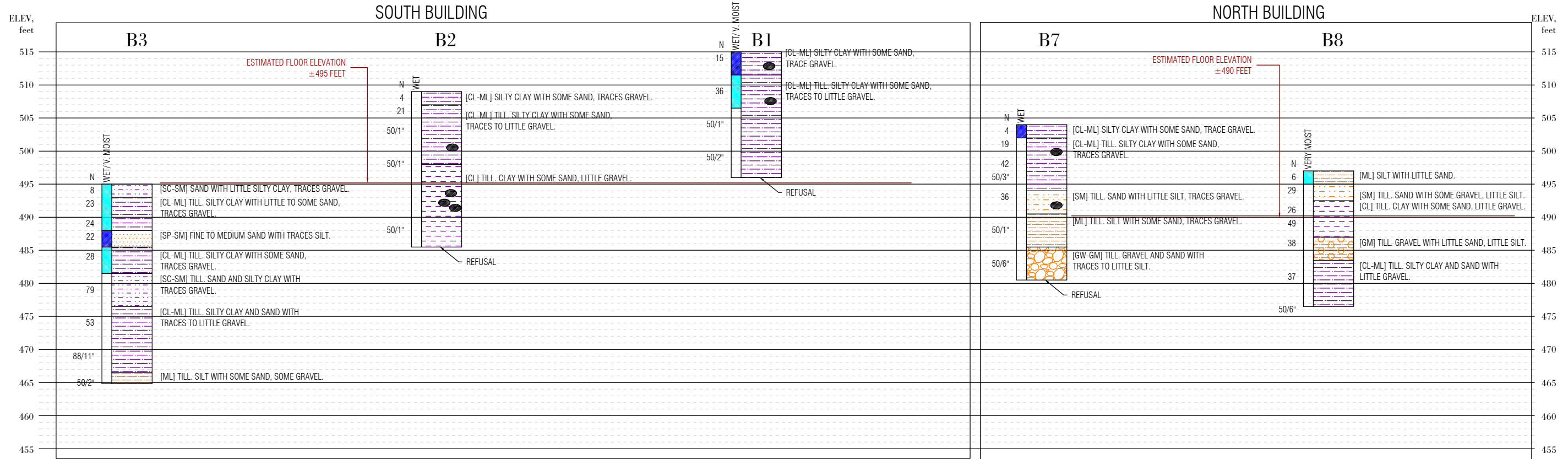
# GENERALIZED SUBSURFACE PROFILE

NO HORIZONTAL SCALE.  
USCS SOIL CLASSIFICATIONS ARE IN BRACKETS.

IN GENERAL, RED PATTERNS INDICATE RELATIVELY CLEAN SANDY OR GRAVELLY SOILS,  
PURPLE PATTERNS INDICATE SOILS WITH SIGNIFICANT CLAY CONTENT AND ORANGE  
PATTERNS INDICATE SOILS WITH A SIGNIFICANT SILT CONTENT.

● BOULDER(S)

THESE SECTIONS ARE GENERALIZED REPRESENTATIONS OF THE SUBSURFACE PROFILE,  
BASED ON THE SUBSURFACE EXPLORATION DATA, OBSERVATIONS, RESEARCH, AND OTHER  
RELEVANT INFORMATION. THE SOILS INFORMATION PRESENTED HEREIN SHOULD BE  
INTERPRETED IN CONJUNCTION WITH THE INFORMATION FROM THE BORING LOGS AND THE  
GEOTECHNICAL INVESTIGATION REPORT. SITE CONDITIONS MAY DIFFER FROM THOSE  
ENCOUNTERED AT THE BORING LOCATIONS.



**KEVIN L. PATTON, P.E.**  
36 PATTON ROAD  
NEWBURGH, NY 12550  
845 275-7732  
PATTONGEOTECH.COM

DEWPOINT DOLSONTOWN  
TOWN OF WAWAYANDA, N.Y.  
SUBSURFACE PROFILE

REV.	DATE	BY
0	5/25/2022	KLP

<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/22/2021	Project No.:	21416
	WEATHER:	Clear		

**SOIL BORING LOG**

DRILLING COMPANY:	General Borings	LOCATION:	South Building, NE corner	<b>BORING NO.</b>	<b>B1</b>
DRILLER AND HELPER:	James Casson, ---	APPROX. ELEV.:	515 feet		
HAMMER TYPE:	Automatic	WATER DEPTH:			
INSPECTOR:	Wyeth Patton				

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	10	CL-ML	1	1	14	50/1	Wet	Silty clay with some sand, trace gravel Yellowish olive-brown PEN = 2.8 ksf	Boulder 2'
5											
5-7	S2	SS	20	CL-ML	8	13	23	50/4	Very Moist	Till - Silty clay with some sand, traces-little gravel Brown with grey mottling PEN = 10 ksf	Boulder 7-8'
10											
10-12	S3	SS	4	CL-ML	50/3				Moist	Same Brown PEN = 16 ksf	
15											
15-17	S4	SS	5	CL-ML	44	50/2			Moist	Same Medium-dark brown PEN = 11 ksf	
20											Refusal 19'
25											
30											
35											
40											
45											

COMMENTS:			
DRILLING METHOD: HSA - Hollow-Stem Auger		MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE
	PEN - HAND PENETROMETER	TOR - TORVANE	V - VANE SHEAR

<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/21-22/2021	Project No.:	21416
	WEATHER:	Clear, Rain showers		

**SOIL BORING LOG**

DRILLING COMPANY:	General Borings	LOCATION:	South Building, north side	<b>BORING NO.</b>	<b>B2</b>
DRILLER AND HELPER:	James Casson, ---		east		
HAMMER TYPE:	Automatic	APPROX. ELEV.:	509 ft		
INSPECTOR:	Wyeth Patton	WATER DEPTH:			

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	22	CL-ML	1	2	2	10	Moist	Silty clay with some sand, traces gravel Brown with grey mottling PEN = 11 ksf	
2-4	S2	SS	10	CL-ML	10	13	18	22	Moist	Till - silty clay with some sand, traces gravel Brown with grey mottling PEN = 15 ksf	
5											
5-7	S3	SS	1	CL-ML	50/1				Moist	Same Brown. Small sample.	8' Refusal, Offset
10											
10-12	S4	SS	1	-	50/1				Moist	Cobble/gravel fragments. Brown. Small sample.	
15											
15-20	Run 1	C	30	Boulder	-				-	Cored 2.5 ft through boulder, continued core 2.5 ft beyond, in soil. Drove split spoon at 20-22 ft. Re-drilled boulder with roller bit.	Refusal 15' Cored through boulder
20		C									
20-22	S5	SS	3	CL	33	50/1			Wet	Till - Clay with some sand, little gravel Olive grey. PEN 12 ksf Attempted to drill with auger, met refusal with steel/weld failure of the first 5-ft auger section.	Refusal 23 1/2'
25											
30											
35											
40											
45											

COMMENTS:			
DRILLING METHOD: HSA - Hollow-Stem Auger		MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE
	PEN - HAND PENETROMETER	TOR - TORVANE	V - VANE SHEAR

<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/22/2021	Project No.:	21416
	WEATHER:	Rain Showers		

### SOIL BORING LOG

DRILLING COMPANY:	General Borings	LOCATION:	South Building, north side	<b>BORING NO.</b>	<b>B3</b>
DRILLER AND HELPER:	James Casson, ---		west		
HAMMER TYPE:	Automatic	APPROX. ELEV.:	495 ft		
INSPECTOR:	Wyeth Patton	WATER DEPTH:			

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	14	SC-SM	2	3	5	6	Very Moist	Sand with little silty clay, traces gravel	
2-4	S2	SS	20	CL-ML	6	10	13	11	Very Moist	Brown, faint mottling Till - Silty clay with little to some sand, traces gravel. Brown, slightly mottled gray. PEN 12ksf	
5											
5-7	S3	SS	24	CL-ML	10	12	12	16	Very Moist	Till - same Brown with slight grey mottling PEN = 11 ksf	
7-9	S4	SS	20	SP-SM	6	12	10	8	Wet	Sand (FM) with traces silt Brown PEN = 2.8 ksf	
10											
10-12	S5	SS		CL-ML	7	12	16	22	Very Moist	Till - silty clay with some sand, traces gravel Brown with grey mottling PEN = 19 ksf	
15											
15-17	S6	SS		SC-SM	33	35	44	50	Moist	Till - sand and silty clay with traces gravel Brown PEN = 27+ ksf	
20											
20-22	S7	SS		CL-ML	21	26	27	37	Moist	Till - Silty clay and sand (Fmc) with traces to little gravel. Olive grey. PEN = 27+ ksf	
25											
25-27	S8	SS		CL-ML	32	38	50/5		Moist	Till - Silty clay with traces sand, trace gravel Olive grey PEN = 14 ksf	
30											
30-32	S9	SS	2	ML	50/2				Moist	Till - silt with some sand, some gravel Grey. Small sample.	
35											
40											
45											

COMMENTS:			
DRILLING METHOD: HSA - Hollow-Stem Auger		MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE
	PEN - HAND PENETROMETER	TOR - TORVANE	V - VANE SHEAR

<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/22,25/2021	Project No.:	21416
	WEATHER:	Rain Showers		

### SOIL BORING LOG

DRILLING COMPANY:	General Borings	LOCATION:	South Building, south side west	<b>BORING NO.</b>  <b>B4</b>
DRILLER AND HELPER:	James Casson, ---	APPROX. ELEV.:	494 feet	
HAMMER TYPE:	Automatic	WATER DEPTH:		
INSPECTOR:	Wyeth Patton			

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	10	ML	2	1	7	14	Very Moist	Silt with some sand, traces gravel, trace roots Yellowish brown PEN = 2 ksf	
2-4	S2	SS	2	ML	17	12	15	21	Moist	Silt with some sand, little gravel Brown. Small sample.	
5											
5-7	S3	SS	22	SM	8	14	15	15	Moist	Till - sand with some silt, little gravel. Strongly mottled brown and grey with orange.	PEN = 11 ksf
7-9	S4	SS	20	CL-ML	18	16	15	20	Wet	Till - silty clay with some sand, little gravel Olive brown PEN = 6 ksf	
10											
10-12	S5	SS	0		21	37	26	36		No Recovery	
15											
15-17	S6	SS	14	SM	15	28	22	25	Very Moist	Till - sand with little to some silt, little gravel Brown, slightly mottled. PEN = 15 ksf Small sample.	
20											
20-22	S7	SS	3	CL-ML	35	50/4			Wet	Till - Silty clay with little sand, little gravel Grey with slight brown mottling. Small sample.	
25											
25-27	S8	SS	0		34	50/4				No Recovery	
30											
30-32	S9	SS	18	ML	20	33	38	50	Very Moist	Till - silt with little sand, traces gravel Grey. PEN = 12 ksf	
35											
40											
45											

**COMMENTS:**

DRILLING METHOD:	HSA - Hollow-Stem Auger	MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES		
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE	AUG - AUGER CUTTINGS	
	PEN - HAND PENETROMETER		TOR - TORVANE	V - VANE SHEAR	

<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/25/2022	Project No.:	21416
	WEATHER:	Clear		

**SOIL BORING LOG**

DRILLING COMPANY:	General Borings	LOCATION:	South Building, east from center	<b>BORING NO.</b>	<b>B5</b>
DRILLER AND HELPER:	James Casson, ---	APPROX. ELEV.:	510 ft		
HAMMER TYPE:	Automatic	WATER DEPTH:			
INSPECTOR:	Wyeth Patton				

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	12	ML	2	2	3	4	Very Moist	Silt with little sand, trace gravel Brown PEN = 5 ksf	
2-4	S2	SS	14	SC-SM	4	8	21	30	Moist	Till. Sand and silty clay with little gravel. Strongly mottled brown and grey with orange.	PEN = 8 ksf
5											
5-7	S3	SS	24	SC-SM	12	12	14	15	Very Moist	Till. Sand with some silty clay, little gravel. Strongly mottled brown and grey with orange.	PEN = 7 ksf
7-9	S4	SS	21	SC-SM	17	17	32	27	Very Moist	Till - same. Olive brown PEN = 15 ksf	
10											
10-12	S5	SS	18	SC-SM	14	19	50/6		Very Moist	Till - sand and silty clay with little gravel Olive brown PEN = 15 ksf	Grinding 12-13'
15											
15-17	S6	SS	5	SM	34	50/2			Moist	Till. Sand with traces to little silt, little gravel Olive brown PEN = 4.5 ksf	Grinding 18'
20											
20-22	S7	SS	8	SM	32	50/5			Moist	Till - sand with some silt, traces gravel Olive brown. PEN = 6 ksf	
25											
25-27	S8	SS	1	CL-ML	50/2				Wet	Till - silty clay with some sand, little gravel Grey. Small sample.	
30											
30-32	S9	SS	9	CL-ML	28	50/5			Moist	Till - silty clay with little sand, traces gravel Grey. PEN = 16 ksf	
35											
40											
45											

COMMENTS:			
DRILLING METHOD:	HSA - Hollow-Stem Auger	MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE
	PEN - HAND PENETROMETER	TOR - TORVANE	V - VANE SHEAR



<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/25-26/2022	Project No.:	21416
	WEATHER:	Rain Showers		

**SOIL BORING LOG**

DRILLING COMPANY:	General Borings	LOCATION:	South Building, SE corner	<b>BORING NO.</b>	<b>B6</b>
DRILLER AND HELPER:	James Casson, ---	APPROX. ELEV.:	486 ft		
HAMMER TYPE:	Automatic	WATER DEPTH:	7.38 ft on 5-25-22 (29 days)		
INSPECTOR:	Wyeth Patton				

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	8	ML	2	3	2	2	Very Moist	Silt with traces to little sand, traces gravel, trace small roots. Brown.	
2-4	S2	SS	20	CL-ML	3	11	11	9	Moist	Till - silty clay with some sand, trace gravel Brown PEN = 9 ksf	Standpipe piezometer installed to 11.9 ft below
5											
5-7	S3	SS	20	SM	7	15	28	29	Moist	Till - sand with little silt, little gravel Olive brown PEN = 10 ksf	grade, well screen on bottom 3 feet.
7-9	S4	SS	20	SC-SM	31	22	21	30	Moist	Till - sand with some silty clay, traces gravel Olive brown PEN = 16 ksf	
10											
10-12	S5	SS	18	SM	10	24	24	48	Moist	Till - Sand and silt with traces gravel Grey. PEN = 19 ksf	
15											
15-17	S6	SS	10	ML	48	50/4			Moist	Till - Silt with some sand, trace gravel Grey PEN 9 ksf	
20											
20-22	S7	SS	9	ML	21	41	45	50/3	Moist	Till - Silt with traces sand, trace gravel Grey PEN 12 ksf	
25											
30											
35											
40											
45											

COMMENTS:			
DRILLING METHOD: HSA - Hollow-Stem Auger		MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE
	PEN - HAND PENETROMETER	TOR - TORVANE	V - VANE SHEAR

<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/26/2022	Project No.:	21416
	WEATHER:	Rain Showers		

**SOIL BORING LOG**

DRILLING COMPANY:	General Borings	LOCATION:	North Building, SW corner	<b>BORING NO.</b>	<b>B7</b>
DRILLER AND HELPER:	James Casson, ---	APPROX. ELEV.:	504 ft		
HAMMER TYPE:	Automatic	WATER DEPTH:			
INSPECTOR:	Wyeth Patton				

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	20	CL-ML	2	1	3	9	Wet	Silty clay with some sand, trace gravel Olive brown PEN = 1.5 ksf	
2-4	S2	SS	20	CL-ML	8	9	10	12	Moist	Till - silty clay with some sand, traces gravel Strongly mottled brown and grey with orange,	PEN = 13 ksf
5											Grinding 4' - cobble
5-7	S3	SS	8	CL-ML	10	18	24	23	Moist	Till - same Brown	
7-9	S4	SS	4	CL-ML	50/3				Moist	Till - same Brown PEN = 9 ksf	
10											
10-12	S5	SS	20	SM	29	18	18	19	Moist	Till - sand with little silt, traces gravel Olive brown	Grinding 12'
15											
15-17	S6	SS	4	ML	41	50/1			Moist	Till - silt with some sand, traces gravel Olive brown PEN = 6 ksf	
20											
20-22	S7	SS	4	GW-GM	50/6				Moist	Till - Gravel and sand with traces to little silt. Brown PEN = 12 ksf	Refusal 23.5 ft
25											
30											
35											
40											
45											

COMMENTS:			
DRILLING METHOD: HSA - Hollow-Stem Auger		MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE
	PEN - HAND PENETROMETER	TOR - TORVANE	V - VANE SHEAR

<b>KEVIN L. PATTON, P.E.</b> <b>36 PATTON ROAD</b> <b>NEWBURGH, NY 12550</b> <b>PATTONGEOTECH.COM 845 275-7732</b>	CLIENT:	RDM Group		
	PROJECT:	Dewpoint Dolsontown Rd., Town of Wawayanda, N.Y.		
	DATE:	4/26/2022	Project No.:	21416
	WEATHER:	Rain Showers		

**SOIL BORING LOG**

DRILLING COMPANY:	General Borings	LOCATION:	North Building, NE corner	<b>BORING NO.</b>	<b>B8</b>
DRILLER AND HELPER:	James Casson, ---	APPROX. ELEV.:	497 ft		
HAMMER TYPE:	Automatic	WATER DEPTH:			
INSPECTOR:	Wyeth Patton				

Feet	SAMPLE			USCS SOIL CLASS	SPT TEST, BLOWS/6"				MOISTURE	DESCRIPTION	NOTES
	#	Type	Rec.		0-6	6-12	12-18	18-24			
0-2	S1	SS	3	ML	2	3	3	3	Very Moist	Silt with little sand, half-inch diameter root.	
2-4	S2	SS	12	SM	6	12	17	22	Moist	Till - sand with some gravel, little silt Brown, slightly mottled.	
5											
5-7	S3	SS	22	CL	10	11	15	13	Moist	Till - Clay with some sand, little gravel Olive brown PEN = 12 ksf	
7-9	S4	SS	6	CL	16	28	21	30	Moist	Till - Same Olive brown PEN = 20 ksf	Note: Lab sample had 49% passing the #200 sieve,
10											classified as 'SC.'
10-12	S5	SS	1	GM	15	17	21	18	Moist	Till. Gravel with little sand, little silt Olive brown. Small sample.	
15											
15-17	S6	SS	12	CL-ML	19	19	18	20	Moist	Till. Silty clay and sand with little gravel Olive brown. PEN 18 ksf	
20											
20-22	S7	SS	0		50/6					No Recovery	
25											
30											
35											
40											
45											

COMMENTS:			
DRILLING METHOD: HSA - Hollow-Stem Auger		MR - Mud-Rotary	MEASUREMENTS IN FEET AND INCHES
SAMPLE/TEST TYPE	SS - SPLIT SPOON	C - CORE	T - UNDISTURBED TUBE
	PEN - HAND PENETROMETER	TOR - TORVANE	V - VANE SHEAR

**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, NY 12550**  
**845 275-7732    PATTONGEOTECH.COM**

CLIENT:	RDM Group		
PROJECT:	Dewpoint Dolsontown		
PROJECT No.:	21416	SAMPLE LOT No.:	220426-1
DATE SAMPLED:	4/21,22,25/2022	DATE TESTED:	5/18/2022
SAMPLED BY:	Wyeth Patton	TESTED BY:	Wyeth Patton

<b>MOISTURE CONTENT OF SOIL</b>
TEST METHOD: ASTM D2216

SAMPLE NO.	DEPTH, FT.	% MOISTURE
B1 S2	6	12.5
B1 S3	11	10.9
B2 S2	3	11.4
B2 S5	21	9.3
B3 S2	3	12.2
B3 S3	6	11.8
B3 S4	8	14.2
B3 S6	16	9.0
B3 S7	21	8.3
B3 S8	26	11.0
B4 S3	6	11.6
B4 S4	8	11.9
B4 S6	16	9.9
B4 S7	21	13.1
B4 S9	31	11.8
B5 S2	3	8.0
B5 S3	6	11.2
B5 S4	8	11.2
B5 S5	11	9.8
B5 S6	16	7.8
B5 S7	21	8.8
B6 S2	3	11.9
B6 S3	6	8.8
B6 S4	8	10.5
B6 S5	11	11.6
B6 S6	16	7.6
B6 S7	21	9.6

Moisture content is expressed as a percent of the dry mass of the soil.

Reviewed by: *Kevin Patton*

**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, NY 12550**  
**845 275-7732    PATTONGEOTECH.COM**

CLIENT:	RDM Group		
PROJECT:	Dewpoint Dolsontown		
PROJECT No.:	21416	SAMPLE LOT No.:	220426-1
DATE SAMPLED:	4/26/2022	DATE TESTED:	5/18/2022
SAMPLED BY:	Wyeth Patton	TESTED BY:	Wyeth Patton

<b>MOISTURE CONTENT OF SOIL</b>
TEST METHOD: ASTM D2216

	SAMPLE NO.	DEPTH, FT.	% MOISTURE
r	B7 S2	3	11.8
	B7 S3	6	11.8
	B7 S5	11	13.1
	B7 S6	16	9.3
	B7 S7	21	3.7
	B8 S2	3	8.9
	B8 S3	6	10.3
	B8 S6	16	9.2

Moisture content is expressed as a percent of the dry mass of the soil.

Reviewed by: *Kevin Patton*

Form NMC

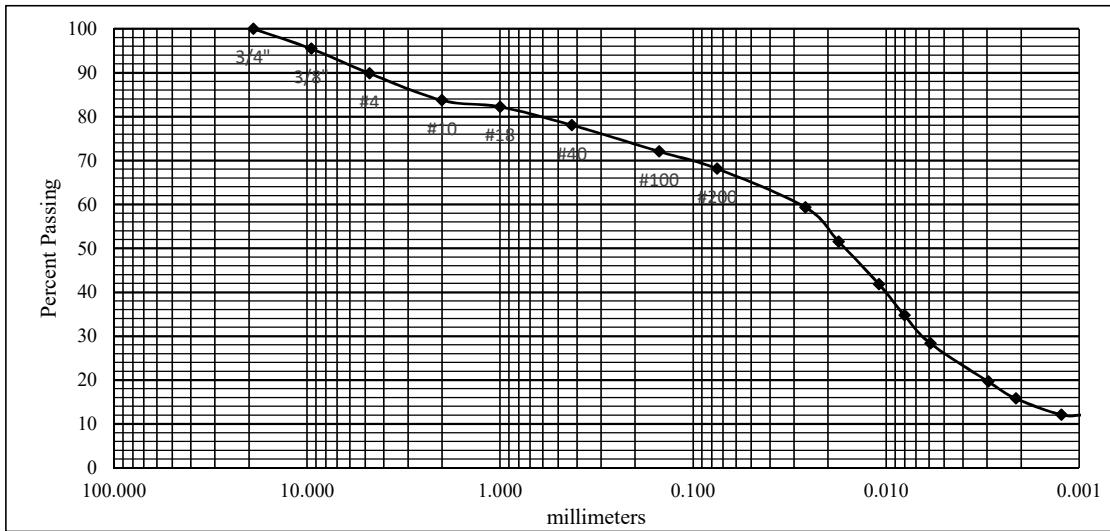
**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, NY 12550**  
**845 275-7732 PATTONGEOTECH.COM**

CLIENT:	RDM Group		
PROJECT:	Dewpoint Dolsontown		
PROJECT No.:	21416	SAMPLE LOT No.:	220426-1
DATE SAMPLED:	4/25/2022	DATE TESTED:	5/18/2022
SAMPLED BY:	Wyeth Patton	TESTED BY:	Wyeth Patton

**SIEVE-AND-HYDROMETER ANALYSIS TEST REPORT**  
TEST METHOD(S): ASTM D422, AASHTO T88

<b>Sample Location</b>	B5-S9
<b>Depth</b>	31 feet

Sieve Size		Percent Retained	Percent Passing	Specification
inches	mm			
3/4"	19.0	0	100	
3/8"	9.5	5	95	
#4	4.75	5	90	
#10	2.00	6	84	
#18	1.00	2	82	
#40	0.425	4	78	
#100	0.150	6	72	
#200	0.075	4	68	
Hydrometer Analysis	0.050	3	65	
	0.020	10	55	
	0.010	15	40	
	0.005	14	26	
	0.002	11	15	
	0.001	3	12	



<b>USDA Particle Size Classification:</b>	<b>USDA Textural Class:</b> Gravelly Silt Loam
Gravel, 3" to 2.00mm: 16	<b>USCS Classification (ASTM D2487/D2488):</b> CL-ML, Sandy Silty Clay
Sand, 2.00 to 0.050mm: 19	
Silt, 0.050 to 0.002mm: 50	Atterberg Limits were determined by: Test
Clay, <0.002mm: 15	
Total: 100	

Reviewed by: Kevin Patton

Form HYD

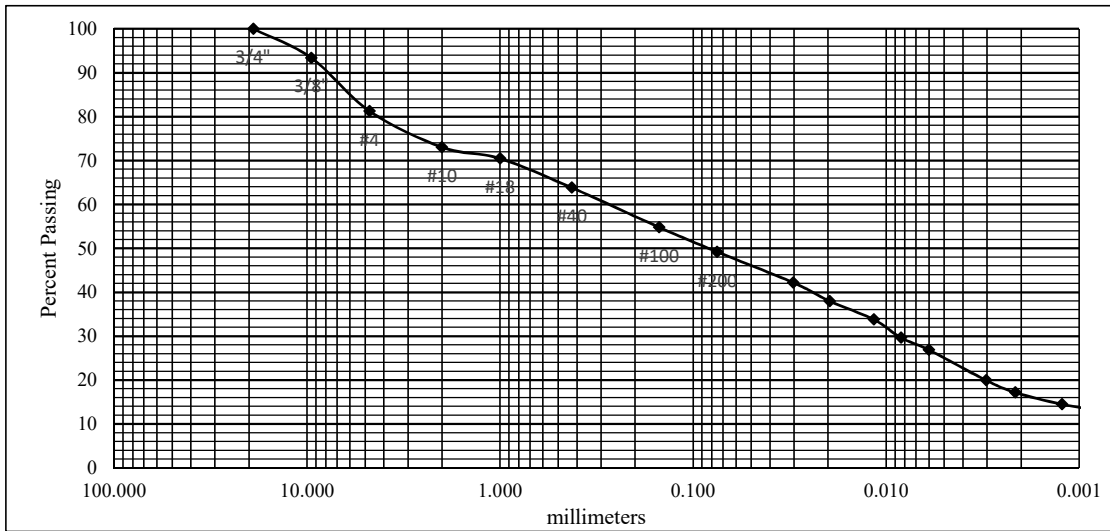
**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, NY 12550**  
**845 275-7732 PATTONGEOTECH.COM**

CLIENT:	RDM Group		
PROJECT:	Dewpoint Dolsontown		
PROJECT No.:	21416	SAMPLE LOT No.:	220426-1
DATE SAMPLED:	4/26/2022	DATE TESTED:	1/0/1900
SAMPLED BY:	Wyeth Patton	TESTED BY:	0

**SIEVE-AND-HYDROMETER ANALYSIS TEST REPORT**  
TEST METHOD(S): ASTM D422, AASHTO T88

<b>Sample Location</b>	B8-S4
<b>Depth</b>	8 feet

Sieve Size		Percent Retained	Percent Passing	Specification
inches	mm			
3/4"	19.0	0	100	
3/8"	9.5	7	93	
#4	4.75	12	81	
#10	2.00	8	73	
#18	1.00	3	70	
#40	0.425	6	64	
#100	0.150	9	55	
#200	0.075	6	49	
Hydrometer Analysis	0.050	3	46	
	0.020	8	38	
	0.010	6	32	
	0.005	7	25	
	0.002	8	17	
	0.001	3	14	



<b>USDA Particle Size Classification:</b>	<b>USDA Textural Class:</b> Gravelly Loam
Gravel, 3\" to 2.00mm	27
Sand, 2.00 to 0.050mm:	27
Silt, 0.050 to 0.002mm:	29
Clay, <0.002mm	17
Total	100
	<b>USCS Classification (ASTM D2487/D2488):</b> SC, Clayey Sand with Gravel
	Atterberg Limits were determined by: Test

Reviewed by: Kevin Patton

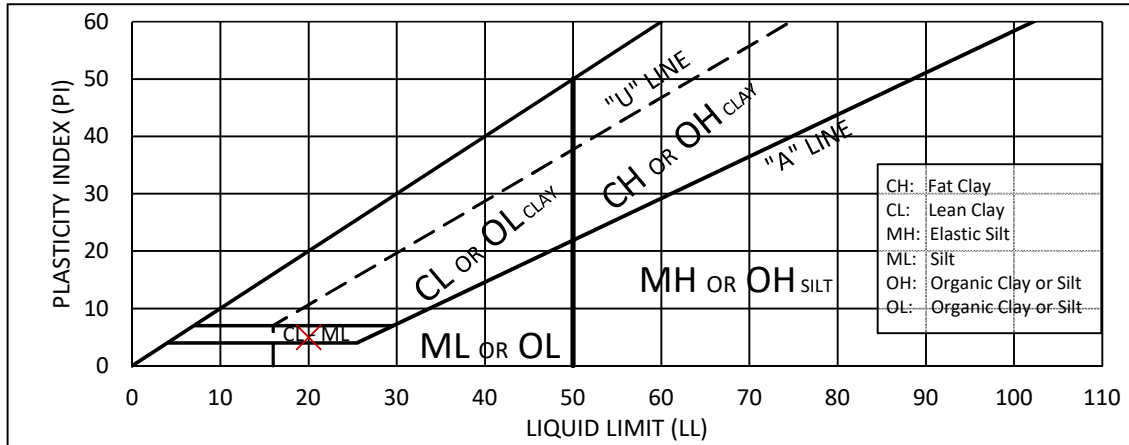
Form HYD

**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, NY 12550**  
**845 275-7732 PATTONGEOTECH.COM**

CLIENT:	RDM Group		
PROJECT:	Dewpoint Dolson town		
PROJECT No.:	21416	SAMPLE LOT No.:	220426-1
DATE SAMPLED:	4/25/2022	DATE TESTED:	5/18/2022
SAMPLED BY:	Wyeth Patton	TESTED BY:	Wyeth Patton

<b>ATTERBERG LIMITS TEST</b>
TEST METHODS: ASTM D4318/ AASHTO T89, T90

<b>Sample Location</b>	B5-S9
<b>Depth</b>	31 feet
Percent Passing #40	78
<b>Liquid Limit (LL)</b>	<b>20</b>
<b>Plastic Limit (PL)</b>	<b>15</b>
<b>Plasticity Index (PI)</b>	<b>5</b>
USCS Class of -#40	CL-ML, Silty Clay



LL, PL and PI values are percent moisture of the soil by dry mass.

Test is performed on the 'matrix' fraction of the soil, finer than the #40 (0.425mm) sieve.

The Liquid Limit is the moisture content at which the matrix fraction of the soil changes from a stiff to a flowing consistency. The plastic limit is the moisture content at which it changes from cohesive to crumbly. The Plasticity Index is the Liquid Limit minus the Plastic Limit.

Reviewed by: *Kevin Patton*

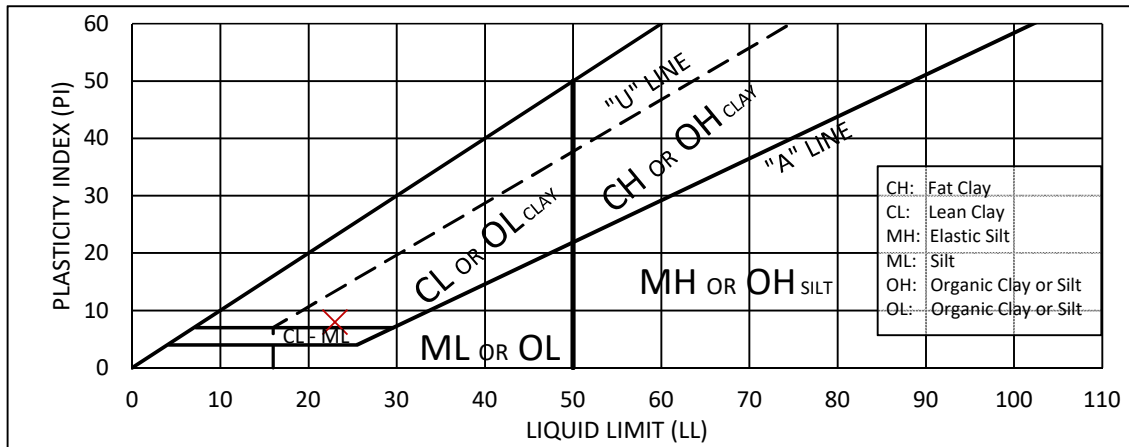


**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, NY 12550**  
**845 275-7732 PATTONGEOTECH.COM**

CLIENT:	RDM Group		
PROJECT:	Dewpoint Dolsonstown		
PROJECT No.:	21416	SAMPLE LOT No.:	220426-1
DATE SAMPLED:	4/26/2022	DATE TESTED:	5/18/2022
SAMPLED BY:	Wyeth Patton	TESTED BY:	Wyeth Patton

<b>ATTERBERG LIMITS TEST</b>
TEST METHODS: ASTM D4318/ AASHTO T89, T90

<b>Sample Location</b>	B8-S4
<b>Depth</b>	8 feet
Percent Passing #40	64
<b>Liquid Limit (LL)</b>	<b>23</b>
<b>Plastic Limit (PL)</b>	<b>15</b>
<b>Plasticity Index (PI)</b>	<b>8</b>
USCS Class of -#40	CL, Lean Clay



LL, PL and PI values are percent moisture of the soil by dry mass.

Test is performed on the 'matrix' fraction of the soil, finer than the #40 (0.425mm) sieve.

The Liquid Limit is the moisture content at which the matrix fraction of the soil changes from a stiff to a flowing consistency. The plastic limit is the moisture content at which it changes from cohesive to crumbly. The Plasticity Index is the Liquid Limit minus the Plastic Limit.

Reviewed by: *Kevin Patton*

**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, NY 12550**  
**845 275-7732    kevin@pattongeotech.com**

CLIENT:	RDM Group		
PROJECT:	Dewpoint Dolsontown		
PROJECT No.:	21416	SAMPLE LOT No.:	220426-1
DATE SAMPLED:	4/22/2022	DATE TESTED:	5/10/2022
SAMPLED BY:	Wyeth Patton	TESTED BY:	Kevin Patton

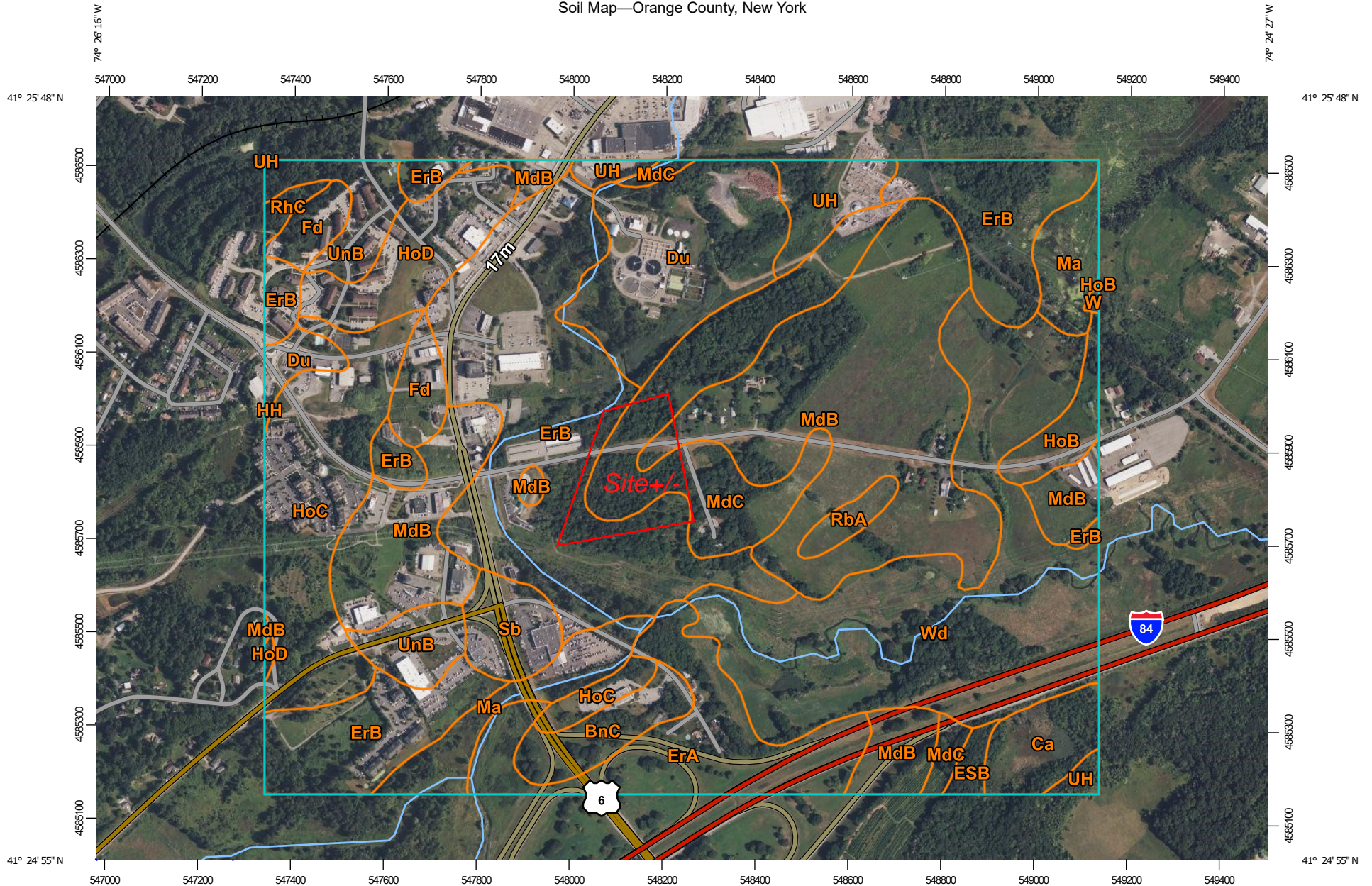
**DENSITY AND MOISTURE CONTENT OF SOIL**

Sample	Depth, ft	Moist Density, pcf	Dry Density, pcf	Percent Moisture
B3-S5	11	140	123	13.8

Moisture content was determined per ASTM D2216 and is expressed as a percent of the dry mass of the soil.  
Density values were determined from the wet and dry masses of the specimen, with volume calculated from measured dimensions.

Reviewed by: *Kevin Patton*

Soil Map—Orange County, New York



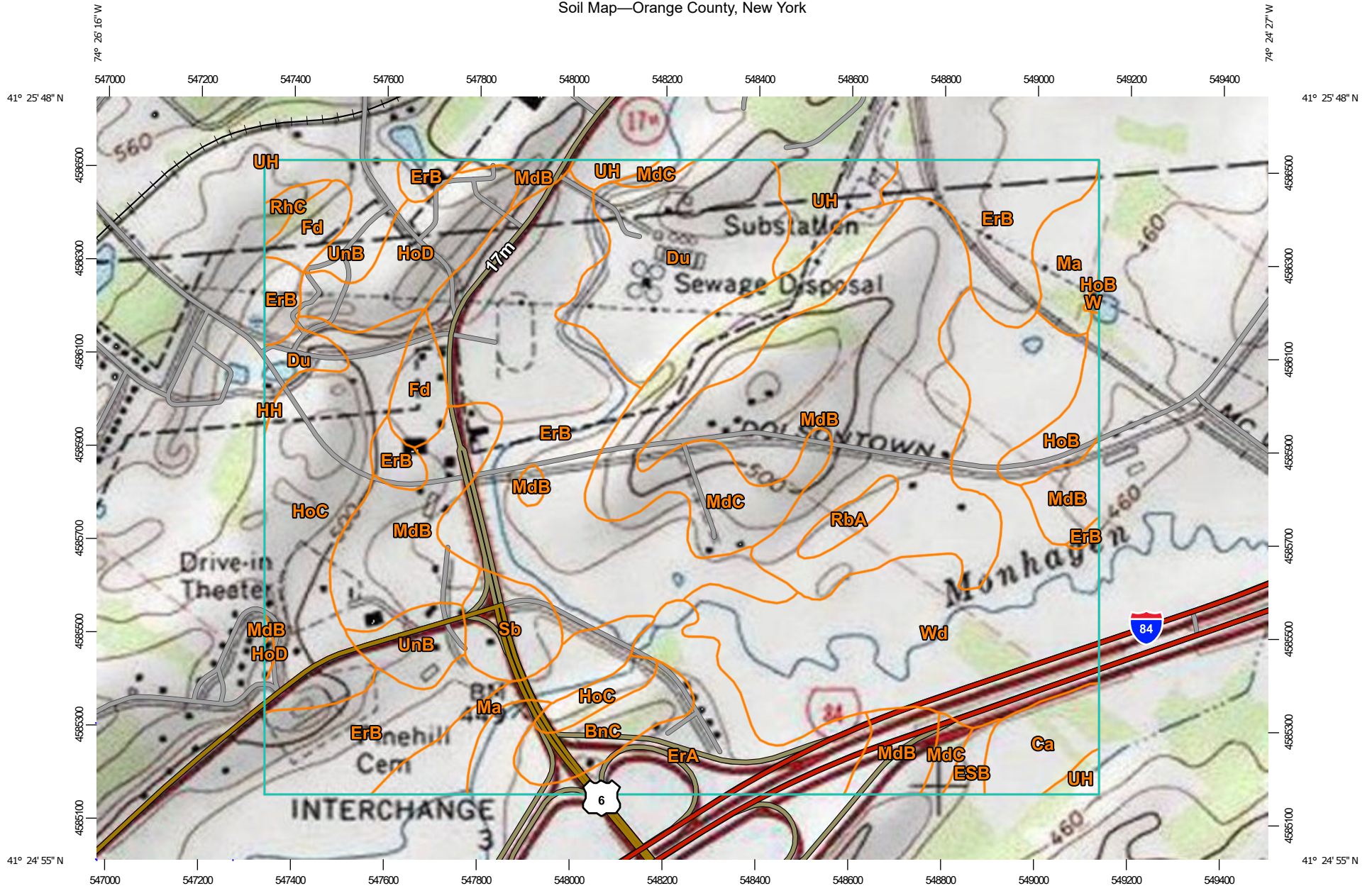
Map Scale: 1:11,500 if printed on A landscape (11" x 8.5") sheet.

0 150 300 600 900 Meters  
0 500 1000 2000 3000 Feet

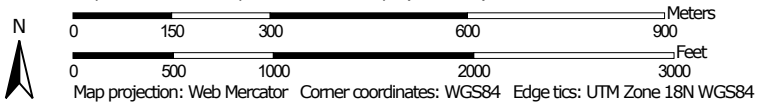
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84



Soil Map—Orange County, New York




Map Scale: 1:11,500 if printed on A landscape (11" x 8.5") sheet.



### MAP LEGEND

**Area of Interest (AOI)**

 Area of Interest (AOI)




















**Soils**


 Soil Map Unit Polygons

 Soil Map Unit Lines






 Soil Map Unit Points

**Special Point Features**

-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

-  Topographic Map

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Orange County, New York  
 Survey Area Data: Version 22, Aug 29, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BnC	Bath-Nassau channery silt loams, 8 to 15 percent slopes	10.1	1.7%
Ca	Canandaigua silt loam	10.3	1.7%
Du	Dumps	39.4	6.5%
ErA	Erie gravelly silt loam, 0 to 3 percent slopes	32.9	5.4%
ErB	Erie gravelly silt loam, 3 to 8 percent slopes	126.1	20.8%
ESB	Erie extremely stony soils, gently sloping	2.3	0.4%
Fd	Fredon loam	10.7	1.8%
HH	Histic Humaquepts, ponded	0.2	0.0%
HoB	Hoosic gravelly sandy loam, 3 to 8 percent slopes	6.7	1.1%
HoC	Hoosic gravelly sandy loam, 8 to 15 percent slopes	43.7	7.2%
HoD	Hoosic gravelly sandy loam, 15 to 25 percent slopes	18.6	3.1%
Ma	Madalin silt loam	21.0	3.5%
MdB	Mardin gravelly silt loam, 3 to 8 percent slopes	114.3	18.8%
MdC	Mardin gravelly silt loam, 8 to 15 percent slopes	39.5	6.5%
RbA	Rhinebeck silt loam, 0 to 3 percent slopes	3.5	0.6%
RhC	Riverhead sandy loam, 8 to 15 percent slopes	1.8	0.3%
Sb	Scarboro mucky fine sandy loam, 0 to 3 percent slopes	9.5	1.6%
UH	Udorthents, smoothed	12.5	2.1%
UnB	Unadilla silt loam, 0 to 8 percent slopes	17.2	2.8%
W	Water	0.3	0.0%
Wd	Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded	86.2	14.2%
<b>Totals for Area of Interest</b>		<b>606.8</b>	<b>100.0%</b>

## Engineering Properties

This table gives the engineering classifications and the range of engineering properties for the layers of each soil in the survey area.

*Hydrologic soil group* is a group of soils having similar runoff potential under similar storm and cover conditions. The criteria for determining Hydrologic soil group is found in the National Engineering Handbook, Chapter 7 issued May 2007(<http://directives.sc.egov.usda.gov/OpenNonWebContent.aspx?content=17757.wba>). Listing HSGs by soil map unit component and not by soil series is a new concept for the engineers. Past engineering references contained lists of HSGs by soil series. Soil series are continually being defined and redefined, and the list of soil series names changes so frequently as to make the task of maintaining a single national list virtually impossible. Therefore, the criteria is now used to calculate the HSG using the component soil properties and no such national series lists will be maintained. All such references are obsolete and their use should be discontinued. Soil properties that influence runoff potential are those that influence the minimum rate of infiltration for a bare soil after prolonged wetting and when not frozen. These properties are depth to a seasonal high water table, saturated hydraulic conductivity after prolonged wetting, and depth to a layer with a very slow water transmission rate. Changes in soil properties caused by land management or climate changes also cause the hydrologic soil group to change. The influence of ground cover is treated independently. There are four hydrologic soil groups, A, B, C, and D, and three dual groups, A/D, B/D, and C/D. In the dual groups, the first letter is for drained areas and the second letter is for undrained areas.

The four hydrologic soil groups are described in the following paragraphs:

*Group A.* Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

*Group B.* Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

*Group C.* Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

*Group D.* Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

*Depth* to the upper and lower boundaries of each layer is indicated.



*Texture* is given in the standard terms used by the U.S. Department of Agriculture. These terms are defined according to percentages of sand, silt, and clay in the fraction of the soil that is less than 2 millimeters in diameter. "Loam," for example, is soil that is 7 to 27 percent clay, 28 to 50 percent silt, and less than 52 percent sand. If the content of particles coarser than sand is 15 percent or more, an appropriate modifier is added, for example, "gravelly."

*Classification* of the soils is determined according to the Unified soil classification system (ASTM, 2005) and the system adopted by the American Association of State Highway and Transportation Officials (AASHTO, 2004).

The Unified system classifies soils according to properties that affect their use as construction material. Soils are classified according to particle-size distribution of the fraction less than 3 inches in diameter and according to plasticity index, liquid limit, and organic matter content. Sandy and gravelly soils are identified as GW, GP, GM, GC, SW, SP, SM, and SC; silty and clayey soils as ML, CL, OL, MH, CH, and OH; and highly organic soils as PT. Soils exhibiting engineering properties of two groups can have a dual classification, for example, CL-ML.

The AASHTO system classifies soils according to those properties that affect roadway construction and maintenance. In this system, the fraction of a mineral soil that is less than 3 inches in diameter is classified in one of seven groups from A-1 through A-7 on the basis of particle-size distribution, liquid limit, and plasticity index. Soils in group A-1 are coarse grained and low in content of fines (silt and clay). At the other extreme, soils in group A-7 are fine grained. Highly organic soils are classified in group A-8 on the basis of visual inspection.

If laboratory data are available, the A-1, A-2, and A-7 groups are further classified as A-1-a, A-1-b, A-2-4, A-2-5, A-2-6, A-2-7, A-7-5, or A-7-6. As an additional refinement, the suitability of a soil as subgrade material can be indicated by a group index number. Group index numbers range from 0 for the best subgrade material to 20 or higher for the poorest.

*Percentage of rock fragments* larger than 10 inches in diameter and 3 to 10 inches in diameter are indicated as a percentage of the total soil on a dry-weight basis. The percentages are estimates determined mainly by converting volume percentage in the field to weight percentage. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

*Percentage (of soil particles) passing designated sieves* is the percentage of the soil fraction less than 3 inches in diameter based on an oven-dry weight. The sieves, numbers 4, 10, 40, and 200 (USA Standard Series), have openings of 4.76, 2.00, 0.420, and 0.074 millimeters, respectively. Estimates are based on laboratory tests of soils sampled in the survey area and in nearby areas and on estimates made in the field. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

*Liquid limit and plasticity index* (Atterberg limits) indicate the plasticity characteristics of a soil. The estimates are based on test data from the survey area or from nearby areas and on field examination. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

References:

American Association of State Highway and Transportation Officials (AASHTO). 2004. Standard specifications for transportation materials and methods of sampling and testing. 24th edition.



American Society for Testing and Materials (ASTM). 2005. Standard classification of soils for engineering purposes. ASTM Standard D2487-00.

## Report—Engineering Properties

Absence of an entry indicates that the data were not estimated. The asterisk "\*" denotes the representative texture; other possible textures follow the dash. The criteria for determining the hydrologic soil group for individual soil components is found in the National Engineering Handbook, Chapter 7 issued May 2007(<http://directives.sc.egov.usda.gov/OpenNonWebContent.aspx?content=17757.wba>). Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

Engineering Properties—Orange County, New York														
Map unit symbol and soil name	Pct. of map unit	Hydrologic group	Depth	USDA texture	Classification		Pct Fragments		Percentage passing sieve number—				Liquid limit	Plasticity index
					Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200		
			<i>In</i>				<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>
ErB—Erie gravelly silt loam, 3 to 8 percent slopes														
Erie	80	D	0-9	Gravelly silt loam	GM, ML, SM	A-2, A-4	0- 0- 0	0- 2- 5	65-85-90	50-75-75	35-65-70	20-60-65	30-35-40	5-8 -10
			9-18	Channery fine sandy loam, channery silt loam, channery loam	CL-ML, CL, GC, SC	A-1, A-2, A-4	0- 0- 2	0- 2- 10	65-85-90	50-75-75	35-65-70	20-55-65	15-20-25	5-8 -10
			18-54	Channery silt loam, channery silty clay loam, very channery loam	CL, GC, SC	A-2, A-4, A-6	0- 2- 5	0- 2- 20	50-80-85	35-70-70	25-65-70	20-55-65	25-30-35	10-13-15
			54-70	Channery silt loam, channery silty clay loam, very channery loam	CL, GC, SC	A-2, A-6	0- 2- 5	0- 2- 25	50-80-85	35-70-70	25-65-70	20-55-65	25-30-35	10-13-15

**KEVIN L. PATTON, P.E.**  
**36 PATTON ROAD**  
**NEWBURGH, N.Y. 12550**  
845 275-7732 PATTONGEOTECH.COM

CLIENT:	RDM Group	PROJECT:	Dewpoint Dolsontown
	1 International Drive, Suite 410		Town of Wawayanda, N.Y.
	Mahwah, NJ 07430		
		PROJ. No.:	21416
		DATE:	March 18, 2022

Summary of Completed Stormwater Infiltration Tests

The following tests have been completed so far. There are three tests remaining, to be installed by the drill rig at depths of six and nine feet. The approximate test locations are shown on the attached plan dated 1-4-22; most of the actual test locations were shifted slightly to avoid wet areas, stone walls, trees or other interfering conditions. Groundwater was shallow, with the stabilized water level at less than ten inches below grade in four of the holes, at seventeen to 24 inches in five holes, and at 53 inches in one, on the south side of the site. The perc test results were less than 0.5 inches per hour in four of the holes, about one inch per hour in two of them, and relatively fast (3.5 to 19.4 inches per hour) in the remaining four. The variability of the perc rates is due to the soil texture; in some locations the perc tests are in dense clayey soil, in others they are in looser or silty soil. This layering changes unpredictably, both laterally and vertically; the soils may be very different at two locations that appear to be very similar on the surface, such as at tests P1 and P2.

Stormwater Infiltration Tests - North Parcel				
Test Location	P6	P7	P8	P9
Test Depth, inches	24"	24"	24"	24"
Perc Rate, in/hr	18.1	0.1	0.9	3.5
GW Level, MW*	8"	28.75"	23"	4"

Stormwater Infiltration Tests - South Parcel						
Test Location	P1	P2	P3	P4	U1	U2
Test Depth, inches	24"	24"	24"	24"	36"	36"
Perc Rate, in/hr	0.1	7.6	0.3	19.4	1.3	0.3
GW Level, MW*	6.25"	24"	53"	27.5"	17"	8.25"

\*Groundwater depth in adjacent monitoring well, inches below grade.  
Measured approximately two weeks after well installation.

Additional information will be provided as it becomes available.

Kevin L. Patton, P.E.



Engineering Properties--Orange County, New York														
Map unit symbol and soil name	Pct. of map unit	Hydrologic group	Depth	USDA texture	Classification		Pct Fragments		Percentage passing sieve number--				Liquid limit	Plasticity index
					Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200		
			<i>In</i>				<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>	<i>L-R-H</i>
MdC--Mardin gravelly silt loam, 8 to 15 percent slopes														
Mardin	85	D	0-8	Channery silt loam, silt loam, gravelly silt loam, channery loam	GC-GM, MH, ML	A-2-4, A-4, A-7-5	0- 0- 3	0- 4- 19	43-70-90	41-68-90	33-62-89	28-54-82	27-35-56	6-9 -16
			8-15	Channery silt loam, gravelly loam, gravelly silt loam, channery loam, silt loam, flaggy silt loam	GC-GM, CL	A-2-4, A-4, A-6	0- 0- 3	0- 4- 18	44-71-91	41-69-90	34-61-88	28-54-81	22-27-38	6-9 -15
			15-20	Gravelly silt loam, loam, gravelly loam, channery silt loam, channery loam, silt loam	CL-ML, CL, GM	A-2-4, A-4, A-6	0- 0- 3	0- 4- 18	46-72-91	43-71-91	34-63-88	26-51-77	17-23-32	2-7 -12
			20-72	Very flaggy loam, very channery loam, channery silt loam, gravelly loam, very channery silt loam, channery loam, gravelly silt loam, very flaggy silt loam	CL, GM	A-1-b, A-6	0- 3- 17	3- 6- 40	33-74-82	30-73-81	23-63-80	18-55-73	16-28-35	2-12-17

## Data Source Information

Soil Survey Area: Orange County, New York

Survey Area Data: Version 22, Aug 29, 2021



# Appendix 18 | Erosion and Sediment Control Plan and Details



## Engineering & Design

Colliers Engineering & Design is a trusted provider of multi-discipline engineering, design and consulting services providing customized solutions for public and private clients through a network of offices nationwide.

For a full listing of our office locations, please visit [colliersengineering.com](http://colliersengineering.com).

1 877 627 3772



*Civil/Site • Traffic/Transportation • Governmental • Survey/Geospatial  
Infrastructure • Geotechnical/Environmental • Telecommunications • Utilities/Energy*

## Section 4



**PHASE 1A LITERATURE SEARCH AND SENSITIVITY ASSESSMENT  
PHASE 1B ARCHAEOLOGICAL FIELD RECONNAISSANCE SURVEY**

**DEWPOINT SOUTH: WAREHOUSE CONSTRUCTION  
PROJECT**

1030 DOLSONTOWN ROAD,  
WAWAYANDA, ORANGE COUNTY, NEW YORK

PREPARED FOR:

RDM GROUP  
262 GREENWICH AVENUE, SUITE A  
MAHWAH, NJ, 07430



HUDSON VALLEY  
CULTURAL RESOURCE CONSULTANTS, LTD.  
PO BOX 264, SALT POINT, NY 12578

NOVEMBER 2021



## MANAGEMENT SUMMARY

SHPO Project Review Number (if available): **21PR03137**

Involved State and Federal Agencies: **NYS DEC, SEQRA**

Phase of Survey: **Phase 1A Literature Search & Sensitivity Assessment & Phase 1B Archaeological Field Reconnaissance Survey**

Location Information:

Location: **1030 Dolsontown Road**

Minor Civil Division: **Town of Wawayanda**

County: **Orange County**

Survey Area (English & Metric)

Length: **1140'/347.5 m**

Width: **575'/175.3 m**

Number of Acres: **±11.6 acres (4.69 hectares)**

Number of Acres Surveyed: **±7.03 (2.84 h)**

USGS 7.5 Minute Quadrangle Map: **Middletown, NY 2019**

Archaeological Survey Overview

Number & Interval of Shovel Tests: **82 @ 50' Intervals**

Results of Archaeological Survey

Number & name of precontact sites identified: **No sites identified**

Number & name of historic sites identified: **0**

Number & name of sites recommended for Phase II/Avoidance: **N/A**

Results of Architectural Survey

Number of buildings/structures/cemeteries within Project APE: **0**

Number of buildings/structures/cemeteries adjacent to Project APE: **0**

Number of previously determined NR listed or eligible buildings/structures/cemeteries/districts: **0**

Number of identified eligible buildings/structures/cemeteries/districts: **0**

Report Author (s): **Beth Selig, MA, RPA,**

Date of Report: **November 16, 2021**

# TABLE OF CONTENTS

LIST OF FIGURES

LIST OF TABLES

LIST OF PHOTOGRAPHS

I. PHASE 1A LITERATURE SEARCH AND SENSITIVITY ASSESSMENT .....	1
A. DEWPOINT SOUTH: WAREHOUSE PROJECT DESCRIPTION.....	1
B. ENVIRONMENTAL CONDITIONS .....	4
• ECOLOGY .....	4
• GEOLOGY.....	4
• DRAINAGE.....	4
• SOILS .....	4
C. RECORDED ARCHAEOLOGICAL SITES AND SURVEYS .....	9
• PREVIOUSLY RECORDED ARCHAEOLOGICAL SITES.....	9
• PREVIOUSLY COMPLETED ARCHAEOLOGICAL SURVEYS .....	10
D. NATIVE AMERICAN CONTEXT .....	10
E. HISTORIC CONTEXT .....	11
• CARTOGRAPHIC RESEARCH .....	11
• AERIAL REVIEW.....	17
F. NATIONAL REGISTER ELIGIBLE/LISTED SITES .....	20
G. ASSESSMENT OF SENSITIVITY FOR CULTURAL RESOURCES .....	20
• PRECONTACT SENSITIVITY .....	20
• HISTORIC SENSITIVITY .....	20
H. SUMMARY AND RECOMMENDATIONS.....	20
II. PHASE 1B ARCHAEOLOGICAL FIELD RECONNAISSANCE SURVEY .....	21
I. ARCHAEOLOGICAL SURVEY METHODOLOGY .....	21
J. ARCHAEOLOGICAL SURVEY RESULTS .....	21
K. CONCLUSIONS AND RECOMMENDATIONS.....	24
L. BIBLIOGRAPHY .....	26

APPENDIX A: SHOVEL TEST RECORDS

## LIST OF FIGURES

- Figure 1: 2019 USGS Topographical Map. Middletown, NY Quadrangle. 7.5 Minute Series. (Source: USGS.gov.) Scale: 1" =1400'.
- Figure 2: 2019 Aerial image showing the location of the Project APE. (Source: USGS.gov.) Scale: 1" =605'.
- Figure 3: Aerial Image showing soil units within the Project Parcel. (Source: Natural Resources Conservation Service.) Scale: 1" =290'.
- Figure 4: 1851 Sidney, J. C. *Map of Orange County, New York*. (Source: Library of Congress) Scale: 1" =2800'.
- Figure 5: 1875 F.W. Beers *Atlas of the County of Orange*. (Source: Historic Map Works) Scale: 1" =1495'.
- Figure 6: 1903 J. Lathrop *Atlas of Orange County*. (Source: Hudson River Valley Heritage) Scale: 1" =1020'.
- Figure 7: 1908 Goshen NY USGS Topographical Quadrangle. (Source: USGS.gov) Scale: 1" =1495'.
- Figure 8: 1969 USGS Topographical Map. Middletown NY Quadrangle. 7.5 Minute Series. (Source: USGS.gov) Scale: 1" =1600'.
- Figure 9: 1968 aerial image of the Project Area. (Source: Earth Explorer). Scale: 1" =660'.
- Figure 10: Dewpoint South: Warehouse Construction Project. Phase 1B Archaeological Field Reconnaissance Survey. Scale 1"= 100'.

## LIST OF TABLES

- Table 1: Soil Unit Descriptions (Natural Resources Conservation Service)
- Table 2: Previously Recorded Archaeological Sites within a one mile radius of the Project APE.

## LIST OF PHOTOGRAPHS

- Photo 1: The Project Parcel is bordered to the north by Dolsontown Road. View to the east.
- Photo 2: The Project Parcel is lightly wooded with a moderate understory. View to the southeast.
- Photo 3: Piles of debris are located in the northern portion of the Project APE. View to the north.
- Photo 4: A dirt track leading to an overhead transmission line is located between two wetland areas. View to the south.
- Photo 5: Areas of saturated soil were noted in the central portion of the Project Parcel. View to the south.
- Photo 6: View to the west along Dolsontown Road and the Project APE's northern boundary.
- Photo 7: The level areas within the Project APE are lightly wooded. View to the east.
- Photo 8: The southern boundary is defined by a stone retaining wall. View to the south.
- Photo 9: View to the southwest along the southern boundary of the APE.
- Photo 10: In the southern portion of the property the soils were saturated and had surface water. View to the south.
- Photo 11: Steep slopes are located in the southeastern portion of the Project APE. View to the east.
- Photo 12: The landscape within the APE descends to the wetlands in the western portion. View to the southwest.
- Photo 13: Stone walls are located in the southern and central portion of the Project APE. View to the north.
- Photo 14: A small knoll is located in the eastern portion of the Project APE. View to the north.

## I. PHASE 1A LITERATURE SEARCH AND SENSITIVITY ASSESSMENT

### A. DEWPOINT SOUTH: WAREHOUSE PROJECT DESCRIPTION

In October of 2021 Hudson Valley Cultural Resource Consultants (HVCRC) was retained by RDM Group to complete a Phase 1A Literature Search and Sensitivity Assessment and Phase 1B Archaeological Field Reconnaissance Survey for the proposed Dewpoint South: Warehouse Project in the Town of Wawayanda, Orange County, New York.

The purpose of the Phase 1 Cultural Resources Survey is to determine whether previously identified cultural resources (historic and archeological sites) are located within the boundaries of the proposed project, and to evaluate the potential for previously unidentified cultural resources to be located within the boundaries of the Project Area of Potential Effect (APE). All work was completed in accordance with the *Standards for Cultural Resource Investigations and the Curation of Archeological Collections published by the New York Archeological Council (NYAC)* and recommended for use by New York State Office of Parks, Recreation and Historic Preservation (OPRHP). The report has been prepared according to New York State OPRHP's *Phase 1 Archaeological Report Format Requirements*, established in 2005.

The background research as well as the cultural and environmental overviews were completed by Beth Selig, MA, RPA, President and Principal Investigator with HVCRC. A project site visit was conducted by Franco Zani Jr., on October 27, 2021 observe and photograph existing conditions within the Project APE. The information gathered during the walkover reconnaissance is included in the relevant sections of this report.

The proposed Dewpoint South Warehouse Project (hereafter "the Project APE") consists of constructing a 125,000 sq.ft., warehouse within the eastern portion of a  $\pm 11.58$  (4.686 h) parcel. The proposed structure will be bordered to the west by parking areas, and to the south and southwest by storm water management basins. Loading docks are proposed on the southern side of the structure. Access to the warehouse will be from Dolsontown Road. The topography of the parcel will be graded and leveled.

The Project APE is located on the northern side of Dolsontown Road, in the Town of Wawayanda. The Project Parcel includes a total of  $\pm 11.58$  acres (4.686 h). Wetlands are located in the western portion of the parcel, bisected by a dirt road that provides vehicular access to the transmission line on the southern boundary of the parcel. The landscape rises from the wetlands to the northeastern portion of the parcel. The northern boundary is Dolsontown Road, and the eastern boundary is Caskey Lane. The property is lightly wooded with a moderate amount of understory.

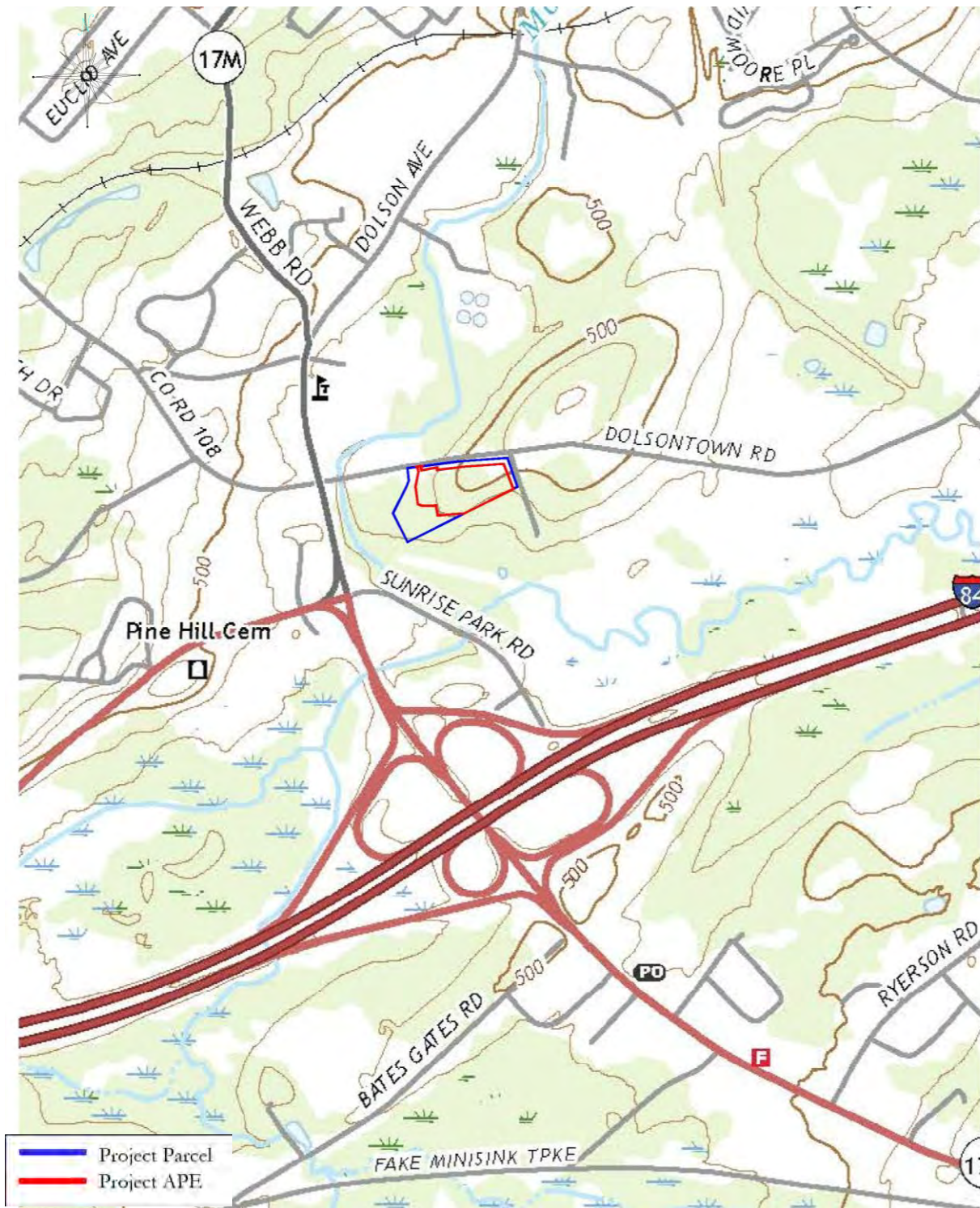


Figure 1: 2019 USGS Topographical Map. Middletown, NY Quadrangle. 7.5 Minute Series. (Source: USGS.gov.) Scale: 1" = 1400'.





Figure 2: 2019 Aerial image showing the location of the Project APE. (Source: USGS.gov.) Scale: 1" =605'.

## B. ENVIRONMENTAL CONDITIONS

The Project Parcel is primarily wooded areas, with a moderate understory. The wetland areas are overgrown. The highest elevation within the Project Parcel is in the northeastern corner, with a height of 540' (164.6 m) Above Mean Sea Level (AMSL). The elevation descends to the north and west with a height of 480' (146.3 m) in the southwestern corner of the APE and 474' (144.5 m) in the northwestern corner.

### ECOLOGY

The Project Parcel lies within the Eastern Broadleaf Forest. This mountainous region is in the transition zone between the boreal spruce-fir forest to the north and the deciduous forest to the south. Growth form and species are very similar to those found to the north, but red spruce tends to replace white spruce (Bailey 1995).

### GEOLOGY

The Project Parcel is situated within the Ridge and Valley physiographic province, which extends from Lake Champlain to Alabama. The portion of the Ridge and Valley Province in which the Project APE is located is specifically identified as the Taconic Allochthon, bordered to the east by the Manhattan Prong and to the west by the Great Valley province (Schubert 1968).

The Hudson Highlands area is a northeast-southwest trending band of igneous and metamorphic rock, which extends from New England through New York, crossing the Hudson River in the vicinity of Cold Spring and West Point. Because of their structural origin and their durability, the Hudson Highlands reach a higher elevation than the physiographic provinces that border them, such as the Hudson-Mohawk Lowlands to the north and the Piedmont Triassic Lowlands to the south. The Hudson Highlands are almost entirely blanketed by a thin layer of glacial till, with frequent bedrock outcrops. Outwash sand and gravel occupy some of the river and stream valleys that border and run through the Highlands (Fisher et al 1970).

In the Rondout and Wallkill valleys, soil deposits consist of lacustrine silt and clay soils with related water-sorted deposits. The Orange County muckland represents the last trace of a pro-glacial lake. The northern portion of Orange County is covered with mostly silt and clay soils of lacustrine, estuarine or marine origin. Some granular materials occur in association with the silts and clays. As the adjoining uplands are approached, glacial till becomes the dominant soil material.

### DRAINAGE

The Project APE is bordered to the west by Monhagen Brook, which flows southeast to the Wallkill River. Native American sites have been recorded by Arthur Parker, former New York State Archaeologist, along the banks of the waterway in Orange and Sullivan Counties.

### SOILS

Soil surveys provide a general characterization of the types and depths of soils that are found in an area. The characteristics of the soils within the Project APE have an important impact on the potential for the presence of cultural material, since the types of soils present affect the ability of an area to support human populations. The Soil Survey's mapped boundaries are considered approximate, as they generally correspond poorly to the actual boundaries of landforms and soils types within an area. The Natural Resources Conservation Service indicates that the soils within the Project APE are well drained and poorly drained gravelly and channery silt loams (Table 1).





Figure 3: Aerial Image showing soil units within the Project Parcel. (Source: Natural Resources Conservation Service.) Scale: 1" =290'.

**Table 1: Soil Unit Descriptions (Natural Resources Conservation Service)**

Map Unit Symbol	Map Unit Name	Soil Horizons & Texture	Slope	Drainage	Landform
ErB	Erie gravelly silt loam	H1 - 0 to 9 inches: gravelly silt loam H2 - 9 to 18 inches: channery silt loam H3 - 18 to 54 inches: channery silt loam H4 - 54 to 70 inches: channery silt loam	3 to 8 %	Somewhat poorly drained	Till plains, drumlinoid ridges, hills
MdB	Mardin gravelly silt loam	Ap - 0 to 8 inches: gravelly silt loam Bw - 8 to 15 inches: gravelly silt loam E - 15 to 20 inches: gravelly silt loam Bx - 20 to 72 inches: gravelly silt loam	3 to 8%	Moderately Well Drained	Hills, mountains
MdC	Mardin gravelly silt loam	Ap - 0 to 8 inches: gravelly silt loam Bw - 8 to 15 inches: gravelly silt loam E - 15 to 20 inches: gravelly silt loam Bx - 20 to 72 inches: gravelly silt loam	8 to 15%	Moderately Well Drained	Hills, mountains





Photo 1: The Project Parcel is bordered to the north by Dolsontown Road. View to the east.



Photo 2: The Project Parcel is lightly wooded with a moderate understory. View to the southeast.





Photo 3: Piles of debris are located in the northern portion of the Project APE. View to the north.



Photo 4: A dirt track leading to an overhead transmission line is located between two wetland areas. View to the south.





Photo 5: Areas of saturated soil were noted in the central portion of the Project Parcel. View to the south.



Photo 6: View to the west along Dolsontown Road and the Project APE's northern boundary.

### C. RECORDED ARCHAEOLOGICAL SITES AND SURVEYS

On October 27, 2021 HVCRC reviewed the combined site files of the New York State Office of Parks, Recreation, and Historic Preservation (OPRHP) and the New York State Museum (NYSM) for information regarding previously recorded archeological sites within one mile (1.6 km) of the Project APE. HVCRC also consulted regional Native American sources (e.g. Beauchamp 1900; Parker 1920; Ritchie 1980; Ritchie and Funk 1973) for descriptions of regional archeological sites.

#### PREVIOUSLY RECORDED ARCHAEOLOGICAL SITES

Twenty archaeological sites have been previously identified within a one mile radius of the Project Parcel. The sites are summarized in the Table below and will not be impacted by the proposed undertaking.

<b>Table 2: Previously Recorded Archaeological Sites within a one mile radius of the Project Parcel</b>				
<b>Site Number</b>	<b>Site Name</b>	<b>Distance from Project</b>	<b>Time Period</b>	<b>Materials Recovered</b>
7119.000008	ORWW-01F	2640' / 0.8 k	Unknown	No information
7119.000015	ORWW-08F	3960' / 1.2 k	Unknown	destroyed
7119.000016	ORWW-09F	1320' / 0.4 k	Precontact	Non-diagnostic surface finds
7119.000017	ORWW-10F	2640' / 0.8 k	Unknown	No information
7119.000018	ORWW-11F	3960' / 1.2 k	Historic	Cemetery
7119.000021	ORWW-14F	2640' / 0.8 k	Unknown	No information
7119.000082	Late Archaic Site (23-129-11)	2640' / 0.8k	Precontact	Late Archaic
7119.000083	Simon Site (23-131-13)	2640' / 0.8 k	Precontact	Transitional, Late Archaic, Woodland
7119.000186	Horizons Site 1	2640' / 0.8 k	Precontact	Late archaic site
7119.000187	Horizons Site 2	3960' / 1.2 k	Precontact	Late Archaic site
7119.000197	Site CPV-1	5280' / 1.6 k	Precontact	Small lithic scatter
7119.000198	Site CPV-2	1320' / 0.4k	Precontact	Small lithic scatter
7119.000199	Site CPV-3	1320' / 0.4k	Precontact	Small lithic scatter
7119.0002	Site CPV-4	2640' / 0.8k	Precontact	Two flakes
7119.000201	Isolated Find CPV-1	1320' / 0.4k	Precontact	Small battered pebble
7119.000202	Isolated Find CPV-2	2640' / 0.8k	Precontact	Chert with cortex
7119.000204	Isolated Find IF-CPV-3	1320' / 0.4k	Precontact	Small biface fragment
7119.000205	Isolated Find IF-CPV-4	2640' / 0.8 k	Precontact	Stray find in plowzone
NYSM 6919		2640' / 0.8 k	Historic	Cemetery
NYSM 6170	Bates	2640' / 0.8 k	Precontact	No information



## PREVIOUSLY COMPLETED ARCHAEOLOGICAL SURVEYS

As part of the research for this report, surveys completed for projects in the general area were consulted. More than eighteen surveys have been completed within a one mile radius of the Project APE. These surveys were completed for both municipal undertakings as well as residential developments and identified both precontact and historic archaeological sites within the vicinity of the Project Parcel.

### D. NATIVE AMERICAN CONTEXT

During the Paleoindian period, mobile bands of hunter-gatherers occupied what is now New York State. These bands exploited the resources of the landscape by hunting game and gathering plants. Paleoindian sites have been in the upland regions a short distance from the Hudson River (Ritchie and Funk 1976). Frequently these sites are associated with sources of stone, as is the case with a site in Greene County where a quarry-workshop complex has been excavated. More frequently, the sites appear to have been temporary campsites located where it would be possible to watch for game as it moved across the landscape (Ritchie 1980). Ritchie (1980) identified more than ten locations within Orange County where fluted points, the hallmark projectile point of this period, have been recovered. The majority of the Paleoindian period sites identified in the Hudson River Valley appear to have been temporary campsites.

With the lowering of the water table during the Archaic period, subsistence methods and technologies changed in response to climatic warming. This was accompanied by an increase in vegetation density and diversity, changing faunal migrations and a change in sea levels (Sirkin 1977). The Archaic Period was likely a time of incipient sedentism among the inhabitants of the area. Changes in settlement and subsistence patterns that occurred during the Late Archaic period reflect an increased exploitation of coastal and riverine resources (Snow 1980). Ground stone food processing tools are more common, reflecting an increase in processed plant resources in the diet. Projectile points commonly found at Late Archaic sites include narrow stemmed, broad stemmed and side notched types (Snow 1980). The Laurentian Tradition of the Late Archaic is the most represented throughout New York State, and is subdivided into a series of phases: Vergennes, Vosburg, Sylvan Lake, River and Snook Kill. Ground stone tools appear, and steatite bowls are associated with the later part of this time period (Pretola and Freedman 2007).

The Woodland period is distinguished from the Archaic in part, by the use of ceramics. Horticulture, although practiced in other parts of North America at an earlier date, does not appear in the Hudson River Valley until c. 1000 AD (Funk 1976). The soil and moisture requirements for the cultivation of maize, beans, and squash created a marked change in the pattern of land use and the selection of locations for villages (Hart and Brumbach 2005). It was no longer necessary for the entire group to move from place to place following a seasonal round of migration fueled by fluctuating sources of food. Cord marked ceramics became common during the Middle Woodland period, and incised vessels, many with a collar area, are typical of Late Woodland cultures (Lavin et al 1993).

Initial contact between Europeans and Native Americans was made when early explorers entered the area to engage in trade. The introduction of European material goods, the demands of trading relationships, rapid colonial expansion, and the spread of diseases brought by the Europeans had profound effects on the settlement and subsistence adaptations of the native populations. Tribal and clan affiliations were affected, and much of the native population was depopulated or displaced. Some estimates suggest that between sixty (60) and ninety (90) percent of the native population was lost to European diseases in the seventeenth century in southern New England and New York (Snow 1980).

## E. HISTORIC CONTEXT

At the time of its formation, Orange County included nearly all of the southern part of New York that bordered the Hudson River. What is now known as Orange County, once included the present County of Rockland, and included the present town of Deerpark, then a part of the town of Mamakating (Stickney 1867). In 1798 the county lines of New York State were revised, and Orange County annexed the towns of Newburgh, New Windsor, Wallkill, Montgomery, and Deerpark. Subsistence farming supported the early communities. By the nineteenth century, corn, wheat, oats, rye, and buckwheat were important crops that were sent via turnpikes and canals to other markets. Fruits were also extensively grown in the Hudson River region (Headley 1908). The fine grasslands of Orange County also supported an early industry focused on horse breeding. Dairy farming was a major agricultural industry, and many areas in Orange County produced cheese and butter.

The Town is included within the Wawayanda Patent, granted in 1703 to John Bridges and eleven associates, by the governor of New York and New Jersey. The patent included 150,000 acres. Part of this large land grant included the Project APE, located southeast of Middletown. The Town of Wawayanda was formed in 1849 and reportedly after a Native American word meaning “way over yonder” (Stickney 1867). It was formed from Minisink, Mount Hope and Deerpark; and in 1855 had a population of 1,218 (Stickney 1867).

In the nineteenth century, the development of the turnpike system throughout Orange County brought additional settlers to the region (Stickney 1867). The turnpikes and other transportation routes were built with the goal of efficient distribution of specific products. As an example, the Mount Hope and Lumberland Turnpike, built in 1812, was constructed to benefit the Goshen men who had invested in Sullivan County woodlands. The turnpike allowed them to transport their lumberjacks and supplies to the woodlands where the forest was harvested, and the lumber was then rafted down the Delaware River to the market in Philadelphia. The lands along the Goshen Turnpike were agricultural through the early part of the twentieth century (Ruttenber and Clark 1881).

The first railroad through the region was owned and operated by the Middletown, Unionville and Watergap Railroad Company in 1868. The presence of a rail station in nearby Unionville allowed local farmers to ship their goods more efficiently to broader markets. Soon, creameries were established at each station in the dairy region. By the 1880's the county contained seventy milk shipping stations, three condenseries, two cheese factories and one butter and cheese factory (Headley 1908). The expanding railroad facilitated growth in the region, both commercially and residentially, however the agricultural economy of the county continued into the twentieth century. By the mid- twentieth century New York State had begun construction on its interstate road system with the establishment of NYS Route 17 and Route 211. Route 17k follows the route of the Newburgh-Cochecton Turnpike (Ruttenber and Clark 1881). Interstate 84 was constructed in the 1960s, bisecting the town of Montgomery, and facilitating continued growth of the commercial industries of the region.

## CARTOGRAPHIC RESEARCH

HVCRC consulted historical documents and maps available at the Library of Congress, David Rumsey Cartography Associates and the New York Public Library. HVCRC examined historical maps of Orange County to identify possible structures, previous road alignments and other landscape features or alterations that could affect the likelihood that archeological and/or historic resources could be located within the Project APE. These maps are included in this report, with the boundaries of the Project APE superimposed. Nineteenth century maps frequently lack the accuracy of location and scale present in modern surveys. As a result of this common level of inaccuracy on the historic maps, the location of the Project APE is drafted relative to the roads, structures, and other features as they are drawn, and should be regarded as approximate.



Figure 4: 1851 Sidney, J. C. *Map of Orange County, New York*. (Source: Library of Congress) Scale: 1" = 2800'.

The 1851 Sidney Map shows the Project Parcel on the northern side of Dolsontown Road, east of Monhagen Brook. This map shows the route of the proposed Erie Railroad to the east. A building identified as the S. (school) House is shown north of the Project APE. A saw mill is shown outside the western APE boundary. To the south is the G. Sweesy house on the northern side of Monhagen Brook.





Figure 5: 1875 F.W. Beers *Atlas of the County of Orange*. (Source: Historic Map Works) Scale: 1" = 1495'.

The 1875 *Atlas of the County of Orange* shows that a number of structures are located along Dolsontown Road east of the Project Parcel. A sawmill is shown to the west of the Project APE, on the eastern side of Monhagen Brook. A grist mill is shown to the north, along Dolsontown Road. The C. Caskey residence is shown to the east. Caskey owns a 160 acre parcel.





Figure 6: 1903 J. Lathrop *Atlas of Orange County*. (Source: Hudson River Valley Heritage) Scale: 1" = 1020'.

The 1903 *Atlas of Orange County* shows that a number of structures are located along Dolsontown Road, to the east of the Project Parcel. There are no structures shown within the boundaries of the Project Parcel. To the east the Caskey residence is now owned by Herman Caskey, and to the southwest are two buildings owned by Johannes Bradley.



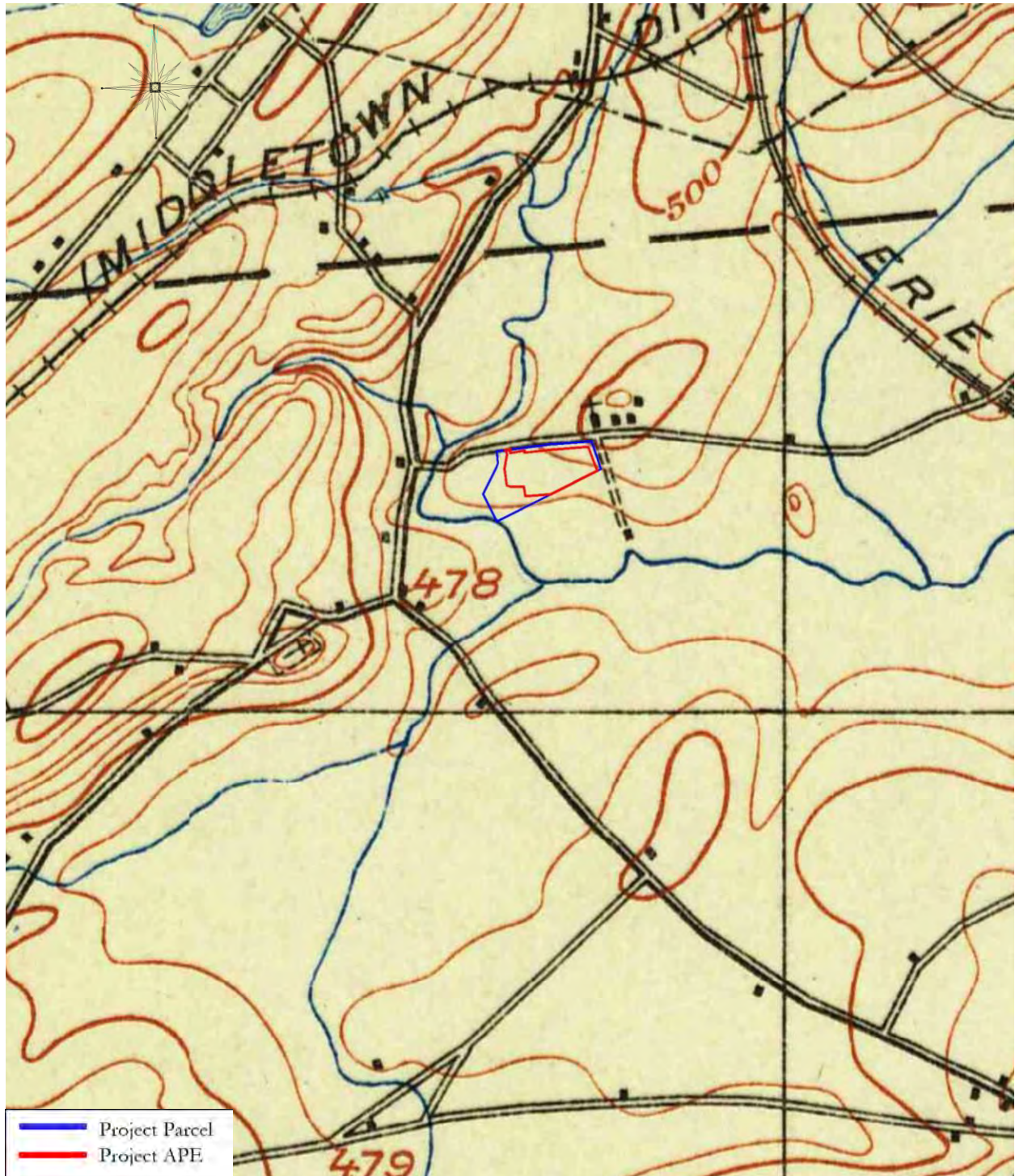


Figure 7: 1908 Goshen NY USGS Topographical Quadrangle. (Source: USGS.gov) Scale: 1" = 1495'.

The USGS topographical maps depict the locations of roads, structures and landscape features; however they do not indicate property landowners. This map indicates four structures are located to the northeast of the Project Parcel. No structures are shown within the boundaries of the Project APE.



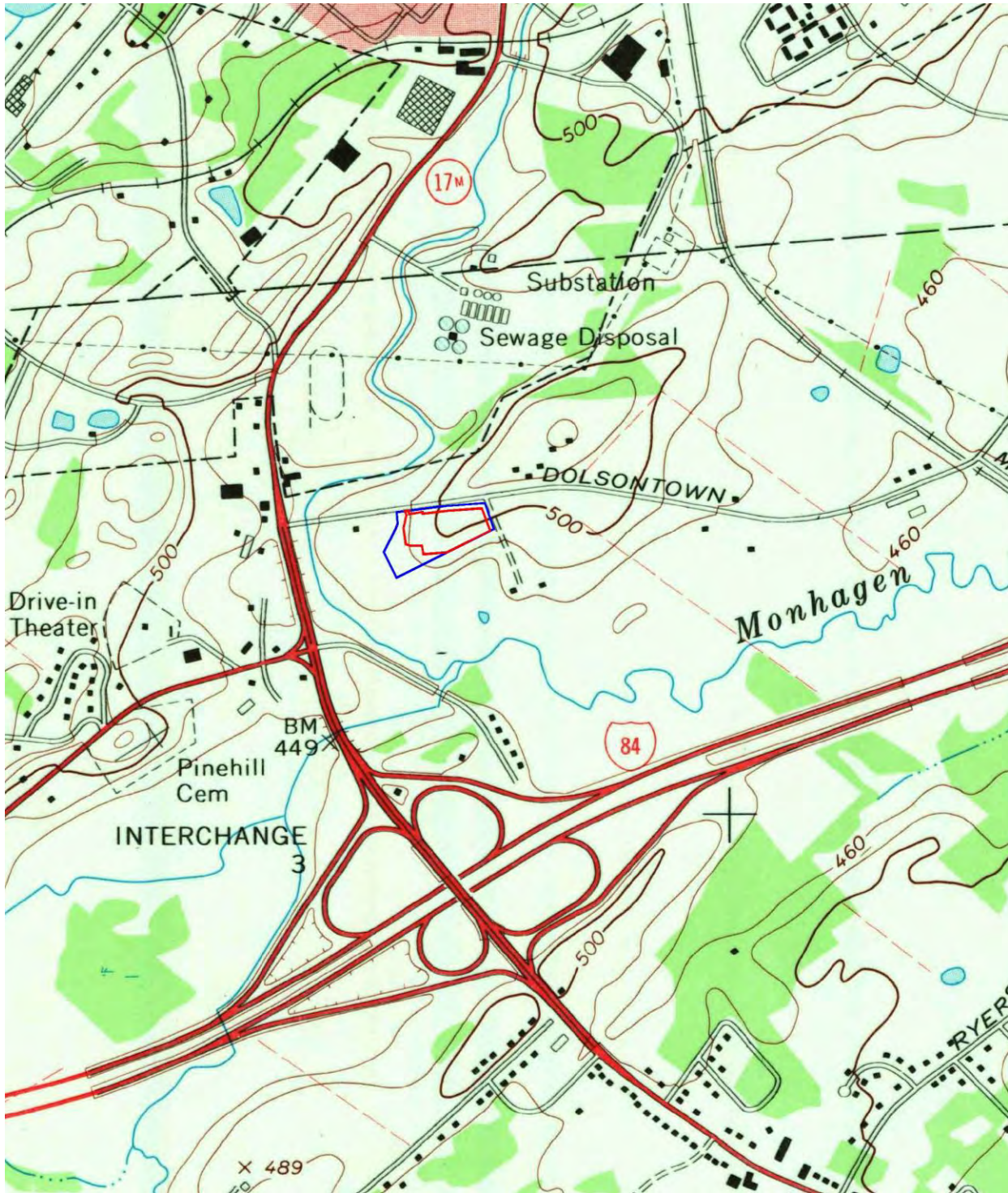


Figure 8: 1969 USGS Topographical Map. Middletown NY Quadrangle. 7.5 Minute Series. (Source: USGS.gov) Scale: 1" = 1600'.

The 1969 USGS topographical map shows that the Project Parcel has been cleared. The Monhagen Brook is shown to the west of the Project Parcel near Route 17M. No structures are shown within the boundaries of the Project APE, which consists of a small knoll with slopes descending south and west to the brook.



AERIAL REVIEW



Figure 9: 1968 aerial image of the Project Area. (Source: Earth Explorer). Scale: 1" = 660'.

The 1968 aerial image indicates that the Project APE is agricultural land. The fields are crossed by a tree line. Areas of scrub brush are visible in the southwestern corner of the parcel.





Photo 7: The level areas within the Project APE are lightly wooded. View to the east.



Photo 8: The southern boundary is defined by a stone retaining wall. View to the south.





Photo 9: View to the southwest along the southern boundary of the APE.



Photo 10: In the southern portion of the property the soils were saturated and had surface water. View to the south.



## E. NATIONAL REGISTER ELIGIBLE/LISTED SITES

The National Register Database and OPRHP files were reviewed to identify structures on or in the vicinity of the Project Parcel that have been listed on the National Register of Historic Places or identified as National Register Eligible. A residential structure located 1197 Dolsontown Road, located 0.45 miles (0.72 k) from the Project boundaries is considered eligible for listing on the National Register of Historic Places. This historic property will not be impacted by the proposed undertaking.

## G. ASSESSMENT OF POTENTIAL CULTURAL RESOURCES

### PRECONTACT PERIOD SENSITIVITY

Precontact period archaeological sensitivity of an area is based primarily on proximity to previously documented Precontact archeological sites, known Precontact period resources, and physiographic characteristics, such as topography and proximity to freshwater. The project's location, adjacent to Monhagen Brook, a tributary of the Wallkill River, and previously identified archaeological sites, along with the level terrain that exists within this Project APE, makes this landscape moderate to highly sensitive for precontact cultural resources.

### HISTORIC SENSITIVITY

Careful examination of the historic and topographical maps available indicate that the Project Parcel has been agricultural land for a significant portion of the nineteenth and early twentieth centuries. The topographical maps and aerial images indicate that there were no structures within or adjacent the boundaries of the parcel in the mid-nineteenth century. Therefore the historic sensitivity of the Project APE is considered to be moderate to low.

## H. SUMMARY AND RECOMMENDATIONS

The environmental conditions present within Dewpoint South: Warehouse Project parcel indicate that the Project APE is sensitive for precontact and historical cultural resources.

It is therefore recommended that a Phase 1B Archaeological Field Reconnaissance Survey be undertaken within the location of the proposed development, in the areas that have been assessed to have the potential to yield cultural resources.



## II. PHASE 1B ARCHAEOLOGICAL FIELD RECONNAISSANCE SURVEY

### I. ARCHAEOLOGICAL SURVEY METHODOLOGY

The results of the Phase 1A confirmed that the Project Parcel is located in an area of precontact period activity. In addition, the landscape closely conforms to an ecological model that indicates that the level, undisturbed portions of the Project APE are moderate to highly sensitive for precontact cultural materials. Phase 1B field investigations took place on November 3, 2021, under the supervision of Franco Zani Jr, and Beth Selig, MA, RPA.

Areas selected for subsurface testing were identified during an intensive walkover inspection which evaluated the landscape to determine areas of prior disturbance, slopes in excess of 12% grade, saturated or wet soils and document evidence of former land usage. Shovel tests were excavated at intervals of 50' (15m) along transects conforming to the land surface and the boundaries of the Project APE. The locations of the tests and disturbed areas were recorded on a scaled map that shows surveyed borders and has the locations of the various structures or features identified (Field Reconnaissance Map).

Shovel tests (STs) approximately 45 cm in diameter, were spaced 50 feet apart and excavated at least 10 cm into sterile subsoil, unless impeded by rocks or other obstructions. This subsurface testing strategy was applied in areas of undisturbed soils and that were well drained and did not contain surface water. All soils excavated from shovel tests were screened through 0.25-inch hardware cloth. Shovel test profiles were recorded on standard field forms which included stratigraphic depths, Munsell soil color, texture and inclusions, disturbances and artifacts (Appendix A). The presence of clearly modern materials, such as plastic fragments, modern bottle glass fragments, or twentieth-century architectural materials were noted on field forms, but HVCRC does not generally collect these materials for analysis or inclusion in the artifact assemblage. If any precontact period or potentially significant historic-period artifacts had been recovered from shovel tests, then these finds would have been bagged, labeled with standard project provenience information. Following completion of the archaeological fieldwork, all recovered materials would be washed, identified, inventoried and re-bagged in labeled clean 4-mil archival quality plastic bags. All artifacts recovered would then be identified and described based on material type and standard descriptive characteristics and included in an artifact inventory.

### J. ARCHAEOLOGICAL SURVEY RESULTS

The Project Parcel is located on the side of a small hill, with the slope descending southwest to large wetlands. The wetlands are bisected by a dirt road that provides access to the transmission line on the southern boundary of the Project Parcel. The southern boundary is defined by a rock wall that in parts, is cut into the slope creating a retaining wall feature. The western portion of the Project Parcel contains substantial wetlands that are surrounded by saturated soils. The Project Parcel is generally wooded with areas of heavy and thick understory. The landscape within the parcel descends from the northeastern corner to the southwestern.





Photo 11: Steep slopes are located in the southeastern portion of the Project APE. View to the east.



Photo 12: The landscape within the APE descends to the wetlands in the western portion. View to the southwest.





Photo 13: Stone walls are located in the southern and central portion of the Project APE. View to the north.



Photo 14: A small knoll is located in the eastern portion of the Project APE. View to the north.

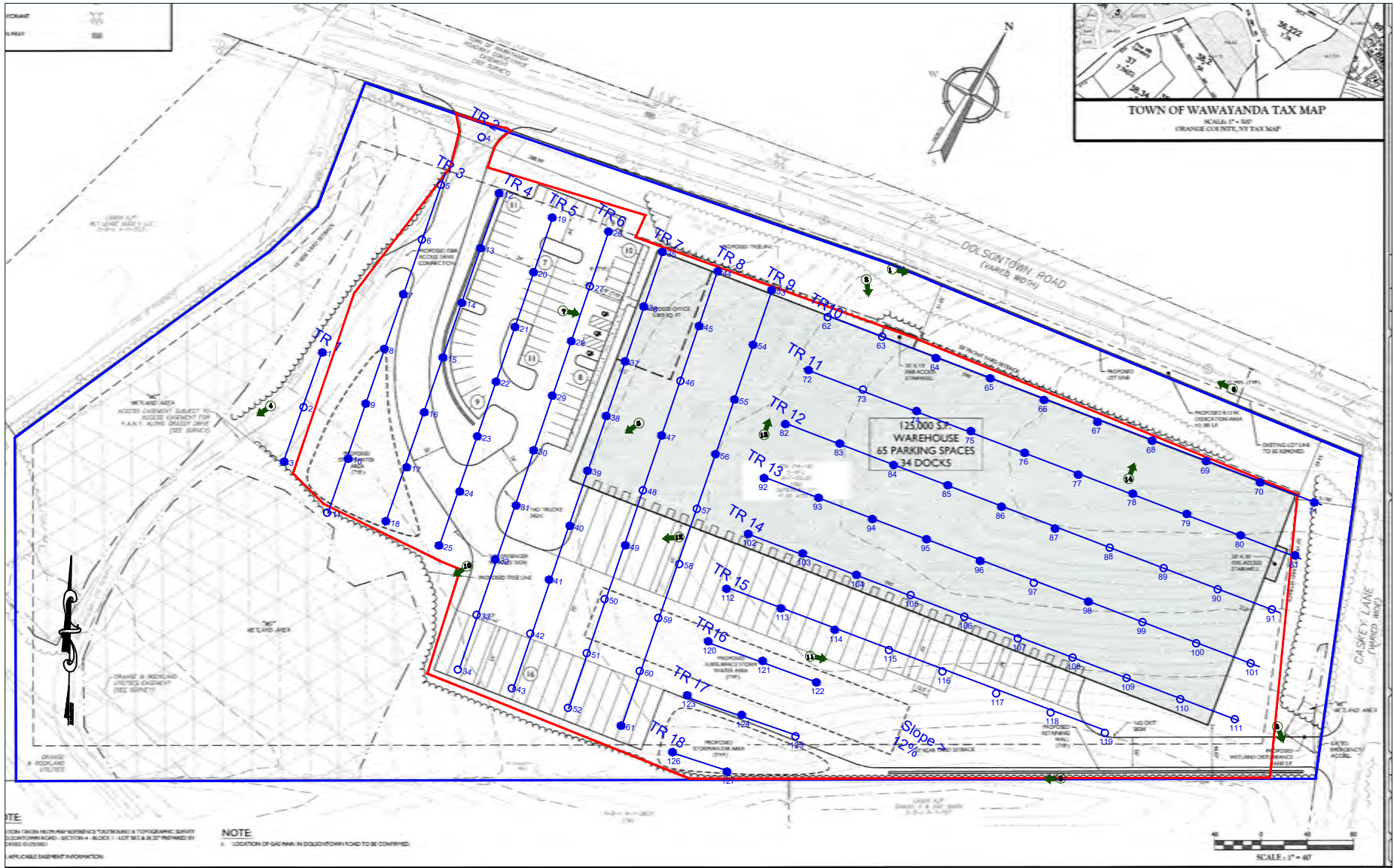


Testing began in the western portion of the Project APE with the transects beginning along Dolsontown Road and ending at the wetland boundary. The areas outside the flagged wetland boundaries contained wet soils. The eastern portion of the Project APE was tested by transects aligned west to east, beginning at the base of the slope and terminating at the eastern APE boundary. A total of one hundred and twenty-seven (127) shovel tests were planned within the Project APE. Due to steep slopes, piles of rock, tree falls and saturated soils forty-five (45) planned shovel tests were not completed.

The soils encountered consisted of a brown silty loam with cobbles overlying a yellowish brown silty clay with gravel and dark grayish brown silty loam with gravel overlying yellowish brown and gray silty clay. No cultural material was recovered from any of the completed shovel tests.

#### K. CONCLUSIONS AND RECOMMENDATIONS

In November 2021, Hudson Valley Cultural Resource Consultants completed a walkover and Phase 1B reconnaissance inspection of the Dewpoint South: Warehouse Project in the Town of Wawayanda, Orange County New York. Based on the results of the survey, no archaeological sites or historic structures are located within the Area of Potential Effect (APE). Therefore, the proposed undertaking will not affect any potentially significant cultural resources. In the opinion of HVCRC that no additional cultural resources investigations are warranted for the proposed Project.

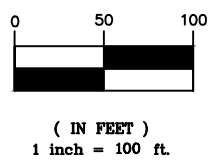


NOTE:  
 1. DATA TAKEN FROM MAP REFERENCE "OUTBOUND & TOPOGRAPHIC SURVEY  
 DOLSONTOWN ROAD - SECTION 4 - BLOCK 1 - LOT 90 & 91" (PREPARED BY  
 GARDNER & WHITNEY)  
 2. APPLICABLE EASEMENT INFORMATION

NOTE:  
 1. LOCATION OF GAS MAIN IN DOLSONTOWN ROAD TO BE CONFIRMED.

**LEGEND**

- ST Sterile Shovel Test Location
- ST Planned Shovel Test, Not Excavated
- ➔ 1 Photographic View
- APE Boundaries



**HUDSON VALLEY**  
 Cultural Resource Consultants, Ltd.  
 Figure 10: Dewpoint South: Warehouse Construction Project  
 Phase 1B Field Reconnaissance Map  
 Scale 1" = 125'

## L. BIBLIOGRAPHY

Bailey, Robert C.

1995 Description of the Ecoregions of the United States.  
<http://www.fs.fed.us/land/ecosysmgmt/index.html>. Accessed October 26, 2021.

Bachman, Charles and C. Corey.

1858 *Map of Orange County, New York from Actual Surveys*. Gillette, Philadelphia, Pennsylvania.

Beauchamps, William M.

1900 *Aboriginal Occupation of New York*. *New York State Museum*. Bulletin Number 32. Volume 7. The University of the State of New York: Albany, NY.

Becker, Marshall J.

1993 The Lenape and Other “Delawarean” Peoples at the time of European Contact: Populations Estimates derived from Archaeological Historical Sources. *Journal of the New York State Archaeological Association*. #105 spring.

Beers F. W.

1875 *Atlas of the County of Orange New York*. F. W. Beers, Ad Ellis, & G.G. Soule: New York.

Colden, Cadwallader, 1688-1776.

1918-1937 The letters and papers of Cadwallader Colden New York, Printed for the New York Historical Society, 1918-37. 9 v.: fronts. (v. 1-2; port., fold. map);

de Laubenfels, D.C.

1975 *Mapping the World's Vegetation: Regionalization of Formations and Flora*. Syracuse University Press.

Dunn, S.

1994 *The Mohican's and Their Land*. Purple Mountain Press. Fleischmann's NY.

Eager, Samuel W

1847 *An Outline History of Orange County*. S.T. Callahan, Newburgh.

Eisenstadt, Peter ed.

2005 *The Encyclopedia of New York State*. Syracuse University Press, Syracuse, NY.

Fisher, Donald W., Yngvar W. Isachsen, Lawrence V. Rickard

1970 *Geologic Map of New York, Lower Hudson Sheet*. New York State Museum and Science Service Map and Chart Series No. 15. New York State Museum, Albany, New York.

Funk, Robert E.

1976 *Recent Contributions to Hudson Valley Prehistory*. New York State Museum Memoir 22. Albany, NY.

Headley, Russel

1908 *The History of Orange County, New York*. Van Deusen and Elms, Middletown, NY

Hull, Richard

1996 *History of Warwick NY*. Royal Fireworks Press of Unionville NY

Küchler, August W.

1964 *Potential Natural Vegetation of the Conterminous United States*. American Geographical Society, New York.

Lathrop, J.M.

1903 *Map of Orange County, New York*. A. H. Mueller & Co.: Philadelphia, PA

- Natural Resources Conservation Service  
<https://websoilsurvey.nrcs.usda.gov>. Accessed October 26, 2021.
- New York State Archaeological Council (NYAC)  
 1994 *Standards for Cultural Resource Investigations and the Curation of Archaeological Collections in New York State*.  
 New York Archaeological Council.
- New York State Office of Parks Recreation and Historic Preservation CRIS  
[cris.parks.ny.gov](http://cris.parks.ny.gov) Accessed October 26, 2021.
- Parker, Arthur  
 1920 *Archaeological History of New York*. New York State Museum Bulletin. No. 237 and 238. The University  
 of the State of New York: Albany, NY.
- Ritchie, William A.  
 1973 *Aboriginal Settlement Patterns in the Northeast*. Memoir 20. New York State Museum and Science Service.  
 Albany, NY.  
 1969 *The Archaeology of New York State*. Natural History Press: Garden City, NY.
- Ruttenber, E. M. & L. H. Clark (Editors)  
 1881 *History of Orange County, New York with Illustrations and Biographical Sketches of Many of Its Pioneers and  
 Prominent Men*. Everts & Peck, Philadelphia, PA.
- Schubert, Christopher J.  
 1968 *The Geology of New York City and Environs*. The Natural History Press: Garden City, NY
- Sidney J. C.  
 1850 *Map of Orange County, New York*. Newell S. Brown: Newburgh.
- Sirkin, Les  
 1977 Late Pleistocene Vegetation and Environments in the Middle Atlantic Region. *Annals of the New  
 York Academy of Science*. February 1977. Vol. 288.
- Snow, Dean R.  
 1980 *The Archaeology of New England*. Academic Press: New York, NY.
- Spectra Inc.  
 2004 Draft Generic Environmental Impact Statement (Dgeis) New York State Statewide Wireless  
 Network (Swn) Geologic Resources Appendix C: Geologic, Structural and Topographic Features of  
 Physiographic Provinces.
- Stilgoe, John R.  
 1982 *Common Landscape of America, 1580-1845*. Yale University Press: New Haven, CT.
- Sulavik, Stephen B  
 2005 *Adirondack: of Indians and Mountains 1535-1838*. Purple Mountain Press. New York.
- United States Department of the Interior.  
 2000 National Register Bulletin. Guidelines for Evaluating and Registering Archeological Properties.  
 National Park Service. Washington, D. C.  
 1985 National Register Bulletin # 24: Technical Information on Comprehensive Planning, Survey of  
 Cultural Resources, and Registration in the National Register of Historic Places. Reprint. National  
 Park Service, Interagency Resources Division. Washington, D.C.

United States Geological Survey

- 2019 United State Geological Survey Topographical Map. Middletown, NY Quadrangle. 7.5 Minute Series.
- 1969 United State Geological Survey Topographical Map. Middletown, NY Quadrangle. 7.5 Minute Series.
- 1908 United State Geological Survey Topographical Map. Goshen, NY Quadrangle. 15 Minute Series.

Versaggi, Nina (Public Archaeological Facility (

- 2000 Stage 1B Cultural Resources Survey. Ball Mine Site. Town of Wawayanda, Orange County, New York.



## APPENDIX A: SHOVEL TEST RECORDS

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
<b>TR 1</b>	1	1	0-4	0-10	10YR 2/1	Black silt with dense gravel	NCM
		2	4-8	10-20	10YR 6/3	Pale brown clay loam with dense gravel	NCM
	2					Not excavated: asphalt/push pile	
	3	1	0-7	0-19	10YR 3/3	Dark brown silty loam with gravel	NCM
		2	7-12	19-30	10YR 5/4	Yellowish brown clay loam with dense gravel	NCM
<b>TR 2</b>	4					Not excavated: compact gravel drive	
<b>TR 3</b>	5					Not excavated: compact gravel drive	
	6					Not excavated: compact gravel drive	
	7	1	0-11	0-27	10YR 4/3	Brown silty loam with cobbles	NCM
		2	11-14	27-35	10YR 5/6	Yellowish brown silty loam with cobbles. , terminated at rock impasse.	NCM
	8	1	0-11	0-29	10YR 4/3	Brown silty loam with cobbles	NCM
		2	11-15	29-39	10YR 5/6	Yellowish brown silty loam with cobbles.	NCM
	9	1	0-8	0-21	10YR 4/3	Brown silty loam with cobbles	NCM
		2	8-12	21-31	10YR 5/6	Yellowish brown silty loam with cobbles.	NCM
	10					Not excavated: dense roots	
	11					Not excavated: rock wall	
<b>TR 4</b>	12	1	0-11	0-28	10YR 4/2	Dark grayish brown silty clay loam with cobbles	NCM
		2	11-15	28-38	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	13	1	0-10	0-26	10YR 4/2	Dark grayish brown silty clay loam with cobbles	NCM
		2	10-12	26-32	10YR 5/6	Yellowish brown clay loam with cobble terminated at rock impasse	NCM
	14	1	0-9	0-22	10YR 4/2	Dark grayish brown silty clay loam with cobbles	NCM
		2	9-12	22-30	10YR 5/6	Yellowish brown clay loam with cobble terminated at rock impasse	NCM
	15	1	0-10	0-26	10YR 4/2	Dark grayish brown silty clay loam with cobbles	NCM
		2	10-14	26-36	10YR 5/6	Yellowish brown clay loam with cobbles	NCM

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
	16	1	0-9	0-24	10YR 4/2	Dark grayish brown silty clay loam with cobbles	NCM
		2	9-12	24-30	10YR 5/6	Yellowish brown clay loam with cobble terminated at rock impasse	NCM
	17	1	0-11	0-28	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	11-15	28-38	10YR 5/6	Yellowish brown clay loam with gravel and cobbles	NCM
	18	1	0-11	0-29	10YR 4/3	Brown silty clay loam with gravel and cobbles. Stopped by roots.	NCM
<b>TR 5</b>	19	1	0-11	0-28	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	11-16	28-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	20	1	0-9	0-24	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	9-14	24-36	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	21	1	0-12	0-30	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	12-16	30-40	10YR 5/4	Yellowish brown silty clay with gravel	NCM
	22	1	0-13	0-32	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	13-17	32-44	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	23	1	0-16	0-40	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	16-20	40-50	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	24	1	0-13	0-34	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	13-18	34-45	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	25	1	0-15	0-39	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	15-20	39-50	10YR 5/6	Yellowish brown silty clay with gravel	NCM
<b>TR 6</b>	26	1	0-11	0-29	10YR 4/3	Brown silty clay loam with gravel and cobble terminated at rock impasse	NCM
	27					Not excavated: rock at surface	
	28	1	0-9	0-24	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	9-14	24-36	10YR 5/6	Yellowish brown clay loam with gravel and cobbles	NCM
	29	1	0-11	0-27	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
		2	11-14	27-35	10YR 5/6	Yellowish brown clay loam with gravel and cobbles. Stopped by roots.	NCM
	30	1	0-11	0-29	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	11-17	29-42	10YR 5/6	Yellowish brown clay loam with gravel and cobbles.	NCM
	31	1	0-9	0-22	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	9-13	22-32	10YR 5/6	Yellowish brown clay loam with gravel and cobbles.	NCM
	32	1	0-12	0-30	10YR 4/3	Brown silty clay loam with gravel and cobble terminated at rock impasse	NCM
	33					Not excavated: slope > 12%	
	34					Not excavated: slope > 12%	
<b>TR 7</b>	35	1	0-11	0-27	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	11-15	27-39	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	36	1	0-10	0-26	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	10-15	26-39	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	37	1	0-13	0-34	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	13-19	34-47	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	38	1	0-12	0-31	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	12-16	31-41	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	39	1	0-13	0-34	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	13-17	34-44	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	40	1	0-11	0-29	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	11-16	29-41	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	41	1	0-9	0-24	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	9-15	24-37	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	42					Not excavated: slope > 12%	
	43					Not excavated: slope > 12%	

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
<b>TR 8</b>	44	1	0-9	0-23	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	9-13	23-33	10YR 5/6	Yellowish brown clay loam with gravel and cobbles.	NCM
	45	1	0-8	0-21	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	8-12	21-31	10YR 5/6	Yellowish brown clay loam with gravel and cobbles.	NCM
	46					Not excavated: rock at surface, fallen trees	
	47	1	0-9	0-24	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	9-14	24-35	10YR 5/6	Yellowish brown clay loam with gravel and cobbles.	NCM
	48					Not excavated: fallen tree	
	49	1	0-11	0-27	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	11-15	27-37	10YR 5/6	Yellowish brown clay loam with gravel and cobbles.	Discarded clear bot
	50					Not excavated: slope > 12%	
	51					Not excavated: slope > 12%, fallen trees	
	52					Not excavated: rock wall	
<b>TR 9</b>	53	1	0-8	0-20	10YR 3/2	Very dark grayish brown silty loam with cobbles. Stopped by roots.	Discarded clear bot
	54	1	0-10	0-25	10YR 3/2	Very dark grayish brown silty loam with cobbles.	NCM
		2	10-15	25-38	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	55	1	0-6	0-15	10YR 3/2	Very dark grayish brown silty loam with cobbles. Stopped by roots.	NCM
	56					Not excavated: rock wall	
	57					Not excavated: rock wall	
	58					Not excavated: Slope > 12%	
	59					Not excavated: slope > 12%	
	60					Not excavated: slope > 12%	
	61	1	0-11	0-28	10YR 4/3	Brown silty clay loam with gravel and cobbles, terminated at rock impasse	NCM
<b>TR 10</b>	62					Not excavated: slope > 12%	

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
	63					Not excavated: slope > 12%	
	64	1	0-9	0-23	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	9-14	23-35	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	65	1	0-10	0-24	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	10-13	24-34	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	66	1	0-9	0-23	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	9-15	23-37	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	67	1	0-10	0-26	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	10-16	26-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	68	1	0-11	0-29	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	11-16	29-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	69	1	0-12	0-30	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	12-16	30-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	70	1	0-6	0-14	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	6-14	14-35	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	71		0-11	0-27	10YR 4/2	Dark grayish brown silty loam with gravel, , terminated at rock impasse at 27cm	NCM
<b>TR 11</b>	72	1	0-9	0-22	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	9-11	22-28	10YR 5/3	Brown silty clay with large cobbles. , terminated at rock impasse.	NCM
	73					Not excavated: slope > 12%	
	74	1	0-8	0-21	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	8-14	21-35	10YR 5/6	Yellowish brown clay loam with gravel and cobbles	NCM
	75	1	0-8	0-21	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	8-11	21-27	10YR 5/6	Yellowish brown clay loam with gravel and cobbles. , terminated at rock impasse	NCM
	76	1	0-9	0-24	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
		2	9-14	24-36	10YR 5/6	Yellowish brown clay loam with gravel and cobbles. , terminated at rock	NCM
	77	1	0-11	0-29	10YR 4/2	Dark grayish brown silty loam with gravel and large cobbles	NCM
		2	11-16	29-40	10YR 5/6	Yellowish brown silty clay	NCM
	78	1	0-8	0-21	10YR 4/2	Dark grayish brown silty loam with gravel and large cobbles	NCM
		2	8-15	21-37	10YR 5/6	Yellowish brown silty clay	NCM
	79	1	0-9	0-24	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	9-14	24-35	10YR 5/6	Yellowish brown silty clay	NCM
	80	1	0-10	0-26	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	10-15	26-39	10YR 5/6	Yellowish brown silty clay	NCM
	81	1	0-11	0-27	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	11-15	27-39	10YR 5/6	Yellowish brown silty clay	NCM
<b>TR 12</b>	82	1	0-10	0-26	10YR 4/2	Dark grayish brown silty loam with gravel and large cobbles	NCM
		2	10-16	26-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	83	1	0-11	0-27	10YR 4/2	Dark grayish brown silty loam with gravel and large cobbles	NCM
		2	11-15	27-37	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	84	1	0-11	0-28	10YR 4/2	Dark grayish brown silty loam with gravel and large cobbles	NCM
		2	11-16	28-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	85	1	0-12	0-30	10YR 4/2	Dark grayish brown silty loam with gravel and large cobbles	NCM
		2	12-16	30-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	86	1	0-11	0-29	10YR 4/2	Dark grayish brown silty loam with gravel and large cobbles	NCM
		2	11-16	29-40	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	87	1	0-13	0-33	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	13-18	33-46	10YR 5/6	Yellowish brown silty clay	NCM
	88					Not excavated: slope > 12%	

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
	89					Not excavated: slope > 12%	
	90					Not excavated: slope > 12%	
	91					Not excavated: slope > 12%	
<b>TR 13</b>	92	1	0-7	0-19	10YR 4/3	Brown silty clay loam with cobbles and gravel. , terminated at rock impasse..	NCM
	93	1	0-11	0-28	10YR 4/3	Brown silty clay loam with cobbles and gravel.	NCM
		2	11-15	28-38	10YR 5/6	Yellowish brown clay loam with gravel.	NCM
	94	1	0-9	0-22	10YR 4/3	Brown silty clay loam with cobbles and gravel.	NCM
		2	9-13	22-34	10YR 5/6	Yellowish brown clay loam with gravel.	NCM
	95	1	0-9	0-23	10YR 4/3	Brown silty clay loam with cobbles and gravel. , terminated at rock impasse..	NCM
		2	9-12	23-30	10YR 5/6	Yellowish brown clay loam with gravel. , terminated at rock impasse.	NCM
	96	1	0-9	0-24	10YR 4/3	Brown silty clay loam with cobbles and gravel. , terminated at rock impasse..	NCM
		2	9-12	24-31	10YR 5/6	Yellowish brown clay loam with gravel. , terminated at rock impasse.	NCM
	97					Not excavated: slope > 12%	
	98	1	0-7	0-18	10YR 4/3	Brown silty clay loam with cobbles and gravel. , terminated at rock impasse..	NCM
		2	7-12	18-30	10YR 5/6	Yellowish brown clay loam with gravel.	NCM
	99					Not excavated: slope > 12%	
	100					Not excavated: slope > 12%	
	101					Not excavated: slope > 12%	
<b>TR 14</b>	102	1	0-9	0-24	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	9-15	24-37	10YR 5/6, 10YR 5/1	Yellowish brown and gray silty clay	NCM
	103	1	0-9	0-23	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	9-13	23-33	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	104	1	0-11	0-27	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	11-15	27-39	10YR 5/6, 10YR 5/1	Yellowish brown and gray silty clay	NCM



Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
	105					Not excavated: slope > 12%	
	106					Not excavated: slope > 12%	
	107					Not excavated: slope > 12%	
	108					Not excavated: slope > 12%	
	109					Not excavated: slope > 12%	
	110					Not excavated: slope > 12%	
	111					Not excavated: slope > 12%	
<b>TR 15</b>	112	1	0-11	0-27	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	11-15	27-37	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	113	1	0-10	0-25	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	10-15	25-39	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	114	1	0-6	0-19	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	6-12	19-30	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	115					Not excavated: slope > 12%	
	116					Not excavated: slope > 12%	
	117					Not excavated: slope > 12%	
	118					Not excavated: slope > 12%	
	119					Not excavated: slope > 12%	
<b>TR 16</b>	120	1	0-11	0-27	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	11-15	27-39	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	121	1	0-11	0-27	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	11-16	27-40	10YR 5/6, 10YR 5/1	Yellowish brown and gray silty clay	NCM
	122	1	0-9	0-22	10YR 4/2	Dark grayish brown silty loam with gravel and cobbles	NCM
		2	9-15	22-37	10YR 5/6, 10YR 5/1	Yellowish brown and gray silty clay	NCM

Transect	ST	Level	Depth (in)	Depth (cm)	Munsell	Soil Description	Cultural Material
<b>TR 17</b>	123	1	0-9	0-23	10YR 4/3	Brown silty clay loam with gravel	NCM
		2	9-13	23-33	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	124	1	0-8	0-21	10YR 4/3	Brown silty clay loam with gravel and cobbles	NCM
		2	8-12	21-31	10YR 5/6	Yellowish brown clay loam with cobbles	NCM
	125					Not excavated: slope > 12%	
<b>TR 18</b>	126	1	0-10	0-26	10YR 4/2	Dark grayish brown silty loam with gravel	NCM
		2	10-14	26-36	10YR 5/6	Yellowish brown silty clay with gravel	NCM
	127	1	0-17	0-42	10YR 3/3	Dark brown silty loam with gravel and large cobbles	NCM
		2	17-22	42-56	10YR 5/6	Yellowish brown clay loam	NCM

## Section 5

## Memorandum

To: Justin Dates, R.L.A., LEED AP

From: Philip Grealy, Ph.D., P.E.

Date: February 8, 2022

**Revised August 22, 2022**

Subject: Dewpoint South - Noise Evaluation

Project No.: 20006912A

---

We have completed our sound level measurements and analysis for the above project site located at Tax Lot #4-1-50.32 located on Dolsontown Road in the Town of Wawayanda, New York. The sound level readings were collected following standard procedures as described in more detail below. We have also compared these levels to the future sound levels associated with the typical activities expected on the site and as they relate to the adjacent proposed warehouse development on Dolsontown Road. We have also compared these to the Town of Wawayanda Code requirements and NYSDEC guidelines.

### [Typical Noise Parameters](#)

The Equivalent Sound Level or  $L_{eq}$  is related to the average of the sound energy over time. The  $L_{eq}$  integrates fluctuating sound levels over a period of time to express them as a steady state sound level. As an example, if two sounds are measured and one sound has twice the energy but lasts half as long, the two sounds would be characterized as having the same equivalent sound level. Equivalent Sound Level is considered to be directly related to the effects of sound on people since it expresses the equivalent magnitude of the sound as a function of frequency of occurrence and time. It is also useful in establishing the ambient sound levels at a potential noise source.

Designations for sound levels also include those as  $L_{10}$  or  $L_{90}$ . These designations refer to the sound pressure level (SPL) that is exceeded for 10% of the time over which the sound is measured, in the case of  $L_{10}$ , and 90% of the time, in the case of  $L_{90}$ . For example, an  $L_{90}$  of 70 dBA means that 70 dBA is exceeded for 90% of the time for which the measurement was taken.  $L_{max}$  represents the maximum observed sound level during the measurement period.

### [Existing Ambient Noise Levels \(Figure No. 1 and Tables No. 1 and 2\)](#)

The predominant area background noise source is from traffic along the I-84 corridor as well as local traffic along the NYS Route 17M and Dolsontown Road corridors.

Existing noise measurement surveys were conducted at three locations (receptors) around the site, including at the adjacent and nearby residential property boundaries, to provide a representative sampling of ambient noise levels in the area (see Figure No. 1 for receptor locations). The noise

measurements were collected by representatives of Colliers Engineering & Design. The noise measurements were taken with a Brüel and Kjaer Type 1-Precision integrating Sound Level Meter – Type 2236. The meter was calibrated prior to actual measurements using a Brüel and Kjaer Acoustical Calibrator Model No. 4231. The actual measurements and calibration procedures followed were completed in conformance with American National Standards Institute (ANSI) criteria as well as those outlined in the NYSDEC guidelines for “Assessing and Mitigating Noise Impacts” dated February 2, 2001.

The microphones used in the measurements were located, without obstruction from stationary objects, at a height of approximately five feet above the ground surface. Measurements taken included a  $L_{eq}$  level,  $L_{10}$ ,  $L_{50}$ ,  $L_{90}$ ,  $L_{min}$  and  $L_{max}$  for each location. The measurements were collected at 15-minute intervals to identify the noise character at each receptor. The existing sound level measurements were taken on January 25, 2022 and January 26, 2022.

The primary receptors in the area include the private residences along the east side of Sunrise Park Road, the residences located on the north side of Dolsontown Road, i.e., 1065, 1069, and 1073, and the residences located on Caskey Lane.

The receptors evaluated are identified on Figure No. 1 and described below:

- R1 – On the east side of the cul-de-sac at the end of Caskey Lane
- R2 – On the north side of Dolsontown Road near 1081 Dolsontown Road for representation of the existing residences at 1073, 1069, and 1065
- R3 – On the northeast side of Sunrise Park Road adjacent to the property line of the 55 Sunrise Park Road single family residential home

Appendix A contains a figure identifying the receptor locations and photographs of these measurement locations are also attached.

The measurements were taken at these three locations along the perimeter of the property to identify background ambient sound levels at these residential receptors. They are summarized on the Noise Data Summary tables, which summarize various noise characteristics measured including  $L_{eq}$ ,  $L_{10}$ ,  $L_{90}$ ,  $L_{max}$  and  $L_{min}$  for each receptor. The Noise Data Summary Tables also summarize other critical information include temperature, wind conditions, coordinates and the factors influencing noise levels. Note that the  $L_{eq}$  is the typical standard used for evaluating potential noise impacts.

For reference, Table No. 1 is also attached and summarizes the range of typical environmental scenarios, while Table No. 2 summarizes the Federal Highway Administration’s Design Noise Levels.

The existing background levels are the result of general background traffic noise from traffic on I-84 as well as Dolsontown Road, nature noises, airplane flyovers and other local background sources. As can be seen from a review of the tables, the typical  $L_{eq}$  levels ranging from the low 40’s to the mid/high 50’s dBA range at the different receptors along the perimeter of the site. Appendix B

contains the various tables. Appendix C contains a summary of the noise receptor location descriptions and field measurement conditions.

The NYSDEC guidelines for “Assessing and Mitigating Noise Impacts” dated February 2, 2001 summarizes several parameters related to sound pressure levels. Some of the key items are provided herein.

- Sound Level Reduction Over Distance – It is important to have an understanding of the way noise decreases with distance. The decrease in sound level from any single noise source normally follows the “inverse square law.” That is, sound pressure level (SPL) changes in inverse proportion to the square of the distance from the sound source. At distances greater than 50 feet from a sound source, every doubling of the distance produces a 6 dB reduction in the sound. Therefore, a sound level of 70 dB at 50 feet would have a sound level of approximately 64 dB at 100 feet. At 200 feet sound from the same source would be perceived at a level of approximately 58 dB.
- Most humans find a sound level of 60-70 dBA as beginning to create a condition of significant noise effect (EPA 550/9-79-100, November 1978).
- Sound pressure level increases ranging from 0-3 dB should have no appreciable effect on receptors. Increases from 3-6 dB may have potential for adverse noise impact only in cases where the most sensitive of receptors are present. Table B below from the DEC policy provides some more detail on this.

Table A

HUMAN REACTION TO INCREASES IN SOUND PRESSURE LEVEL

Increase in Sound Pressure (dB)	Human Reaction
Under 5	Unnoticed to tolerable
5 – 10	Intrusive
10 – 15	Very noticeable
15 – 20	Objectionable
Over 20	Very objectionable to intolerable

Source: NYSDEC “Assessing and Mitigating Noise Impacts” revised February 2, 2001 (Table B, Page 15)

### Comparison of Future Noise Levels with Ambient Levels (Tables No. 3 and 4)

Table No. 3 provides a summary of the computed  $L_{eq}$  sound pressure levels (dBA) for the Existing, No-Build, and Build conditions based on expected traffic volumes and onsite vehicle movements at the facility.

In addition to the NYSDEC guidance, the Town of Wawayanda Code in Chapter 195, "Zoning," Article IV General Supplementary Regulations at §195-23 "General Commercial and Industrial Standards" Item D states "Noise shall not exceed an intensity of 65 decibels as measured 100 feet from the boundaries of the lot where such use is situated."

### Recommendations

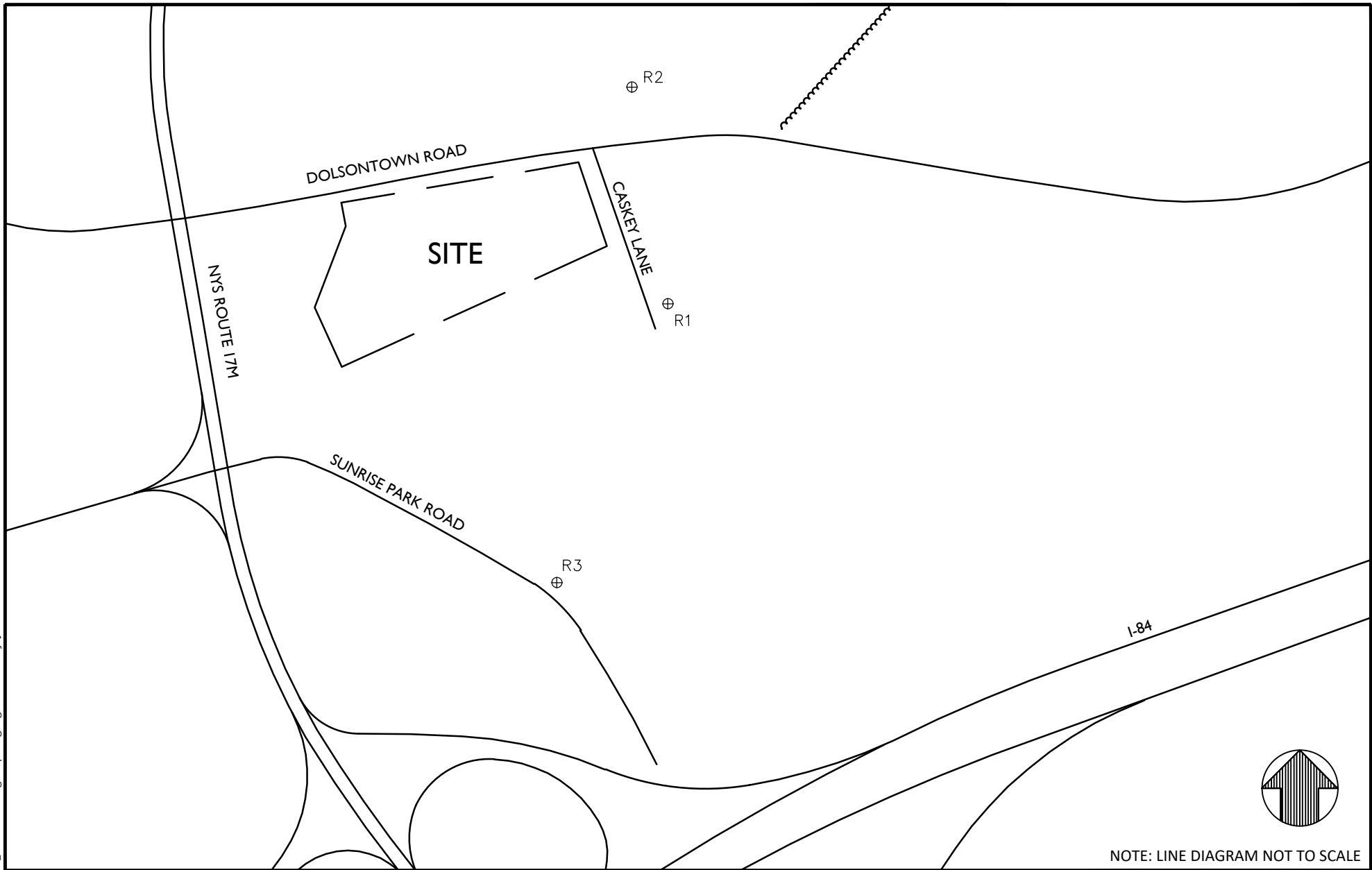
As can be seen from a review of the sound level tables, the increases in noise levels at the receptors as a result of the project traffic movements and other onsite activities are expected to be typically less than 5 dbA at all receptors. The position of the building on the site provides a physical barrier, which will attenuate sound emanating at the south side of the building from the residences to the northeast along Dolsontown Road. It should be noted that the proposed retaining wall along the southern portion of the property should provide some attenuation for nearby residential properties in reducing possible future noise sources originating on site. However, in order to reduce future noise levels to the greatest extent reasonably possible, the following is a summary of recommendations to be implemented as mitigation:

1. The construction equipment used on-site will have to be inspected periodically to ensure that properly functioning muffler systems are used on all equipment.
2. All equipment should not idle unnecessarily while on site.
3. The HVAC equipment should also be positioned to face away from the adjacent residence as part of the final building design/HVAC equipment layout.
4. Installation of a solid fence along the southeastern portion of the site on top of the retaining wall.
5. Any onsite equipment should be equipped with alternate backup safety alarms such as "white noise" alarms, alternate radar, or infrared alarm systems.

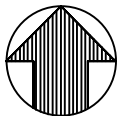
# Dewpoint South

## Appendix A | Figures





NOTE: LINE DIAGRAM NOT TO SCALE



Engineering & Design

www.colliersengineering.com



Copyright © 2022, Colliers Engineering & Design. All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, reused, disclosed, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

REV	DATE	DRAWN BY	DESCRIPTION

DEWPOINT SOUTH

TAX LOT: 4-1-50.32  
TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK



Know what's below.  
Call before you dig.

FOR STATE SPECIFIC DIRECT PHONE NUMBERS  
VISIT: WWW.CALL811.COM



Engineering & Design

**PROTECT YOURSELF**  
ALL STATES REQUIRE NOTIFICATION  
OF EXCAVATORS, DESIGNERS, OR  
ANY PERSON PREPARING TO  
DISTURB THE EARTH'S SURFACE  
ANYWHERE IN ANY STATE

WESTCHESTER  
400 Columbus Avenue,  
Suite 180E  
Valhalla, NY 10595  
Phone: 914.347.7500  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
DOING BUSINESS AS MASER CONSULTING  
ENGINEERING & LAND SURVEYING

NOISE IMPACT EVALUATION			
SCALE:	DATE:	DRAWN BY:	CHECKED BY:
AS SHOWN	1/24/2022	J.F.M.	P.J.G.
PROJECT NUMBER:	DRAWING NAME:		
20006912A	220822\FM_NOISE READING MAP		
SHEET TITLE:			
NOISE RECEPTOR LOCATIONS			
SHEET NUMBER:			
FIGURE 1			

# Dewpoint South

## Appendix B | Tables

**TABLE NO 1.**  
**RANGE OF TYPICAL ENVIRONMENTAL A-WEIGHTED NOISE LEVELS**

SITUATION	NOISE LEVEL (dBA) (1,2)
Discotheque/Rock Band at 5m	110
Jet Flyover at 1,000 feet	105
Gas Lawn Mower at 3 feet	98
Inside Subway Train	95
Shouting at 3 feet	78
Gas Lawn Mower at 100 feet	70
Normal Speech at 3 feet	65
Background Office Noise	50
Library	34 -40
Optimum Sleeping Level	35 or less
Threshold of Hearing	5

1) *The Audible Landscape: Manual for Highway Noise and Land Use*, Table A-16, Page 91, USDOT, 1974

2) *Transportation Planning Handbook*, Institute of Transportation Engineers, Figure 8-2, Edition, 1999

**TABLE NO. 2**  
**FHWA DESIGN LEVELS**

ACTIVITY CATEGORY	DESIGN NOISE LEVEL (dBA)		DESCRIPTION OF ACTIVITY CATEGORY (2)
	$L_{eq}$	$L_{10}$	
A	57 (EXTERIOR)	60 (EXTERIOR)	Tracts where serentiy and quiet are expecially important.
B	67 (EXTERIOR)	70 (EXTERIOR)	Residences, motels, schools, churches, hospitals, etc.
C	72 (EXTERIOR)	75 (EXTERIOR)	Developed lands other than thos above.
E	52 (EXTERIOR)	55 (EXTERIOR)	Buidling interiors.

1) Source: Federal Highway Administration, *Procedures for the Abatement of Highway Traffic Noise and Construction Noise*, Federal Register 41 (80), Washington, D.C.

2) Either  $L_{eq}$  or  $L_{10}$  can be used - not both - and an hourly measure applies. The land-use descriptions are further qualified in the reference and a category D is also reserved for undeveloped land. The interior noise levels may be established by subtracting from outdoor levels the attenuation expected of the particular wall and window constructions involved.

**Table No. 3**  
**(AM)**

*Summary of Existing and Projected Noise Levels (Leq-dBA)*

<b>Receptor</b>	<b>Existing</b>	<b>No-Build</b>	<b>Build</b>	<b>Build Comb</b>	<b>Δ NB -&gt; BD</b>	<b>Δ NB -&gt; BD COMB</b>
R1	53.4	54.1	54.2	57.3	0.1	3.2
R2	57.9	58.6	58.7	58.7	0.1	0.1
R3	53.2	53.7	53.8	53.8	0.1	0.1

**(PM)**

*Summary of Existing and Projected Noise Levels (Leq-dBA)*

<b>Receptor</b>	<b>Existing</b>	<b>No-Build</b>	<b>Build</b>	<b>Build Comb</b>	<b>Δ NB -&gt; BD</b>	<b>Δ NB -&gt; BD COMB</b>
R1	52.0	52.6	52.8	56.6	0.2	4.0
R2	57.7	58.3	58.5	58.5	0.2	0.2
R3	56.6	56.8	57.0	57.0	0.2	0.2

Notes:

- 1) The Build Combined scenario includes both the RDM Simon and Dewpoint South developments.

**TABLE NO. 4**  
**HUMAN REACTION TO INCREASES IN SOUND PRESSURE LEVEL**

<b>INCREASE IN SOUND PRESSURE (dBA)</b>	<b>HUMAN REACTION</b>
2-3	BARELY PRECEPTIBLE
3-5	NOTICEABLE
10	SOMEWHAT INTRUSIVE-DOUBLING OF LOUDNESS
10-15	VERY NOTICEABLE
15-20	OBJECTIONABLE
OVER 20	VERY OBJECTIONABLE TO INTOLERABLE

Source: *Fundamentals and Abatement of Highway Traffic Noise*, FHWA, 1973.

# Dewpoint South

## Appendix C | Noise Receptor Locations & Field Measurement Characteristics



Receptor-R1 - Located on the east side of the cul-de-sac at the end of Caskey Lane



Receptor-R1 – Located on the east side of the cul-de-sac at the end of Caskey Lane





Receptor-R2 – Located on the north side of Dolsontown Road directly east of 1081 Dolsontown Road



Receptor-R2 – Located on the north side of Dolsontown Road directly east of 1081 Dolsontown Road



Receptor-R3 – Located on the north side of Sunrise Park Road directly northwest of the 55 Sunrise Park Road Single Family Residential Home.



Receptor-R3 – Located on the north side of Sunrise Park Road directly northwest of the 55 Sunrise Park Road Single Family Residential Home.

## **Receptor Location #1 Description**

Receptor Location #1 is located on the east side of the cul-de-sac at the end of Caskey Lane.

## **Field Measurement Conditions**

### **Weekday (AM)**

1/25/2022 – Start time: 7:18 AM, Wind Max: 0.4 MPH, Wind Average: 0.2 MPH, 25°F

1/25/2022 – Start time: 8:37 AM, Wind Max: 1.2 MPH, Wind Average: 0.6 MPH, 27°F

1/25/2022 – Start time: 10:01 AM, Wind Max: 1.4 MPH, Wind Average: 1.0 MPH, 32°F

### **Weekday (PM)**

1/25/2022 – Start time: 1:05 PM, Wind Max: 1.2 MPH, Wind Average: 0.8 MPH, 34°F

1/25/2022 – Start time: 2:15 PM, Wind Max: 0.8 MPH, Wind Average: 0.5 MPH, 34°F

1/26/2022 – Start time: 3:26 PM, Wind Max: 5.5 MPH, Wind Average: 3.0 MPH, 23°F

1/26/2022 – Start time: 4:35 PM, Wind Max: 1.5 MPH, Wind Average: 0.7 MPH, 21°F

## **Receptor Location #2 Description**

Receptor Location #2 is located on the north side of Dolsontown Road directly east of 1081 Dolsontown Road

## **Field Measurement Conditions**

### **Weekday (AM)**

1/25/2022 – Start time: 7:47 AM, Wind Max: 0.5 MPH, Wind Average: 0.3 MPH, 25°F

1/25/2022 – Start time: 9:05 AM, Wind Max: 0.6 MPH, Wind Average: 0.5 MPH, 28°F

1/25/2022 – Start time: 10:23 AM, Wind Max: 1.1 MPH, Wind Average: 0.7 MPH, 34°F

### **Weekday (PM)**

1/25/2022 – Start time: 1:28 PM, Wind Max: 0.6 MPH, Wind Average: 0.3 MPH, 36°F

1/26/2022 – Start time: 3:51 PM, Wind Max: 1.0 MPH, Wind Average: 0.4 MPH, 23°F

1/26/2022 – Start time: 4:57 PM, Wind Max: 1.1 MPH, Wind Average: 0.5 MPH, 19°F

## **Receptor Location #3 Description**

Receptor Location #3 is located on the north side of Sunrise Park Road directly northwest of the 55 Sunrise Park Road Single Family Residential Home.

## **Field Measurement Conditions**

### **Weekday (AM)**

1/25/2022 – Start time: 8:14 AM, Wind Max: 0.3 MPH, Wind Average: 0.2 MPH, 27°F

1/25/2022 – Start time: 9:30 AM, Wind Max: 0.7 MPH, Wind Average: 0.5 MPH, 30°F

1/25/2022 – Start time: 10:48 AM, Wind Max: 1.6 MPH, Wind Average: 1.2 MPH, 34°F

### **Weekday (PM)**

1/25/2022 – Start time: 1:54 PM, Wind Max: 2.0 MPH, Wind Average: 1.3 MPH, 34°F

1/26/2022 – Start time: 4:15 PM, Wind Max: 1.1 MPH, Wind Average: 0.6 MPH, 23°F

1/26/2022 – Start time: 5:32 PM, Wind Max: 1.3 MPH, Wind Average: 0.7 MPH, 19°F

# Dewpoint South

## Appendix D | Noise Modeling Summary Worksheets



REPORT:	<b>Results: Sound Levels - Input Heights</b>			REPORT DATE:	8 February 2022
TNM VERSION:	3.1.7970.37608			CALCULATION DATE:	2/8/2022 2:05:20 PM
CALCULATED WITH:	3.1.7970.37608			ORGANIZATION:	Colliers Engineering & Design
CASE:	AMEX			PROJECT/CONTRACT:	20006912A
ANALYSIS BY:	J.F.M.				
DEFAULT GROUND TYPE:	FieldGrass				
ATMOSPHERICS:	68°F, 50%			Average pavement type shall be used unless a state highway agency substantiates the use of a different type with approval of FHWA.	
PAVEMENT TYPE(S) USED:	Average				

Results for:	DU	Noise Reduction			Barrier Cost				
		Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs	
		dB	dB	dB	\$	\$	\$	\$	
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

Receiver				Modeled Traffic Noise Levels									
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					With Abatement Barriers				
				LAeq		Increase over Existing		Type of Impact	Calc. LAeq	Noise Reduction		Calc. Minus Goal	
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal		
				dBA	dBA	dBA	dBA		dBA	dBA	dBA	dBA	
Receiver-1	1	1	53.4	51.0	0.0	-2.4	10.0	Sound Level	51.0	0.0	8.0	-8.0	
Receiver-2	2	1	57.9	57.0	0.0	-0.9	10.0	Sound Level	57.0	0.0	8.0	-8.0	
Receiver-3	3	1	53.2	53.3	0.0	0.1	10.0	Sound Level	53.3	0.0	8.0	-8.0	

<b>REPORT:</b>	<b>Results: Sound Levels - Input Heights</b>			<b>REPORT DATE:</b>	8 February 2022
<b>TNM VERSION:</b>	3.1.7970.37608	<b>CALCULATION DATE:</b>	2/8/2022 2:08:06 PM		
<b>CALCULATED WITH:</b>	3.1.7970.37608	<b>ORGANIZATION:</b>	Colliers Engineering & Design		
<b>CASE:</b>	AMNB	<b>PROJECT/CONTRACT:</b>	20006912A		
<b>ANALYSIS BY:</b>	J.F.M.				
<b>DEFAULT GROUND TYPE:</b>	FieldGrass				
<b>ATMOSPHERICS:</b>	68°F, 50%	Average pavement type shall be used unless a state highway agency substantiates the use of a different type with approval of FHWA.			
<b>PAVEMENT TYPE(S) USED:</b>	Average				

Results for:		DUs	Noise Reduction			Barrier Cost			
			Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs
			dB	dB	dB	\$	\$	\$	\$
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

Receiver				Modeled Traffic Noise Levels									
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					With Abatement Barriers				
				LAeq		Increase over Existing		Type of Impact	Calc. LAeq	Noise Reduction		Calc. Minus Goal	
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal		
				dBA	dBA	dBA	dBA		dBA	dBA	dBA	dBA	dBA
Receiver-1	1	1	54.0	51.4	0.0	-2.6	10.0	Sound Level	51.4	0.0	8.0	-8.0	
Receiver-2	2	1	58.5	57.5	0.0	-1.0	10.0	Sound Level	57.5	0.0	8.0	-8.0	
Receiver-3	3	1	53.7	53.6	0.0	-0.1	10.0	Sound Level	53.6	0.0	8.0	-8.0	



<b>REPORT:</b>	<b>Results: Sound Levels - Input Heights</b>			<b>REPORT DATE:</b>	8 February 2022
<b>TNM VERSION:</b>	3.1.7970.37608	<b>CALCULATION DATE:</b>	2/8/2022 2:29:12 PM		
<b>CALCULATED WITH:</b>	3.1.7970.37608	<b>ORGANIZATION:</b>	Colliers Engineering & Design		
<b>CASE:</b>	AMBD	<b>PROJECT/CONTRACT:</b>	20006912A		
<b>ANALYSIS BY:</b>	J.F.M.				
<b>DEFAULT GROUND TYPE:</b>	FieldGrass				
<b>ATMOSPHERICS:</b>	68°F, 50%	Average pavement type shall be used unless a state highway agency substantiates the use of a different type with approval of FHWA.			
<b>PAVEMENT TYPE(S) USED:</b>	Average				

Results for:		DUs	Noise Reduction			Barrier Cost			
			Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs
			dB	dB	dB	\$	\$	\$	\$
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

Receiver				Modeled Traffic Noise Levels										
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					Type of Impact	With Abatement Barriers				
				LAeq		Increase over Existing		Calc. LAeq dBA		Noise Reduction		Calc. Minus Goal dBA		
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal			
				dBA	dBA	dBA	dBA			dBA	dBA			
Receiver-1	1	1	54.2	51.2	0.0	-3.0	10.0	Sound Level	51.2	0.0	8.0	-8.0		
Receiver-2	2	1	58.7	57.8	0.0	-0.9	10.0	Sound Level	57.8	0.0	8.0	-8.0		
Receiver-3	3	1	53.9	53.8	0.0	-0.1	10.0	Sound Level	53.8	0.0	8.0	-8.0		

<b>REPORT:</b>	<b>Results: Sound Levels - Input Heights</b>			<b>REPORT DATE:</b>	8 February 2022
<b>TNM VERSION:</b>	3.1.7970.37608	<b>CALCULATION DATE:</b>	2/8/2022 2:33:45 PM		
<b>CALCULATED WITH:</b>	3.1.7970.37608	<b>ORGANIZATION:</b>	Colliers Engineering & Design		
<b>CASE:</b>	AMBD COMB	<b>PROJECT/CONTRACT:</b>	20006912A		
<b>ANALYSIS BY:</b>	J.F.M.				
<b>DEFAULT GROUND TYPE:</b>	FieldGrass				
<b>ATMOSPHERICS:</b>	68°F, 50%	Average pavement type shall be used unless a state highway agency substantiates the use of a different type with approval of FHWA.			
<b>PAVEMENT TYPE(S) USED:</b>	Average				

Results for:		DUs	Noise Reduction			Barrier Cost			
			Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs
			dB	dB	dB	\$	\$	\$	\$
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

Receiver				Modeled Traffic Noise Levels									
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					With Abatement Barriers				
				LAeq		Increase over Existing		Type of Impact	Calc. LAeq dBA	Noise Reduction		Calc. Minus Goal dBA	
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal		
				dBA	dBA	dBA	dBA			dBA	dBA		
Receiver-1	1	1	54.2	57.3	0.0	3.1	10.0	Sound Level	57.3	0.0	8.0	-8.0	
Receiver-2	2	1	58.7	58.0	0.0	-0.7	10.0	Sound Level	58.0	0.0	8.0	-8.0	
Receiver-3	3	1	53.9	53.8	0.0	-0.1	10.0	Sound Level	53.8	0.0	8.0	-8.0	

REPORT:	<b>Results: Sound Levels - Input Heights</b>			REPORT DATE:	8 February 2022
TNM VERSION:	3.1.7970.37608			CALCULATION DATE:	2/8/2022 2:42:18 PM
CALCULATED WITH:	3.1.7970.37608			ORGANIZATION:	Colliers Engineering & Design
CASE:	PMEX			PROJECT/CONTRACT:	20006912A
ANALYSIS BY:	J.F.M.				
DEFAULT GROUND TYPE:	FieldGrass				
ATMOSPHERICS:	68°F, 50%			Average pavement type shall be used unless a state highway agency substantiates the use of a different type with approval of FHWA.	
PAVEMENT TYPE(S) USED:	Average				

Results for:	DUs	Noise Reduction			Barrier Cost				
		Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs	
		dB	dB	dB	\$	\$	\$	\$	
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

Receiver				Modeled Traffic Noise Levels									
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					With Abatement Barriers				
				LAeq		Increase over Existing		Type of Impact	Calc. LAeq	Noise Reduction		Calc. Minus Goal	
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal		
				dBA	dBA	dBA	dBA		dBA	dBA	dBA	dBA	dBA
Receiver-1	1	1	52.0	51.0	0.0	-1.0	10.0	Sound Level	51.0	0.0	8.0	-8.0	
Receiver-2	2	1	57.7	58.1	0.0	0.4	10.0	Sound Level	58.1	0.0	8.0	-8.0	
Receiver-3	3	1	56.6	52.8	0.0	-3.8	10.0	Sound Level	52.8	0.0	8.0	-8.0	

**REPORT: Results: Sound Levels - Input Heights**  
 TNM VERSION: 3.1.7970.37608      REPORT DATE: 8 February 2022  
 CALCULATED WITH: 3.1.7970.37608      CALCULATION DATE: 2/8/2022 2:47:11 PM  
 CASE: PMNB      ORGANIZATION: Colliers Engineering & Design  
 ANALYSIS BY: J.F.M.      PROJECT/CONTRACT: 20006912A  
 DEFAULT GROUND TYPE: FieldGrass  
 ATMOSPHERICS: 68°F, 50%      Average pavement type shall be used unless a state highway agency  
 PAVEMENT TYPE(S) USED: Average      substantiates the use of a different type with approval of FHWA.

Results for:		DUs	Noise Reduction			Barrier Cost			
			Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs
			dB	dB	dB	\$	\$	\$	\$
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

Receiver				Modeled Traffic Noise Levels										
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					Type of Impact	With Abatement Barriers				
				LAeq		Increase over Existing		Calc. LAeq dBA		Noise Reduction		Calc. Minus Goal dBA		
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal			
				dBA	dBA	dBA	dBA			dBA	dBA			
Receiver-1	1	1	52.5	51.5	0.0	-1.0	10.0	Sound Level	51.5	0.0	8.0	-8.0		
Receiver-2	2	1	58.2	58.6	0.0	0.4	10.0	Sound Level	58.6	0.0	8.0	-8.0		
Receiver-3	3	1	56.8	53.1	0.0	-3.7	10.0	Sound Level	53.1	0.0	8.0	-8.0		

REPORT:	<b>Results: Sound Levels - Input Heights</b>			REPORT DATE:	8 February 2022
TNM VERSION:	3.1.7970.37608			CALCULATION DATE:	2/8/2022 2:52:38 PM
CALCULATED WITH:	3.1.7970.37608			ORGANIZATION:	Colliers Engineering & Design
CASE:	PMBD			PROJECT/CONTRACT:	20006912A
ANALYSIS BY:	J.F.M.				
DEFAULT GROUND TYPE:	FieldGrass				
ATMOSPHERICS:	68°F, 50%			Average pavement type shall be used unless a state highway agency substantiates the use of a different type with approval of FHWA.	
PAVEMENT TYPE(S) USED:	Average				

Results for:		DUs	Noise Reduction			Barrier Cost			
			Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs
			dB	dB	dB	\$	\$	\$	\$
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

Receiver				Modeled Traffic Noise Levels									
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					With Abatement Barriers				
				LAeq		Increase over Existing		Type of Impact	Calc. LAeq	Noise Reduction		Calc. Minus Goal	
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal		
				dBA	dBA	dBA	dBA		dBA	dBA	dBA	dBA	
Receiver-1	1	1	52.8	50.4	0.0	-2.4	10.0	Sound Level	50.4	0.0	8.0	-8.0	
Receiver-2	2	1	58.5	57.8	0.0	-0.7	10.0	Sound Level	57.8	0.0	8.0	-8.0	
Receiver-3	3	1	57.0	53.2	0.0	-3.8	10.0	Sound Level	53.2	0.0	8.0	-8.0	

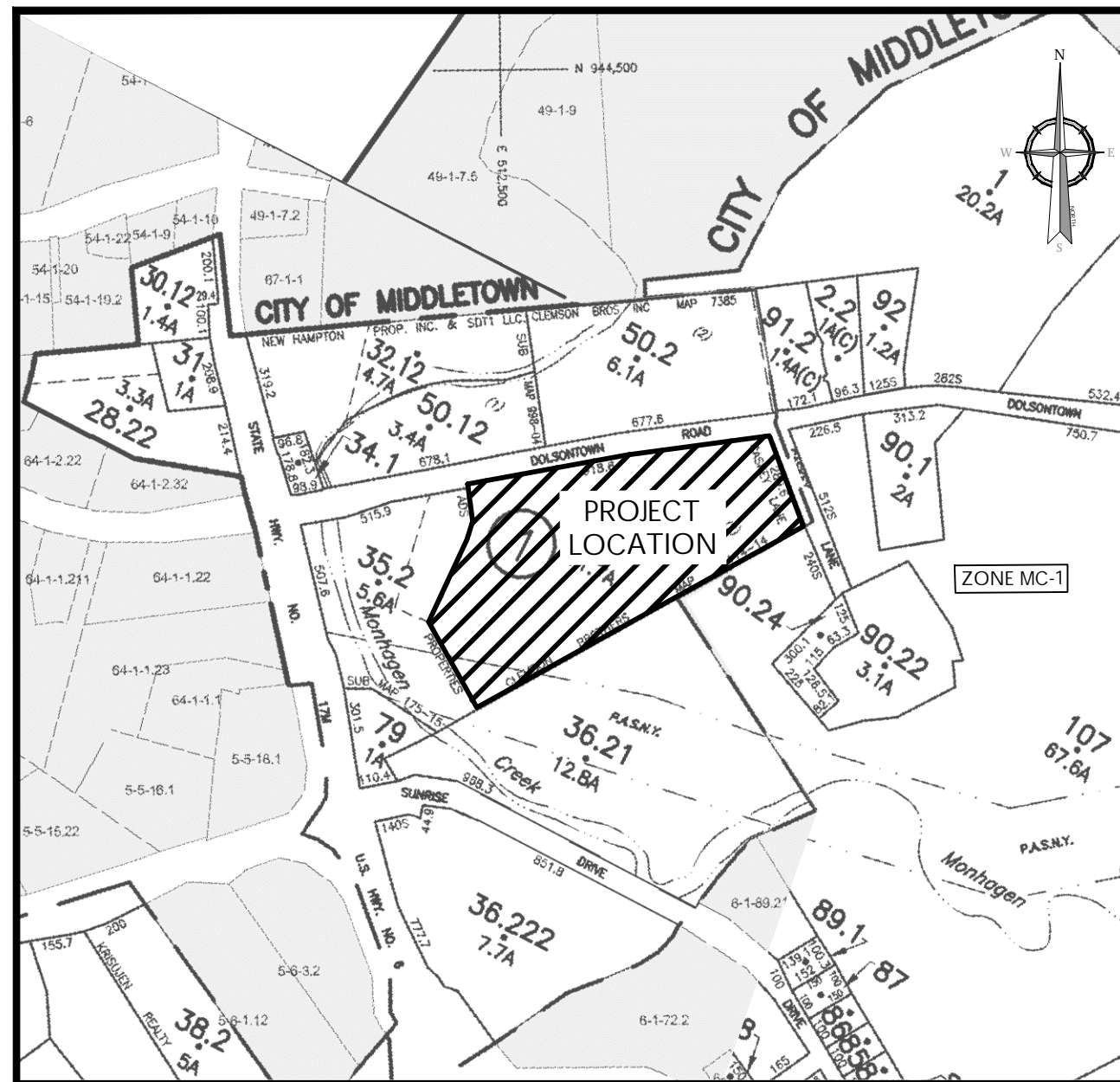
<b>REPORT:</b>	<b>Results: Sound Levels - Input Heights</b>			<b>REPORT DATE:</b>	8 February 2022
<b>TNM VERSION:</b>	3.1.7970.37608	<b>CALCULATION DATE:</b>	2/8/2022 2:59:50 PM		
<b>CALCULATED WITH:</b>	3.1.7970.37608	<b>ORGANIZATION:</b>	Colliers Engineering & Design		
<b>CASE:</b>	PMBD COMB	<b>PROJECT/CONTRACT:</b>	20006912A		
<b>ANALYSIS BY:</b>	J.F.M.				
<b>DEFAULT GROUND TYPE:</b>	FieldGrass				
<b>ATMOSPHERICS:</b>	68°F, 50%	Average pavement type shall be used unless a state highway agency substantiates the use of a different type with approval of FHWA.			
<b>PAVEMENT TYPE(S) USED:</b>	Average				

Results for:		DUs	Noise Reduction			Barrier Cost			
			Min	Avg	Max	Area / Volume	Lineal	Total	Total/DUs
			dB	dB	dB	\$	\$	\$	\$
Receivers in the Barrier Design:	All	3	0.0	0.0	0.0	0	0	0	0
	All Impacted	3	0.0	0.0	0.0	0	0	0	0
Meeting Noise Reduction Goal:	All	0	---	---	---	0	0	0	---
	All Impacted	0	---	---	---	0	0	0	---

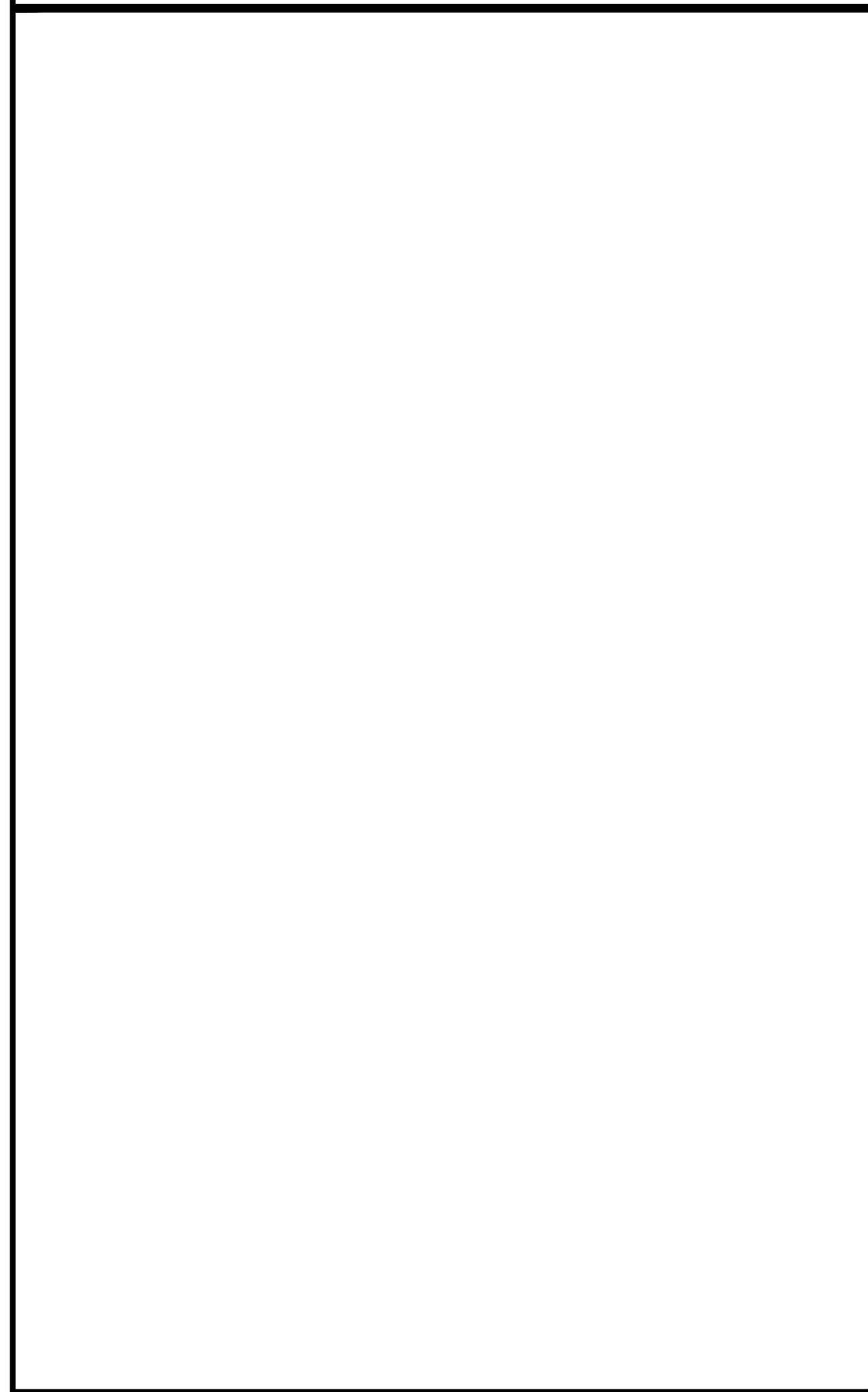
Receiver				Modeled Traffic Noise Levels									
Name	No.	DUs	Existing LAeq dBA	All Abatement Barriers at Zero Height					With Abatement Barriers				
				LAeq		Increase over Existing		Type of Impact	Calc. LAeq	Noise Reduction		Calc. Minus Goal	
				Calc.	Absolute Criterion	Calc.	Relative Criterion			Calc.	Goal		
				dBA	dBA	dBA	dBA		dBA	dBA	dBA	dBA	dBA
Receiver-1	1	1	52.8	56.6	0.0	3.8	10.0	Sound Level	56.6	0.0	8.0	-8.0	
Receiver-2	2	1	58.5	58.0	0.0	-0.5	10.0	Sound Level	58.0	0.0	8.0	-8.0	
Receiver-3	3	1	57.0	53.2	0.0	-3.8	10.0	Sound Level	53.2	0.0	8.0	-8.0	

## Section 6



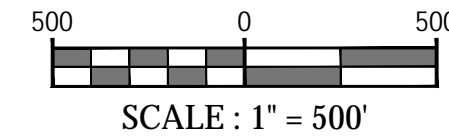


**TOWN OF WAWAYANDA TAX MAP**  
SCALE: 1" = 500'  
SOURCE: ORANGE COUNTY, NY TAX MAP



**SITE LOCATION MAP**

SOURCE: NEW YORK STATE CLEARING HOUSE



# PRELIMINARY SITE PLANS FOR DEWPOINT SOUTH SECTION 4, BLOCK 1, LOT 50.32 TOWN OF WAWAYANDA ORANGE COUNTY, NEW YORK STATE

**GENERAL INFORMATION**

- THE SUBJECT PROPERTY IS KNOWN AS SECTION 4, BLOCK 1, LOT 50.32 IN THE TOWN OF WAWAYANDA ORANGE COUNTY, NEW YORK.
- THE PROPERTY IS LOCATED IN THE MC-1 (MIXED COMMERCIAL) ZONE DISTRICT AND CONTAINS A TOTAL TRACT AREA OF 507.975 SF, 11.66 ACRES.  
OWNER/APPLICANT: DEWPOINT DEVELOPMENT LLC  
1 INTERNATIONAL BOULEVARD - SUITE 410  
MAHWAH, NEW JERSEY 07430  
GDRP 271 LLC  
2718 65<sup>TH</sup> STREET,  
BROOKLYN, NEW YORK 11204
- BOUNDARY AND TOPOGRAPHIC INFORMATION SHOWN HEREON IS TAKEN FROM A PLAN ENTITLED "OUTBOUND & TOPOGRAPHIC SURVEY PLAN FOR DOLSONTOWN ROAD SECTION 4, BLOCK 1, LOT 50.32" AND PREPARED BY JOHN W. MCCORD, SR. DATED JANUARY 25, 2021, LAST REVISED SEPTEMBER 01, 2021.
- THE HORIZONTAL DATUM IS RELATIVE TO NAD83. THE VERTICAL DATUM IS RELATIVE TO N.A.V.D. 1988.
- THE LIMITS OF FRESHWATER WETLANDS SHOWN HEREON WERE FIELD DELINEATED BY COLLIERS ENGINEERING & DESIGN ON NOVEMBER 3, 2021 AND A PRECONSTRUCTION NOTIFICATION APPLICATION TO THE ARMY CORPS OF ENGINEERS TO VERIFY THE SAME IS PENDING.
- NO 100 YEAR FLOOD PLAINS ARE KNOWN TO EXIST ON THE SITE PER THE FLOOD INSURANCE RATE MAPS 36071C0266E DATED 8/03/2009 PREPARED BY THE FEDERAL EMERGENCY MANAGEMENT AGENCY.
- THIS SET OF PLANS IS NOT DEPICTING ENVIRONMENTAL CONDITIONS OR A CERTIFICATION/WARRANTY REGARDING THE PRESENCE OR ABSENCE OF ENVIRONMENTALLY IMPACTED SITE CONDITIONS. COLLIERS ENGINEERING & DESIGN HAS PERFORMED NO EXPLORATORY OR TESTING SERVICES, INTERPRETATIONS, CONCLUSIONS OR OTHER SITE ENVIRONMENTAL SERVICES RELATED TO THE DETERMINATION OF THE POTENTIAL FOR CHEMICAL, TOXIC, RADIOACTIVE OR OTHER TYPE OF CONTAMINANTS AFFECTING THE PROPERTY AND THE UNDERSIGNED PROFESSIONAL IS NOT QUALIFIED TO DETERMINE THE EXISTENCE OF SAME. SHOULD ENVIRONMENTAL CONTAMINATION OR WASTE BE DISCOVERED, THE OWNER AND CONTRACTOR SHALL BE RESPONSIBLE FOR COMPLYING WITH ALL APPLICABLE LAWS AND REGULATIONS.
- THIS IS A SITE DEVELOPMENT PLAN AND UNLESS SPECIFICALLY NOTED ELSEWHERE HEREON, IS NOT A SURVEY.
- DO NOT SCALE DRAWINGS AS THEY PERTAIN TO ADJACENT AND SURROUNDING PHYSICAL CONDITIONS, BUILDINGS, STRUCTURES, ETC. THEY ARE SCHEMATIC ONLY, EXCEPT WHERE DIMENSIONS ARE SHOWN THERETO.
- THIS SET OF PLANS HAS BEEN PREPARED FOR THE PURPOSES OF MUNICIPAL AND AGENCY REVIEW AND APPROVAL. THIS SET OF PLANS SHALL NOT BE UTILIZED AS CONSTRUCTION DOCUMENTS UNTIL ALL APPROVALS REQUIRED HAVE BEEN OBTAINED. ALL CONDITIONS OF APPROVAL HAVE BEEN SATISFIED AND THE DRAWINGS HAVE BEEN STAMPED "ISSUED FOR CONSTRUCTION". THIS SHALL INCLUDE APPROVAL OF ALL CATALOG CUTS, SHOP DRAWINGS AND/OR DESIGN CALCULATIONS AS REQUIRED BY THE PROJECT OWNER AND/OR MUNICIPAL ENGINEER.
- THE CONTRACTOR IS RESPONSIBLE FOR PROJECT SAFETY, INCLUDING PROVISION OF ALL APPROPRIATE SAFETY DEVICES AND TRAINING REQUIRED.
- PRIOR TO ANY EXCAVATION, THE CONTRACTOR SHALL CALL 811 TO REQUEST A UTILITY MARKOUT.
- INFORMATION HEREON INCORPORATES THE CONTENT IN THE FOLLOWING REPORTS:  
- "STORMWATER POLLUTION PREVENTION PLAN (SWPPP) PREPARED FOR DEWPOINT DEVELOPMENT LLC" BY COLLIERS ENGINEERING & DESIGN, DATED JANUARY 2023.

**SITE NOTES**

- BUILDING FOOTPRINT DIMENSIONS SHOWN HEREON ARE APPROXIMATE. FINAL BUILDING FOOTPRINT DIMENSIONS FOR THE BUILDING SHALL BE FURNISHED ON THE INDIVIDUAL ARCHITECTURAL PLANS AT THE TIME OF APPLICATION FOR A BUILDING PERMIT. ALL STRUCTURES SHALL CONFORM TO THE APPROVED BULK ZONING REQUIREMENTS.
- CURBS SHALL BE DEPRESSED FLUSH WITH PAVEMENT, AND HANDICAP ACCESSIBLE RAMPS INSTALLED WHERE SIDEWALKS AND CROSSWALKS INTERSECT SAME. DETECTABLE WARNINGS SHALL BE INCLUDED ON HANDICAP ACCESSIBLE RAMPS.
- TRAFFIC SIGNAGE AND STRIPING SHALL CORRESPOND TO THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES.
- REFUSE AND RECYCLABLES SHALL BE STORED WITHIN OUTDOOR ROLL-OFF CONTAINERS AND PICKED UP BY PRIVATE WASTE DISPOSAL HAULER.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROPER DISPOSAL OF ALL WASTE MATERIALS IN ACCORDANCE WITH GOVERNING REGULATIONS AND AGENCIES.
- THERE SHALL BE NO ON-SITE BURIAL OF CONSTRUCTION MATERIALS, TREE BRANCHES, STUMPS, OR OTHER DELETERIOUS MATERIALS.
- MATERIALS, WORKMANSHIP, AND CONSTRUCTION FOR THE SITE IMPROVEMENTS SHOWN HEREON SHALL BE IN ACCORDANCE WITH:  
A. NEW YORK STATE DEPARTMENT OF TRANSPORTATION "STANDARD SPECIFICATIONS", 2018 AS SUPPLEMENTED.  
B. CURRENT PREVAILING MUNICIPAL, COUNTY, AND/OR STATE AGENCY SPECIFICATIONS, STANDARDS, CONDITIONS, AND REQUIREMENTS.  
C. CURRENT PREVAILING UTILITY COMPANY/AUTHORITY SPECIFICATIONS, STANDARDS, AND REQUIREMENTS.  
D. CURRENT MANUFACTURER SPECIFICATIONS, STANDARDS, AND REQUIREMENTS.

**UTILITY NOTES**

- EXISTING UTILITY INFORMATION SHOWN HEREON HAS BEEN COLLECTED FROM VARIOUS SOURCES AND IS NOT GUARANTEED AS TO ACCURACY OR COMPLETENESS. THE CONTRACTOR SHALL VERIFY ALL INFORMATION TO HIS SATISFACTION PRIOR TO EXCAVATION. WHERE EXISTING UTILITIES ARE TO BE CROSSED BY PROPOSED CONSTRUCTIONS, TEST PITS SHALL BE DUG BY THE CONTRACTOR PRIOR TO CONSTRUCTION TO ASCERTAIN EXISTING INVERTS, MATERIALS, AND SIZES. TEST PIT INFORMATION SHALL BE GIVEN TO THE ENGINEER PRIOR TO CONSTRUCTION TO PERMIT ADJUSTMENTS AS REQUIRED TO AVOID CONFLICTS. THE CONTRACTOR SHALL NOTIFY THE UNDERSIGNED PROFESSIONAL IMMEDIATELY IF ANY FIELD CONDITIONS ENCOUNTERED DIFFER MATERIALLY FROM THOSE REPRESENTED HEREON. SUCH CONDITIONS COULD RENDER THE DESIGNS HEREON INAPPROPRIATE OR INEFFECTIVE.
- UTILITY RELOCATIONS SHOWN HEREON, IF ANY, ARE FOR INFORMATIONAL PURPOSES ONLY AND MAY NOT REPRESENT ALL REQUIRED UTILITY RELOCATIONS. THE CONTRACTOR IS RESPONSIBLE FOR PERFORMING AND/OR COORDINATING ALL REQUIRED UTILITY RELOCATIONS IN COOPERATION WITH THE RESPECTIVE UTILITY COMPANY/AUTHORITIES.
- STORM SEWERS SHALL BE CLASS III (OR HIGHER IF NOTED) REINFORCED CONCRETE PIPE (RCP) WITH "O" RING GASKETS OR INTERNALLY PRELUBRICATED GASKET (TYLOX SUPERSEAL OR EQUIVALENT, ADS N-12 HIGH DENSITY POLYETHYLENE PIPE (HDPE), AS NOTED ON THE PLAN, OR APPROVED EQUAL. PROPER PIPE COVERAGE SHALL BE MAINTAINED DURING ALL PHASES OF CONSTRUCTION. PIPE LENGTHS SHOWN HEREON ARE FROM CENTER OF STRUCTURE TO CENTER OF STRUCTURE.
- WATER SERVICE TO BE PROVIDED FROM THE EXISTING WATER MAIN LINE ON DOLSONTOWN ROAD, OWNED AND OPERATED BY THE TOWN OF WAWAYANDA WATER DEPARTMENT. PROPOSED WATER MAIN EXTENSIONS AND FIRE HYDRANT LOCATIONS ARE SUBJECT TO MUNICIPAL REVIEW AND APPROVAL. PIPE MATERIALS SHALL BE CEMENT LINED DUCTILE IRON PIPE, CLASS 52 AS NOTED ON THE PLANS. WATER MAINS SHALL BE INSTALLED TO PROVIDE A MINIMUM 4'-6" OF COVER FROM THE TOP OF PIPE TO THE PROPOSED GRADE.
- SANITARY SEWER SERVICE SHALL BE PROVIDED BY GRAVITY CONNECTION TO EXISTING SEWER MAIN ON DOLSONTOWN ROAD, OWNED AND OPERATED BY THE TOWN OF WAWAYANDA SEWER DEPARTMENT. PROPOSED SEWER MAIN EXTENSIONS AND MANHOLE LOCATIONS ARE SUBJECT TO MUNICIPAL REVIEW AND APPROVAL. PIPE MATERIALS SHALL BE PVC SDR-35, EXCEPT AS NOTED OTHERWISE ON THE PLANS. EXCEPT WHERE SHALLOWER DEPTHS ARE PERMITTED BY THE MUNICIPALITY OR UTILITY AUTHORITY, SEWER LINES, INCLUDING FORCE MAINS AND LATERALS, SHALL BE INSTALLED TO PROVIDE A MINIMUM 4 FEET OF COVER FROM THE TOP OF PIPE TO PROPOSED GRADE.
- ALL WATER MAINS SHOULD BE SEPARATED FROM SANITARY SEWER AND INDUSTRIAL DISCHARGE LINES BY A MINIMUM HORIZONTAL DISTANCE OF 10 FEET. IF SUCH HORIZONTAL SEPARATION IS NOT POSSIBLE, THE WATER AND SEWER LINES SHALL BE IN SEPARATE TRENCHES (STEP TRENCHES ARE PROHIBITED) WITH THE TOP OF THE SEWER LINE AT LEAST 18 INCHES BELOW THE BOTTOM OF THE WATER MAIN ENCASED IN CONCRETE OR WITH SUCH SEPARATION EXPRESSLY APPROVED BY THE DEPARTMENT OF HEALTH.
- AT THE CROSSINGS OF SEWER LINES AND WATER MAINS, THE TOP OF THE SEWER LINES SHALL BE AT LEAST 18 INCHES BELOW THE BOTTOM OF THE WATER MAIN SUBJECT TO APPROVAL BY THE PROJECT ENGINEER. IF SUCH VERTICAL SEPARATION IS NOT POSSIBLE, THE WATER LINE SHALL BE ENCASED IN CONCRETE.
- GAS, ELECTRIC, LIGHTING, CABLE TELEVISION, AND ELECTRICAL SERVICE PLANS, IF REQUIRED, SHALL BE PREPARED BY THE RESPECTIVE UTILITY COMPANIES THAT SERVICE THE AREA PRIOR TO SITE CONSTRUCTION AND SHALL BE INSTALLED PER ORDINANCE OR LOCAL UTILITY COMPANIES REQUIREMENTS.
- TELEPHONE, ELECTRIC, AND GAS LINES WILL BE INSTALLED UNDERGROUND. CROSSINGS OF PROPOSED PAVEMENTS WILL BE INSTALLED PRIOR TO THE CONSTRUCTION OF PAVEMENT BASE COURSE.

**Colliers**  
Engineering & Design  
www.colliersengineering.com

Copyright © 2023 Colliers Engineering & Design. All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, reprinted, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER** CONSULTANTS

**811** PROTECT YOURSELF  
ALL STATES REQUIRE NOTIFICATION OF EXCAVATIONS, DISBURSERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
Know what's below. Call before you dig.  
FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DRAWN BY	DESCRIPTION
1	02/09/22	CDR	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GES SUBMISSION
2	01/17/23	CDR	REVISED PER PLANNING BOARD COMMENTS

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
NEW YORK LICENSED PROFESSIONAL ENGINEER  
LICENSE NUMBER: 103788  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
N.Y. C.O.A.#: 0077609

**PRELIMINARY SITE PLANS**  
FOR  
**DEWPOINT SOUTH**  
  
SECTION 4  
BLOCK 1  
LOT 50.32  
  
TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK STATE

**Colliers** 555 Hudson Valley Avenue  
Suite 101  
New Windsor, NY 12553  
Phone: 845.644.4495  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
DOING BUSINESS AS MASER CONSULTING  
ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN	DATE: 01/10/2022	DRAWN BY: SMB	CHECKED BY: CDR
-----------------	------------------	---------------	-----------------

PROJECT NUMBER: 20009912A	DRAWING NAME: C-COVER-SOUTH
---------------------------	-----------------------------

SHEET TITLE  
**COVER SHEET**

SHEET NUMBER  
**01 of 17**

2023/01/10 12:41 PM C:\Users\kellyb\OneDrive\Documents\Projects\DEWPOINT SOUTH\DWG\C1-COVER.dwg BY: KELLY BARRER







**BULK TABLE**

ZONING DISTRICT: MC-1 (MIXED COMMERCIAL)  
SPECIAL USE SUBJECT TO SITE PLAN APPROVAL - WAREHOUSE

MINIMUM	REQUIRED	EXISTING	PROPOSED	REMARKS
LOT AREA	2 ACRES	11.66 ACRES (507,975 SQ.FT.)	11.58 ACRES (504,790 SQ. FT.)	OK
FRONT YARD SETBACK	50 FEET	N/A	50.93 FEET (DOLSONTOWN RD) 94.21 FEET (CASKEY LANE)	OK
REAR YARD SETBACK	30 FEET	N/A	61.65 FEET	OK
SIDE YARD SETBACK				
ONE	15 FEET	N/A	245.66 FEET	OK
BOTH	N/A	N/A	N/A	OK
LOT WIDTH	100 FEET	N/A	930 FEET	OK
MAXIMUM				
BUILDING HEIGHT	65 FEET	N/A	55 FEET	OK
LOT COVERAGE	70%	N/A	50.6% (±255,040 SQ. FT.)	OK
BUILDING COVERAGE	50%	N/A	24.6% (125,000 SQ. FT.)	OK

**PARKING REQUIREMENTS:**

OFFICE USE:  
1 PER 300 SF OF FLOOR AREA  
5,000 SF = 17 SPACES REQUIRED

WAREHOUSE USE:  
1 PER 5,000 SF OF FLOOR AREA (ESTIMATED NEED PER APPLICANT)  
125,000 SF = 25 SPACES REQUIRED

TOTAL PARKING REQUIRED = 42 SPACES  
TOTAL PARKING PROVIDED = 65 SPACES

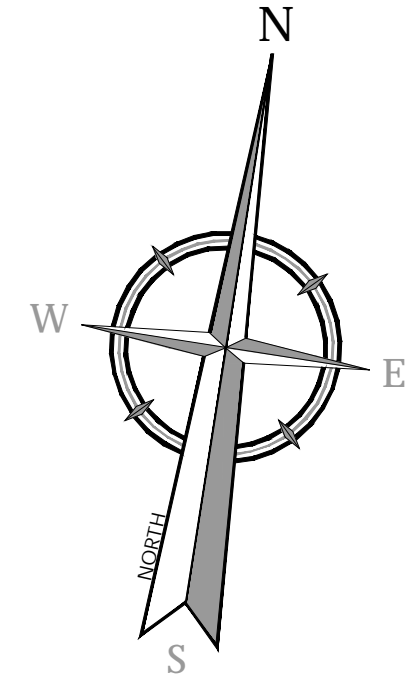
NOTE:  
1. ITE PARKING GENERATION MANUAL:  
WAREHOUSING USE - AVERAGE RATE OF 0.39 SPACES PER 1,000 S.F. GROSS FLOOR AREA  
125,000 GROSS SQ. FT. / 1,000 X 0.39 = 49 SPACES

**TAX LOT:**

4-1-50.32  
±507,975 SQ. FT.  
±11.66 ACRES

**OWNER/APPLICANT:**

DEWPOINT DEVELOPMENT LLC.  
1 INTERNATIONAL BOULEVARD - SUITE 410  
MAHWAH, NEW JERSEY 07430  
GDBP 2171 LLC.  
2118 61<sup>ST</sup> STREET  
BROOKLYN, NEW YORK 11204

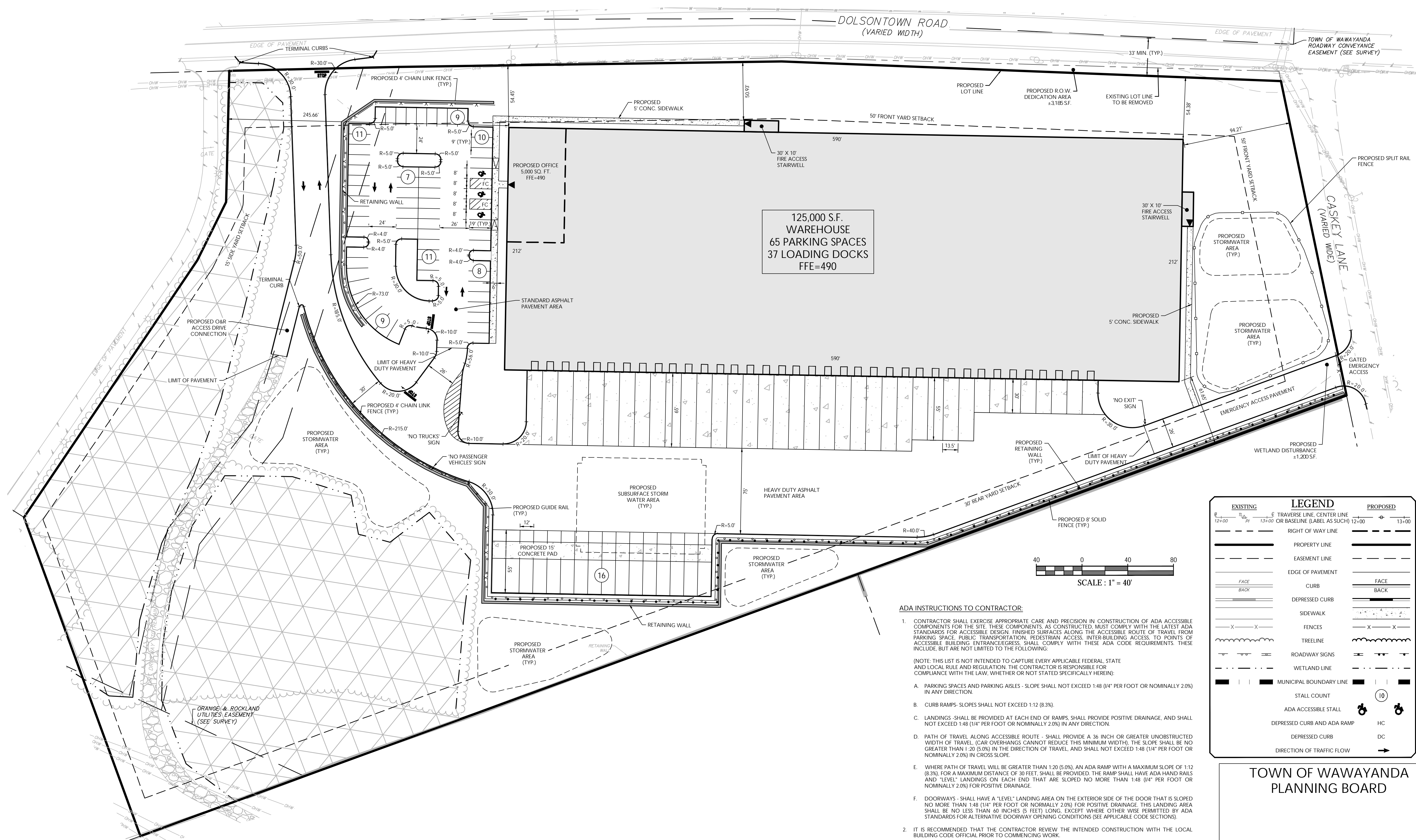


**Colliers**  
Engineering & Design  
www.colliersengineering.com

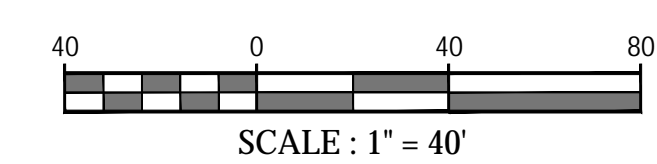
Copyright © 2022 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, redrawn, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER** CONSULTANTS

**811** PROTECT YOURSELF  
ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DESIGNERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
Know what's below. Call before you dig.  
FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM



125,000 S.F. WAREHOUSE  
65 PARKING SPACES  
37 LOADING DOCKS  
FFE=490



EXISTING	LEGEND	PROPOSED
12+00	TRaverse LINE, CENTER LINE OR BASELINE (LABEL AS SUCH) 12+00	13+00
---	RIGHT OF WAY LINE	---
---	PROPERTY LINE	---
---	EASEMENT LINE	---
---	EDGE OF PAVEMENT	---
---	CURB	---
---	DEPRESSED CURB	---
---	SIDEWALK	---
---	FENCES	---
---	TREELINE	---
---	ROADWAY SIGNS	---
---	WETLAND LINE	---
---	MUNICIPAL BOUNDARY LINE	---
---	STALL COUNT	10
---	ADA ACCESSIBLE STALL	♿
---	DEPRESSED CURB AND ADA RAMP	HC
---	DEPRESSED CURB	DC
---	DIRECTION OF TRAFFIC FLOW	→

**ADA INSTRUCTIONS TO CONTRACTOR:**

- CONTRACTOR SHALL EXERCISE APPROPRIATE CARE AND PRECISION IN CONSTRUCTION OF ADA ACCESSIBLE COMPONENTS FOR THE SITE. THESE COMPONENTS, AS CONSTRUCTED, MUST COMPLY WITH THE LATEST ADA STANDARDS FOR ACCESSIBLE DESIGN. FINISHED SURFACES ALONG THE ACCESSIBLE ROUTE OF TRAVEL FROM PARKING SPACE, PUBLIC TRANSPORTATION, PEDESTRIAN ACCESS, INTER-BUILDING ACCESS, TO POINTS OF ACCESSIBLE BUILDING ENTRANCE/EGRESS, SHALL COMPLY WITH THESE ADA CODE REQUIREMENTS. THESE INCLUDE, BUT ARE NOT LIMITED TO THE FOLLOWING:
  - PARKING SPACES AND PARKING AISLES - SLOPE SHALL NOT EXCEED 1:48 (1/4" PER FOOT OR NOMINALLY 2.0%) IN ANY DIRECTION.
  - CURB RAMPS - SLOPES SHALL NOT EXCEED 1:12 (8.3%).
  - LANDINGS - SHALL BE PROVIDED AT EACH END OF RAMPS, SHALL PROVIDE POSITIVE DRAINAGE, AND SHALL NOT EXCEED 1:48 (1/4" PER FOOT OR NOMINALLY 2.0%) IN ANY DIRECTION.
  - PATH OF TRAVEL ALONG ACCESSIBLE ROUTE - SHALL PROVIDE A 36 INCH OR GREATER UNOBSTRUCTED WIDTH OF TRAVEL (CAR OVERHANGS CANNOT REDUCE THIS MINIMUM WIDTH). THE SLOPE SHALL BE NO GREATER THAN 1:20 (5.0%) IN THE DIRECTION OF TRAVEL, AND SHALL NOT EXCEED 1:48 (1/4" PER FOOT OR NOMINALLY 2.0%) IN CROSS SLOPE.
  - WHERE PATH OF TRAVEL WILL BE GREATER THAN 1:20 (5.0%), AN ADA RAMP WITH A MAXIMUM SLOPE OF 1:12 (8.3%), FOR A MAXIMUM DISTANCE OF 30 FEET, SHALL BE PROVIDED. THE RAMP SHALL HAVE ADA HAND RAILS AND "LEVEL" LANDINGS ON EACH END THAT ARE SLOPED NO MORE THAN 1:48 (1/4" PER FOOT OR NOMINALLY 2.0%) FOR POSITIVE DRAINAGE.
  - DOORWAYS - SHALL HAVE A "LEVEL" LANDING AREA ON THE EXTERIOR SIDE OF THE DOOR THAT IS SLOPED NO MORE THAN 1:48 (1/4" PER FOOT OR NOMINALLY 2.0%) FOR POSITIVE DRAINAGE. THIS LANDING AREA SHALL BE NO LESS THAN 60 INCHES (5 FEET) LONG, EXCEPT WHERE OTHER WISE PERMITTED BY ADA STANDARDS FOR ALTERNATIVE DOORWAY OPENING CONDITIONS (SEE APPLICABLE CODE SECTIONS).
- IT IS RECOMMENDED THAT THE CONTRACTOR REVIEW THE INTENDED CONSTRUCTION WITH THE LOCAL BUILDING CODE OFFICIAL PRIOR TO COMMENCING WORK.

REV.	DATE	DESCRIPTION
1	02/04/22	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIS SUBMISSION
2	01/10/23	REVISED PER PLANNING BOARD COMMENTS

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

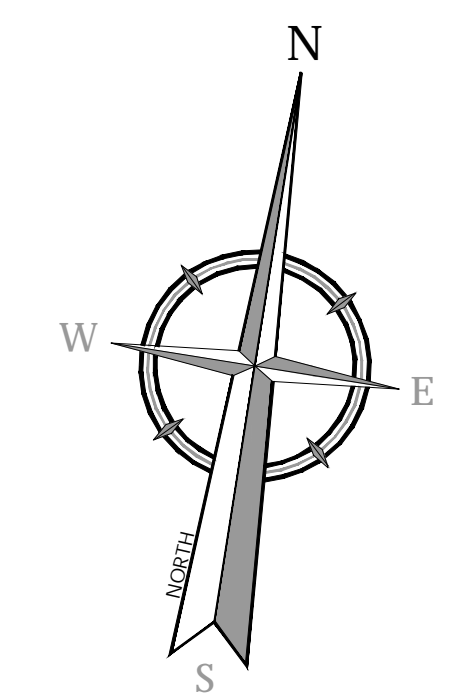
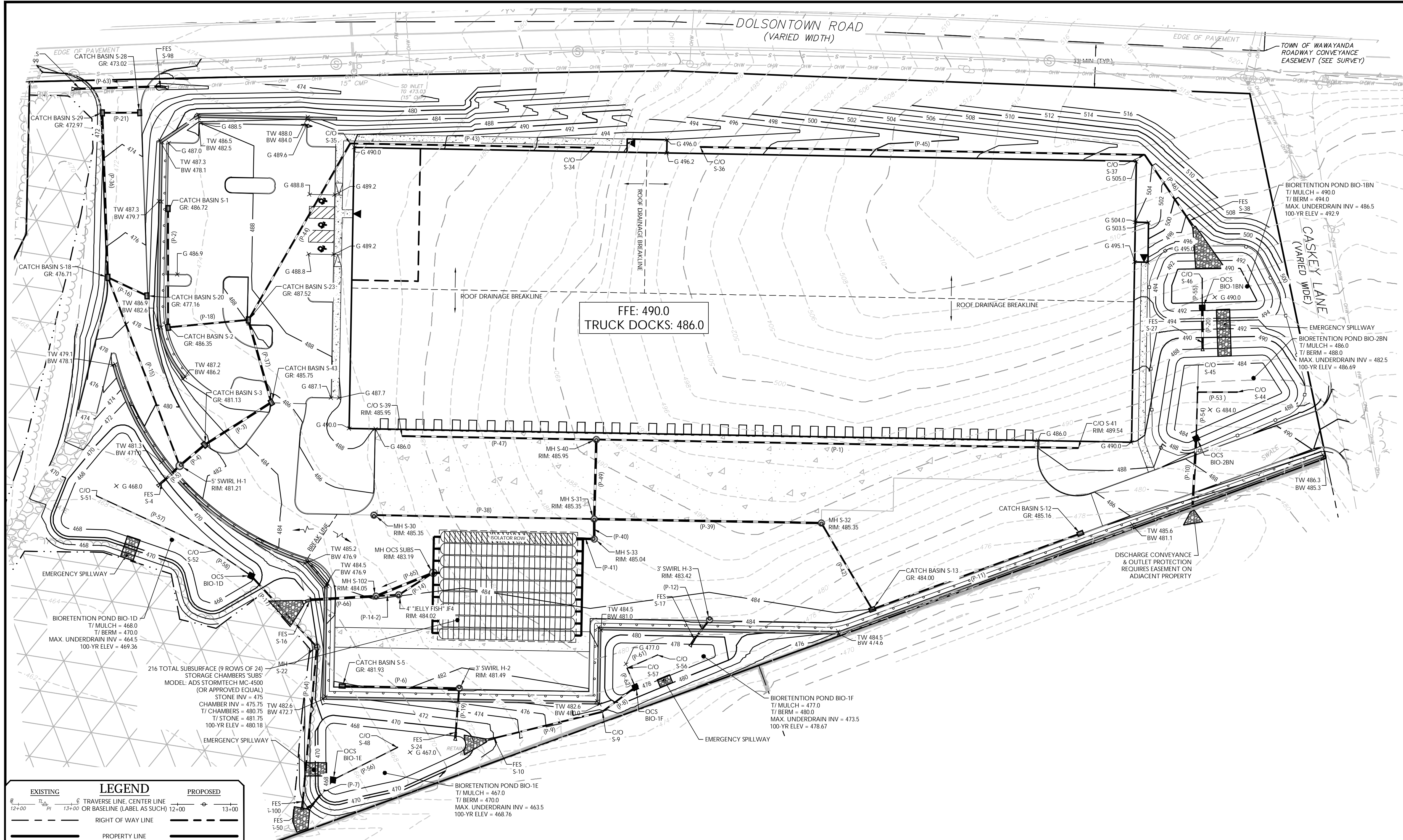
**Cory Daniel Robinson**  
NEW YORK LICENSED PROFESSIONAL ENGINEER  
LICENSE NUMBER: 103788  
COLLIERS ENGINEERING & DESIGN CT. P.C.  
N.Y. C.O.A.#: 0017609

PRELIMINARY SITE PLANS  
FOR  
**DEWPOINT SOUTH**  
SECTION 4  
BLOCK 1  
LOT 50.32  
TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK STATE

**Colliers** 555 Hudson Valley Avenue  
Suite 101  
New Windsor, NY 12553  
Phone: 845.544.4495  
COLLIERS ENGINEERING & DESIGN CT. P.C.  
DOING BUSINESS AS MASER CONSULTANTS  
ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN DATE: 01/10/2022 DRAWN BY: SMB CHECKED BY: CDR  
PROJECT NUMBER: 2000912A DRAWING NUMBER: C-LAY1-SOUTH  
SHEET TITLE: DIMENSION PLAN  
SHEET NUMBER: 03 of 17





**SOUTH drainage Pipe Table**

Pipe I.D.	Description	Length	Invert Up	Invert Dn	Slope
P-1	12" ROOF LEADER	363'	483.64	480.00	1.00%
P-2	12" HDPE	90'	484.00	482.21	2.00%
P-3	18" HDPE	60'	479.70	478.51	2.00%
P-4	18" HDPE	25'	469.51	468.17	5.45%
P-5	18" HDPE	17'	468.17	468.01	0.95%
P-6	12" HDPE	88'	478.00	467.68	11.69%
P-7	12" HDPE	23'	463.50	462.93	2.46%
P-8	12" HDPE	31'	473.50	472.89	1.97%
P-9	12" HDPE	84'	472.89	471.21	2.00%
P-10	18" HDPE	52'	480.50	478.00	4.85%
P-11	12" HDPE	167'	481.68	478.34	2.00%
P-12	12" HDPE	19'	480.62	480.24	2.00%
P-13	12" HDPE	31'	472.00	471.69	1.00%
P-14	12" HDPE	17'	471.19	471.00	1.11%
P-15	12" HDPE	152'	468.78	468.17	0.40%
P-16	12" HDPE	33'	473.75	473.10	2.00%
P-17	12" HDPE	73'	464.50	463.92	0.80%
P-18	12" HDPE	61'	482.21	480.99	2.00%
P-19	12" HDPE	33'	467.68	467.00	2.04%
P-20	18" HDPE	26'	483.15	482.62	2.00%
P-21	12" HDPE	28'	470.30	470.02	1.00%
P-36	12" HDPE	124'	470.02	468.78	1.00%
P-37	18" HDPE	65'	480.99	479.70	2.00%
P-38	12" TRENCH DRAIN	166'	481.30	477.98	2.00%
P-39	18" TRENCH DRAIN	771'	482.50	479.07	2.00%
P-40	18" HDPE	15'	478.80	477.90	5.92%
P-41	18" HDPE	13'	477.90	476.46	10.89%
P-42	12" HDPE	76'	478.34	476.83	2.00%
P-43	12" ROOF LEADER	184'	492.50	488.82	2.00%
P-44	12" HDPE	154'	488.82	485.75	2.00%
P-45	12" ROOF LEADER	335'	494.00	487.29	2.00%
P-46	12" HDPE	60'	487.29	486.09	2.00%
P-47	12" ROOF LEADER	147'	482.93	480.00	2.00%
P-49	18" HDPE	60'	480.00	478.80	2.00%
P-53	8" PVC UNDERDRAIN	30'	480.50	480.50	0.00%
P-54	8" PVC UNDERDRAIN	35'	480.50	480.50	0.00%
P-55	6" PVC UNDERDRAIN	22'	486.50	486.50	0.00%
P-56	6" PVC UNDERDRAIN	55'	463.50	463.50	0.00%
P-57	6" PVC UNDERDRAIN	98'	464.50	464.50	0.00%
P-58	6" PVC UNDERDRAIN	34'	464.50	464.50	0.00%
P-61	6" PVC UNDERDRAIN	25'	473.50	473.50	0.00%
P-62	6" PVC UNDERDRAIN	16'	473.50	473.50	0.00%
P-63	15" HDPE	61'	471.00	468.50	4.12%
P-64	12" HDPE	117'	463.92	462.98	0.80%
P-65	18" HDPE	47'	478.50	477.56	2.02%
P-66	18" HDPE	49'	470.75	470.00	1.52%

**LEGEND**

EXISTING      PROPOSED

TRANSVERSE LINE, CENTER LINE 12+00  
OR BASELINE (LABEL AS SUCH) 12+00

RIGHT OF WAY LINE 13+00

PROPERTY LINE

EDGE OF PAVEMENT

FACE CURB

DEPRESSED CURB

SIDEWALK

FENCES

TREELINE

ROADWAY SIGNS

WETLAND LINE

MUNICIPAL BOUNDARY LINE

B' INLET

E' INLET

STORM MANHOLE

SANITARY MANHOLE

FLARED END SECTION

HEADWALL

HYDRANT

POLE MOUNTED LIGHT

CONTOURS

SPOT ELEVATION

DIRECTION OF OVERLAND FLOW

TOP OF CURB ELEVATION

BOTTOM OF CURB ELEVATION

TOP OF DEPRESSED CURB ELEVATION

**SOUTH drainage Structure Table**

Structure I.D.	Description	Rim/Grate	Pipes (In)	Inverts (In)	Pipes (Out)	Inverts (Out)
BIO-1B	48 in. x 48 in. OCS	492.50	6" PVC UNDERDRAIN	486.50	18" HDPE	483.15
BIO-1D	48 in. x 48 in. OCS	468.60	6" PVC UNDERDRAIN	464.50	12" HDPE	464.50
BIO-1E	48 in. x 48 in. OCS	468.50	6" PVC UNDERDRAIN	463.50	12" HDPE	463.50
BIO-1F	48 in. x 48 in. OCS	478.50	6" PVC UNDERDRAIN	473.50	12" HDPE	473.50
BIO-2B	48 in. x 48 in. OCS	486.50	8" PVC UNDERDRAIN	480.50	18" HDPE	480.50
H-1	60 in. dia. CYLINDER MH	481.21	18" HDPE	468.17	18" HDPE	468.17
H-2	48 in. dia. CYLINDER MH	481.49	12" HDPE	467.68	12" HDPE	467.68
H-3	48 in. dia. CYLINDER MH	483.42	12" HDPE	480.62	12" HDPE	480.62
JF4	48 in. dia. CYLINDER MH	484.02	12" HDPE	471.69	12" HDPE	471.19
OCS SUBS	60 in. dia. CYLINDER MH	483.19	12" HDPE	472.00	12" HDPE	472.00
S-1	30 in. x 48 in. Catch Basin	486.72	12" HDPE	484.00	12" HDPE	484.00
S-2	30 in. x 48 in. Catch Basin	486.35	12" HDPE	482.21	12" HDPE	482.21
S-3	30 in. x 48 in. Catch Basin	481.13	18" HDPE	478.51	18" HDPE	469.51
S-4	12 inch Flared End Section	469.54	18" HDPE	468.01	18" HDPE	478.00
S-5	30 in. x 48 in. Catch Basin	481.93	12" HDPE	478.00	12" HDPE	478.00
S-9	12 in. Clean Out	477.56	12" HDPE	472.89	12" HDPE	472.89
S-10	12 inch Flared End Section	473.76	12" HDPE	471.21	12" HDPE	471.21
S-12	30 in. x 48 in. Catch Basin	485.16	12" HDPE	481.68	12" HDPE	481.68
S-13	30 in. x 48 in. Catch Basin	484.00	12" HDPE	478.34	12" HDPE	478.34
S-16	18 inch Flared End Section	471.63	18" HDPE	470.00	18" HDPE	470.00

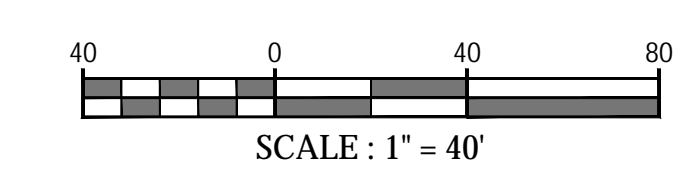
**SOUTH drainage Structure Table**

Structure I.D.	Description	Rim/Grate	Pipes (In)	Inverts (In)	Pipes (Out)	Inverts (Out)
S-17	12 inch Flared End Section	481.34	12" HDPE	480.24		
S-18	30 in. x 48 in. Catch Basin	476.71	12" HDPE	468.78	12" HDPE	468.78
S-20	30 in. x 48 in. Catch Basin	477.16	12" HDPE	473.10	12" HDPE	473.75
S-22	48 in. dia. CYLINDER MH	469.72	12" HDPE	463.92	12" HDPE	463.92
S-23	30 in. x 48 in. Catch Basin	487.52	12" HDPE	480.99	18" HDPE	480.99
S-24	12 inch Flared End Section	465.62	12" HDPE	467.00		
S-27	12 inch Flared End Section	484.15	18" HDPE	482.62		
S-28	30 in. x 48 in. Catch Basin	473.02	12" HDPE	470.00	12" HDPE	470.30
S-29	30 in. x 48 in. Catch Basin	472.97	12" HDPE	470.02	12" HDPE	470.02
S-30	48 in. dia. CYLINDER MH	485.35	12" TRENCH DRAIN	481.30	12" TRENCH DRAIN	481.30
S-31	48 in. dia. CYLINDER MH	485.35	12" TRENCH DRAIN	477.98	18" HDPE	478.80
S-32	48 in. dia. CYLINDER MH	485.35	12" HDPE	476.83	18" TRENCH DRAIN	482.50
S-33	48 in. dia. CYLINDER MH	485.04	18" HDPE	477.90	18" HDPE	477.90
S-34	6 in. Clean Out	495.28	12" ROOF LEADER	492.50		
S-35	6 in. Clean Out	489.92	12" ROOF LEADER	488.82	12" HDPE	488.82
S-36	6 in. Clean Out	496.72	12" ROOF LEADER	494.00		
S-37	6 in. Clean Out	504.50	12" ROOF LEADER	487.29	12" HDPE	487.29
S-38	12 inch Flared End Section	494.13	12" HDPE	486.09		
S-39	6 in. Clean Out	485.95	12" ROOF LEADER	482.93		
S-40	48 in. dia. CYLINDER MH	485.95	12" ROOF LEADER	480.00	18" HDPE	480.00

**SOUTH drainage Structure Table**

Structure I.D.	Description	Rim/Grate	Pipes (In)	Inverts (In)	Pipes (Out)	Inverts (Out)
S-41	6 in. Clean Out	489.54		480.00	12" ROOF LEADER	483.64
S-43	30 in. x 48 in. Catch Basin	485.75		479.70	18" HDPE	479.70
S-44	6 in. Clean Out	484.00		480.50	8" PVC UNDERDRAIN	480.50
S-45	6 in. Clean Out	484.00	8" PVC UNDERDRAIN	480.50	8" PVC UNDERDRAIN	480.50
S-46	6 in. Clean Out	490.00		486.50	6" PVC UNDERDRAIN	486.50
S-48	6 in. Clean Out	467.00		463.50	6" PVC UNDERDRAIN	463.50
S-50	12 inch Flared End Section	464.03	12" HDPE	462.93		
S-51	6 in. Clean Out	468.00		464.50	6" PVC UNDERDRAIN	464.50
S-52	6 in. Clean Out	468.00		464.50	6" PVC UNDERDRAIN	464.50
S-56	6 in. Clean Out	477.00		473.50	6" PVC UNDERDRAIN	473.50
S-57	6 in. Clean Out	477.00	6" PVC UNDERDRAIN	473.50	6" PVC UNDERDRAIN	473.50
S-98	15 inch Flared End Section	469.78		471.00	15" HDPE	471.00
S-99	15 inch Flared End Section	468.56	15" HDPE	468.50		
S-100	12 inch Flared End Section	462.19	12" HDPE	462.98		
S-102	48 in. dia. CYLINDER MH	484.05	12" HDPE	471.00	18" HDPE	470.75

- GRADING NOTES:**
- PROPOSED GRADE ELEVATIONS SHOWN AT BUILDING LINE ARE GROUND ELEVATIONS.
  - PROPOSED SPOT ELEVATIONS IN PAVEMENT AREAS ARE TOP OF FINISHED PAVEMENT.
  - PROVIDE POSITIVE DRAINAGE AWAY FROM BUILDING FOUNDATION.



**TOWN OF WAWAYANDA PLANNING BOARD**

**Colliers Engineering & Design**

www.colliersengineering.com

Copyright © 2023 Colliers Engineering & Design. All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, distributed or used for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF. ALL STATES REQUIRE NOTIFICATION OF EXCAVATIONS, DISBURSERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE. Know what's below. Call before you dig. FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DRAWN BY	DESCRIPTION
1	02/04/22	CDR	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIS SUBMISSION
2	01/10/23	CDR	REVISED PER PLANNING BOARD COMMENTS

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
NEW YORK LICENSED PROFESSIONAL ENGINEER  
LICENSE NUMBER: 103788  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
N.Y. C.O.A.#: 0017609

**PRELIMINARY SITE PLANS**

FOR **DEWPOINT SOUTH**

SECTION 4  
BLOCK 1  
LOT 50.32

TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK STATE

**Colliers Engineering & Design**

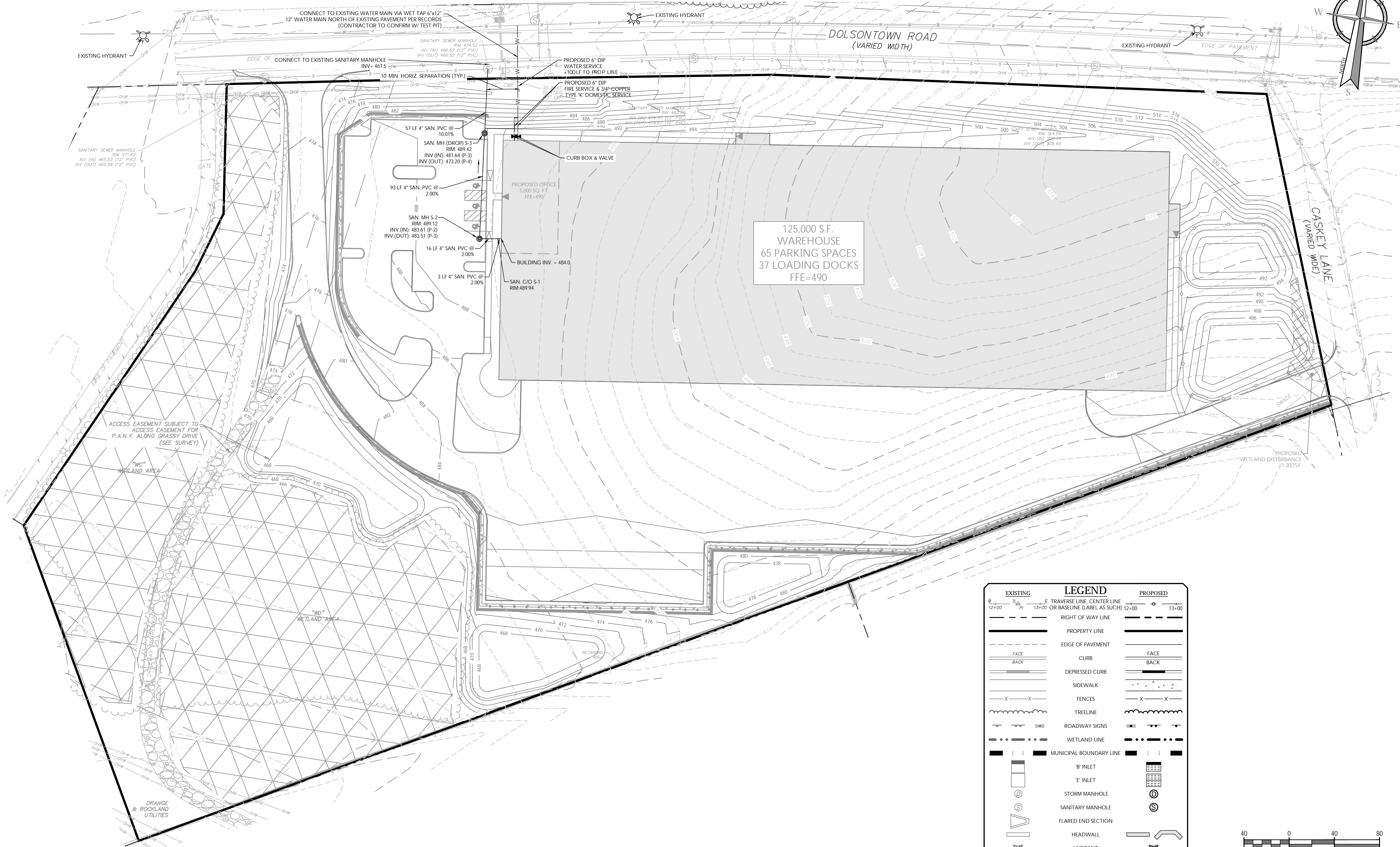
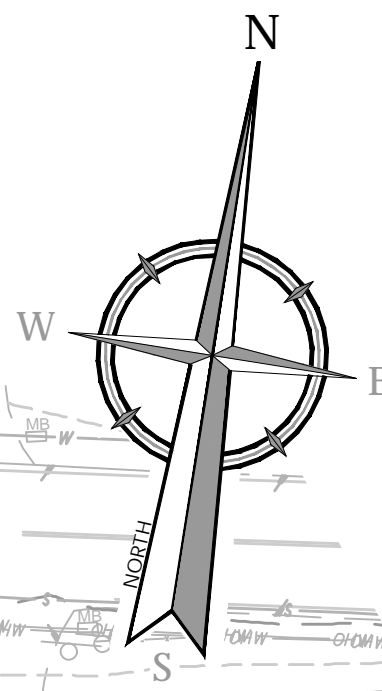
NEWBURGH  
555 Hudson Valley Avenue  
Suite 101  
New Windsor, NY 12553  
Phone: 845.564.4495  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
DOING BUSINESS AS MASER CONSULTANTS  
ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN      DATE: 01/10/2022      DRAWN BY: SMB      CHECKED BY: CDR  
PROJECT NUMBER: 20009912A      DRAWING NUMBER: C-GRAD-SOUTH

SHEET TITLE: **GRADING PLAN - SOUTH**

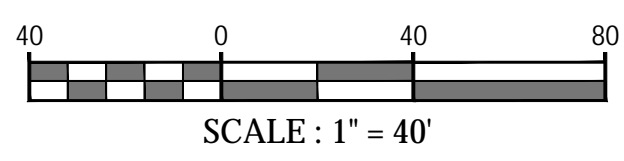
SHEET NUMBER: **04 of 17**





125,000 S.F.  
WAREHOUSE  
65 PARKING SPACES  
37 LOADING DOCKS  
FFE=490

EXISTING	LEGEND	PROPOSED
	TRAVERSE LINE, CENTER LINE OR BASELINE (LABEL AS SUCH)	
	RIGHT OF WAY LINE	
	PROPERTY LINE	
	EDGE OF PAVEMENT	
	CURB	
	DEPRESSED CURB	
	SIDEWALK	
	FENCES	
	TREELINE	
	ROADWAY SIGNS	
	WETLAND LINE	
	MUNICIPAL BOUNDARY LINE	
	8" INLET	
	15" INLET	
	STORM MANHOLE	
	SANITARY MANHOLE	
	FLARED END SECTION	
	HEADWALL	
	HYDRANT	
	POLE MOUNTED LIGHT	
	CABLE TV CONDUIT	
	WATER MAIN	
	GAS MAIN	
	TELEPHONE CONDUIT	
	ELECTRIC CONDUIT	
	SANITARY PIPE	
	STORM PIPE	



TOWN OF WAWAYANDA  
PLANNING BOARD

REV.	DATE	DRAWN BY	DESCRIPTION
1	02/04/22	CDR	REVISED PER PLANNING BOARD COMMENTS
2	01/10/23	CDR	REVISED PER PLANNING BOARD COMMENTS

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
NEW YORK LICENSED PROFESSIONAL ENGINEER  
LICENSE NUMBER: 103788  
COLLIERS ENGINEERING & DESIGN CT. P.C.  
N.Y. C.O.A. #: 0017609

PRELIMINARY SITE PLANS  
FOR  
DEWPOINT SOUTH

SECTION 4  
BLOCK 1  
LOT 50.32  
TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK STATE

**Colliers** NEWBURGH  
555 Hudson Valley Avenue  
Suite 101  
New Windsor, NY 12553  
Phone: 845.644.4495  
COLLIERS ENGINEERING & DESIGN CT. P.C.  
DOING BUSINESS AS MASER CONSULTING  
ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN DATE: 01/10/2022 DRAWN BY: SMB CHECKED BY: CDR  
PROJECT NUMBER: 20000912A DRAWING NAME: C-UTIL\_S0TH

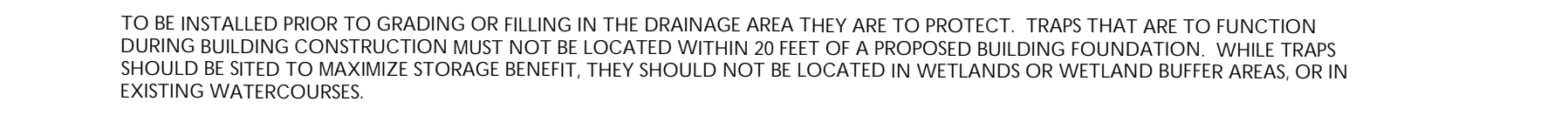
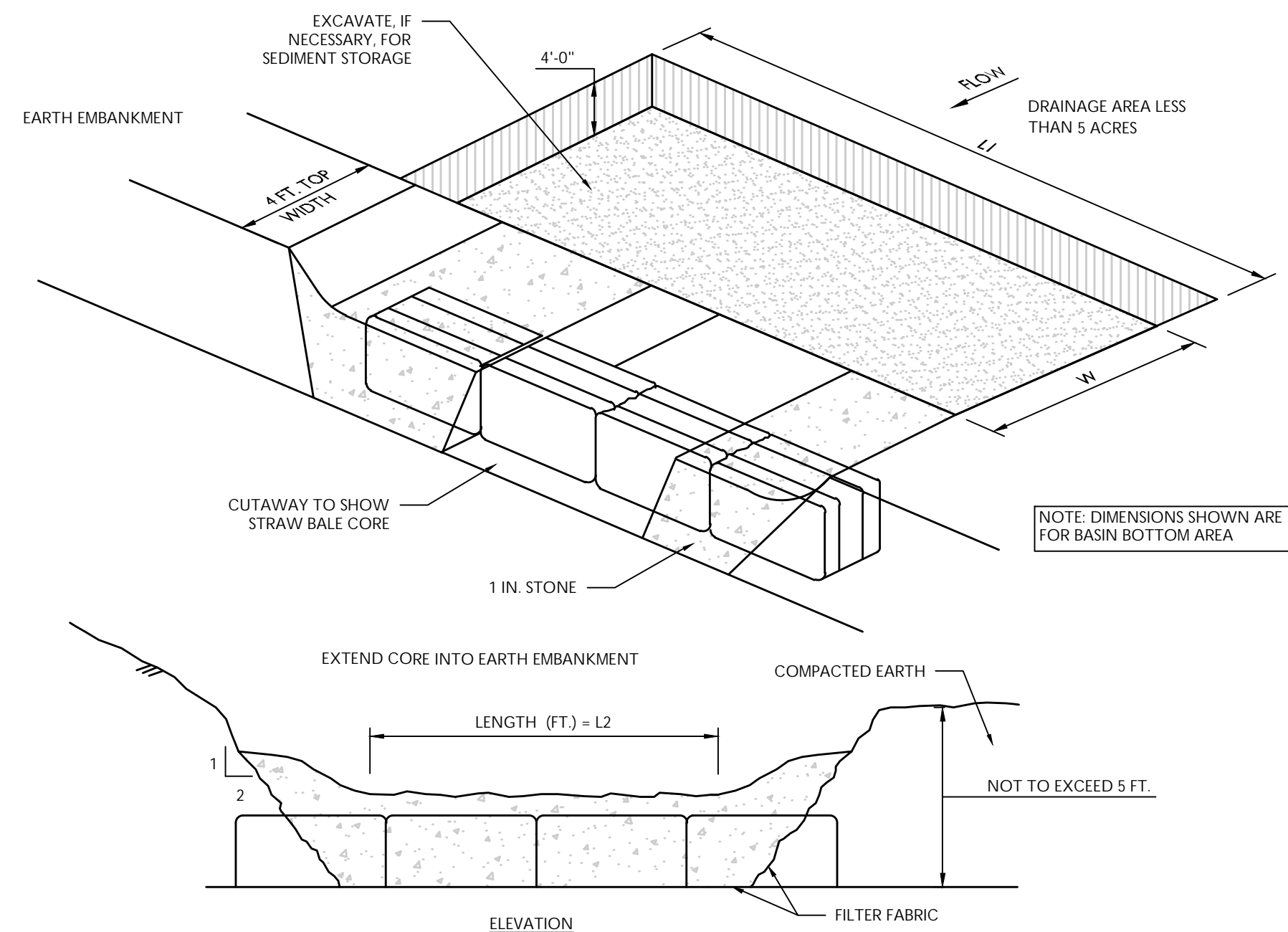
SHEET TITLE: UTILITIES PLAN

SHEET NUMBER: 05 of 17









TO BE INSTALLED PRIOR TO GRADING OR FILLING IN THE DRAINAGE AREA THEY ARE TO PROTECT. TRAPS THAT ARE TO FUNCTION DURING BUILDING CONSTRUCTION MUST NOT BE LOCATED WITHIN 20 FEET OF A PROPOSED BUILDING FOUNDATION. WHILE TRAPS SHOULD BE SITED TO MAXIMIZE STORAGE BENEFIT, THEY SHOULD NOT BE LOCATED IN WETLANDS OR WETLAND BUFFER AREAS, OR IN EXISTING WATERCOURSES.

SEE EROSION AND SEDIMENT CONTROL PLAN FOR LOCATIONS.

**INSTALLATION NOTES:**

1. AREA UNDER EMBANKMENT SHALL BE CLEARED, GRUBBED, AND STRIPPED OF ANY VEGETATION AND ROOT MAT. THE POOL AREA SHALL BE CLEARED AS WELL.
2. THE FILL MATERIAL FOR THE EMBANKMENT SHALL BE FREE OF ROOTS OR OTHER WOODY VEGETATION AS WELL AS OVER SIZED STONES, ROCKS, ORGANIC MATERIAL AND OTHER QUESTIONABLE MATERIAL. THE EMBANKMENT SHALL BE COMPACTED BY TRAVERSING WITH EQUIPMENT WHILE IT IS BEING CONSTRUCTED.
3. SEDIMENT SHALL BE REMOVED AND TRAP RESTORED TO ITS ORIGINAL DIMENSIONS WHEN THE SEDIMENT HAS ACCUMULATED TO 12 THE DESIGN DEPTH OF THE TRAP. REMOVED SEDIMENT SHALL BE DEPOSITED IN A SUITABLE AREA AND IN SUCH A MANNER THAT IT WILL NOT ERODE.
4. THE STRUCTURE SHALL BE INSPECTED AFTER EACH RAIN AND REPAIRS MADE AS NEEDED.
5. CONSTRUCTION OPERATIONS SHALL BE CARRIED OUT IN SUCH A MANNER THAT EROSION AND WATER POLLUTION IS MINIMIZED.
6. THE STRUCTURE SHALL BE REMOVED AND THE AREA STABILIZED WHEN THE DRAINAGE AREA HAS BEEN PROPERLY STABILIZED.
7. ALL CUT AND FILL SLOPES SHALL BE 1:2 OR FLATTER.
8. THE STONE USED IN THE OUTLET SHALL BE SMALL RIPRAP 4"-8" ALONG WITH A 1" THICKNESS OF 2" AGGREGATE PLACED ON THE UP-GRADE SIDE ON THE SMALL RIPRAP OR EMBEDDED FILTER CLOTH IN THE RIPRAP.

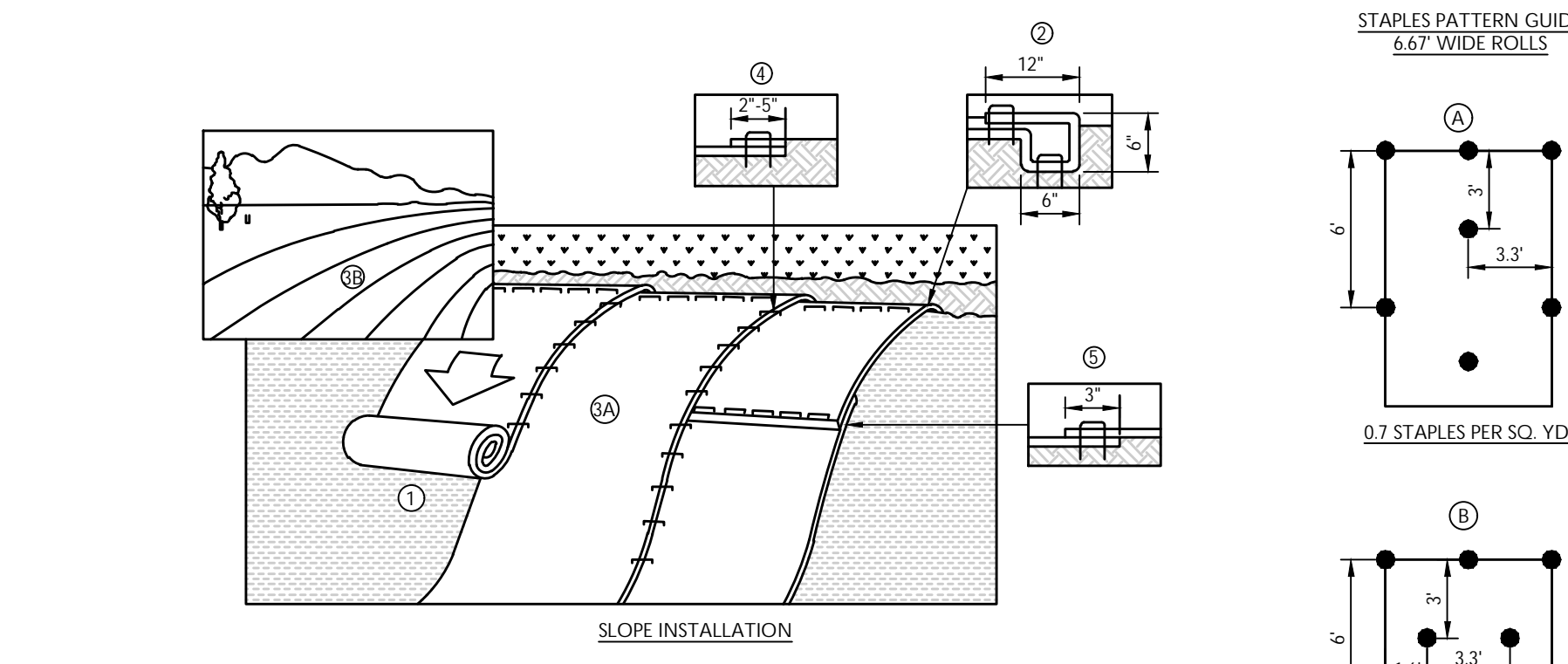
**NOTES:**

1. 3,600 CUBIC FEET OF STORAGE REQUIRED PER ACRE OF DISTURBANCE.
- \*THIS IS THE MINIMUM AMOUNT OF SEDIMENT TRAPS, ADDITIONAL MAY BE REQUIRED BASED UPON OTHER ON-SITE CONDITIONS AND CONTRACTOR SCHEDULE AND PHASING ACTIVITIES.

**SIZING CALCULATIONS**

### 1 STONE OUTLET SEDIMENT TRAP DETAIL

NOT TO SCALE MCNY-SOIL-EROS-1601 07/01/19

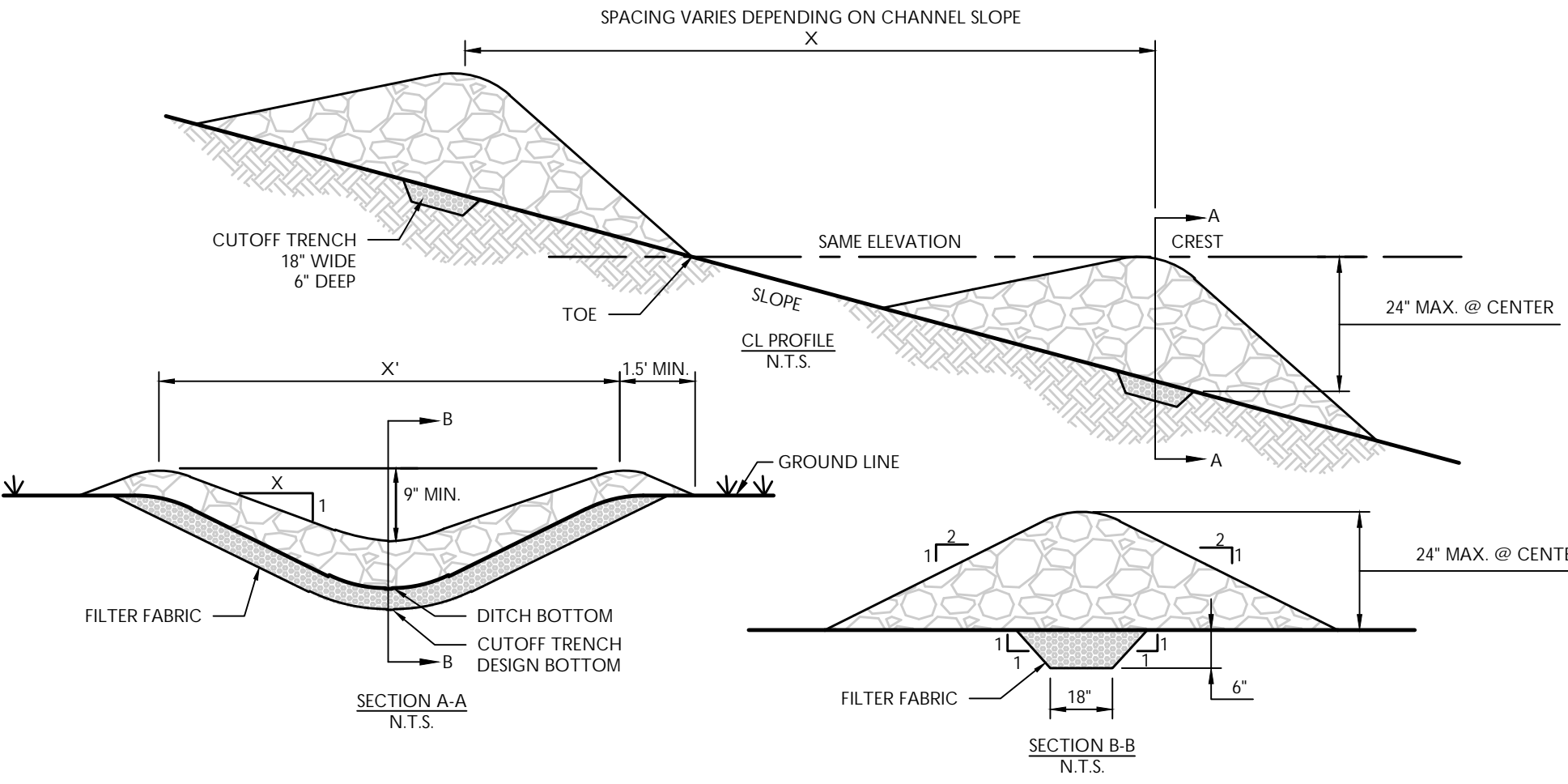


**NOTES:**

1. PREPARE SOIL BEFORE INSTALLING ROLLED EROSION CONTROL PRODUCTS (RECPs), INCLUDING ANY NECESSARY APPLICATION OF LIME, FERTILIZER AND SEED.
  - WHEN USING MATTING WITH SEED, DO NOT SEED THE AREA. FOLLOW MANUFACTURER'S RECOMMENDATIONS.
2. BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE RECPs IN A 6" DEEP x 6" WIDE TRENCH WITH APPROXIMATELY 12" OF RECPs EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE RECPs WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN THE BOTTOM OF THE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF RECPs BACK OVER SEED AND COMPACTED SOIL. SECURE RECPs OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE RECPs.
3. ROLL THE RECPs (A) DOWN OR (B) HORIZONTALLY STEP BY STEP ACROSS THE SLOPE TAMPERING IT DOWN ALONG THE WAY. RECPs SHALL UNROLL WITH APPROPRIATE SIDE TIGHTLY AGAINST THE SOIL SURFACE. RECPs MUST BE SECURELY FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE. WHEN USING THE DOT SYSTEM, STAPLES/STAKES SHOULD BE PLACED THROUGH EACH OF THE COLORED DOTS CORRESPONDING TO THE APPROPRIATE STAPLE PATTERN.
4. THE EDGES OF PARALLEL RECPs MUST BE STAKED WITH APPROXIMATELY 2" TO 5" OVERLAP DEPENDING ON RECPs TYPE.
5. CONSECUTIVE RECPs SPACED DOWN THE SLOPE MUST BE PLACED END OVER END (SHINGLE STYLE) WITH AN APPROXIMATE 3" OVERLAP. STAPLE THROUGH OVERLAPED AREA, APPROXIMATELY 12" APART ACROSS ENTIRE RECPs WIDTH.
  - IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY SECURE THE RECPs.

### 2 EROSION MATTING (CURLEX ENFORCER I) DETAIL

NOT TO SCALE MCNY-SOIL-EROS-2200 07/01/19



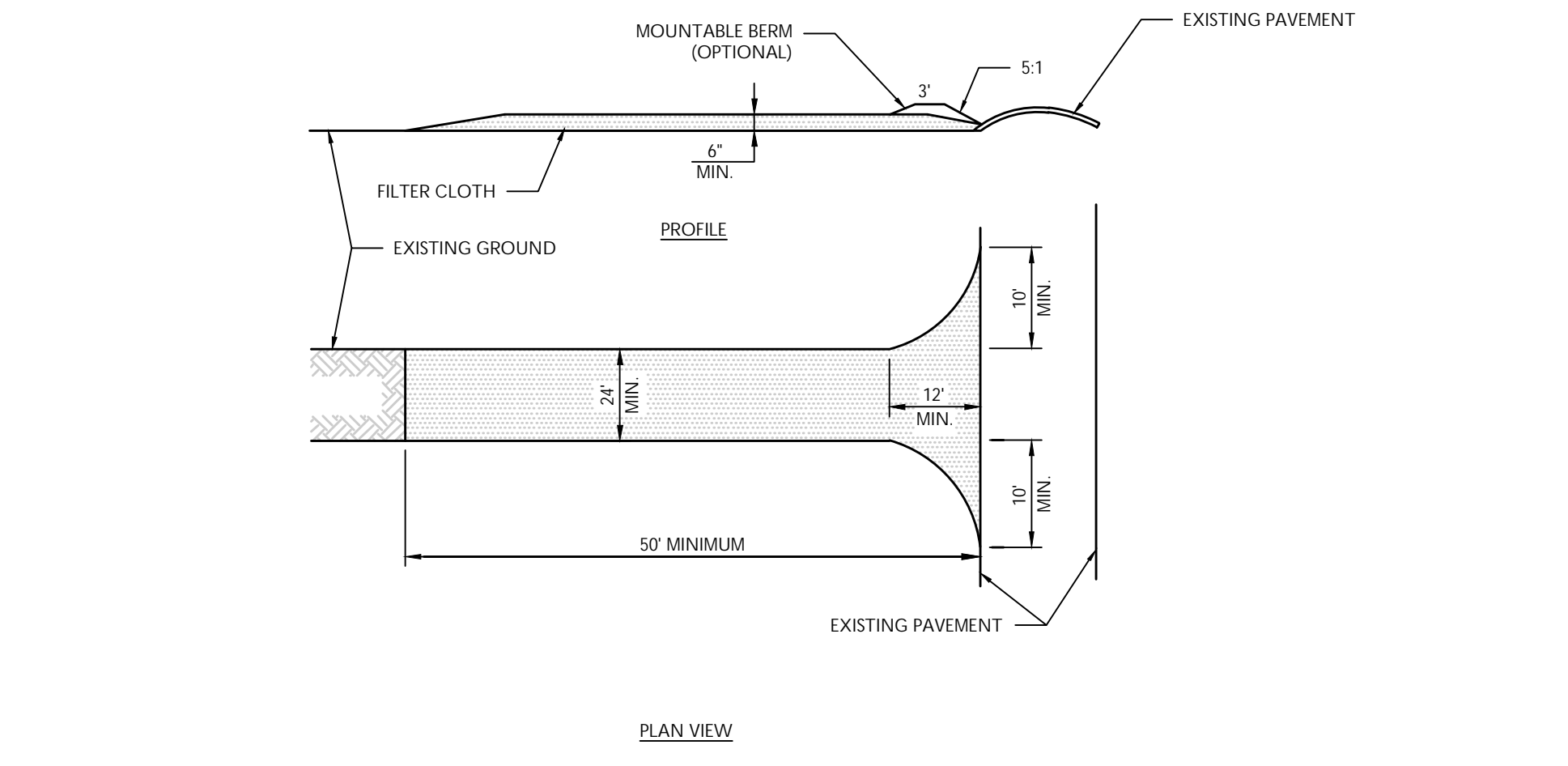
**CONSTRUCTION SPECIFICATIONS**

1. STONE WILL BE PLACED ON A FILTER FABRIC FOUNDATION TO THE LINES, GRADES AND LOCATIONS SHOWN ON THE PLAN.
2. SET SPACING OF CHECK DAMS TO ASSUME THAT THE ELEVATIONS OF THE CREST OF THE DOWNSTREAM DAM IS AT THE SAME ELEVATION OF THE TOE OF THE UPSTREAM DAM.
3. EXTEND THE STONE A MINIMUM OF 1.5 FEET BEYOND THE DITCH BANKS TO PREVENT CUTTING AROUND THE DAM.
4. PROTECT THE CHANNEL DOWNSTREAM OF THE LOWEST CHECK DAM FROM SCOUR AND EROSION WITH STONE OR LINER AS APPROPRIATE.
5. ENSURE THAT CHANNEL APPURTENANCES SUCH AS CULVERT ENTRANCES BELOW CHECK DAMS ARE NOT SUBJECT TO DAMAGE OR BLOCKAGE FROM DISPLACED STONE.

MAXIMUM DRAINAGE AREA: 2 ACRES

### 3 STONE CHECK DAM DETAIL

NOT TO SCALE MCNY-SOIL-EROS-2301 07/01/19

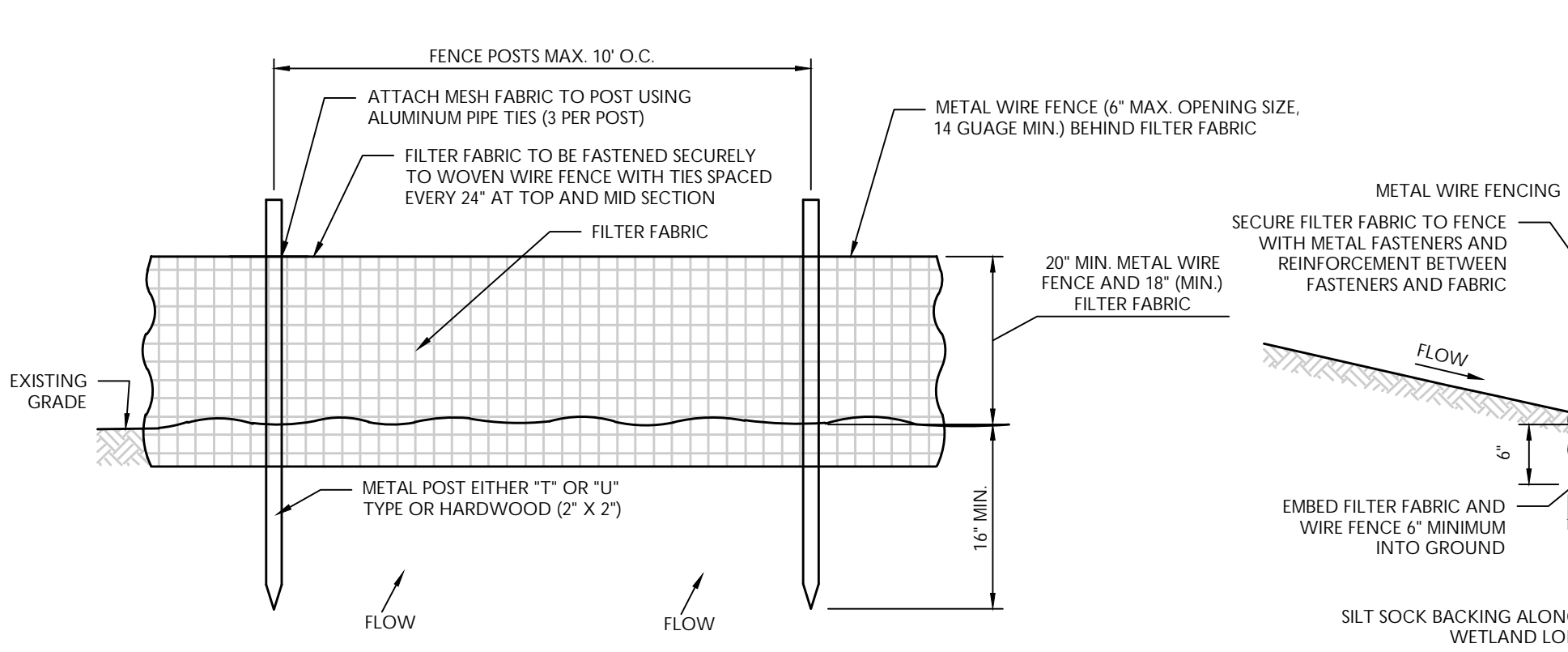


**NOTES:**

1. STONE SIZE - USE 2" STONE, OR RECLAIMED OR RECYCLED CONCRETE EQUIVALENT. LENGTH: NOT LESS THAN 50 FEET. THICKNESS: NOT LESS THAN (6) INCHES
2. WIDTH - 24"
3. FILTER CLOTH - WILL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING OF STONE.
4. SURFACE WATER - ALL SURFACE WATER FLOWING OR DIVERTED TOWARD CONSTRUCTION ENTRANCES SHALL BE PIPED ACROSS THE ENTRANCE. IF PIPING IS IMPRACTICAL, A MOUNTING BERM WITH 5:1 SLOPES WILL BE PERMITTED.
5. MAINTENANCE - THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHTS-OF-WAY. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHTS-OF-WAY MUST BE REMOVED IMMEDIATELY.
6. WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON AN AREA STABILIZED WITH STONE AND WHICH DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE. PERIODIC INSPECTION AND NEEDED MAINTENANCE SHALL BE PROVIDED BY THE CONTRACTOR AS REQUIRED.

### 4 STABILIZED CONSTRUCTION ENTRANCE DETAIL

NOT TO SCALE MCNY-SOIL-EROS-1000 07/01/19



**NOTES:**

1. GEOTEXTILE TO BE FASTENED SECURELY TO FENCE POST BY USING WIRE TIES OR HOE RINGS USE 3 FASTENERS PER POST.
2. SPlicing OF INDIVIDUAL ROLLS SHALL NOT OCCUR AT LOW POINTS.
3. ALL SILT FENCE TO BE INSPECTED AND REMEDIAL MAINTENANCE PERFORMED BY THE CONTRACTOR AS REQUIRED. MATERIAL REMOVED WHEN "BULGES" DEVELOP IN THE SILT FENCE.
4. WHEN TWO SECTIONS OF FILTER FABRIC ARE JOINED, THEY SHALL BE OVER-WRAPPED BY SIX INCHES AND FOLDED.
5. FILTER FABRIC TO BE EITHER FILTER X, MIRAFI 100X, STABILINKA T140N, OR APPROVED EQUIVALENT.
6. PREFABRICATED UNITS SHALL MEET THE MINIMUM REQUIREMENTS SHOWN.
7. IF SPACE PERMITTED, LOCATE SILT FENCE 10' AWAY FROM TOE OF SLOPE IF THE SLOPE IS STEEPER THAN 1:1.

### 5 REINFORCED SILT FENCE (WITH WIRE FENCE) DETAIL

NOT TO SCALE MCNY-SOIL-EROS-1101 07/01/19

## GENERAL SOIL EROSION AND SEDIMENT CONTROL NOTES

1. ALL SOIL EROSION AND SEDIMENT CONTROL PRACTICES ARE TO BE INSTALLED PRIOR TO ANY MAJOR SOIL DISTURBANCE, OR IN THEIR PROPER SEQUENCE, AND MAINTAINED UNTIL PERMANENT PROTECTION IS ESTABLISHED.
2. ANY DISTURBED AREAS THAT WILL BE LEFT EXPOSED MORE THAN FOURTEEN (14) DAYS FOR DISTURBANCES LESS THAN FIVE (5) ACRES AND SEVEN (7) DAYS FOR DISTURBANCES GREATER THAN FIVE (5) ACRES AND NOT SUBJECT TO CONSTRUCTION TRAFFIC, WILL IMMEDIATELY RECEIVE A TEMPORARY SEEDING. IF THE SEASON PREVENTS THE ESTABLISHMENT OF TEMPORARY COVER, THE DISTURBED AREAS WILL BE MULCHED WITH STRAW, OR EQUIVALENT MATERIAL, AT A RATE OF TWO (2) TONS PER ACRE, ACCORDING TO STATE STANDARDS.
3. PERMANENT VEGETATION TO BE SEED OR SODED ON ALL EXPOSED AREAS WITHIN FIVE (5) DAYS AFTER FINAL GRADING. MULCHING IS REQUIRED ON ALL SEEDING, WHEN HYDROSEEDING, MULCH SHALL NOT BE INCLUDED IN THE TANK WITH THE SEED.
4. ALL WORK TO BE DONE IN ACCORDANCE WITH THE 2016 NEW YORK STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL OR AS AMENDED.
5. A SUBBASE COURSE WILL BE APPLIED IMMEDIATELY FOLLOWING ROUGH GRADING AND INSTALLATION OF IMPROVEMENTS TO STABILIZE STREETS, ROADS, DRIVEWAYS, AND PARKING AREAS. IN AREAS WHERE NO UTILITIES ARE PRESENT, THE SUBBASE SHALL BE INSTALLED WITHIN FIVE (5) DAYS OF THE PRELIMINARY GRADING.
6. IMMEDIATELY FOLLOWING INITIAL DISTURBANCE OR ROUGH GRADING, ALL CRITICAL AREAS SUBJECT TO EROSION (I.E. STEEP SLOPES AND ROADWAY EMBANKMENTS) WILL RECEIVE A TEMPORARY SEEDING IN COMBINATION WITH STRAW MULCH OR A SUITABLE EQUIVALENT, AT A RATE OF TWO (2) TONS PER ACRE, ACCORDING TO STATE STANDARDS.
7. ANY STEEP SLOPES RECEIVING PIPELINE INSTALLATION WILL BE BACKFILLED AND STABILIZED DAILY, AS THE INSTALLATION CONTINUES (I.E. SLOPES GREATER THAN 3:1).
8. THE STANDARD FOR STABILIZED CONSTRUCTION ACCESS REQUIRES THE INSTALLATION OF A STONE PAD, AT ALL CONSTRUCTION DRIVEWAYS, IMMEDIATELY AFTER INITIAL SITE DISTURBANCE.
9. IN ACCORDANCE WITH THE STANDARD FOR MANAGEMENT OF HIGH ACID PRODUCING SOILS, ANY SOIL HAVING A PH OF 4 OR LESS OR CONTAINING IRON SULFIDES SHALL BE COVERED WITH A MINIMUM OF TWELVE (12) INCHES OF SOIL HAVING A PH OF 5 OR MORE PRIOR TO SEEDING PREPARATION. AREAS WHERE TREES OR SHRUBS ARE TO BE PLANTED SHALL BE COVERED WITH A MINIMUM OF TWENTY-FOUR (24) INCHES OF SOIL HAVING A PH OF 5 OR MORE.
10. AT THE TIME THE SITE PREPARATION FOR PERMANENT VEGETATIVE STABILIZATION IS GOING TO BE ACCOMPLISHED, ANY SOIL THAT WILL NOT PROVIDE A SUITABLE ENVIRONMENT TO SUPPORT ADEQUATE VEGETATIVE GROUND COVER SHALL BE REMOVED OR TREATED IN SUCH A WAY THAT IT WILL PERMANENTLY ADJUST THE SOIL CONDITIONS AND PROVIDE SUITABLE FOR VEGETATIVE GROUND COVER. IF THE REMOVAL OR TREATMENT OF THE SOIL WILL NOT PROVIDE SUITABLE CONDITIONS, NON-VEGETATIVE MEANS OF PERMANENT GROUND STABILIZATION WILL HAVE TO BE EMPLOYED.
11. CONDUIT OUTLET PROTECTION MUST BE REVIEWED & SUPPLEMENTED AT ALL OUTFALLS PRIOR TO THE DRAINAGE SYSTEM BECOMING OPERATIONAL.
12. UNFILTERED DEWATERING IS NOT PERMITTED. TAKE ALL NECESSARY PRECAUTIONS DURING ALL DEWATERING OPERATIONS TO MINIMIZE SEDIMENT TRANSFER. ANY DEWATERING METHODS USED MUST BE IN ACCORDANCE WITH STATE STANDARDS.
13. SHOULD THE CONTROL OF DUST AT THE SITE BE NECESSARY, THE SITE WILL BE SPRINKLED UNTIL THE SURFACE IS WET. TEMPORARY VEGETATIVE COVER SHALL BE ESTABLISHED OR MULCH SHALL BE APPLIED IN ACCORDANCE WITH STATE STANDARDS FOR EROSION CONTROL.
14. ALL SOIL WASHED, DROPPED, SPILLED, OR TRACKED OUTSIDE THE LIMIT OF DISTURBANCE OR ONTO PUBLIC RIGHT-OF-WAY WILL BE REMOVED IMMEDIATELY.
15. THE PROPERTY OWNER SHALL BE RESPONSIBLE FOR ANY EROSION AND SEDIMENTATION THAT MAY OCCUR BELOW STORMWATER OUTFALLS OR OFFSITE AS A RESULT OF CONSTRUCTION OF THE PROJECT.
16. STOCKPILE AND STAGING LOCATIONS DETERMINED IN THE FIELD, SHALL BE PLACED WITHIN THE LIMITS OF DISTURBANCE ACCORDING TO THE CERTIFIED PLAN.
17. CONCRETE WASHOUT, DUMPS, & STAGING AREA LOCATIONS SHALL BE DETERMINED BY THE CONTRACTOR AND APPROVED AT THE PRE-CONSTRUCTION MEETING. THEY SHALL BE PLACED IN THE PROXIMITY OF THE CONSTRUCTION ENTRANCE AND STAGING AREAS AND SHALL BE USED PRIOR TO EXITING THE PROJECT SITE. THE LOCATION SHALL BE IN A PRACTICAL, CLEARLY DELINEATED, AREA AND BE MAINTAINED THROUGHOUT CONSTRUCTION.
18. ALL SOIL STOCKPILES ARE TO BE TEMPORARILY STABILIZED IN ACCORDANCE WITH THE NEW YORK STATE STANDARDS AND SPECIFICATIONS FOR SOIL EROSION AND SEDIMENT CONTROL.
19. ALL PERMANENT SOIL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE MAINTAINED BY THE PROPERTY OWNER, AND SHALL BECOME THEIR RESPONSIBILITY.
20. PAVEMENT AREAS ARE TO BE KEPT CLEAN AT ALL TIMES.
21. DURING CONSTRUCTION, ANY ADDITIONAL CONTROL MEASURES AS DEEMED NECESSARY TO PREVENT EROSION OR CONTROL SEDIMENT BEYOND THOSE MEASURES SHOWN ON THE APPROVED PLAN SHALL BE INSTALLED OR EMPLOYED AT THE DIRECTION OF THE MUNICIPAL ENGINEER.
22. ALL TEMPORARY STRUCTURAL EROSION AND SEDIMENT CONTROL MEASURES CAN BE REMOVED, WHEN ALL CONSTRUCTION ACTIVITY IDENTIFIED IN THE SWPPP HAS BEEN COMPLETED, ALL AREAS OF DISTURBANCE HAVE ACHIEVED FINAL STABILIZATION\* AND ALL POST-CONSTRUCTION STORMWATER MANAGEMENT PRACTICES HAVE BEEN CONSTRUCTED IN CONFORMANCE WITH THE SWPPP AND ARE OPERATIONAL.
23. BOTTOM AND BERM ELEVATIONS OF TEMPORARY SEDIMENT BASINS TO BE REVIEWED WITH THE CONTRACTOR BASED ON THEIR PROPOSED CONSTRUCTION SEQUENCE FOR THE PROJECT.

\*FINAL STABILIZATION - MEANS THAT ALL SOIL DISTURBANCE ACTIVITIES HAVE CEASED AND A UNIFORM, PERENNIAL VEGETATIVE COVER WITH A DENSITY OF EIGHTY (80) PERCENT OVER THE ENTIRE PERSISTENT SURFACE HAS BEEN ESTABLISHED, OR OTHER EQUIVALENT STABILIZATION MEASURES, SUCH AS PERENNIAL LANDSCAPE MULCHES, ROCK RIP-RAP OR WASHED/CRUSHED STONE HAVE BEEN APPLIED ON ALL DISTURBED AREAS THAT ARE NOT COVERED BY PERMANENT STRUCTURES, CONCRETE OR PAVEMENT.

**MAINTENANCE PLAN DURING CONSTRUCTION:**

INSPECTION AND MAINTENANCE SHALL BE PERFORMED IN CONFORMANCE WITH CP-0-20-001 OR AS AMENDED. ALL EROSION AND SEDIMENT CONTROL PRACTICES WILL BE CHECKED FOR STABILITY AND OPERATION FOLLOWING EVERY RAINFALL-PRODUCING RAINFALL BUT IN NO CASE LESS THAN ONCE EVERY WEEK. ANY NEEDED REPAIRS WILL BE MADE IMMEDIATELY TO MAINTAIN ALL PRACTICES AS DESIGNED AND INSTALLED FOR THE PROJECT. THE SEDIMENT TRAPS WILL BE CLEANED OUT WHEN THE LEVEL OF SEDIMENT REACHES 25% OF ITS CAPACITY. SEDIMENT WILL BE REMOVED FROM BEHIND THE SILT FENCE WHEN IT BECOMES APPROXIMATELY 6" DEEP AT THE FENCE. THE SILT FENCE WILL BE REPAIRED AS NECESSARY TO MAINTAIN A BARRIER. ALL SEEDED AREAS WILL BE FERTILIZED, RE-SEED AS NECESSARY, AND MULCHED ACCORDING TO SPECIFICATIONS IN THE LANDSCAPE PLAN TO MAINTAIN A VIGOROUS, DENSE VEGETATIVE COVER.

**MAINTENANCE AGREEMENT NOTE:**

THE OWNER/APPLICANT SHALL ENTER INTO AN ENFORCEABLE MAINTENANCE AGREEMENT WITH THE MUNICIPALITY (IF AN MS4 COMMUNITY) RELATED TO MAINTENANCE OF STORMWATER FACILITIES. THE OWNER/APPLICANT IS RESPONSIBLE TO PERFORM ALL REQUIRED MAINTENANCE BOTH DURING CONSTRUCTION AND LONG-TERM. THE NATURE OF THE AGREEMENT IS TO ALLOW THE MUNICIPALITY TO PERFORM MAINTENANCE AT THEIR OPTION SHOULD THE OWNER/APPLICANT FAIL TO ADEQUATELY MAINTAIN THE SYSTEM AS DETERMINED BY THE MUNICIPAL ENGINEER. MAINTENANCE OF THE STORMWATER SYSTEM SHALL BE PERFORMED IN ACCORDANCE WITH THE APPROVED SWPPP AND DETAIL SHEETS.

## TOWN OF WAWAYANDA PLANNING BOARD

### SOIL EROSION & SEDIMENT CONTROL DETAILS

07 of 17

**Colliers Engineering & Design**

www.colliersengineering.com

Copyright © 2022 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, redrawn, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF

ALL STATES REQUIRE NOTIFICATION OF EXCAVATIONS, DISBURSES, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.

Know what's below. Call before you dig.

FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DESCRIPTION
1	02/04/22	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIS SUBMISSION
2	01/11/23	REVISED PER PLANNING BOARD COMMENTS

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
NEW YORK LICENSED PROFESSIONAL ENGINEER  
LICENSE NUMBER: 103788  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
N.Y. C.O.A.#: 0017609

### PRELIMINARY SITE PLANS FOR DEWPOINT SOUTH

SECTION 4  
BLOCK 1  
LOT 50.32

TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK STATE

**Colliers Engineering & Design**

NEWBURGH  
555 Hudson Valley Avenue  
Suite 101  
New Windsor, NY 12553  
Phone: 845.564.4495

COLLIERS ENGINEERING & DESIGN CT, P.C.  
DOING BUSINESS AS MASER CONSULTANTS  
ENGINEERING & LAND SURVEYING

SCALE:	DATE:	DRAWN BY:	CHECKED BY:
AS SHOWN	01/10/2022	SMB	CDR
PROJECT NUMBER:	DRAWING NAME:		
20009912A	C-SES-50TH		
SHEET TITLE:			
SOIL EROSION & SEDIMENT CONTROL DETAILS			
SHEET NUMBER:			
07 of 17			

NOTE: DO NOT SCALE DRAWINGS FOR CONSTRUCTION.







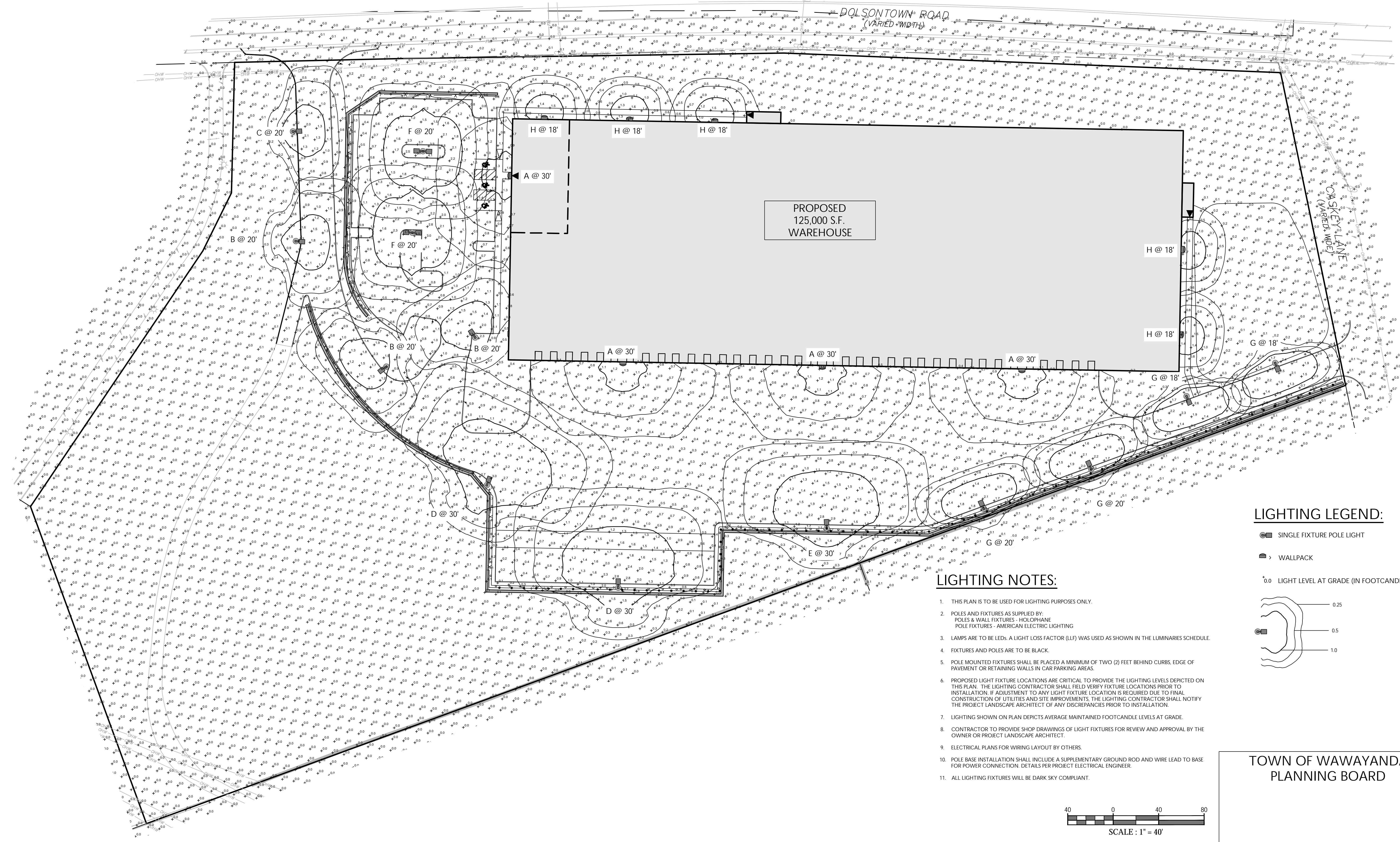
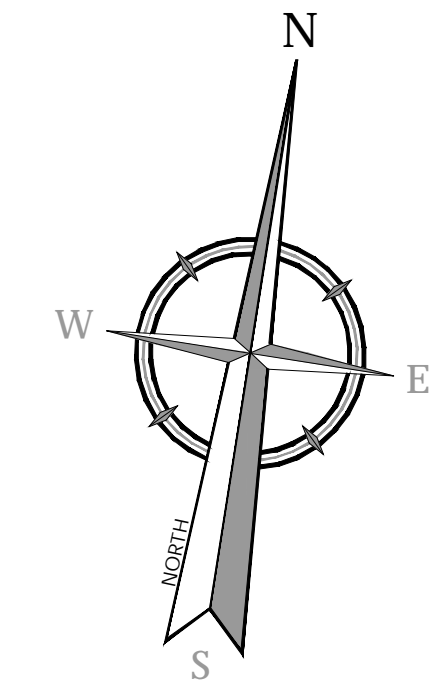


## LUMINAIRE SCHEDULE

KEY	QTY.	DESCRIPTION	ARRANGEMENT	MTG. HT.	LUMENS/LAMP	LLF	CATALOG #
A	4	HOLOPHANE WALL PACK FULL CUTOFF LED	SINGLE	30'	9,883	.97	HLWPC2-P40-30K-MVOLT-T4M-BKSDP-P3
B	3	AMERICAN ELECTRIC LIGHTING ATB0 SERIES LED	SINGLE	20'	6,906	.97	ATB0-P202-MVOLT-R4-4K-BK-UMS-XX
C	1	AMERICAN ELECTRIC LIGHTING ATB0 SERIES LED	SINGLE	20'	6,906	.97	ATB0-P202-MVOLT-R4-4K-BK-HSS-UMS-XX
D	2	AMERICAN ELECTRIC LIGHTING ATB0 SERIES LED	SINGLE	30'	19,810	.97	ATB0-P305-MVOLT-R4-4K-BK-UMS-XX
E	1	AMERICAN ELECTRIC LIGHTING ATB0 SERIES LED	SINGLE	30'	19,810	.97	ATB0-P305-MVOLT-R4-4K-BK-HSS-UMS-XX
F	2	AMERICAN ELECTRIC LIGHTING ATB0 SERIES LED	DOUBLE	20'	6,906	.97	ATB0-P202-MVOLT-R4-4K-BK-UMS-XX
G	4	AMERICAN ELECTRIC LIGHTING ATB0 SERIES LED	SINGLE	18' / 20'	5,346	.97	ATB0-P201-MVOLT-R3-4K-BK-HSS-UMS-XX
H	5	WILLIAMS WPCS LED FULL CUTOFF WALL PACK SMALL	SINGLE	18'	3,000	0.97	WPCS-L30/840-BZ-XX-DIM-UNV

## CALCULATION SUMMARY

DESCRIPTION	CALC. TYPE	UNITS	AVG.	MAX.	MIN.	AVG. / MIN.
PAVEMENT AREA SUMMARY	ILLUMINANCE	FC	0.9	4.1	0.2	4.5:1

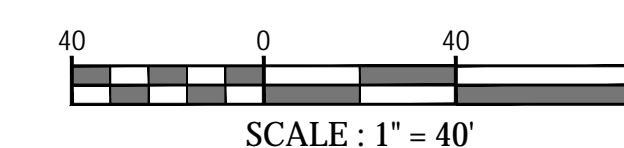


### LIGHTING LEGEND:

- SINGLE FIXTURE POLE LIGHT
- WALLPACK
- LIGHT LEVEL AT GRADE (IN FOOTCANDLES)

### LIGHTING NOTES:

- THIS PLAN IS TO BE USED FOR LIGHTING PURPOSES ONLY.
- POLES AND FIXTURES AS SUPPLIED BY:  
POLES & WALL FIXTURES - HOLOPHANE  
POLE FIXTURES - AMERICAN ELECTRIC LIGHTING
- LAMPS ARE TO BE LEDS. A LIGHT LOSS FACTOR (LLF) WAS USED AS SHOWN IN THE LUMINAIRES SCHEDULE.
- FIXTURES AND POLES ARE TO BE BLACK.
- POLE MOUNTED FIXTURES SHALL BE PLACED A MINIMUM OF TWO (2) FEET BEHIND CURBS, EDGE OF PAVEMENT OR RETAINING WALLS IN CAR PARKING AREAS.
- PROPOSED LIGHT FIXTURE LOCATIONS ARE CRITICAL TO PROVIDE THE LIGHTING LEVELS DEPICTED ON THIS PLAN. THE LIGHTING CONTRACTOR SHALL FIELD VERIFY FIXTURE LOCATIONS PRIOR TO INSTALLATION. IF ADJUSTMENT TO ANY LIGHT FIXTURE LOCATION IS REQUIRED DUE TO FINAL CONSTRUCTION OF UTILITIES AND SITE IMPROVEMENTS, THE LIGHTING CONTRACTOR SHALL NOTIFY THE PROJECT LANDSCAPE ARCHITECT OF ANY DISCREPANCIES PRIOR TO INSTALLATION.
- LIGHTING SHOWN ON PLAN DEPICTS AVERAGE MAINTAINED FOOTCANDLE LEVELS AT GRADE.
- CONTRACTOR TO PROVIDE SHOP DRAWINGS OF LIGHT FIXTURES FOR REVIEW AND APPROVAL BY THE OWNER OR PROJECT LANDSCAPE ARCHITECT.
- ELECTRICAL PLANS FOR WIRING LAYOUT BY OTHERS.
- POLE BASE INSTALLATION SHALL INCLUDE A SUPPLEMENTARY GROUND ROD AND WIRE LEAD TO BASE FOR POWER CONNECTION. DETAILS PER PROJECT ELECTRICAL ENGINEER.
- ALL LIGHTING FIXTURES WILL BE DARK SKY COMPLIANT.



**Colliers**

Engineering & Design

www.colliersengineering.com

Copyright © 2022 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811**

PROTECT YOURSELF  
ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DISBURSERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
Know what's below.  
Call before you dig.  
FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DRAWN BY	DESCRIPTION
1	02/04/22	CDR	REVISED WETLAND IMPACT REDUCTIONS & DETAILS FOR GIS SUBMISSION.
2	01/10/23	CDR	REVISED PER PLANNING BOARD COMMENTS.

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

Justin Eric Dates  
NEW YORK REGISTERED LANDSCAPE ARCHITECT  
LICENSE NUMBER: 001964-01  
COLLIERS ENGINEERING & DESIGN CT. P.C.

PRELIMINARY SITE PLANS

FOR  
DEWPOINT SOUTH

SECTION 4  
BLOCK 1  
LOT 50.32

TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK STATE

**Colliers** 555 Hudson Valley Avenue  
Suite 101  
New Windsor, NY 12553  
Phone: 845.544.4495  
COLLIERS ENGINEERING & DESIGN CT. P.C.  
DOING BUSINESS AS MASER CONSULTANTS  
ENGINEERING & LANDSCAPING

SCALE:	DATE:	DRAWN BY:	CHECKED BY:
AS SHOWN	01/10/2022	SMB	CDR

PROJECT NUMBER:	DRAWING NAME:
20000912A	C-LGHT-S0TH

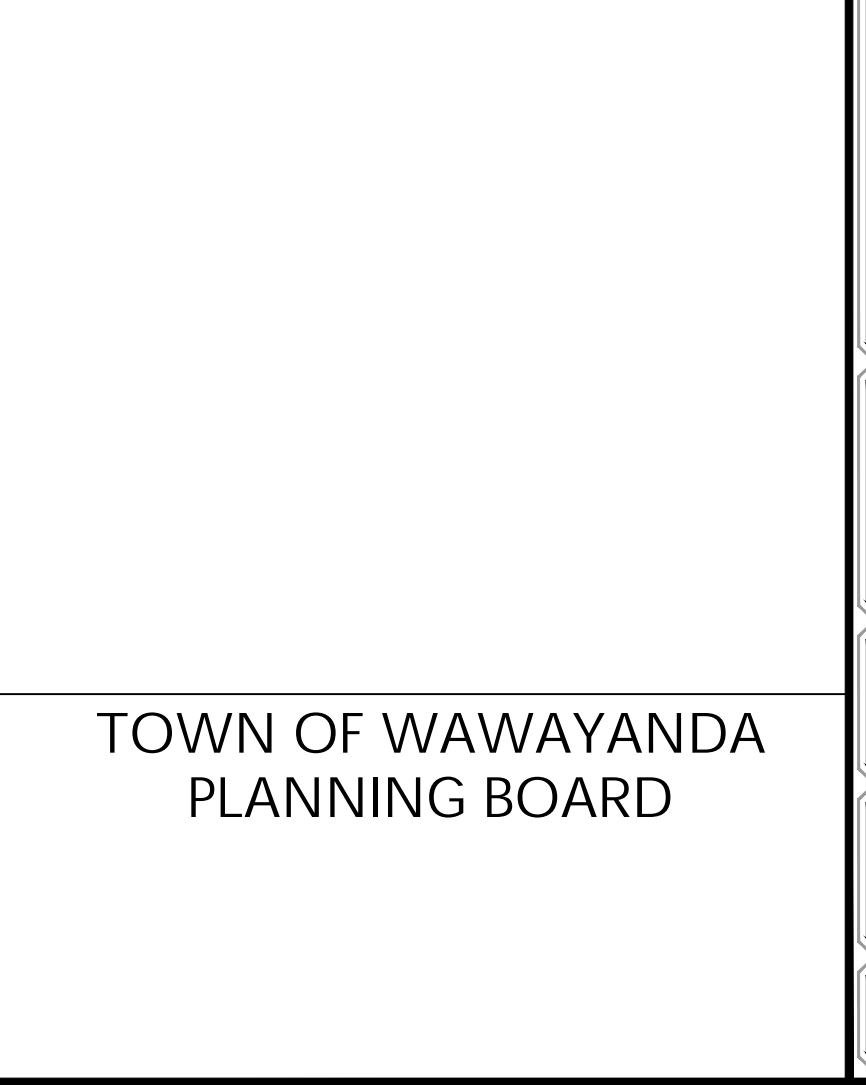
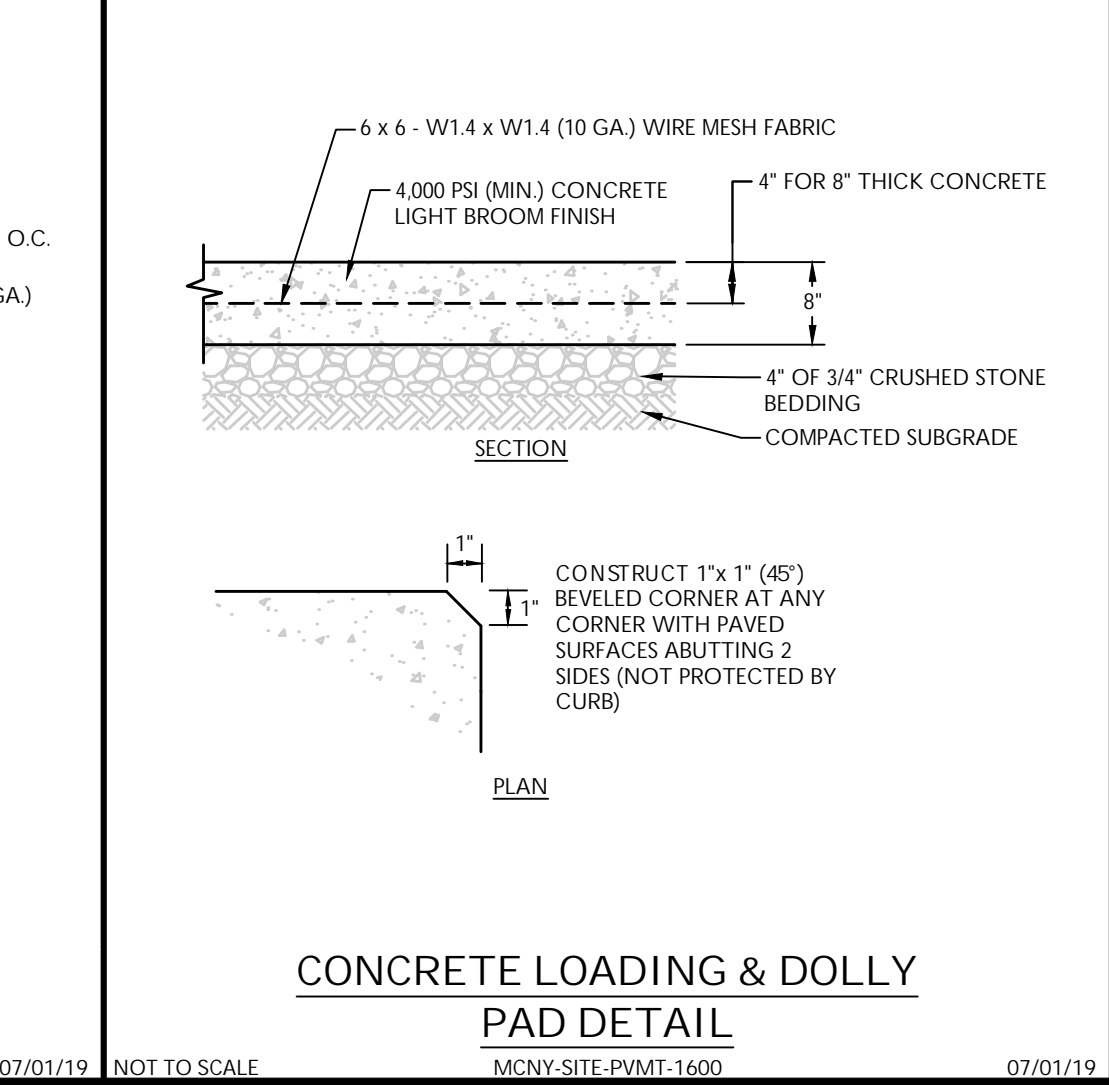
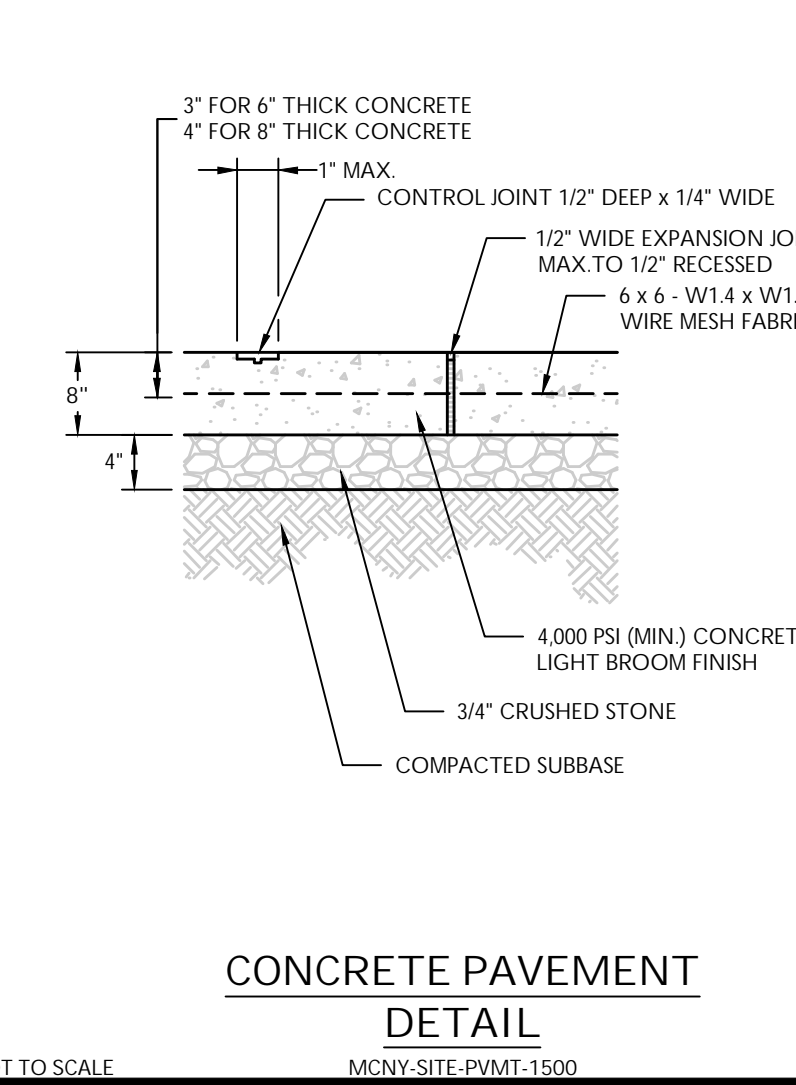
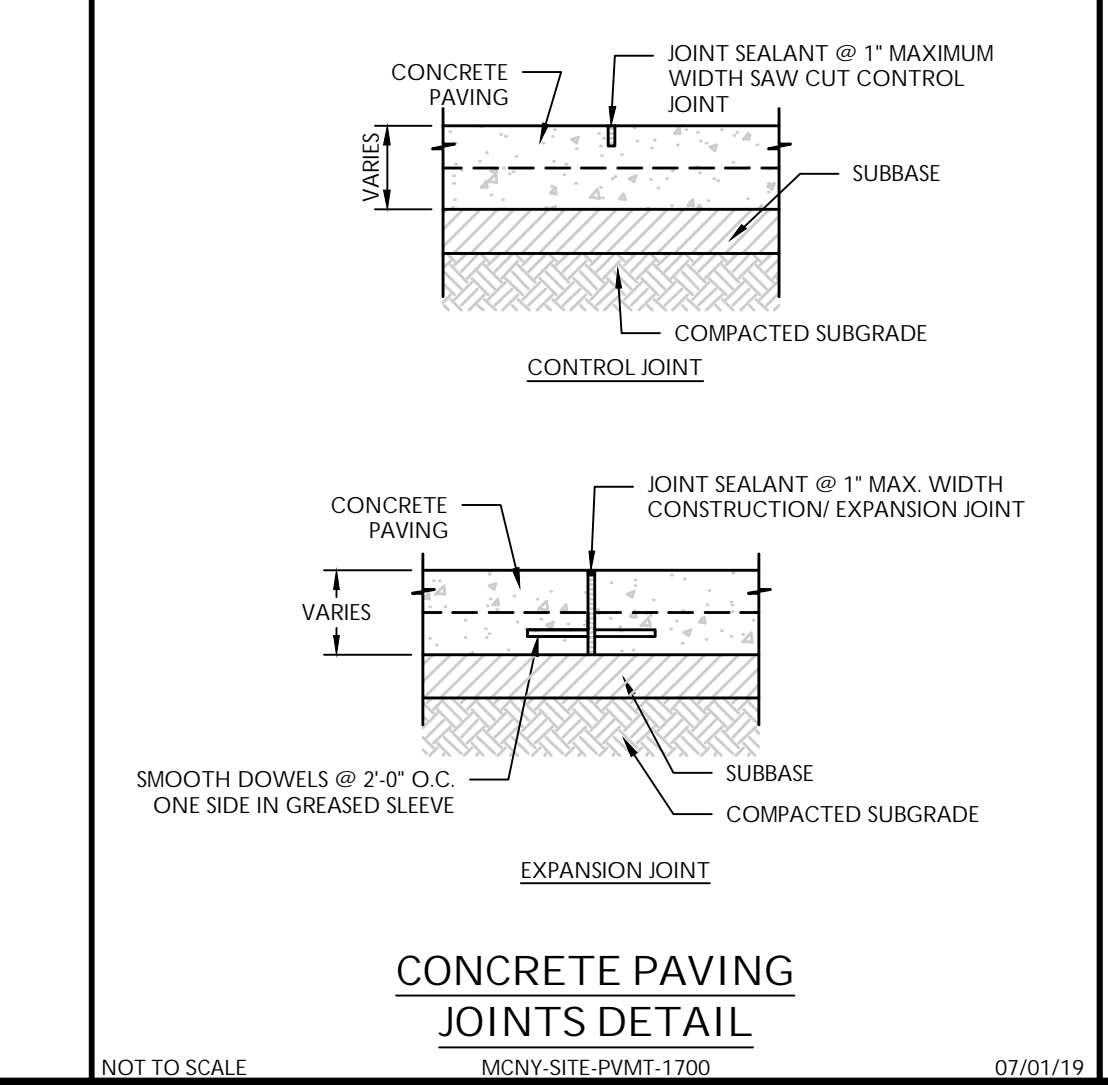
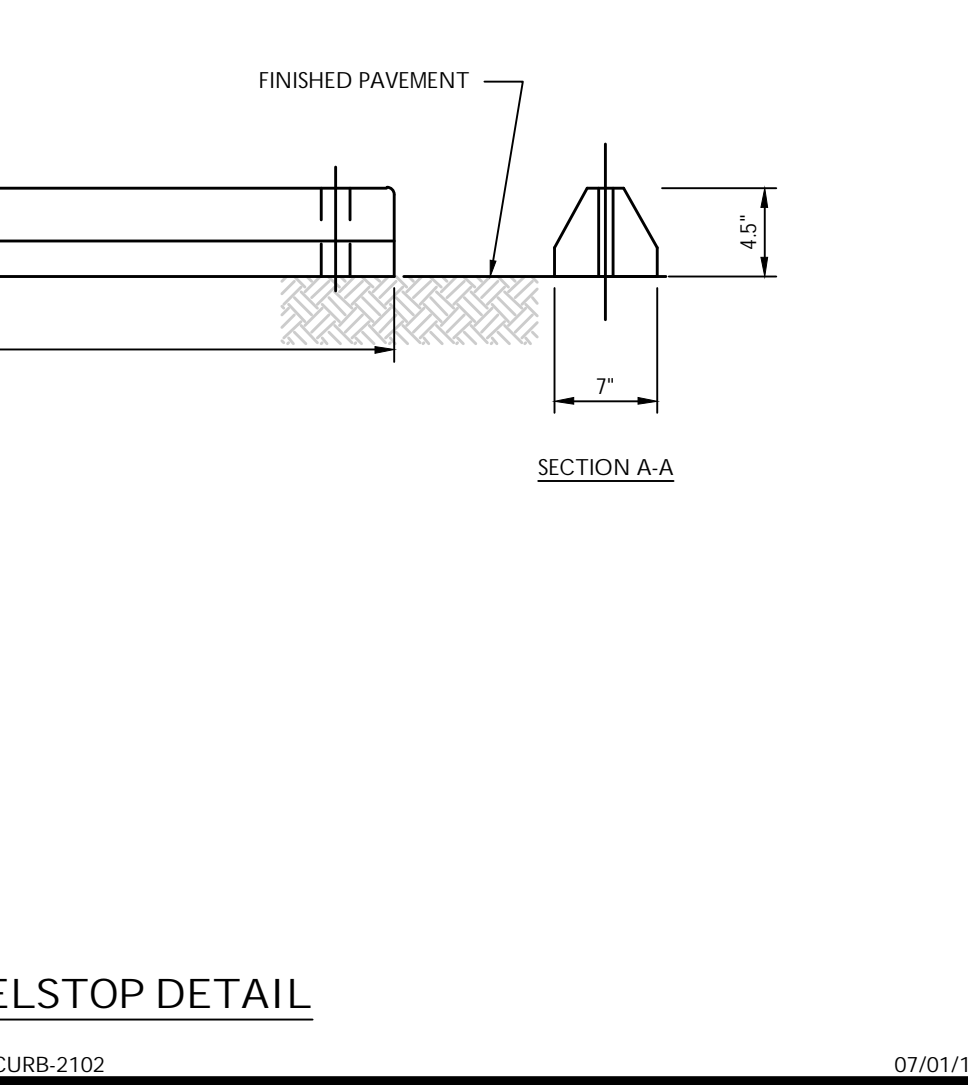
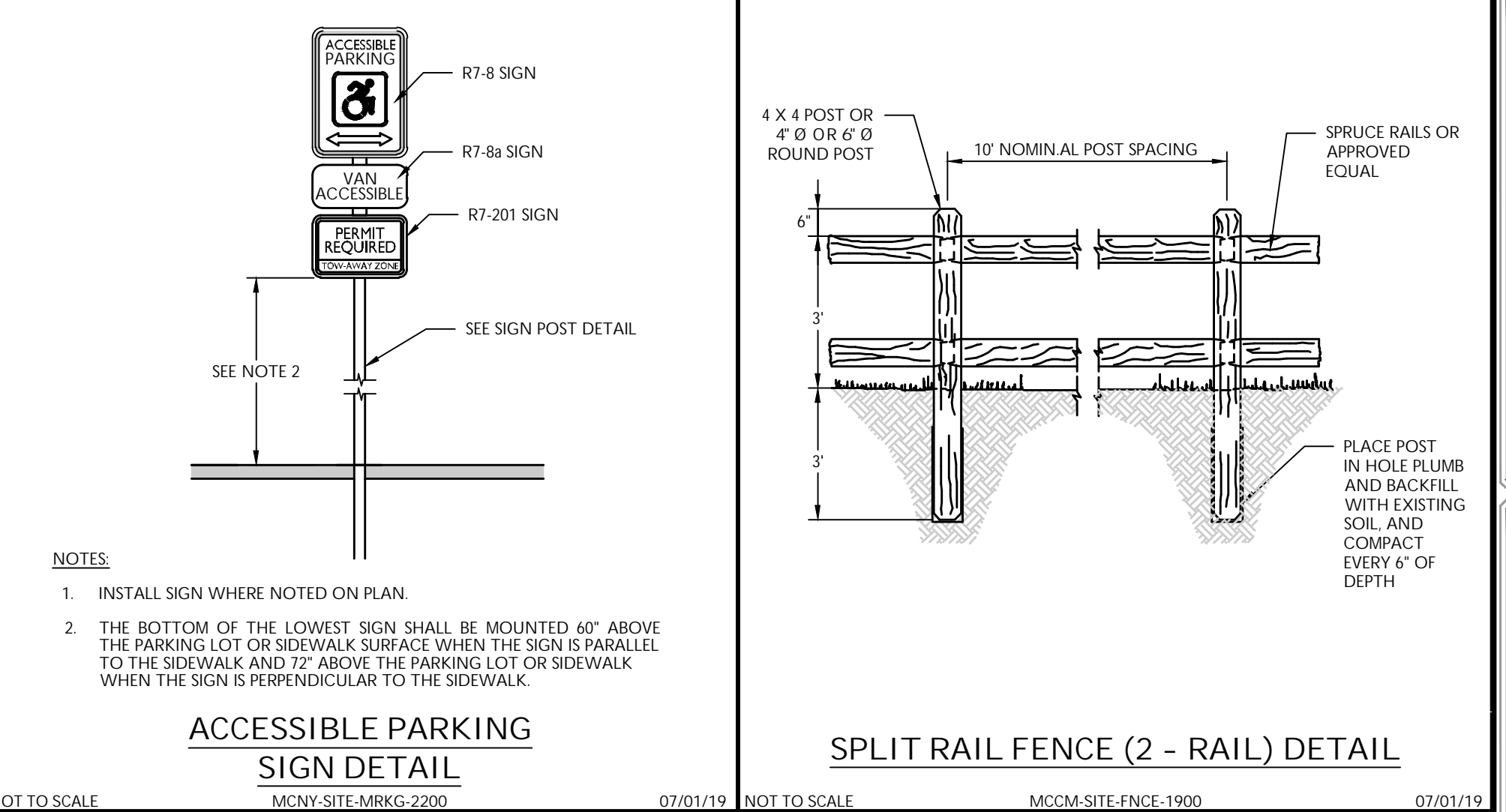
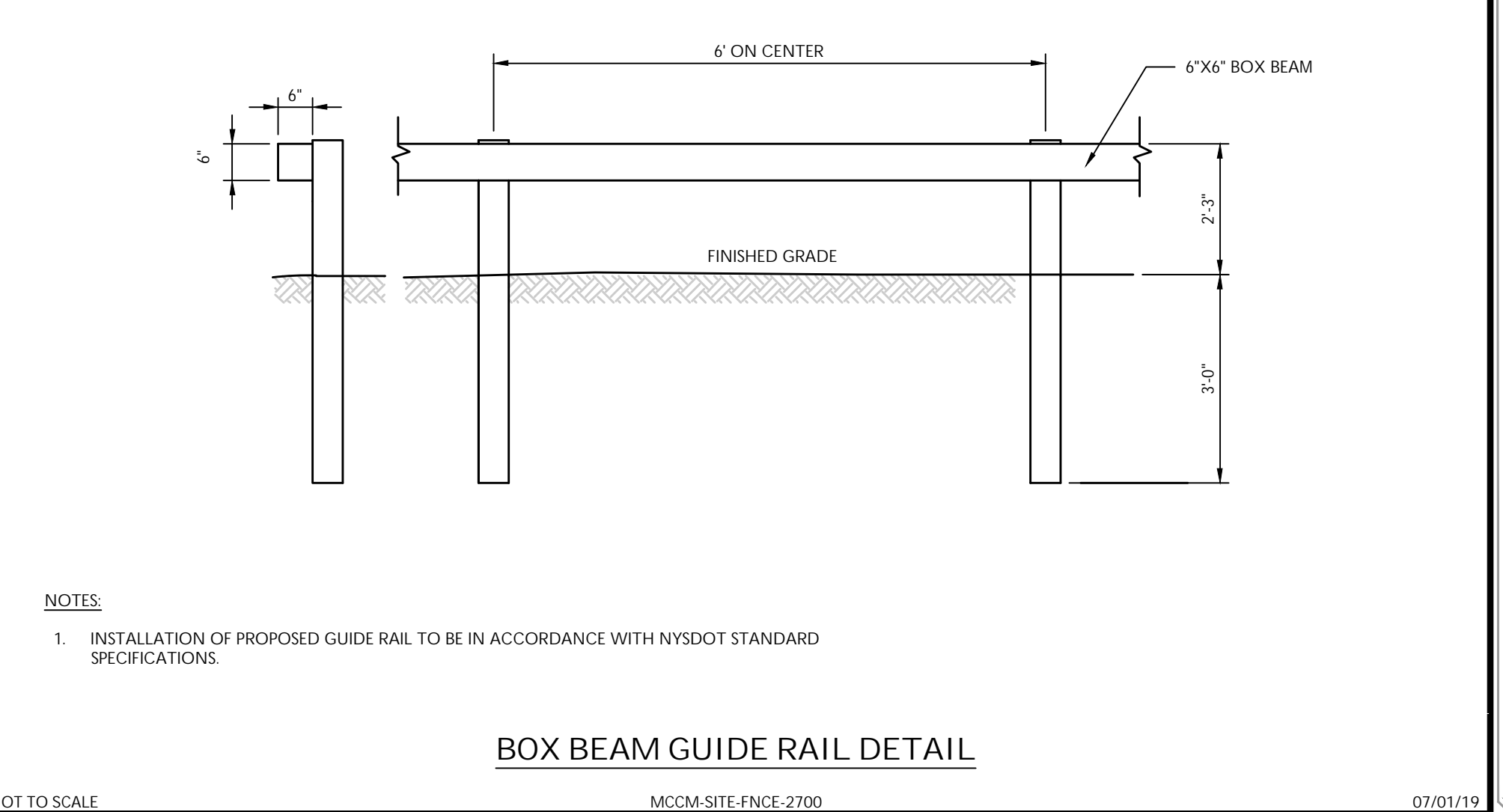
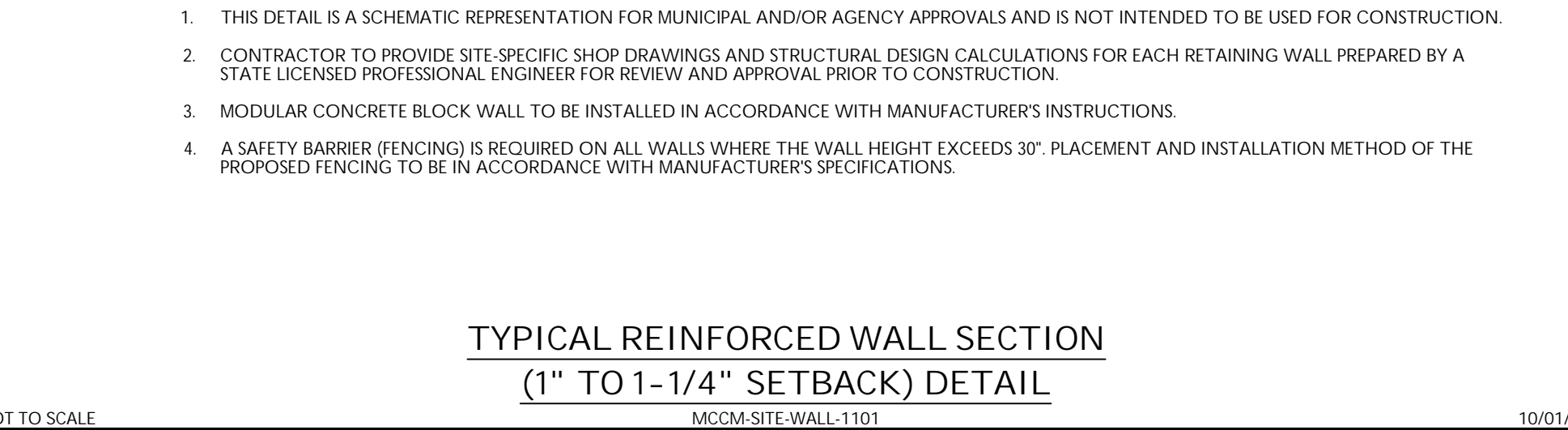
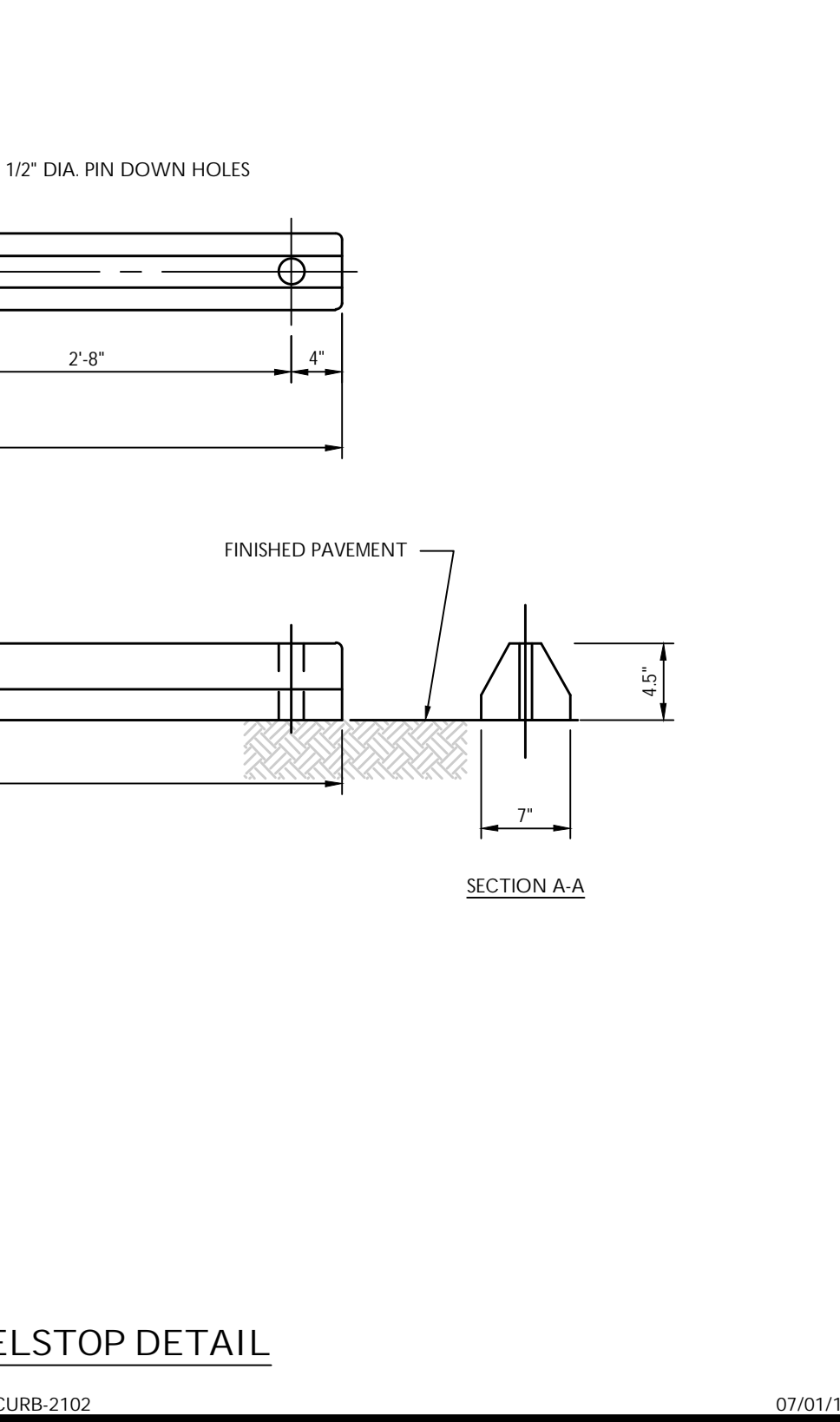
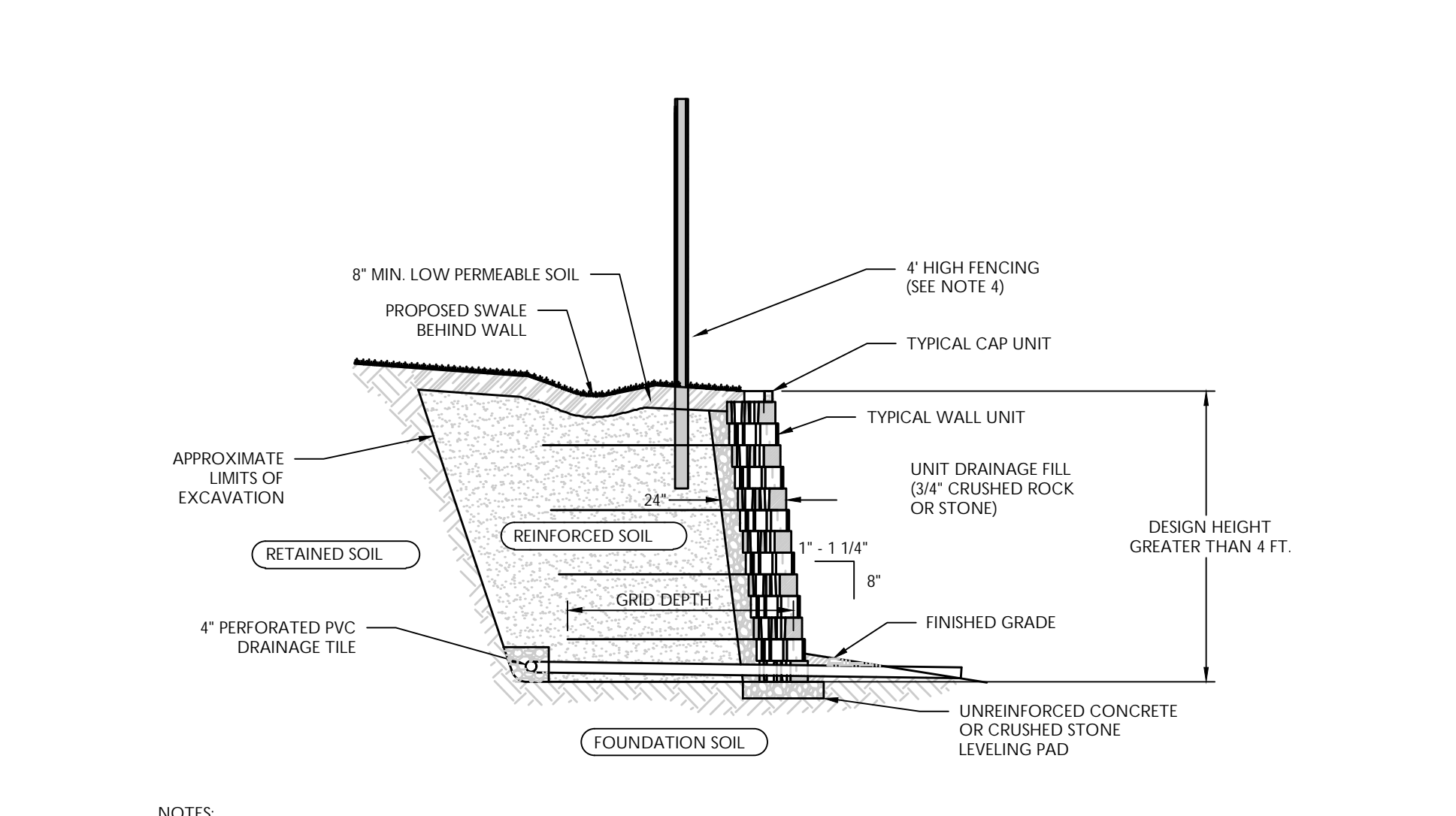
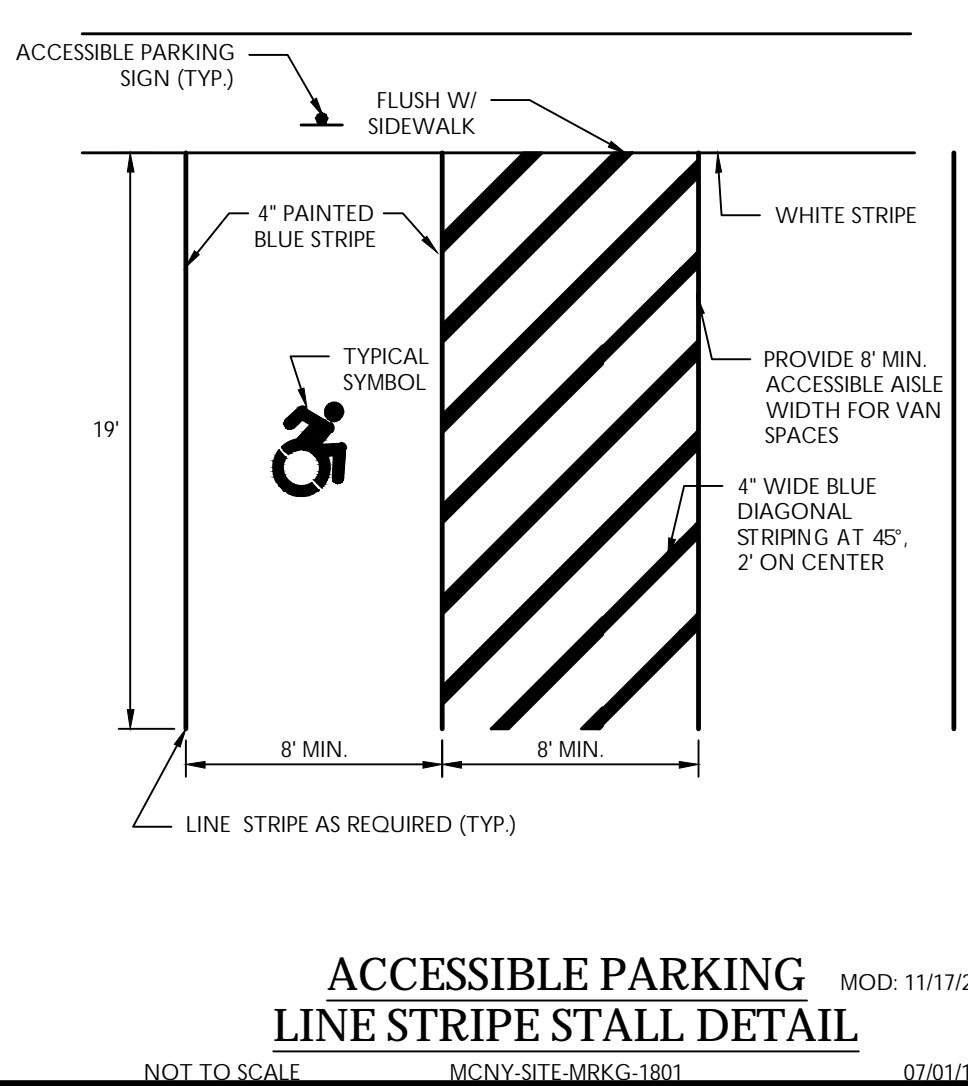
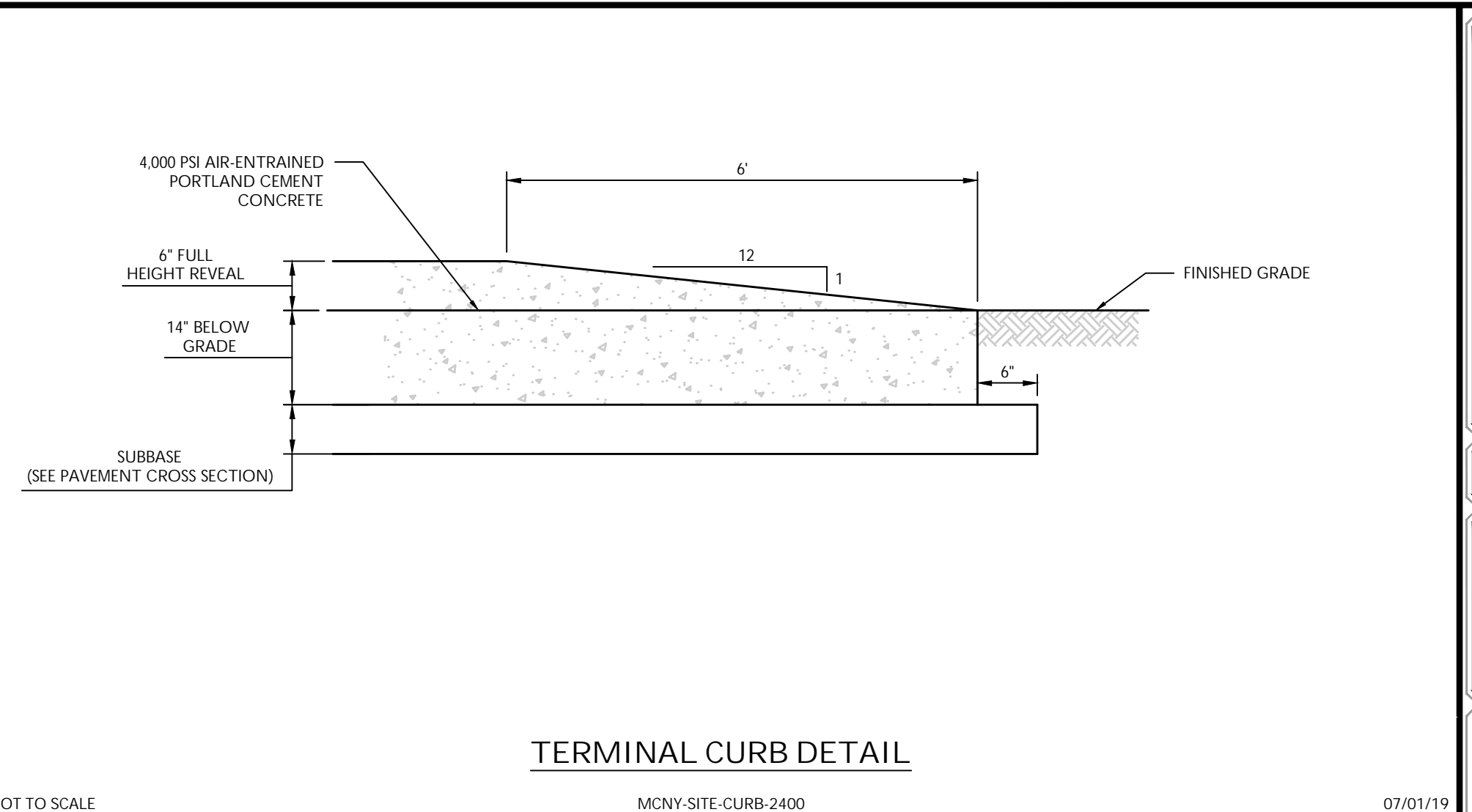
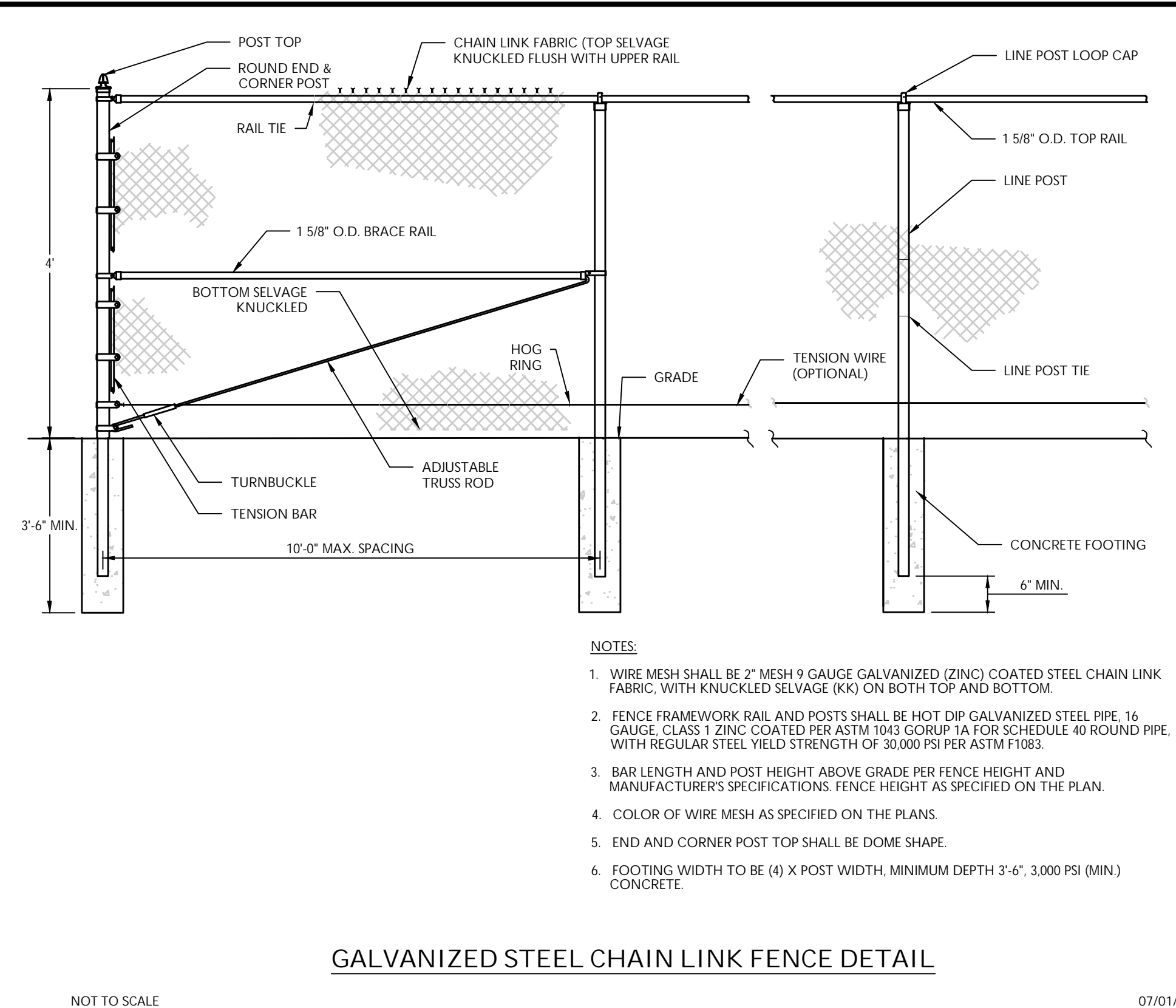
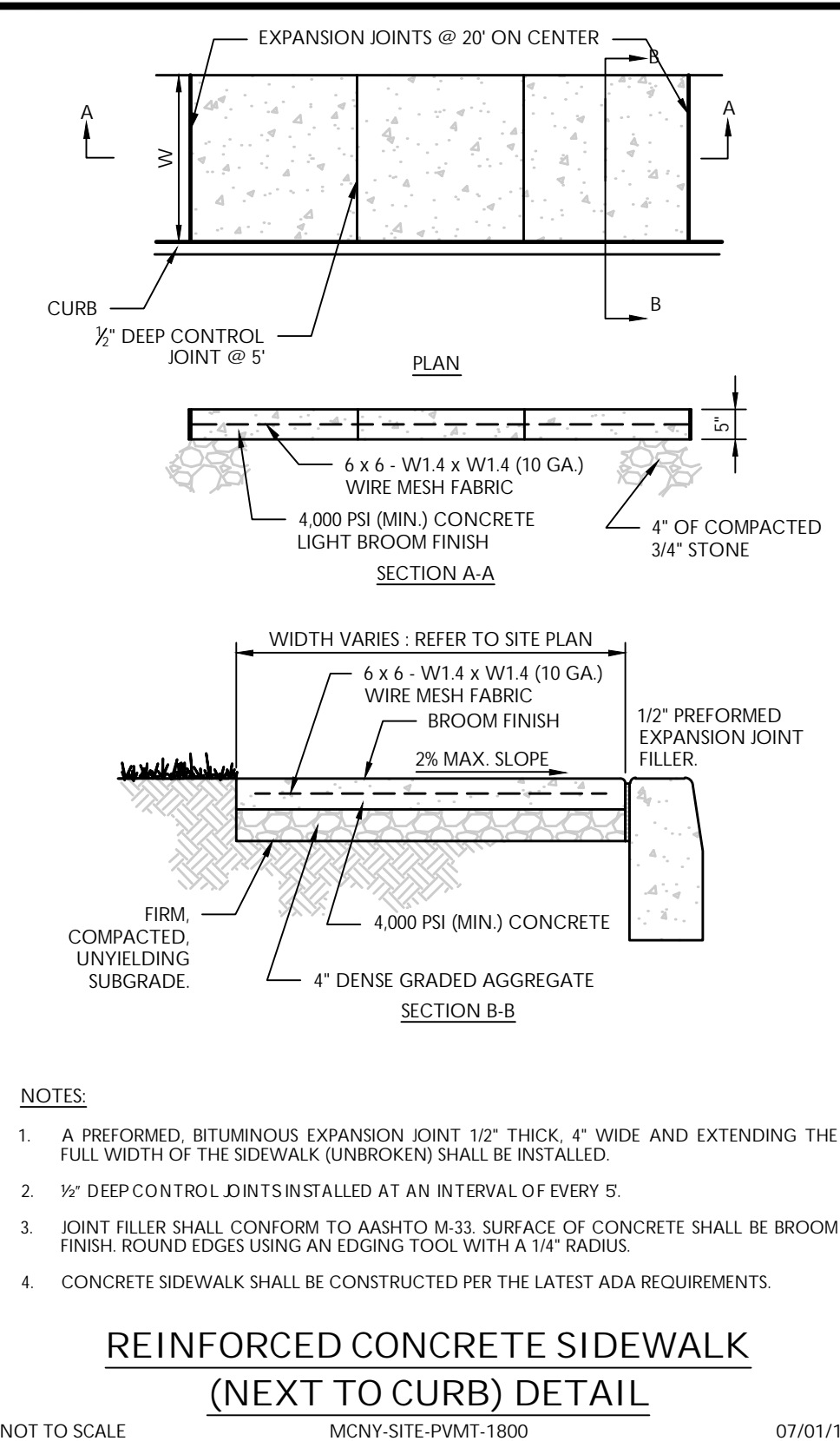
SHEET TITLE:
LIGHTING PLAN

SHEET NUMBER:
10 of 17

NOTE: DO NOT SCALE DRAWINGS FOR CONSTRUCTION.







**Colliers Engineering & Design**

www.colliersengineering.com

Copyright © 2022 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DESIGNERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE. Know what's below. Call before you dig. FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DRAWN BY	DESCRIPTION
1	02/04/22	CDR	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIS SUBMISSION
2	01/10/23	CDR	REVISED PER PLANNING BOARD COMMENTS

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
NEW YORK LICENSED PROFESSIONAL ENGINEER  
LICENSE NUMBER: 103788  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
N.Y. C.O.A. #: 0017609

**PRELIMINARY SITE PLANS FOR DEWPOINT SOUTH**

SECTION 4  
BLOCK 1  
LOT 50.32

**TOWN OF WAWAYANDA ORANGE COUNTY NEW YORK STATE**

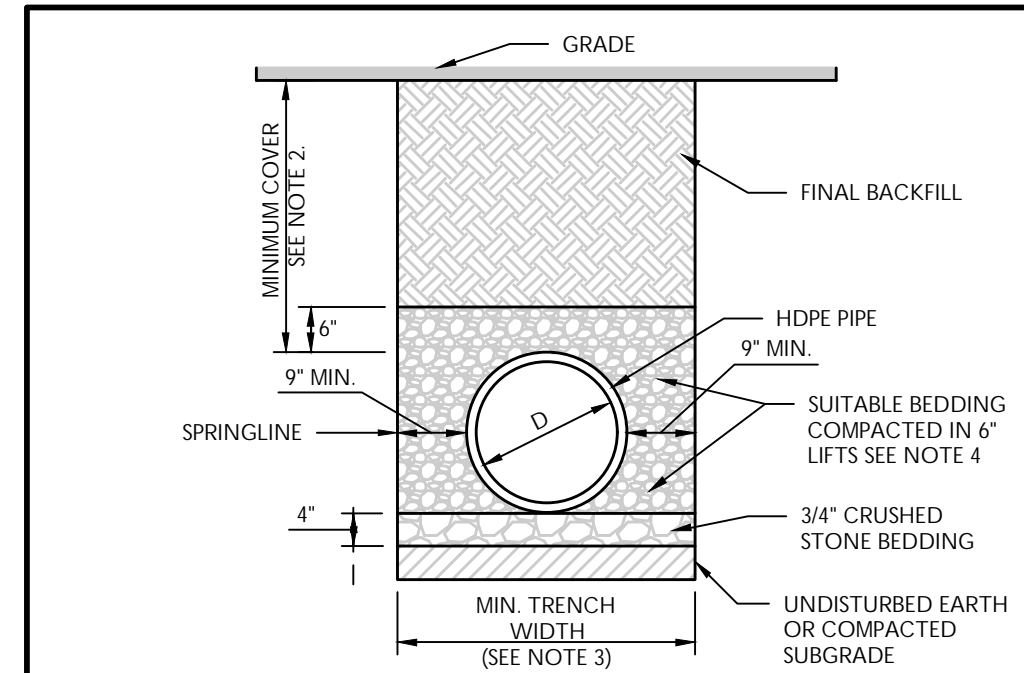
**Colliers Engineering & Design**  
NEWBURGH 555 Hudson Valley Avenue Suite 101 New Windsor, NY 12553 Phone: 845.544.4495 COLLIERS ENGINEERING & DESIGN CT, P.C. DOING BUSINESS AS MASER CONSULTANTS ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN DATE: 01/10/2022 DRAWN BY: SMB CHECKED BY: CDR  
PROJECT NUMBER: 20009912A DRAWING NAME: C-DTL5-SOUTH

SHEET TITLE: CONSTRUCTION DETAILS

SHEET NUMBER: 12 of 17

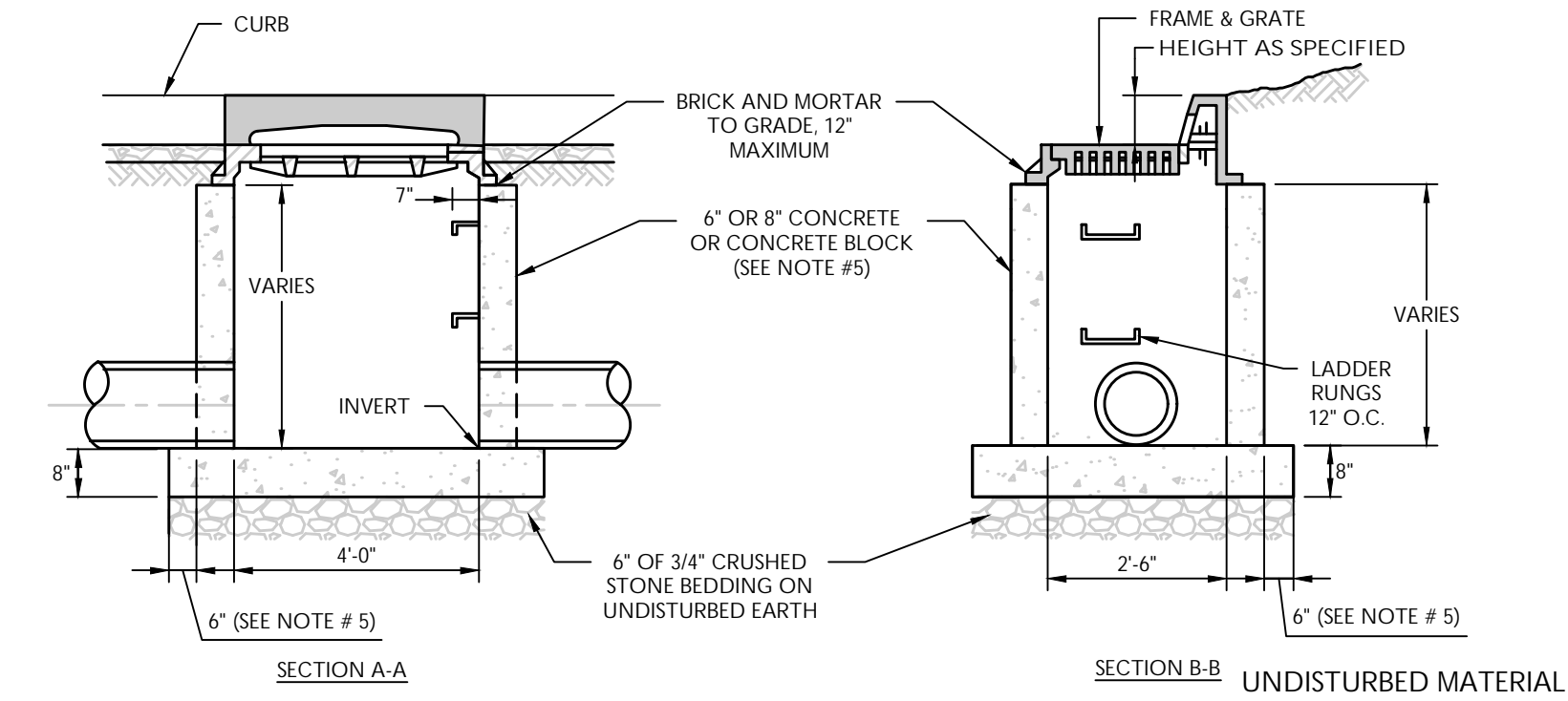
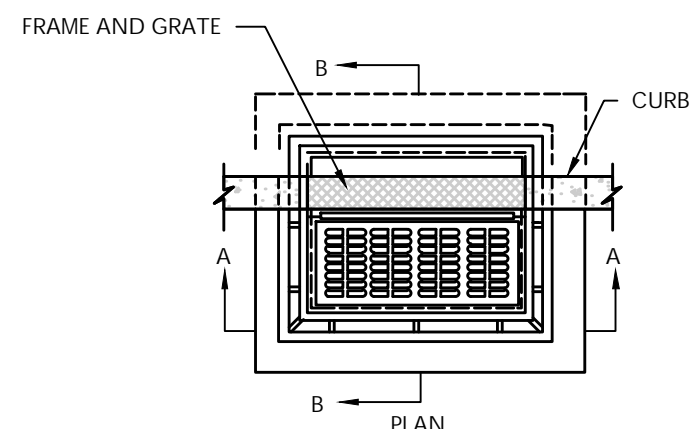
NOTE: DO NOT SCALE DRAWINGS FOR CONSTRUCTION.



- NOTES:**
- ALL PIPE SYSTEMS AND BACKFILL SHALL BE INSTALLED IN ACCORDANCE WITH ASTM D2321.
  - MINIMUM COVER FOR HDPE PIPES IS 12" UP TO 48" DIAMETER PIPE AND 24" OF COVER FOR UP TO 40" DIAMETER PIPE. PIPE COVER IS MEASURED FROM TOP OF PIPE TO THE BOTTOM OF FLEXIBLE PAVEMENT, OR TO THE TOP OF RIGID PAVEMENT, OR TO THE GROUND SURFACE.
  - MINIMUM TRENCH WIDTH PER MANUFACTURER'S RECOMMENDATIONS.
  - SUITABLE BEDDING MATERIAL SHALL BE SAND, WELL GRADED GRAVEL < 2", OR 3/4" CRUSHED STONE.
  - SUITABLE FINAL BACKFILL MATERIAL SHALL BE SITE SOILS, CLEAN FILL, OR ITEM 4 STONE COMPACTED IN MAX. 9' LIFTS.
  - STONES LARGER THAN 2" FOUND IN THE TRENCH SHALL BE REMOVED FOR A DEPTH OF AT LEAST 4" BELOW THE PIPE.
  - FOR INSTALLATION IN PAVEMENT, REFER TO THE APPLICABLE PAVEMENT DETAIL TO ESTABLISH FINAL GRADE. BACKFILL REQUIREMENTS BEYOND THE DEPTH OF THE PAVEMENT DETAIL SHALL BE IN ACCORDANCE WITH THIS DETAIL.
  -

**HDPE STORM PIPE BEDDING DETAIL**

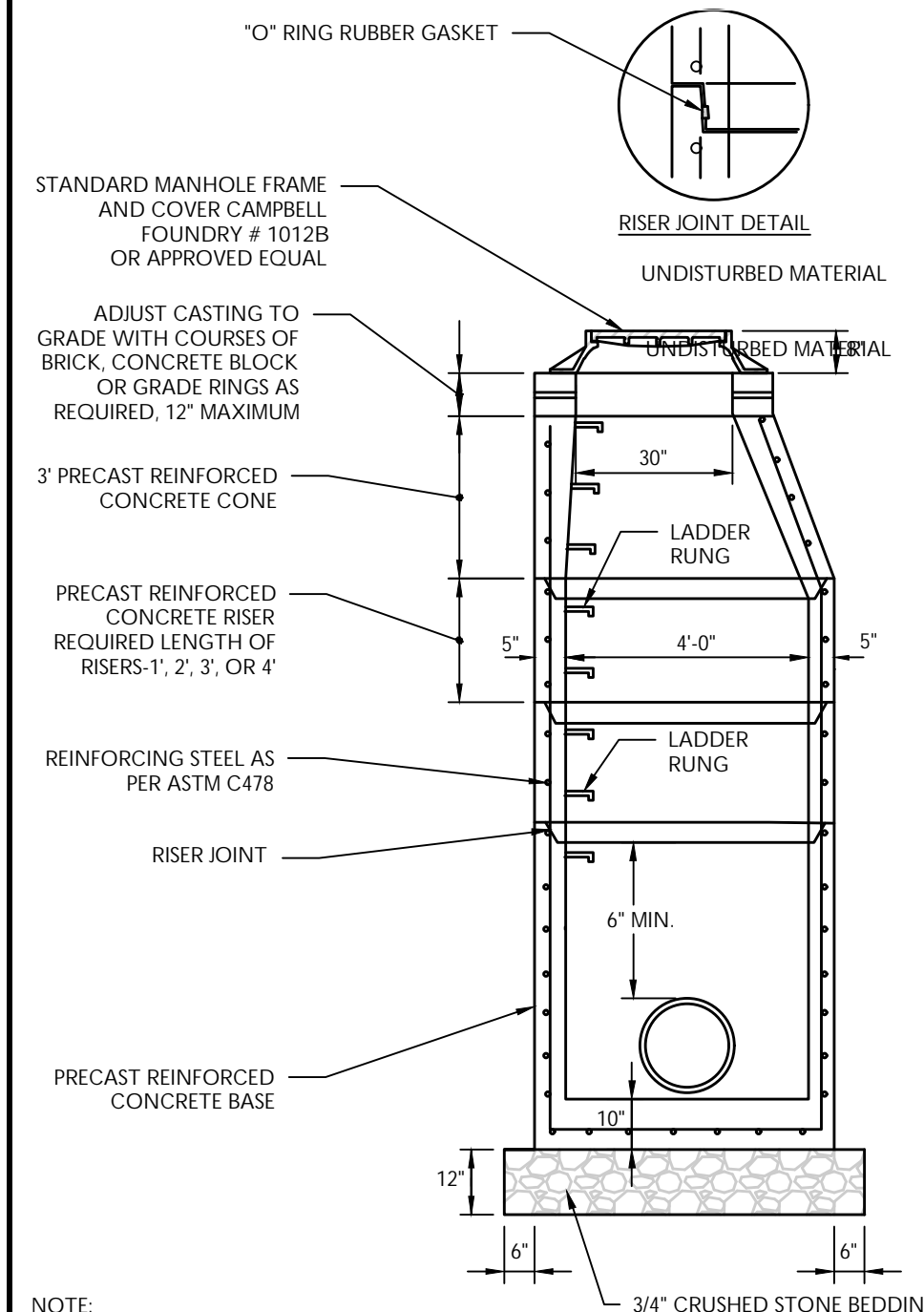
NOT TO SCALE MCNY-UTIL-STRM-2302 07/01/19



**SINGLE CATCH BASIN DETAIL**

NOT TO SCALE MCNY-UTIL-STRM-1100 07/01/19

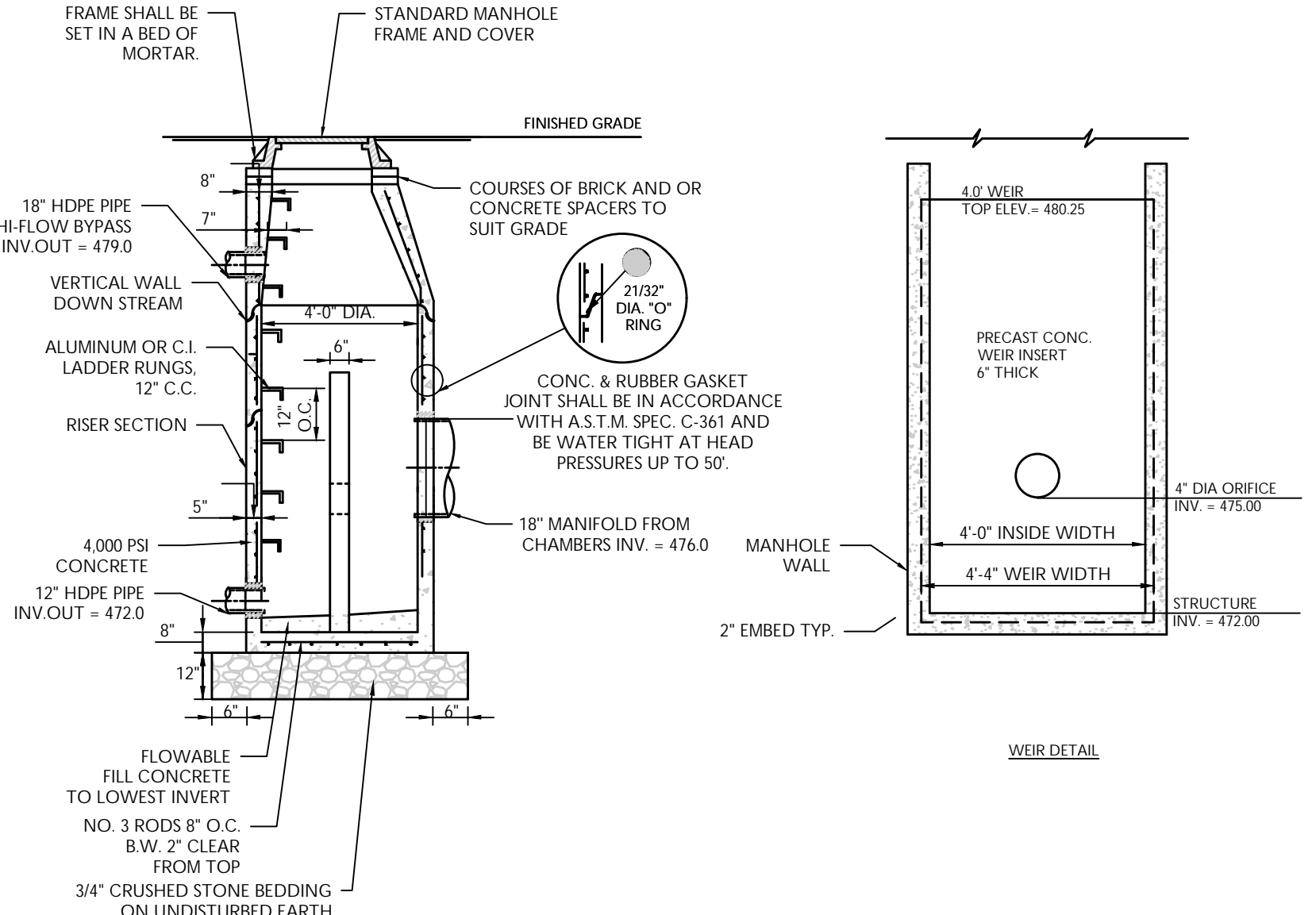
- NOTES:**
- INVERTS TO BE ELIMINATED IN BOTTOM OF TERMINAL INLETS. MINIMUM DIFFERENCE IN INVERTS TO BE 0.1 FEET.
  - THIS INLET SHALL BE CONSTRUCTED OF PRECAST CONCRETE OR SOLID CONCRETE BLOCK. IF CONCRETE BLOCK IS USED, THE BOTTOM SHALL BE AS SHOWN FOR CONCRETE. & THE OUTSIDE OF THE WALLS SHALL BE PLASTERED WITH 1/2" COAT OF 1/2 CEMENT SAND MORTAR. THE INSIDE WALL JOINTS SHALL BE STRUCK AND POINTED.
  - PROVIDE 7/8" DIA. X 7' X 12", 12" O.C. COPOLYMER POLYPROPYLENE PLASTIC STEPS WITH 1/2" DIA. GRADE 60 STEEL REINFORCEMENT BY M.A. INDUSTRIES, PS2-PF OR PS2-B WITH PRECAST PRESS FIT INSERTS, 12" O.C. OR APPROVED EQUIVALENT.
  - INLET FRAME AND GRATES TO BE CAMPBELL FOUNDRY # 2617, OR APPROVED EQUAL.
  - WHEN DEPTH IS GREATER THAN 12' THE WALLS SHOULD BE 8" THICK CONCRETE OR SOLID CONCRETE BLOCK AND THE FOOTING SHALL BE EXTENDED TO 12" BEYOND THE OUTSIDE WALLS.
  - ALL CONCRETE TO BE 4,000 PSI.
  - IN ACID SOILS, TWO COATS OF BITUMASTIC WATER PROOFING SHALL BE APPLIED PER MANUFACTURER'S SPECIFICATION.
  - INLETS SHALL BE CONSTRUCTED IN ACCORDANCE WITH H-20 LOADING REQUIREMENTS.



**PRECAST CONCRETE STORM MANHOLE 4' DIA. DETAIL**

NOT TO SCALE MCNY-UTIL-STRM-1600 07/01/19

- NOTE:**
- IN ACID SOILS, TWO COATS OF BITUMASTIC WATER PROOFING SHALL BE APPLIED PER MANUFACTURER'S SPECIFICATION.
  - ALL CONCRETE TO BE 4,000 PSI.



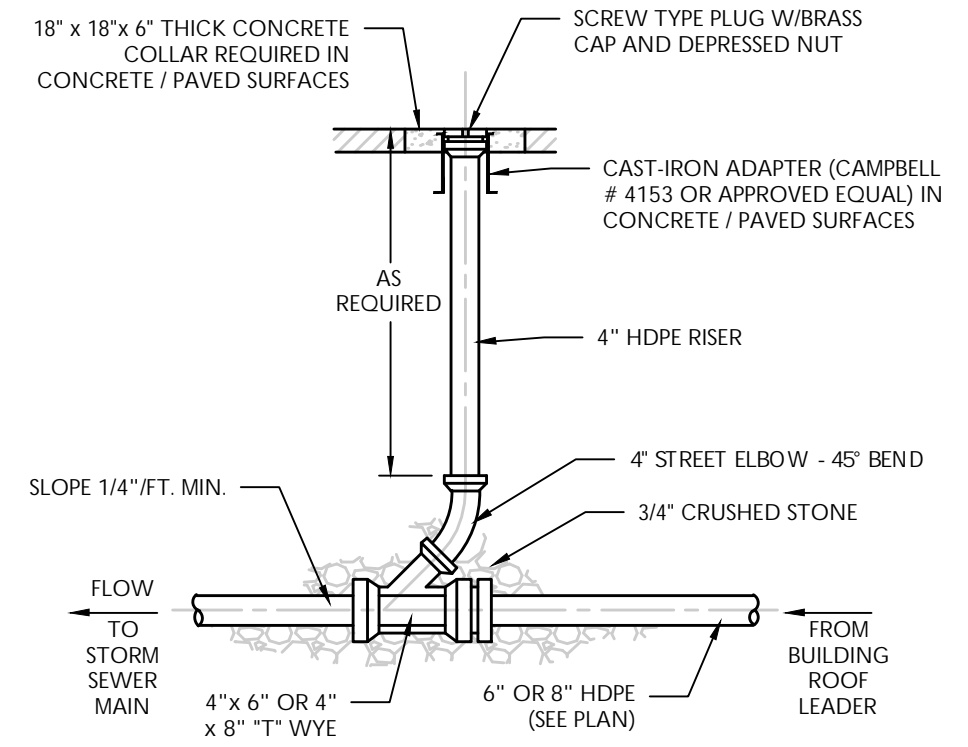
**MANHOLE OUTLET CONTROL STRUCTURE DETAIL (OCS)**

NOT TO SCALE MCNY-UTIL-STRM-1600 07/01/19

BIORETENTION ELEVATIONS					
SYSTEM	OUTLET NAME	OUTLET SIZE	BED ELEVATION	TOP OF BERM ELEVATION	EMERGENCY SPILLWAY EL.
BIO-1D	OCS BIO-1D	4'x4'	468.0	470.0	469.0
BIO-1E	OCS BIO-1E	4'x4'	467.0	470.0	469.0
BIO-1F	OCS BIO-1F	4'x4'	477.0	480.0	479.0
BIO-1BN	OCS BIO-1BN	4'x4'	490.0	494.0	493.0
BIO-2BN	OCS BIO-2BN	4'x4'	484.0	488.0	487.0

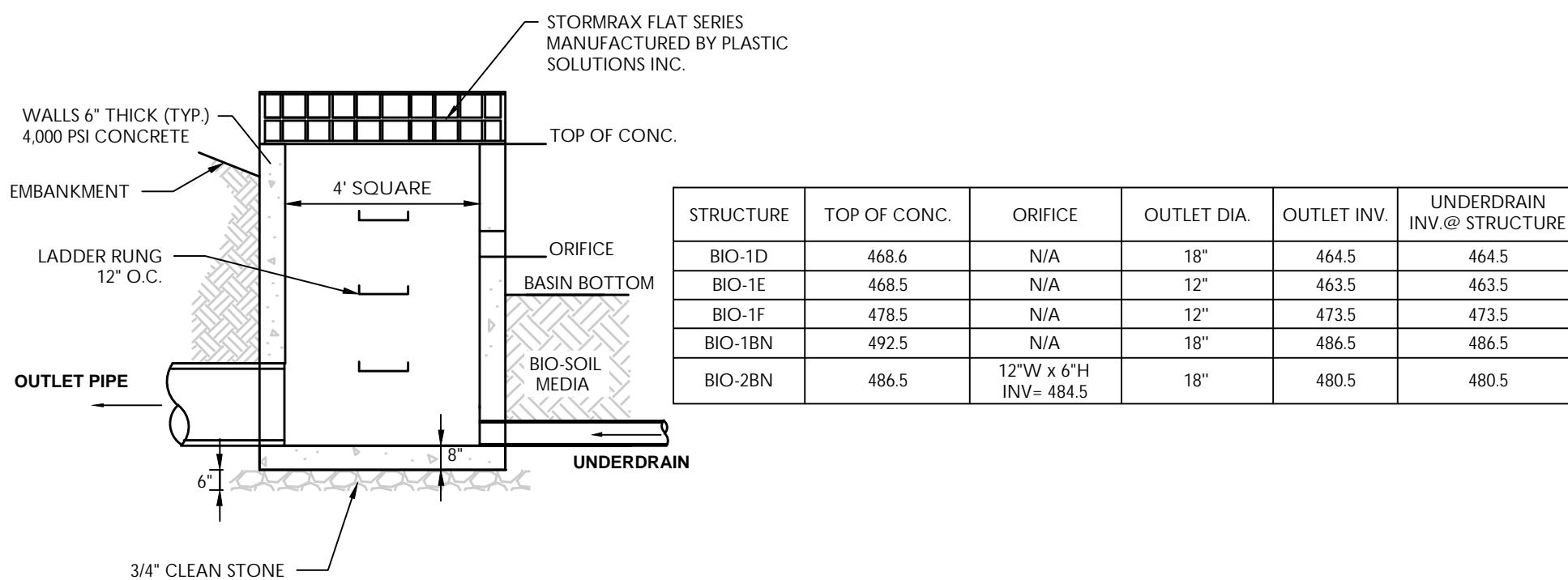
**PLANTING SOIL NOTE:**  
 THE PLANTING SOIL SHOULD BE A SANDY LOAM, LOAMY SAND, LOAM (USDA), OR A LOAM/SAND MIX (SHOULD CONTAIN A MINIMUM 35 TO 60% SAND, BY VOLUME). THE CLAY CONTENT FOR THESE SOILS SHOULD BE LESS THAN 25% BY VOLUME. SOILS SHOULD FALL WITHIN THE SM, OR ML CLASSIFICATIONS ON THE UNIFIED SOIL CLASSIFICATION SYSTEM (USCS). A PERMEABILITY OF AT LEAST 1.0 FEET PER DAY (0.5"/HR) IS REQUIRED (A CONSERVATIVE VALUE OF 0.5 FEET PER DAY IS USED FOR DESIGN). THE SOIL SHOULD BE FREE OF STONES, STUMPS, ROOTS, OR OTHER WOODY MATERIAL. OVER 1" IN DIAMETER, AND BRUSH OR SEED FROM NOXIOUS WEEDS. PLACEMENT OF THE PLANTING SOIL SHOULD BE IN LIFTS OF 12" TO 18", LOOSELY COMPACTED (TAMPED LIGHTLY WITH A DOZER OR BACKHOE BUCKET). THE SPECIFIC CHARACTERISTICS ARE AS FOLLOWS:

PARAMETER	VALUE
PH RANGE	5.2 TO 7.00
ORGANIC MATTER	1.5 TO 4.0%
MAGNESIUM	35 LBS. PER ACRE, MINIMUM
PHOSPHORUS (P <sub>2</sub> O <sub>5</sub> )	75 LBS. PER ACRE, MINIMUM
POTASSIUM (K <sub>2</sub> O)	85 LBS. PER ACRE, MINIMUM
SOLUBLE SALTS	500 ppm
CLAY	10 TO 25%
SILT	30 TO 55%
SAND	35 TO 60%



**ROOF LEADER CLEANOUT DETAIL**

NOT TO SCALE MCNY-UTIL-STRM-1900 07/01/19

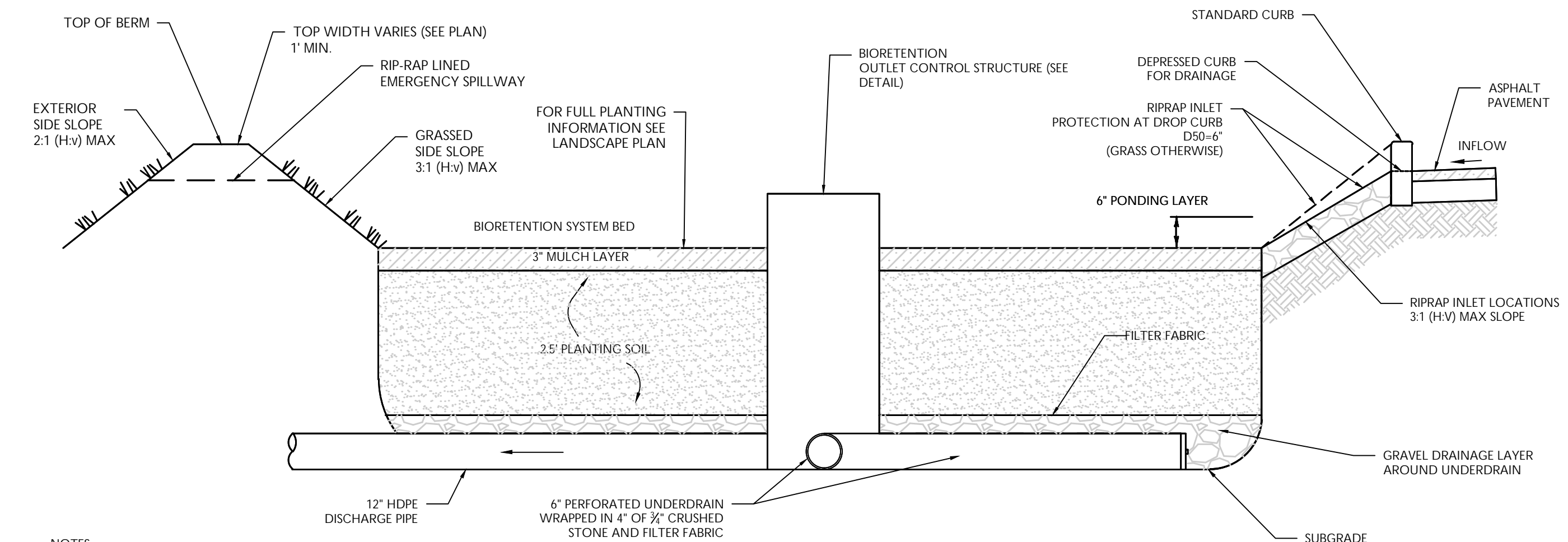


**TYPICAL BIORETENTION POND OUTLET STRUCTURE DETAIL**

NOT TO SCALE MCNY-UTIL-STRM-1800 07/01/19

STRUCTURE	TOP OF CONC.	ORIFICE	OUTLET DIA.	OUTLET INV.	UNDERDRAIN INV. @ STRUCTURE
BIO-1D	468.6	N/A	18"	464.5	464.5
BIO-1E	468.5	N/A	12"	463.5	463.5
BIO-1F	478.5	N/A	12"	473.5	473.5
BIO-1BN	492.5	N/A	18"	486.5	486.5
BIO-2BN	486.5	12"W x 6"H	18"	480.5	480.5

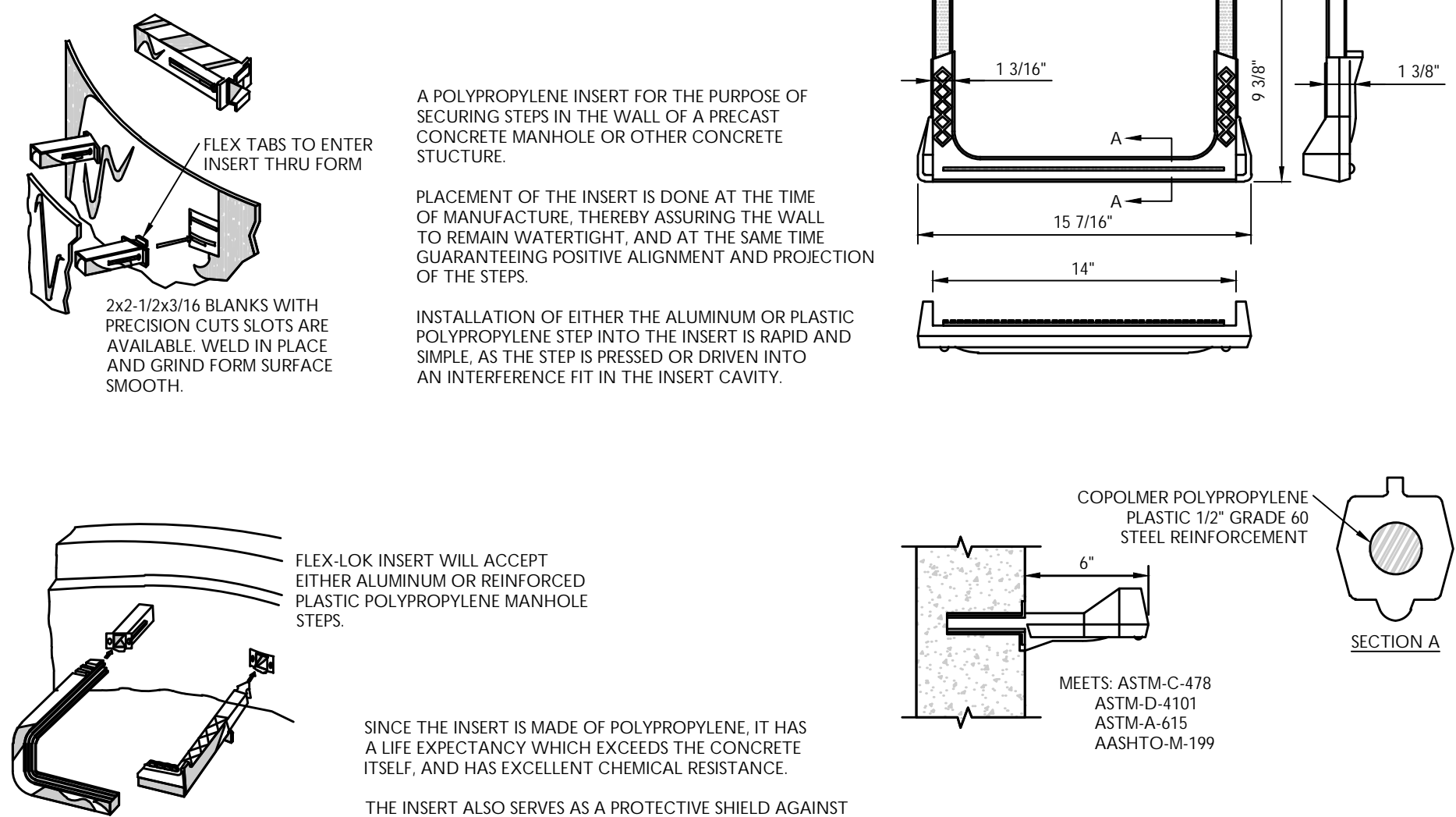
- NOTES:**
- CONTRACTOR TO SUBMIT SHOP DRAWING FOR REVIEW AND APPROVAL.
  - ALL CONCRETE TO BE 4,000 PSI (MIN.)



**BIORETENTION SYSTEM CROSS SECTION DETAIL**

NOT TO SCALE MCNY-UTIL-STRM-2400 07/01/19

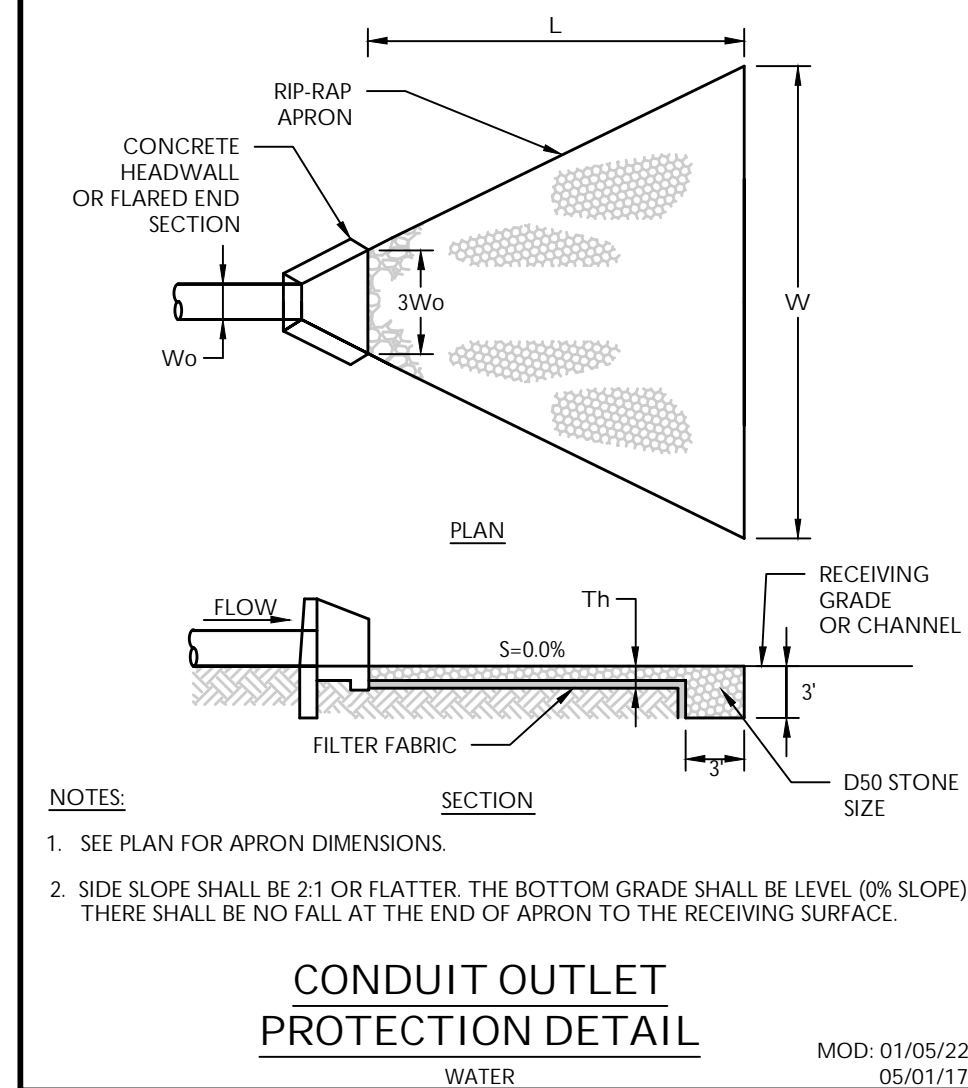
- NOTES:**
- SEE PLAN FOR DROP CURB LOCATIONS AND BIORETENTION AREA CONFIGURATION.
  - PLANTING SOIL TO BE IN ACCORDANCE WITH NEW YORK STATE STANDARDS AND SPECIFICATIONS FOUND WITHIN THE PROJECT SWPPP. CONTRACTOR MUST PROVIDE SUBMITTAL OF PROPOSED BIORETENTION SOIL FOR REVIEW & APPROVAL BY THE ENGINEER.
  - DURING CONSTRUCTION THE CONTRACTOR SHALL MINIMIZE COMPACTION OF BOTH THE BASE OF THE BIORETENTION AREA AND THE REQUIRED BACKFILL. WHEN POSSIBLE, USE EXCAVATION HOES TO REMOVE ORIGINAL SOIL. IF BIORETENTION AREAS ARE EXCAVATED USING A LOADER, THE CONTRACTOR SHOULD USE WIDE TRACK OR MARCH TRACK EQUIPMENT, OR LIGHT EQUIPMENT WITH TURF TIRE TIRES. USE OF EQUIPMENT WITH NARROW TRACKS OR NARROW TIRES, RUBBER TIRES WITH LARGE LUGS, OR HIGH PRESSURE TIRES WILL CAUSE EXCESSIVE COMPACTION RESULTING IN REDUCED INFILTRATION RATES AND STORAGE VOLUMES AND IS NOT ACCEPTABLE. COMPACTION WILL SIGNIFICANTLY CONTRIBUTE TO DESIGN FAILURE.
  - WHEN BACKFILLING THE BIORETENTION FACILITY, PLACE SOIL IN LIFTS 12" OR GREATER. DO NOT USE HEAVY EQUIPMENT WITHIN THE BIORETENTION BASIN. HEAVY EQUIPMENT CAN BE USED AROUND THE PERIMETER OF THE BASIN TO SUPPLY MATERIALS. BIORETENTION SOILS ARE TO BE GRADED BY HAND OR WITH LIGHT EQUIPMENT SUCH AS A COMPACT LOADER OR EQUIPMENT WITH MARSH TRACKS.



**LADDER RUNG (COPOLYMER) DETAIL**

NOT TO SCALE MCNY-UTIL-STRM-1600 07/01/19

- NOTES:**
- STEP INSERTS TO BE AS MANUFACTURED BY A-LOK PRODUCTS OR APPROVED EQUAL.



**CONDUIT OUTLET PROTECTION DETAIL**

NOT TO SCALE MCNY-UTIL-STRM-1600 07/01/19

- NOTES:**
- SEE PLAN FOR APRON DIMENSIONS.
  - SIDE SLOPE SHALL BE 2:1 OR FLATTER. THE BOTTOM GRADE SHALL BE LEVEL (0% SLOPE). THERE SHALL BE NO FALL AT THE END OF APRON TO THE RECEIVING SURFACE.

**TOWN OF WAWAYANDA PLANNING BOARD**

07/01/19

**Colliers Engineering & Design**  
 www.colliersengineering.com  
 Copyright © 2023 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, reused, modified, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF  
 ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DESIGNERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
 Know what's below. Call before you dig.  
 FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DESCRIPTION	DRAWN BY	CHECKED BY
1	02/04/22	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIS SUBMISSION	CDR	CDR
2	01/17/23	REVISED PER PLANNING BOARD COMMENTS	CDR	CDR

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
 NEW YORK LICENSED PROFESSIONAL ENGINEER  
 LICENSE NUMBER: 103788  
 COLLIER ENGINEERING & DESIGN CT. P.C.  
 N.Y. C.O.A.#: 0017609

**PRELIMINARY SITE PLANS FOR DEWPOINT SOUTH**

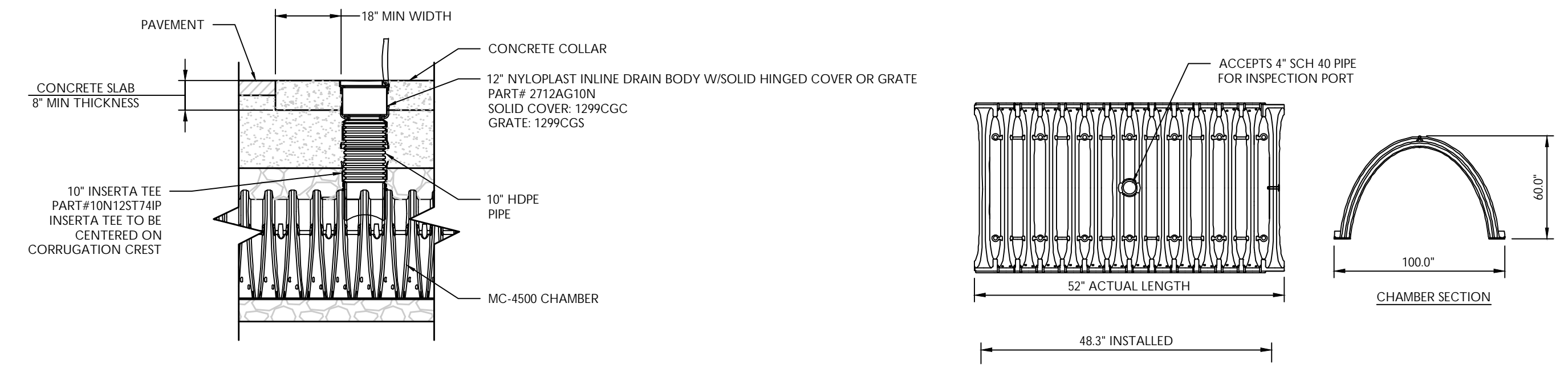
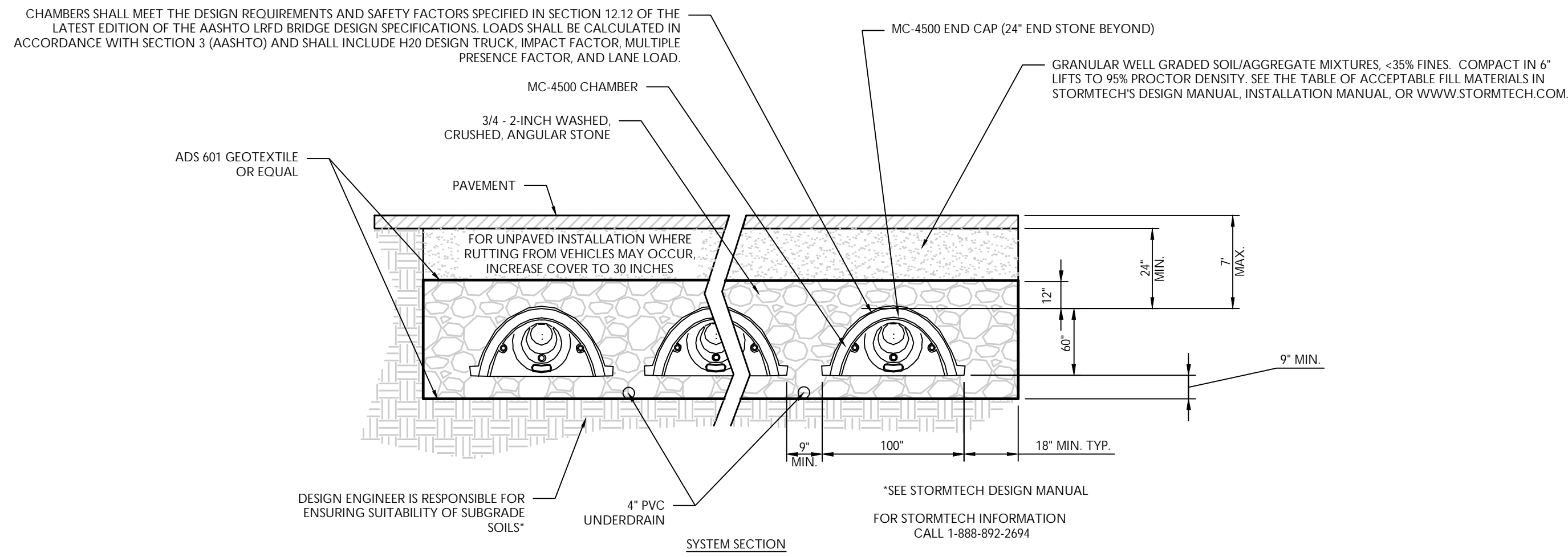
SECTION 4  
 BLOCK 1  
 LOT 50.32  
 TOWN OF WAWAYANDA  
 ORANGE COUNTY  
 NEW YORK STATE

**Colliers Engineering & Design**  
 NEWBURGH  
 555 Hudson Valley Avenue  
 Suite 101  
 New Windsor, NY 12553  
 Phone: 845.544.4495  
 COLLIER ENGINEERING & DESIGN CT. P.C.  
 DOING BUSINESS AS MASER CONSULTANTS  
 ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN DATE: 01/10/2022 DRAWN BY: SMB CHECKED BY: CDR  
 PROJECT NUMBER: 20009912A DRAWING NAME: C-DLS-50TH  
 SHEET TITLE: STORMWATER DETAILS  
 SHEET NUMBER: 13 of 17

NOTE: DO NOT SCALE DRAWINGS FOR CONSTRUCTION.





- STORMTECH NOTES:**
- CHAMBERS SHALL BE STORMTECH MC-4500 OR APPROVED EQUAL.
  - CHAMBERS SHALL BE MADE FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS.
  - CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW.
  - THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12 ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
  - ONLY CHAMBERS THAT ARE APPROVED BY THE ENGINEER WILL BE ALLOWED. THE CONTRACTOR SHALL SUBMIT (3 SETS) OF THE FOLLOWING TO THE ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
    - A STRUCTURAL EVALUATION BY A REGISTERED STRUCTURAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12 ARE MET.
    - STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL CROSS SECTION IS BASED.
  - THE INSTALLATION OF CHAMBERS SHALL BE IN ACCORDANCE WITH THE MANUFACTURER'S LATEST INSTALLATION INSTRUCTIONS.
  - THE STONE USED FOR FILLING THE SUBSURFACE SYSTEM MUST BE CLEAN WASHED STONE FREE OF ALL SEDIMENT, FINES, AND DUST. THE CONTRACTOR MAY BE REQUIRED TO WASH THE STONE ON SITE UNTIL IT IS CLEAN TO THE TOUCH LEAVING NO RESIDUE BEHIND PRIOR TO PLACEMENT IN THE SYSTEM FOOTPRINT.
  - THE PROPOSED SUBSURFACE STORMWATER SYSTEM BOTTOM MUST BE PROTECTED FROM STORM RUNOFF AT ALL TIMES DURING CONSTRUCTION. THE CONTRACTOR IS RESPONSIBLE FOR ENSURING THE INFILTRATION CAPACITY OF THE VIRGIN SOIL IS NOT COMPROMISED.
  - VEHICLE TRAFFIC MUST AVOID THE CHAMBER FOOTPRINT DURING CONSTRUCTION.
  - CONTRACTOR MUST SUBMIT SHOP DRAWINGS TO THE ENGINEER FOR REVIEW & APPROVAL.
  - END STONE TO BE 24\"/>

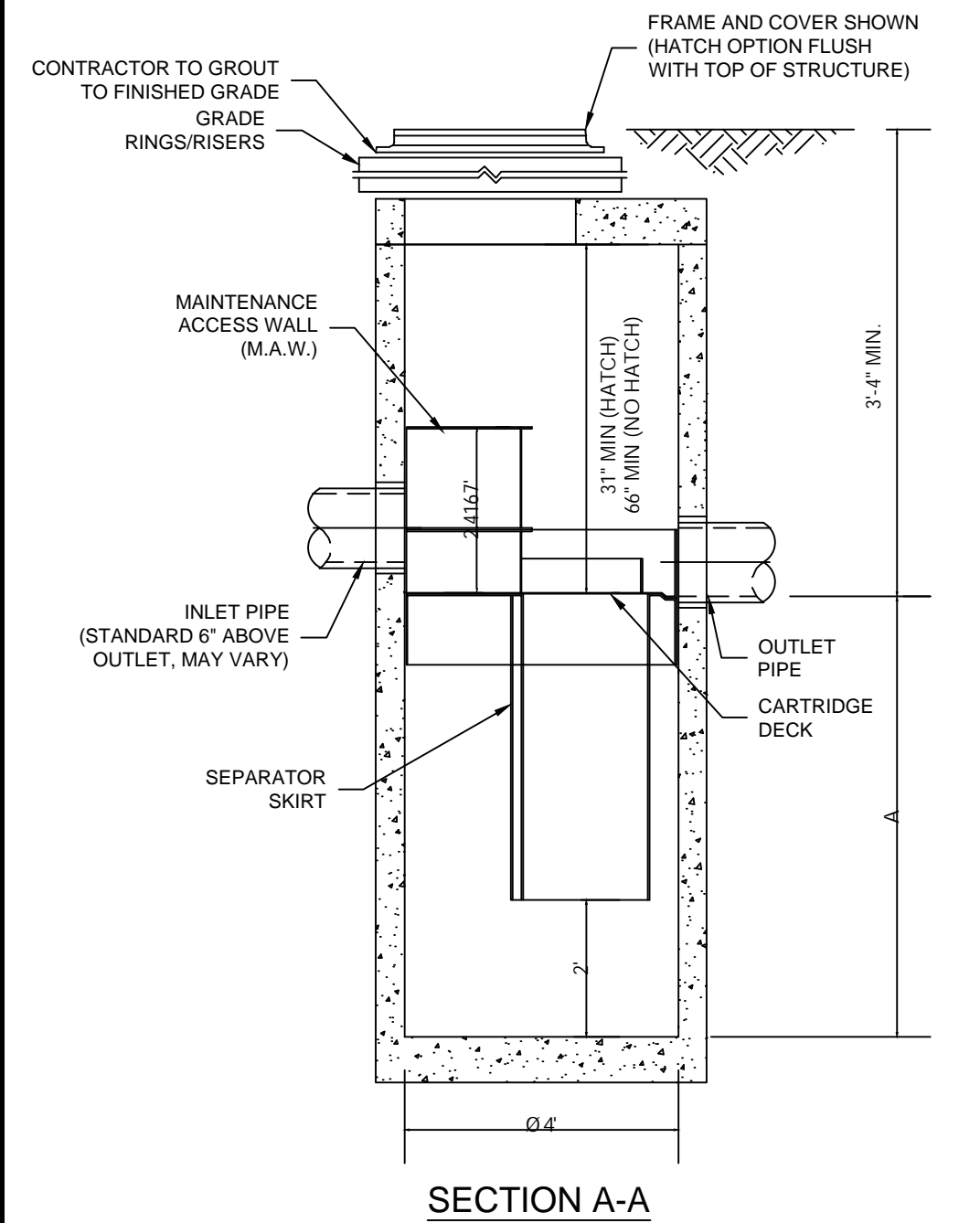
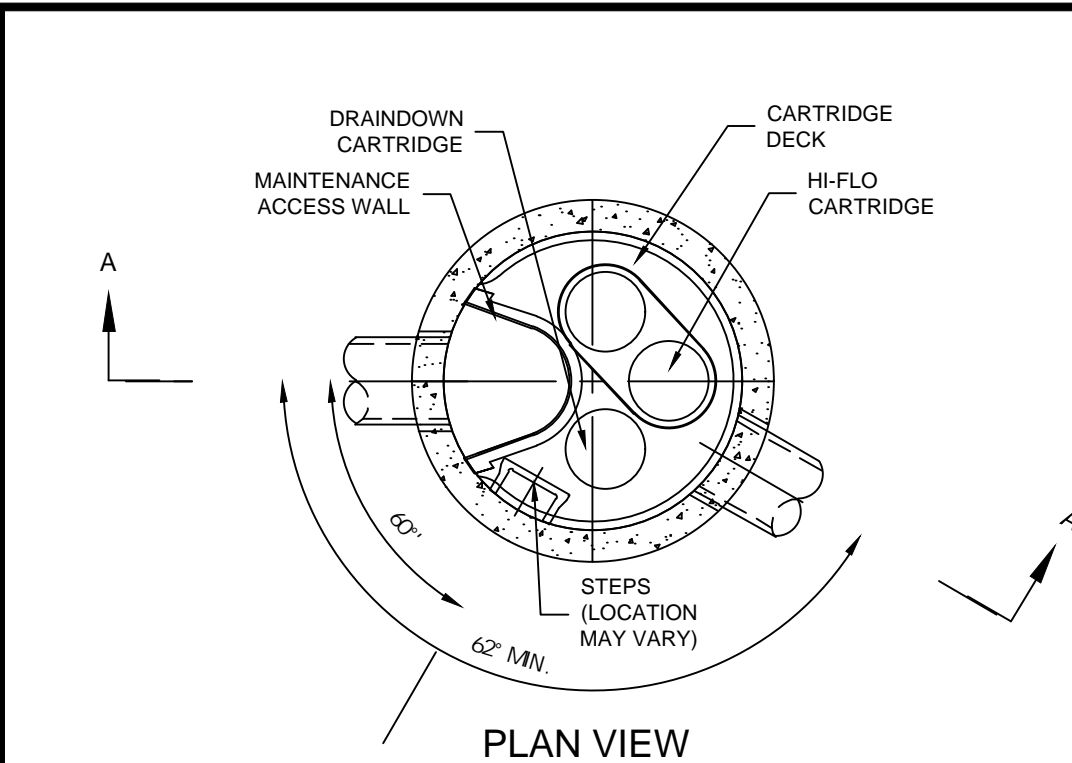
**STORMTECH SUBSURFACE DETAIL**

NOT TO SCALE

MCNY-UTIL-STMW-2500

MOD: 01/20/21  
07/01/19

NOT TO SCALE



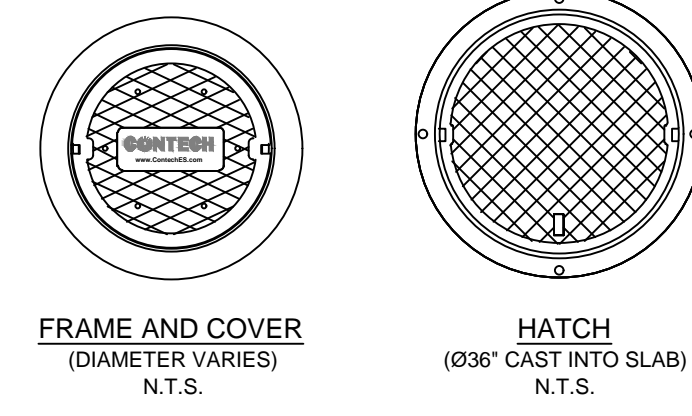
**JELLYFISH JF4 FILTER STANDARD CONFIGURATION DETAIL (OFFLINE)**

MOD: 02/02/23

**JELLYFISH DESIGN NOTES**

JELLYFISH TREATMENT CAPACITY IS A FUNCTION OF THE CARTRIDGE SELECTION AND THE NUMBER OF CARTRIDGES. THE STANDARD MANHOLE STYLE IS SHOWN. 648\"/>

CARTRIDGE SELECTION	54"	40"	27"	18"
CARTRIDGE DEPTH	54"	40"	27"	18"
OUTLET INVERT TO STRUCTURE INVERT (A)	6'-5"	5'-3"	4'-2"	3'-2"
FLOW RATE HIGH-FLO / DRAINDOWN (cfs) (per cart)	0.18 / 0.09	0.13 / 0.065	0.09 / 0.045	0.05 / 0.025
MAX. CARTS HIGH-FLO / DRAINDOWN	2 / 1			



- GENERAL NOTES:**
- CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
  - FOR SITE SPECIFIC DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHT, PLEASE CONTACT YOUR CONTECH ENGINEERED SOLUTIONS REPRESENTATIVE. [www.contech-es.com](http://www.contech-es.com)
  - JELLYFISH WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING. CONTRACTOR TO CONFIRM STRUCTURE MEETS REQUIREMENTS OF PROJECT.
  - STRUCTURE SHALL MEET AASHTO HS-20 OR PER APPROVING JURISDICTION REQUIREMENTS, WHICHEVER IS MORE STRINGENT, ASSUMING EARTH COVER OF 0'-3' AND GROUNDWATER ELEVATION AT OR BELOW THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS SHALL MEET AASHTO M306 LOAD RATING AND BE CAST WITH THE CONTECH LOGO.
  - STRUCTURE SHALL BE PRECAST CONCRETE CONFORMING TO ASTM C-478 AND AASHTO LOAD FACTOR DESIGN METHOD.
  - NO PRODUCT SUBSTITUTIONS SHALL BE ACCEPTED UNLESS SUBMITTED 10 DAYS PRIOR TO PROJECT BID DATE, OR AS DIRECTED BY THE ENGINEER OF RECORD.
- INSTALLATION NOTES:**
- ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
  - CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE STRUCTURE (LIFTING CLUTCHES PROVIDED).
  - CONTRACTOR WILL INSTALL AND LEVEL THE STRUCTURE, SEALING THE JOINTS, LINE ENTRY AND EXIT POINTS (NON-SHRINK GROUT WITH APPROVED WATERSTOP OR FLEXIBLE BOOT).
  - CONTRACTOR TO TAKE APPROPRIATE MEASURES TO PROTECT CARTRIDGES FROM CONSTRUCTION-RELATED EROSION RUNOFF.
  - CARTRIDGE INSTALLATION, BY CONTECH, SHALL OCCUR ONLY AFTER SITE HAS BEEN STABILIZED AND THE JELLYFISH UNIT IS CLEAN AND FREE OF DEBRIS. CONTACT CONTECH TO COORDINATE CARTRIDGE INSTALLATION WITH SITE STABILIZATION AT (866) 740-3318.



3025 Centre Pointe Dr., Suite 400, West Chester, OH 45380  
800-338-1122 513-645-7000 513-645-7993 FAX

**Colliers Engineering & Design**

www.colliersengineering.com

Copyright © 2023 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF  
ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DESIGNERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
Know what's below. Call before you dig.  
FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DRAWN BY	DESCRIPTION
1	02/02/23	CDR	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIS SUBMISSION.
2	01/17/23	CDR	REVISED PER PLANNING BOARD COMMENTS.

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
NEW YORK LICENSED PROFESSIONAL ENGINEER  
LICENSE NUMBER: 103788  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
N.Y. C.O.A. #: 0017609

PRELIMINARY SITE PLANS  
FOR  
DEWPOINT SOUTH

SECTION 4  
BLOCK 1  
LOT 50.32

TOWN OF WAWAYANDA  
ORANGE COUNTY  
NEW YORK STATE

**Colliers Engineering & Design**  
NEWBURGH  
555 Hudson Valley Avenue  
Suite 101  
New Windsor, NY 12553  
Phone: 845.544.4495  
COLLIERS ENGINEERING & DESIGN CT, P.C.  
DOING BUSINESS AS MASER CONSULTING ENGINEERING & LAND SURVEYING.

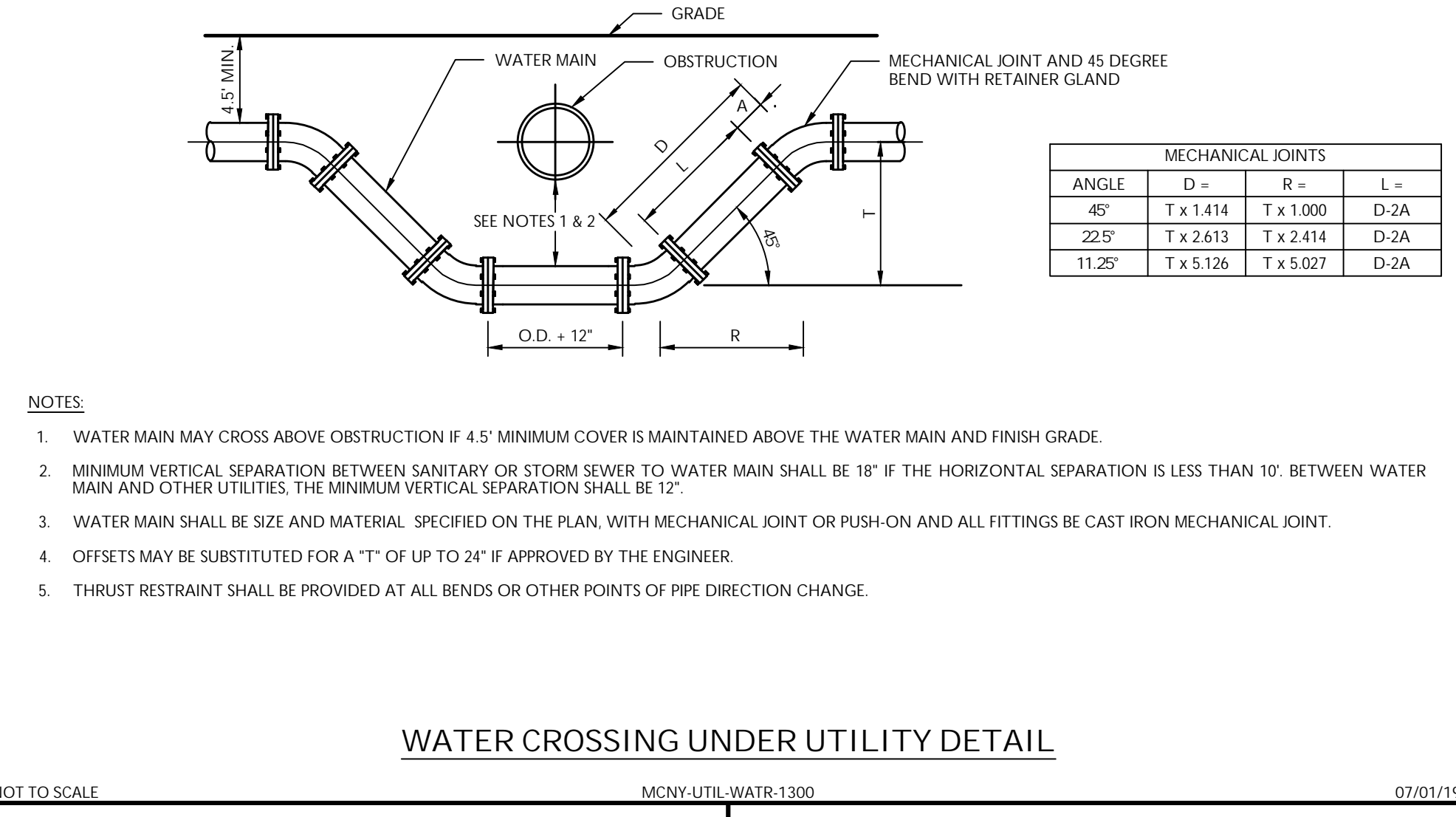
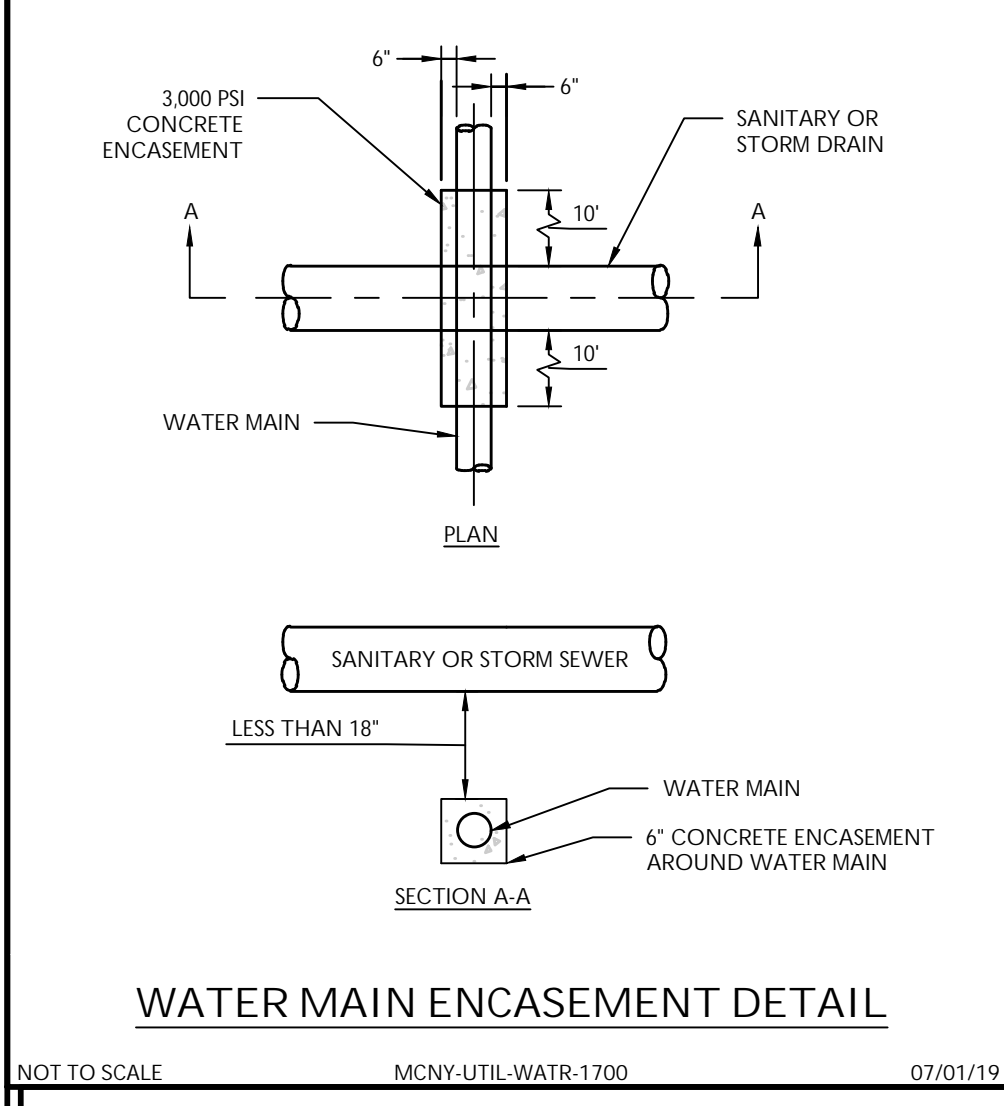
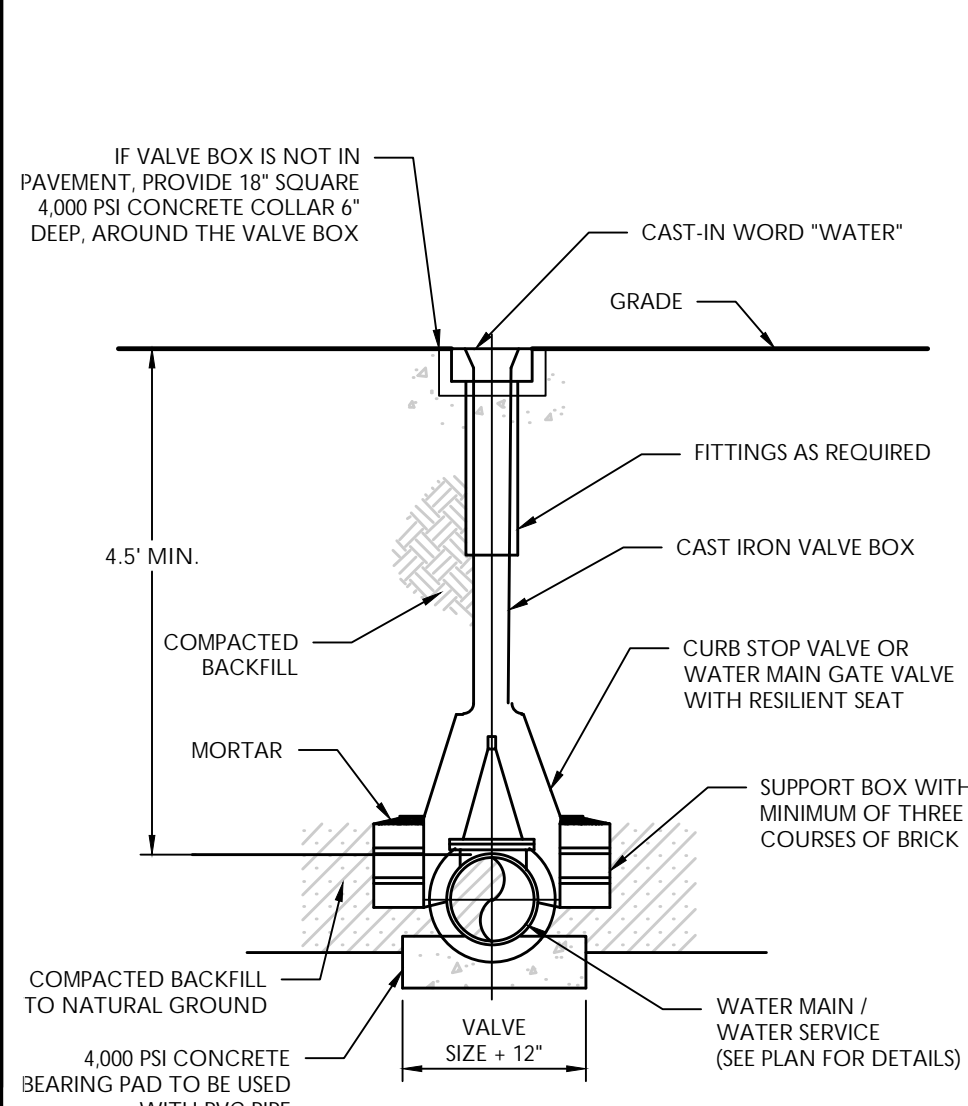
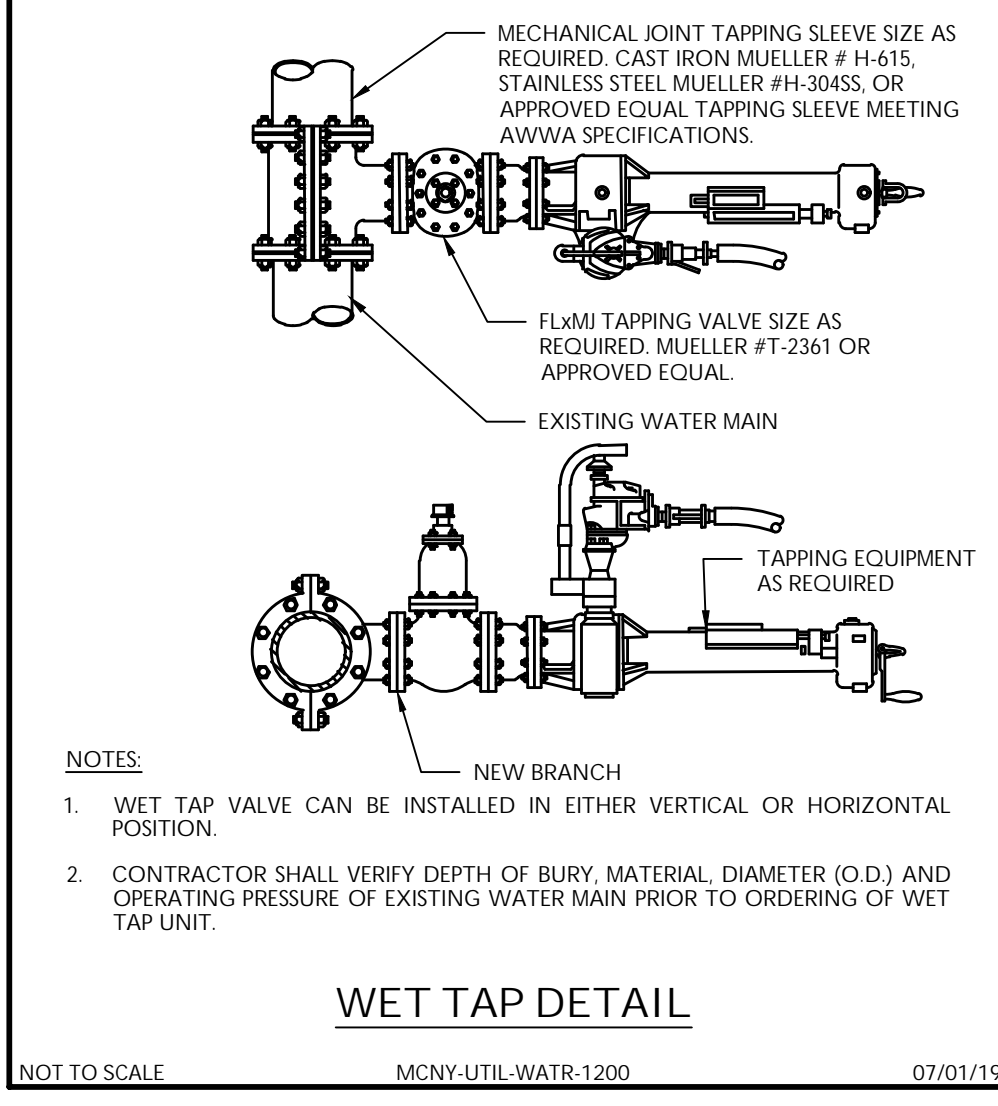
SCALE: AS SHOWN	DATE: 01/10/2022	DRAWN BY: SMB	CHECKED BY: CDR
PROJECT NUMBER: 20009912A	DRAWING NAME: C-DTLS-S0TH		
SHEET TITLE: STORMWATER DETAILS			
SHEET NUMBER: 14 of 17			

TOWN OF WAWAYANDA  
PLANNING BOARD

NOTE: DO NOT SCALE DRAWINGS FOR CONSTRUCTION.

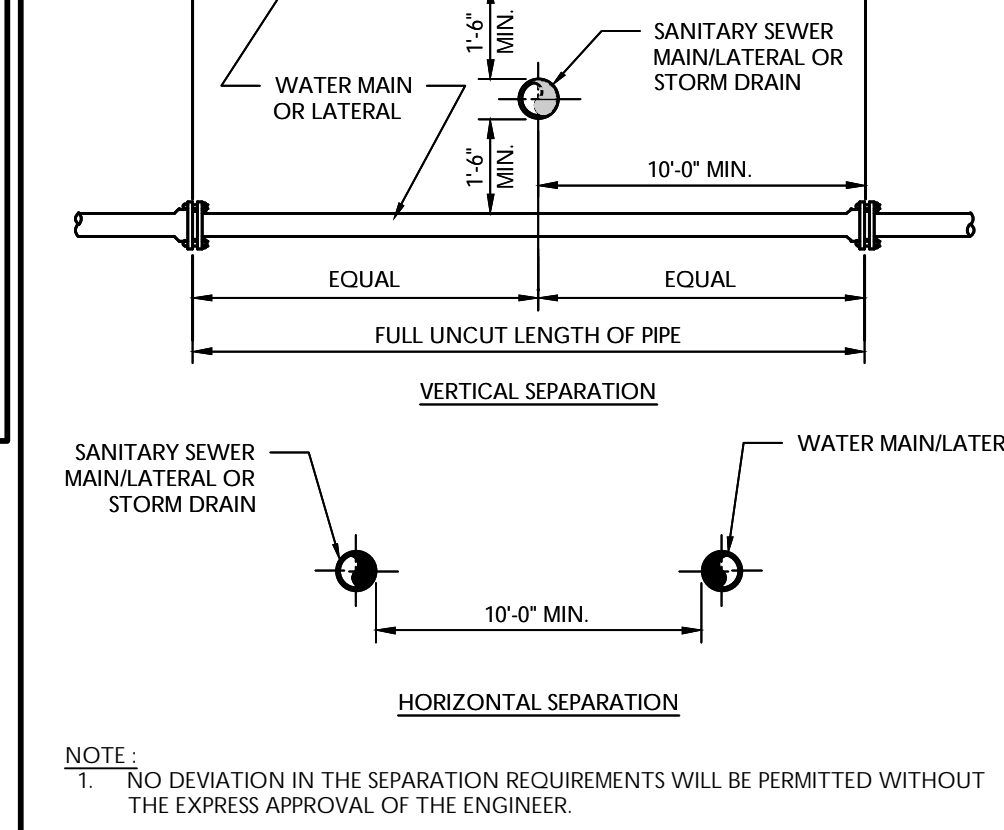
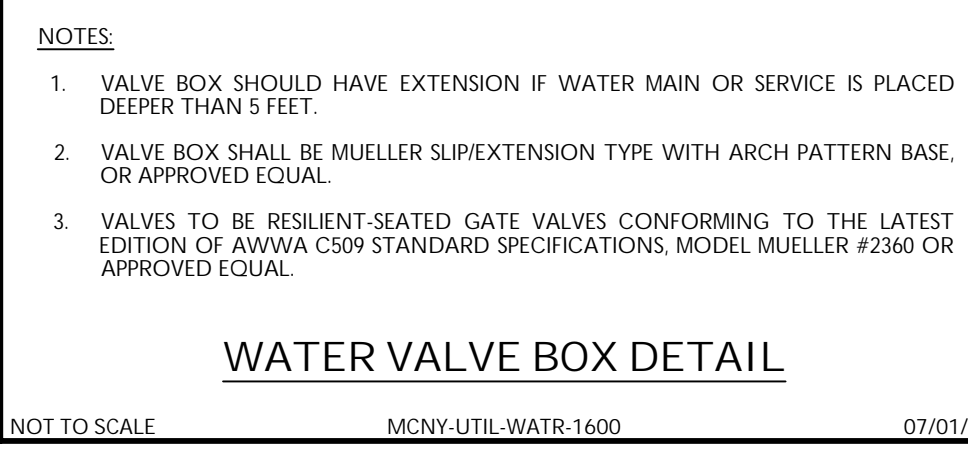
2023/02/02 2:00 PM C:\Users\kellyr\OneDrive\Documents\South\Storm\Plan\c-dtls-s0th.dwg - 14 STORM DETAILS By: KELLY RABER





**WATER NOTES:**

1. ALL METHODS, MATERIALS, FITTINGS, DEVICES, DIMENSIONAL REQUIREMENTS AND PROCEDURES NECESSARY TO COMPLETE THE WORK SHOWN HEREON SHALL MEET THE APPROPRIATE CURRENT AWWA SPECIFICATIONS IN EFFECT AS WELL AS ALL REQUIREMENTS DEEMED APPLICABLE BY THE MUNICIPALITY OR ANY OTHER GOVERNMENTAL BODY HAVING JURISDICTION OVER SAID WORK.
  2. ALL WATER MAIN PIPE SHALL BE AWWA C151/A21.51-02 THICKNESS CLASS FIFTY-TWO (52) CEMENT LINED DUCTILE IRON PUSH-ON (RUBBER GASKET) TYPE, AND INSTALLED WITH THREE (3) BRONZE WEDGES PER JOINT. JOINT INSTALLATION SHALL BE "TYPE 2" AS DESCRIBED IN THE LATEST REVISION OF AWWA C600. MECHANICAL JOINTS SHALL HAVE RETAINER GLANDS.
  3. ALL PIPE FITTINGS SHALL BE IN ACCORDANCE WITH THE LATEST REVISION OF THE AWWA SPECIFICATION C153/A21.53-00.
  4. ALL GATE VALVES SHALL BE "MUELLER" OR APPROVED EQUAL, RESILIENT-SEATED GATE VALVES WITH MECHANICAL JOINT CONNECTIONS. OPENING SHALL BE LEFT (C/W) AND OPERATION SHALL BE BY 2" SQUARE WRENCH NUT. MINIMUM WORKING PRESSURE SHALL BE 250 PSI. GATE VALVES ARE TO BE IN ACCORDANCE WITH LATEST REVISION OF AWWA SPECIFICATION C509.
  5. ALL VALVE BOXES SHALL BE EXTENSION TYPE BY MUELLER SET ON BRICKS AND POSITIONED PERPENDICULAR TO THE PIPE AND ON COMPACTED BACKFILL.
  6. ALL CHANGES IN PIPE LINE DIRECTION, BOTH HORIZONTAL AND VERTICAL SHALL BE TIE-RODDED AND MECHANICALLY RESTRAINED AS DIRECTED BY THE ENGINEER.
  7. FLUSH OUT ALL WATER MAINS AND APPURTENANCES AS DIRECTED BY THE MUNICIPALITY UNTIL THE WATER RUNS CLEAN AND FREE OF RUST AND DIRT. PRESSURIZE ALL LINES AND APPURTENANCES FOR FORTY-EIGHT (48) HOURS, OR AS DIRECTED BY THE MUNICIPALITY TO REVEAL ANY LEAKS OR BROKEN PIPE. THIS SHALL ALL BE DONE EITHER AS A TOTAL PROJECT OR BETWEEN VALVED SECTIONS AS DIRECTED BY THE TOWN. IF PRESSURE TESTING REVEALS ANY LEAKS OR DIFFICULTIES THE CONTRACTOR SHALL PROMPTLY UNCOVER THE LEAK OR BROKEN PIPE AND IMMEDIATELY REPAIR AND RETEST SAME. THIS SHALL BE REPEATED AS MANY TIMES AS MAY BE REQUIRED TO DEMONSTRATE A TIGHT LINE TO THE SATISFACTION OF THE TOWN & PROJECT ENGINEER. THE NEW WATER MAIN AND APPURTENANCES SHALL BE PRESSURE TESTED IN ACCORDANCE WITH THE LATEST REVISION OF AWWA C-600. RESULTS OF TESTS ARE TO BE SUBMITTED AND ACCEPTED BY THE MUNICIPALITY & PROJECT ENGINEER.
  8. THE MUNICIPAL ENGINEER MUST BE NOTIFIED FORTY-EIGHT (48) HOURS PRIOR TO PRESSURE TESTING.
  9. ALL WATER LINES AND APPURTENANCES SHALL BE DISINFECTED TO THE SATISFACTION OF THE MUNICIPALITY, PROJECT ENGINEER, AND IN ACCORDANCE WITH THE STANDARDS OF THE DEPT. OF HEALTH. THIS SHALL ALSO BE DONE IN ACCORDANCE WITH THE LATEST REVISION OF AWWA C651. A MINIMUM OF TWO (2) BACTERIAL TESTS TAKEN TWENTY-FOUR (24) HOURS APART ARE REQUIRED. RESULTS OF TESTS ARE TO BE SUBMITTED AND ACCEPTED BY THE MUNICIPALITY & PROJECT ENGINEER. DISINFECTION PROCEDURE, FEED LOCATIONS, AND SAMPLE LOCATIONS MUST BE REVIEWED AND APPROVED BY THE MUNICIPALITY & PROJECT ENGINEER PRIOR TO TESTING.
    - A. INSPECTING MATERIALS TO BE USED TO ENSURE THEIR INTEGRITY.
    - B. PREVENTING CONTAMINATING MATERIALS FROM ENTERING THE WATER MAIN DURING STORAGE, CONSTRUCTION, OR REPAIR AND NOTING POTENTIAL CONTAMINATION AT THE CONSTRUCTION SITE.
    - C. REMOVING, BY FLUSHING OR OTHER MEANS, THOSE MATERIALS THAT MAY HAVE ENTERED THE WATER MAIN.
    - D. CHLORINATING ANY RESIDUAL CONTAMINATION THAT MAY REMAIN, AND FLUSHING THE CHLORINATED WATER FROM THE MAIN.
    - E. PROTECTING THE EXISTING DISTRIBUTION SYSTEM FROM BACKFLOW CAUSED BY HYDROSTATIC PRESSURE TEST AND DISINFECTION PROCEDURES.
    - F. DOCUMENTING THAT AN ADEQUATE LEVEL OF CHLORINE CONTACTED EACH PIPE TO PROVIDE DISINFECTION.
    - G. DETERMINING THE BACTERIOLOGICAL QUALITY BY LABORATORY TEST AFTER DISINFECTION.
    - H. FINAL CONNECTION OF THE APPROVED NEW WATER SERVICE TO THE ACTIVE DISTRIBUTION SYSTEM.
- THE CONTINUOUS FEED METHOD SHALL BE IMPLEMENTED FOR CHLORINATION, AS DESCRIBED IN AWWA C651, LATEST REVISION. AFTER CHLORINATION, THE CONTRACTOR SHALL FLUSH THE MAINS AS PER FINAL FLUSHING REQUIREMENTS OF AWWA C651, LATEST REVISION. WHEN CUTTING INTO OR REPAIRING AN EXISTING MAIN, DISINFECTION PROCEDURES SHALL BE OBSERVED AS DETAILED IN DISINFECTION PROCEDURES WHEN CUTTING INTO OR REPAIRING EXISTING MAINS OF AWWA C651, LATEST REVISION. THE TABLET METHOD FOR INTRODUCING CHLORINE TO THE SYSTEM SHALL NOT BE PERMITTED.
- VERIFICATION SHALL BE ACCOMPLISHED VIA BACTERIOLOGICAL TESTS. AFTER FINAL FLUSHING AND BEFORE THE NEW WATER MAIN IS CONNECTED TO THE DISTRIBUTION SYSTEM, TWO CONSECUTIVE SETS OF ACCEPTABLE SAMPLES, TAKEN AT LEAST 24 HR APART, SHALL BE COLLECTED FROM THE NEW MAIN. AT LEAST ONE SET OF SAMPLES SHALL BE COLLECTED FROM EVERY 1,200 FT OF THE NEW WATER MAIN, PLUS ONE SET FROM THE END OF THE LINE AND AT LEAST ONE SET FROM EACH BRANCH. SAMPLES SHALL BE TESTED FOR BACTERIOLOGICAL, (CHEMICAL AND PHYSICAL) QUALITY IN ACCORDANCE WITH STANDARD METHODS FOR THE EXAMINATION OF WATER AND WASTEWATER, AND SHALL SHOW THE ABSENCE OF COLIFORM ORGANISMS AND THE PRESENCE OF A CHLORINE RESIDUAL. SAMPLES FOR BACTERIOLOGICAL ANALYSIS SHALL BE COLLECTED IN STERILE BOTTLES TREATED WITH SODIUM THIOSULFATE, AS REQUIRED BY STANDARD METHODS FOR THE EXAMINATION OF WATER AND WASTEWATER. NO HOSE OR FIRE HYDRANT SHALL BE USED IN THE COLLECTION OF SAMPLES. THERE SHOULD BE NO WATER IN THE TRENCH UP TO THE CONNECTION FOR SAMPLING. THE SAMPLING PIPE MUST BE DEDICATED AND CLEAN AND DISINFECTED AND FLUSHED PRIOR TO SAMPLING. A CORPORATION COOK MAY BE INSTALLED IN THE MAIN WITH A COPPER-TUBE GOOSENECK ASSEMBLY. AFTER SAMPLES HAVE BEEN COLLECTED, THE GOOSENECK ASSEMBLY MAY BE REMOVED AND RETAINED FOR FUTURE USE. IF SAMPLES RESULTS FROM THE LAB INDICATE A MEASURED HPC GREATER THAN 500 COLONY-FORMING UNITS (CFU) PER FL, FLUSHING SHOULD BE RESUMED AND ANOTHER COLIFORM AND HPC SET OF SAMPLES SHOULD BE TAKEN UNTIL NO COLIFORMS ARE PRESENT AND THE HPC IS LESS THAN 500 CFU/ML. THE RECORD OF COMPLIANCE SHALL BE THE BACTERIOLOGICAL TEST RESULTS CERTIFYING THAT THE WATER SAMPLED FROM THE NEW WATER MAIN IS FREE OF COLIFORM BACTERIA CONTAMINATION AND IS EQUAL TO OR BETTER THAN THE BACTERIOLOGIC WATER QUALITY IN THE DISTRIBUTION SYSTEM.
- ALL OTHER REQUIREMENTS OF AWWA C651, LATEST REVISION, SHALL BE OBSERVED.
10. WATER SERVICE CROSSING SEWER OR STORM SHALL BE LAID TO PROVIDE A MINIMUM VERTICAL DISTANCE OF 18" BETWEEN THE OUTSIDE OF THE WATER MAIN AND THE OUTSIDE OF THE SEWER OR STORM. THIS SHALL BE THE CASE WHERE THE WATER MAIN IS EITHER ABOVE OR BELOW THE SEWER. AT CROSSINGS, ONE FULL LENGTH OF WATER PIPE SHALL BE LOCATED SO BOTH JOINTS WILL BE AS FAR FROM THE SEWER OR STORM AS POSSIBLE. SPECIAL STRUCTURAL SUPPORT FOR THE WATER AND SEWER MAY BE REQUIRED.
  11. WATER SERVICE SHALL BE LAID AT LEAST 10 FEET HORIZONTALLY FROM ANY EXISTING OR PROPOSED SEWER MAIN OR SERVICE.
  12. WATER TIGHT PLUGS ARE TO BE INSTALLED IN THE ENDS OF PIPES WHEN WORK IS NOT IN PROGRESS.
  13. LEAKAGE AND HYDROSTATIC PRESSURE TESTING SHALL BE PERFORMED AT 1.5 TIMES THE WORKING PRESSURE OR 150 PSI, WHICHEVER IS GREATER.
  14. THE MAXIMUM DEFLECTION ALLOWED AT PIPE JOINTS SHALL BE LIMITED TO 80% OF THAT ALLOWED BY AWWA OR IN ACCORDANCE WITH THE MUNICIPALITY. FOR AWWA ALLOWABLE JOINT DEFLECTIONS SEE LATEST REVISION OF AWWA SPECIFICATION C600.
  15. CONSTRUCTION MUST CONFORM TO ALL ORDINANCES.
  16. CONTRACTOR SHALL VERIFY THE LOCATION AND ELEVATION OF EXISTING WATER AND OTHER UTILITIES PRIOR TO THE COMMENCEMENT OF CONSTRUCTION.
  17. CONTRACTOR TO CALL UNDERGROUND MARK-OUT PRIOR TO COMMENCEMENT OF CONSTRUCTION AT 1-800-962-7962 FOR COMPLETE UTILITIES MARK-OUT.
  18. CONTRACTOR TO CONTACT WATER DEPARTMENT AT LEAST 2 DAYS PRIOR TO CONSTRUCTION.
  19. ALL IMPROVEMENTS SHALL BE INSPECTED BY A PROFESSIONAL ENGINEER LICENSED IN THE STATE OF NEW YORK AND CERTIFICATION SHALL BE PROVIDED TO THE MUNICIPALITY THAT THE SUBJECT IMPROVEMENTS HAVE BEEN CONSTRUCTED IN ACCORDANCE WITH THE APPROVED PLANS.
  20. CONTRACTOR TO NOTIFY ENGINEER OF ANY DEVIATION FROM THE HORIZONTAL OR VERTICAL ALIGNMENTS WITH REGARDS TO EXISTING UTILITIES.
  21. A CERTIFIED AS BUILT MAP OF THE WATER SYSTEM IMPROVEMENTS SHALL BE PROVIDED TO THE MUNICIPALITY'S WATER DEPARTMENT BY A LICENSED DESIGN PROFESSIONAL.



**NUMBER AND SIZE OF RODS REQUIRED AND PIPE LENGTH IN FEET TO BE RESTRAINED**

PIPE SIZE IN INCHES	90° TEE OR DEAD END PLUG		45° BEND		22½° BEND	
	No.	SIZE	No.	SIZE	No.	SIZE
4	2	¾"	2	¾"	2	¾"
6	2	¾"	2	¾"	2	¾"
8	4 or 2	¾" or 1"	50'	2	¾"	15'
10	4 or 2	¾" or 1"	60'	2	¾"	20'
12	4	1"	70'	2	¾"	20'
14	4	1"	80'	2	¾"	25'
16	4	1"	80'	2	¾"	25'

**L\* = LENGTH OF PIPE TO BE RESTRAINED IS FOR EACH SIDE OF BEND**

**NOTES:**

1. USE OF MECHANICAL JOINT RETAINER GLOVES SHALL PROVIDE A THRUST RESTRAINT SYSTEM EQUIVALENT TO THAT LISTED IN THE TABLE FOR CLAMPS AND RODS.
2. LENGTHS ARE BASED ON THE FOLLOWING CRITERIA: 150 PSI MAXIMUM PRESSURE AND 3'-6" OF COVER, THEREFORE THE CALCULATION IS CONSERVATIVE FOR THE PROPOSED MIN. 4'-6" COVER. TABLE IS FOR USE WITH CAST IRON PIPE OR DUCTILE IRON PIPE ONLY. IF TEST CONDITIONS ARE MORE SEVERE OR LARGER PIPES ARE PROPOSED, THEN SPECIAL COMPUTATIONS MUST BE PROVIDED BY LICENSED PROFESSIONAL ENGINEER.

**JOINT RESTRAINT SCHEDULE DETAIL**

NOT TO SCALE MCNY-UTIL-WATR-1300 07/01/19

**LIST OF STANDARD WATER SUPPLY MATERIALS**

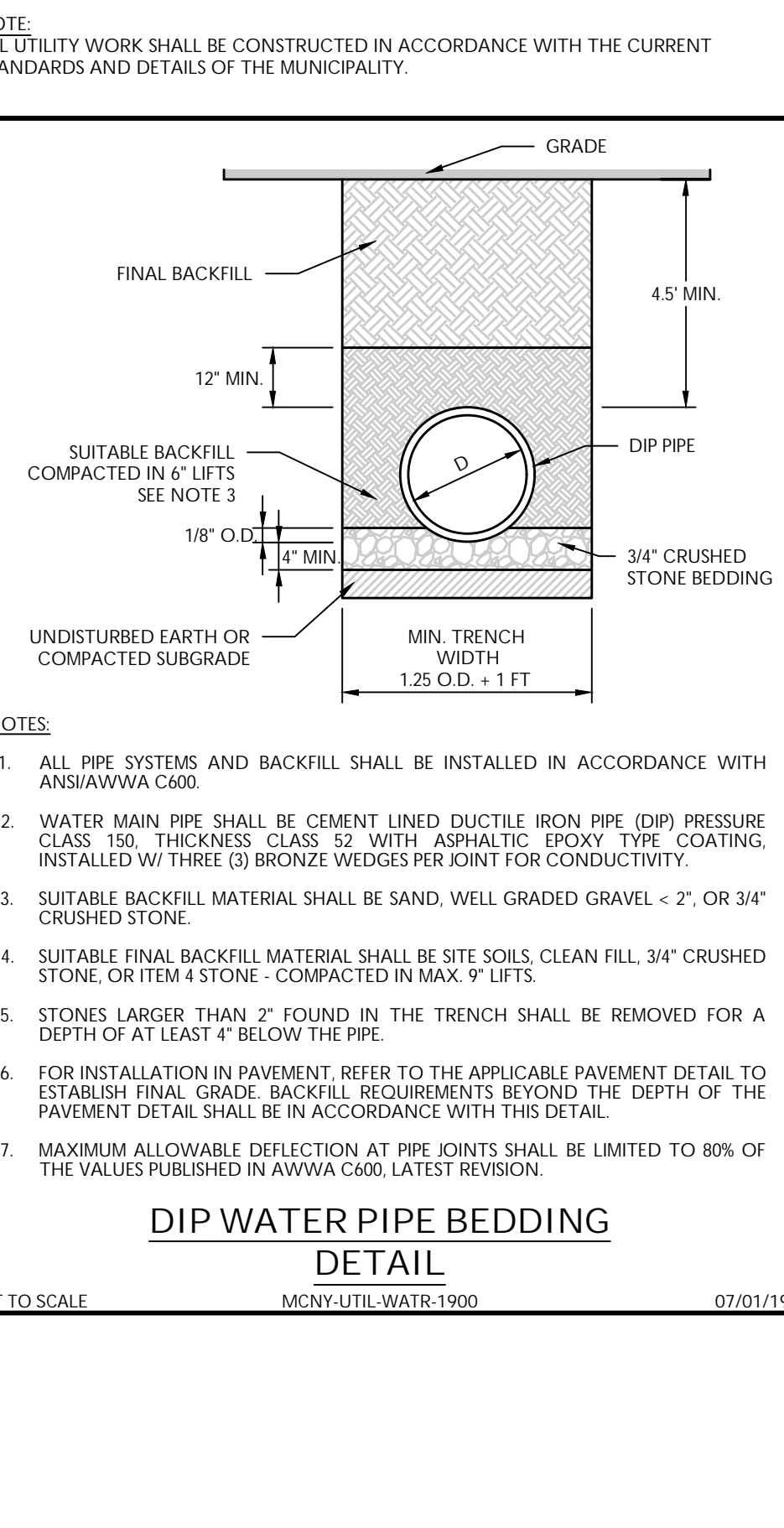
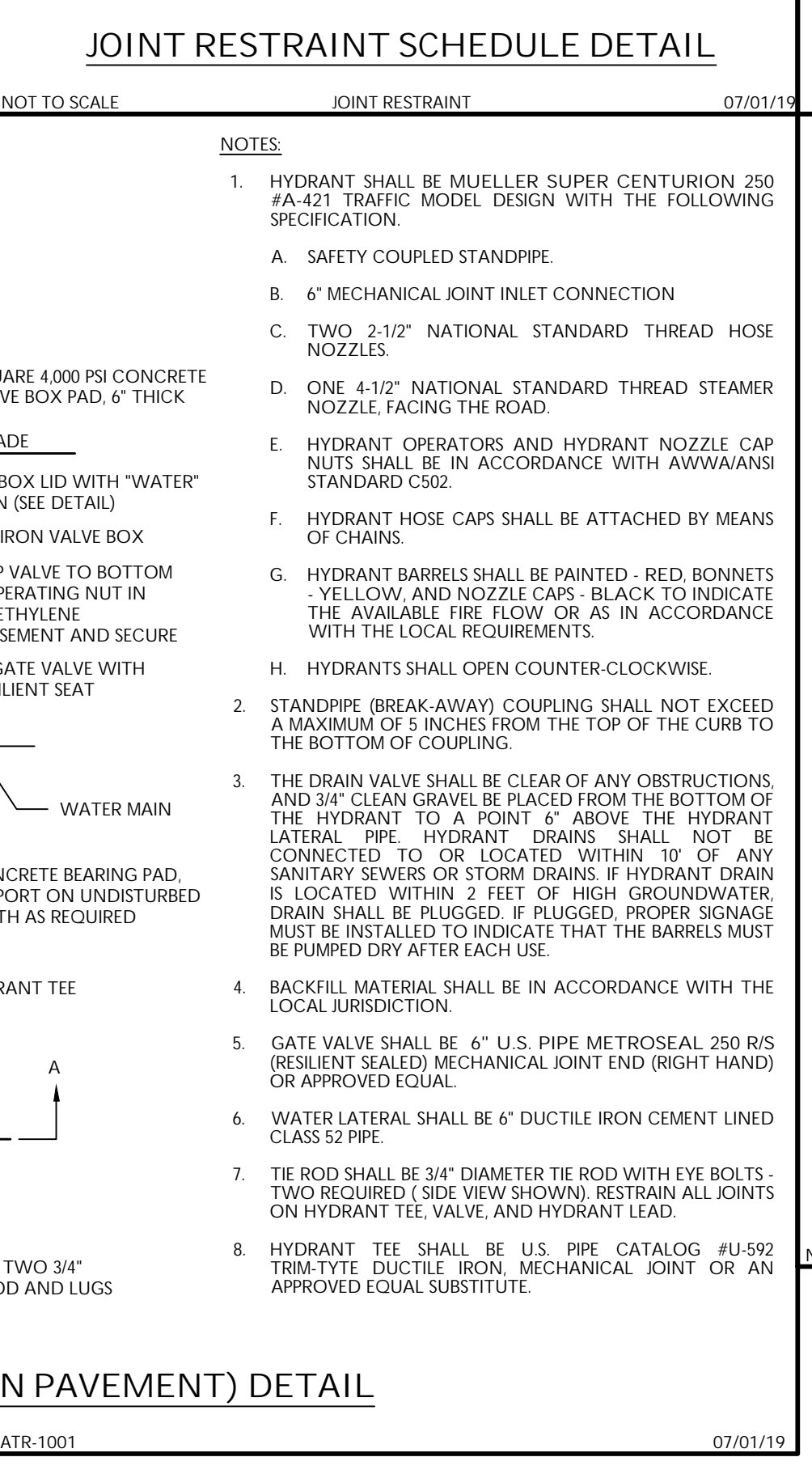
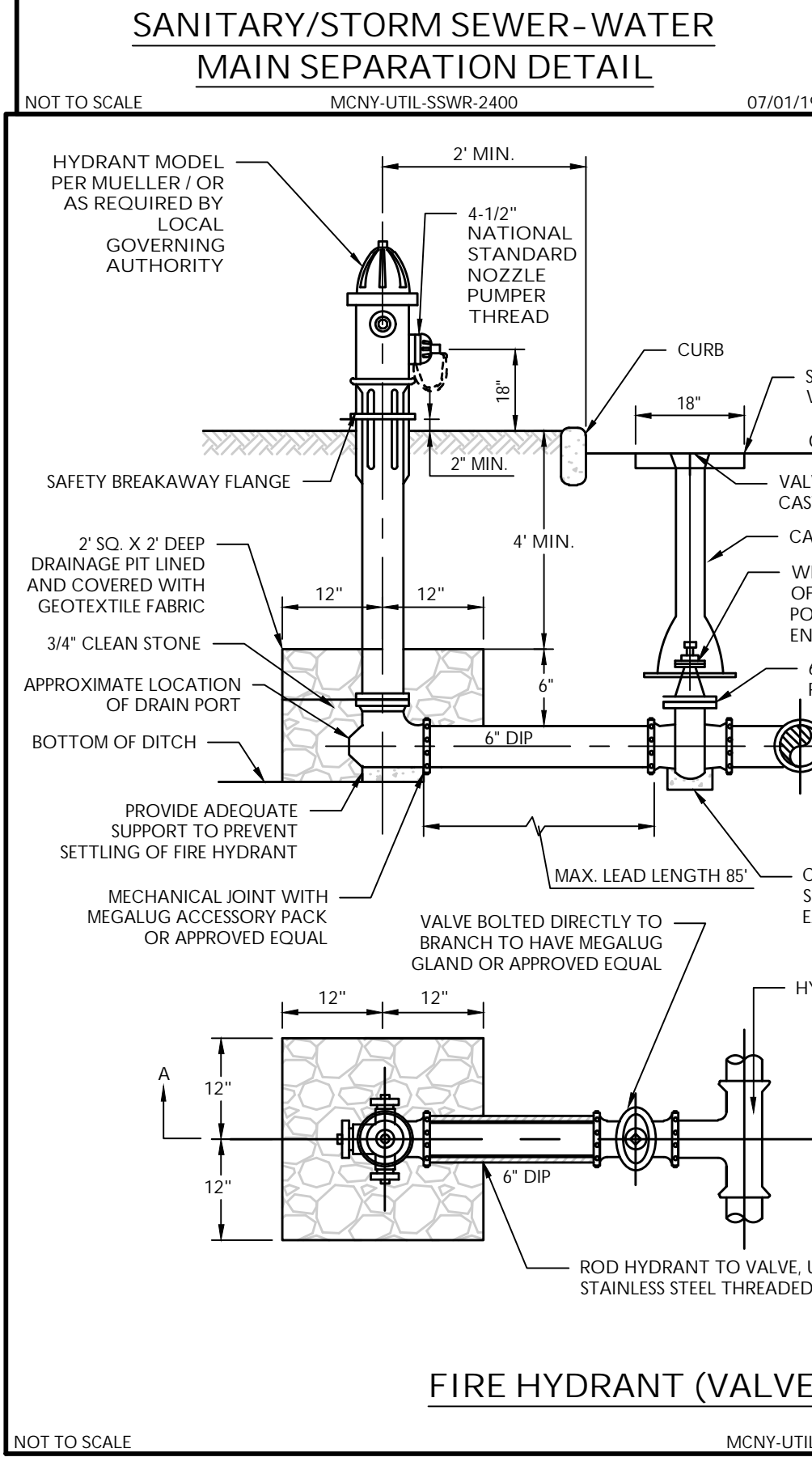
MOD: 04/23/21 07/01/19

ANY EXCEPTIONS TO THE MATERIALS LISTED BELOW SHALL BE APPROVED IN WRITING BY THE ENGINEER.

DESCRIPTION	REVISION	DATE	BY	CHKD	APP'D
HYDRANTS					
VALVES					
VALVE BOXES					
PIPE					
TAPPING SLEEVE					
TAPPING VALVE					
MECHANICAL JOINT RESTRAINTS					
FITTINGS					

**NOTES:**

ALL UTILITY WORK SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE CURRENT STANDARDS AND DETAILS OF THE MUNICIPALITY.



**Colliers Engineering & Design**

www.colliersengineering.com

Copyright © 2022 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DISBURSERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE. Know what's below. Call before you dig. FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DESCRIPTION	DRAWN BY	CHKD	APP'D
1	02/04/22	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIES SUBMISSION	CDR		
2	01/11/23	REVISED PER PLANNING BOARD COMMENTS	CDR		

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
 NEW YORK LICENSED PROFESSIONAL ENGINEER  
 LICENSE NUMBER: 103788  
 COLLIER ENGINEERING & DESIGN CT. P.C.  
 N.Y. C.O.#: 0017609

**PRELIMINARY SITE PLANS FOR DEWPOINT SOUTH**

SECTION 4  
 BLOCK 1  
 LOT 50.32

TOWN OF WAWAYANDA  
 ORANGE COUNTY  
 NEW YORK STATE

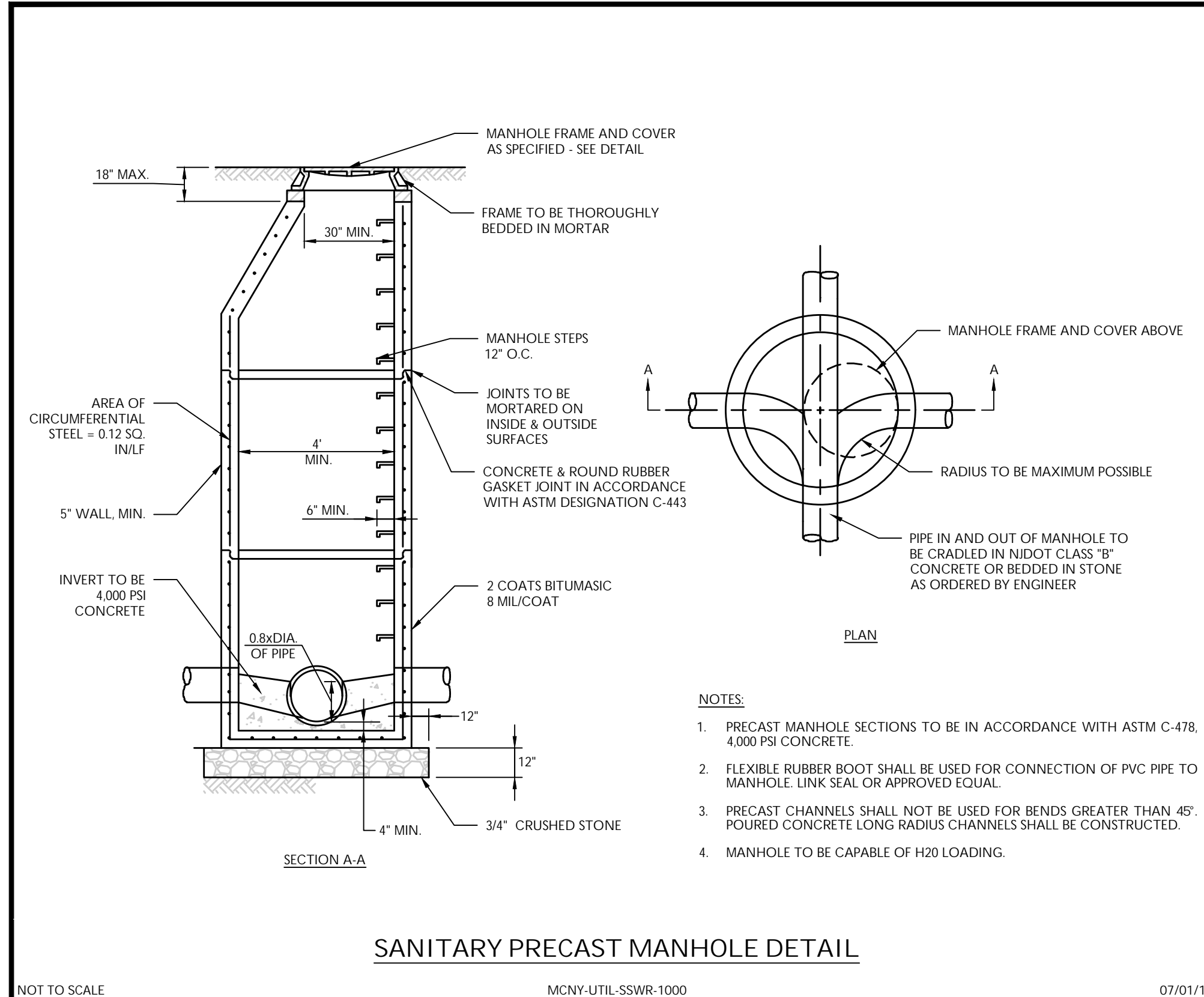
**Colliers Engineering & Design**

NEWBURGH  
 555 Hudson Valley Avenue  
 Suite 101  
 New Windsor, NY 12553  
 Phone: 845.564.4495  
 COLLIER ENGINEERING & DESIGN CT. P.C.  
 DOING BUSINESS AS MASER CONSULTANTS  
 ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN DATE: 01/10/2022 DRAWN BY: SMB CHECKED BY: CDR  
 PROJECT NUMBER: 20009912A DRAWING NAME: C-DT15-S0TH

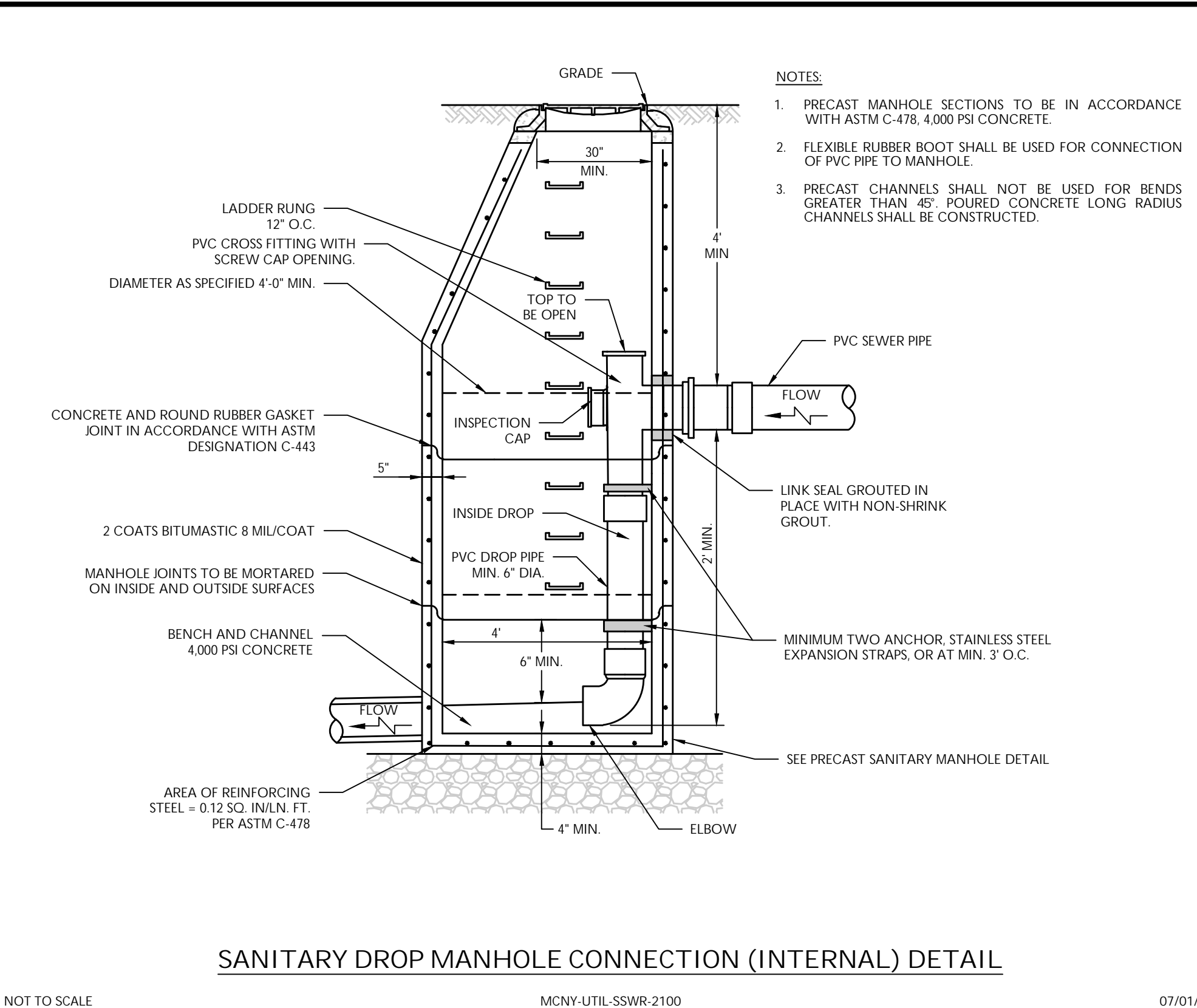
SHEET TITLE: WATER DETAILS

SHEET NUMBER: 15 of 17



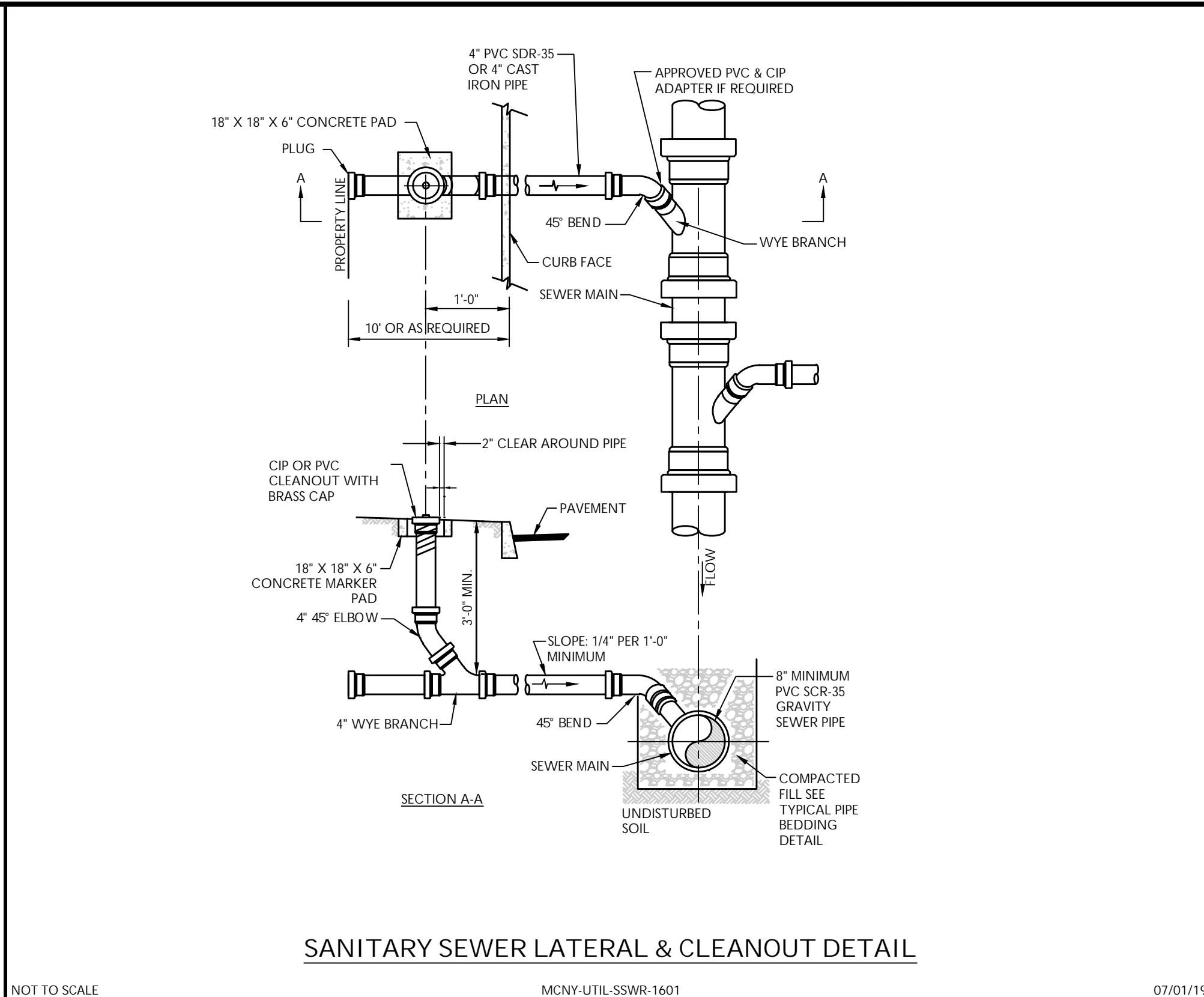
**SANITARY PRECAST MANHOLE DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-1000 07/01/19



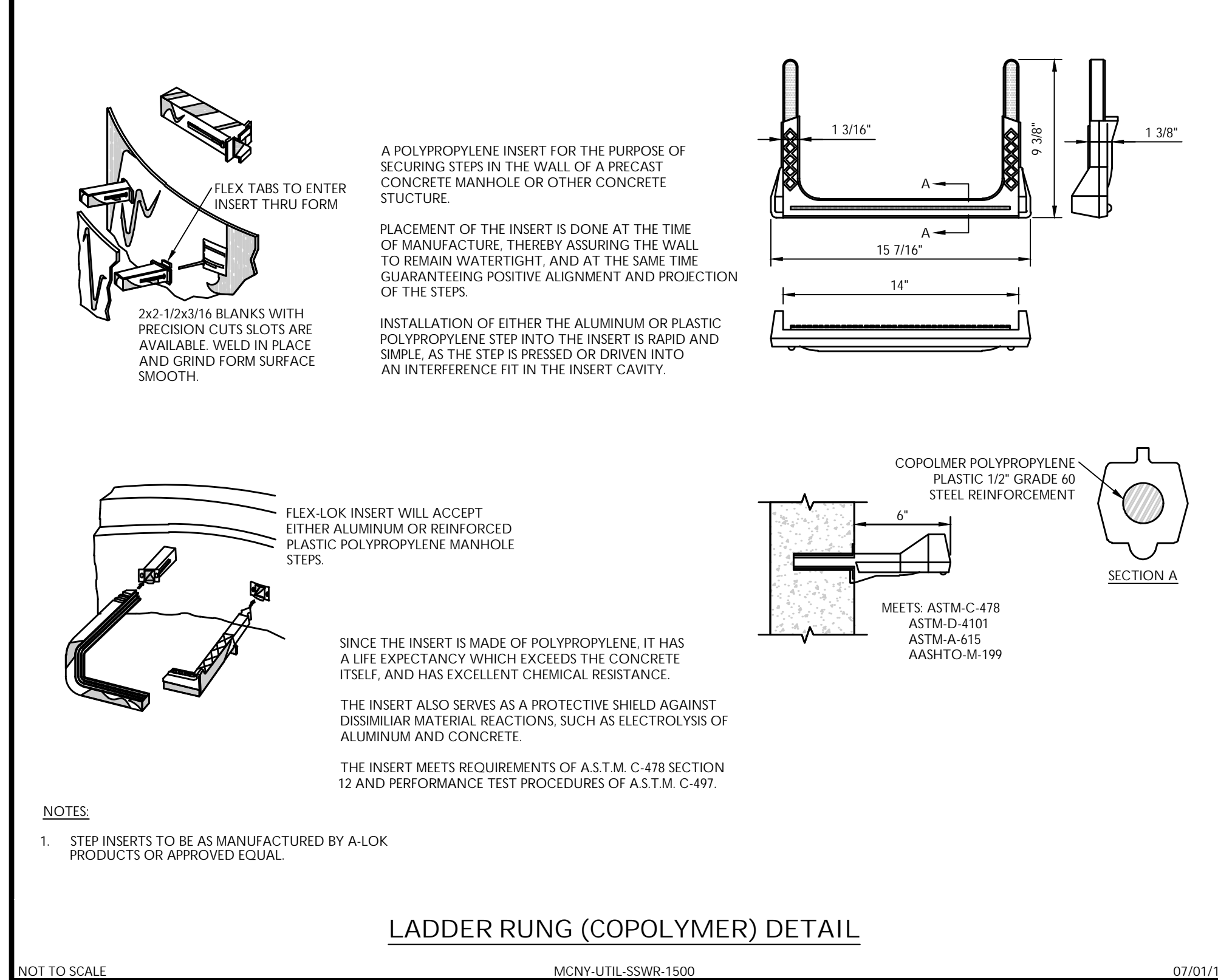
**SANITARY DROP MANHOLE CONNECTION (INTERNAL) DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-2100 07/01/19



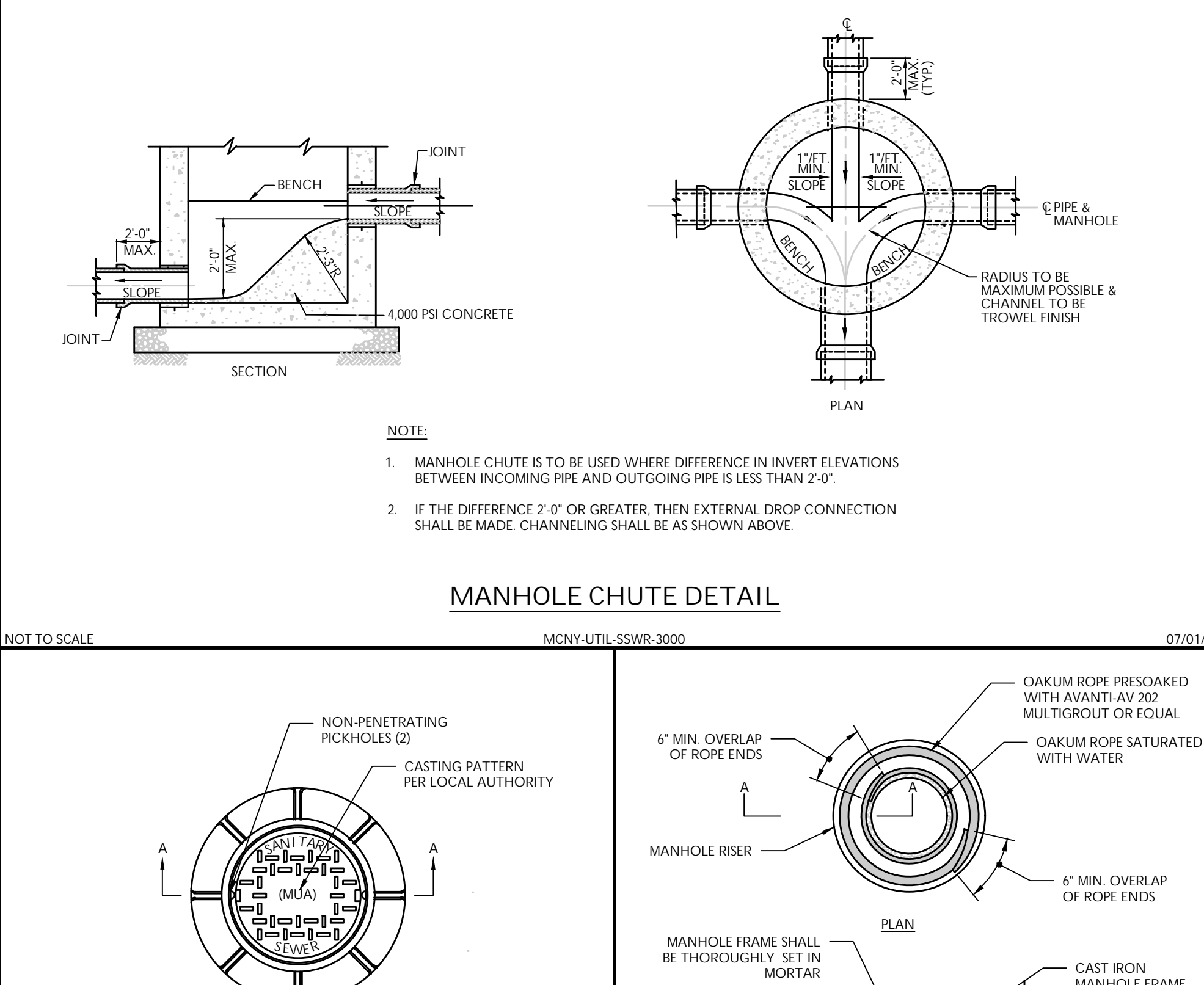
**SANITARY SEWER LATERAL & CLEANOUT DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-1601 07/01/19



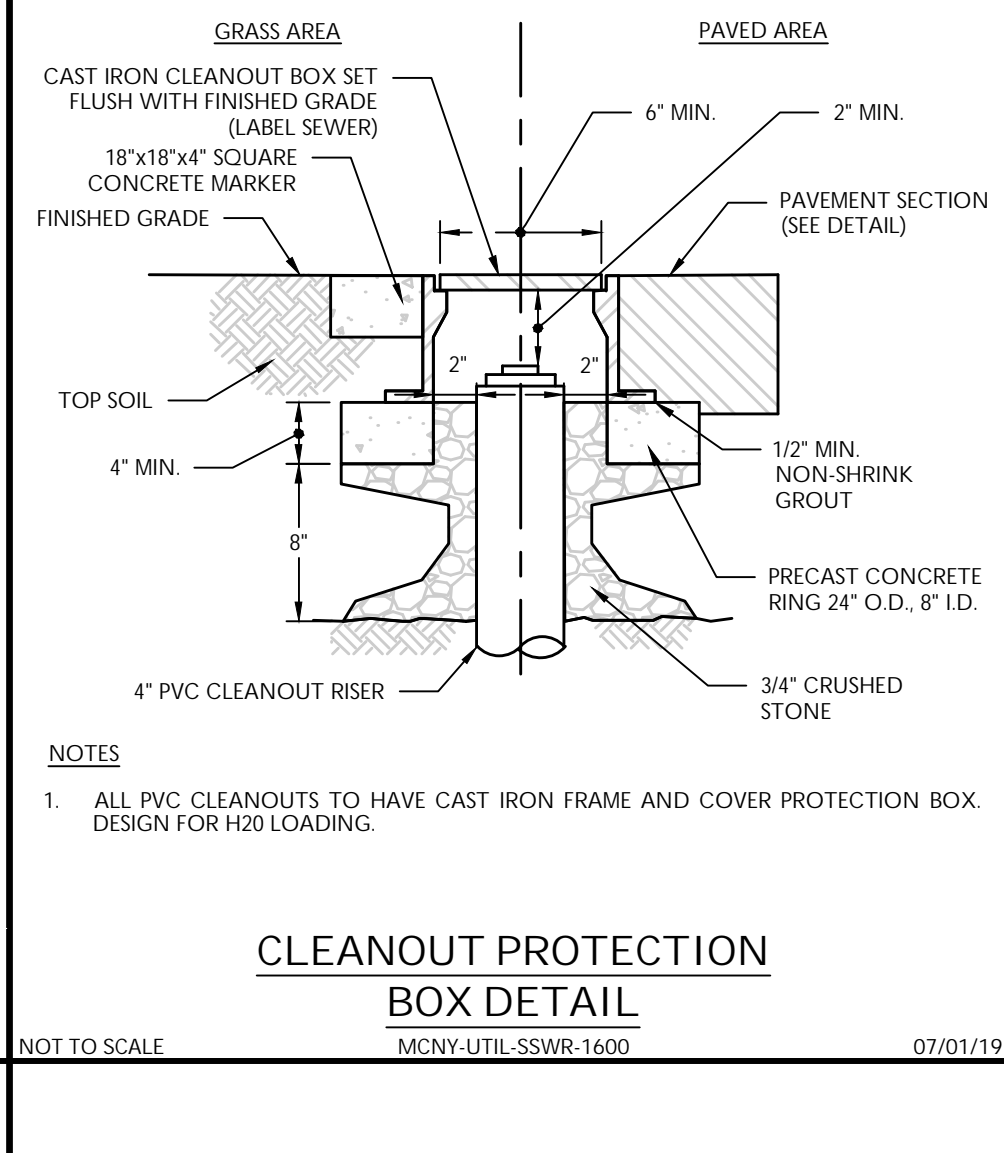
**LADDER RUNG (COPOLYMER) DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-1500 07/01/19



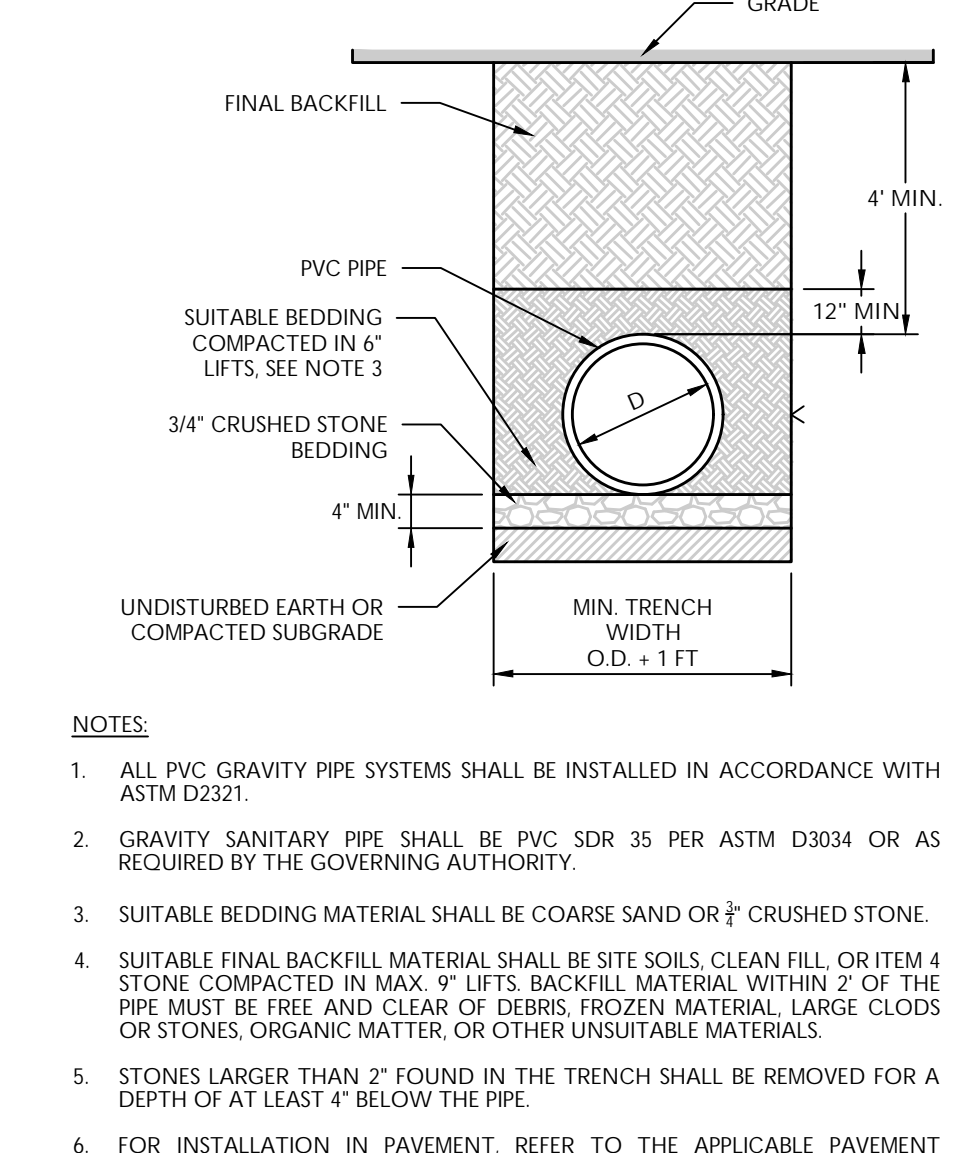
**MANHOLE CHUTE DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-3000 07/01/19



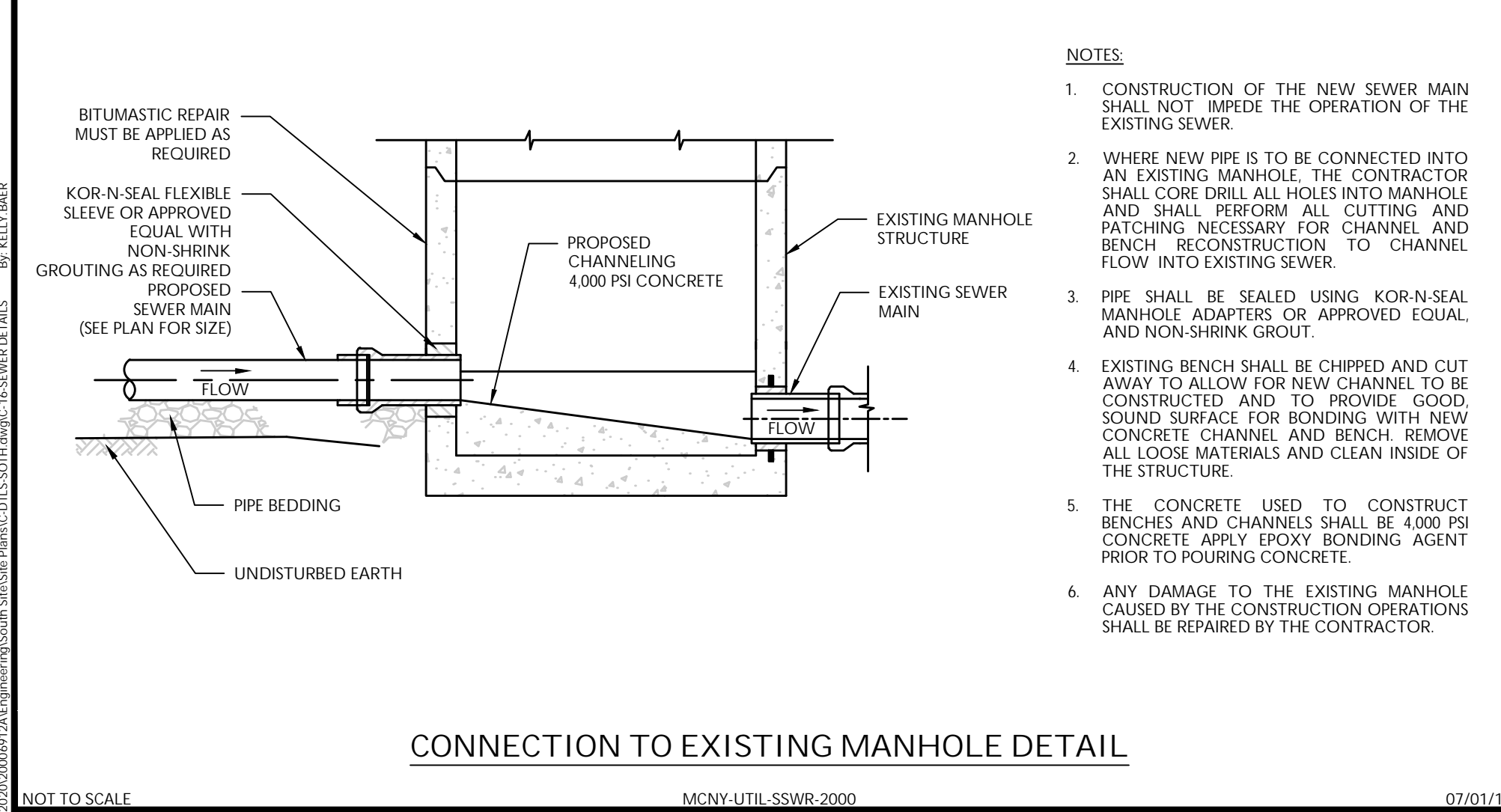
**CLEANOUT PROTECTION BOX DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-1600 07/01/19



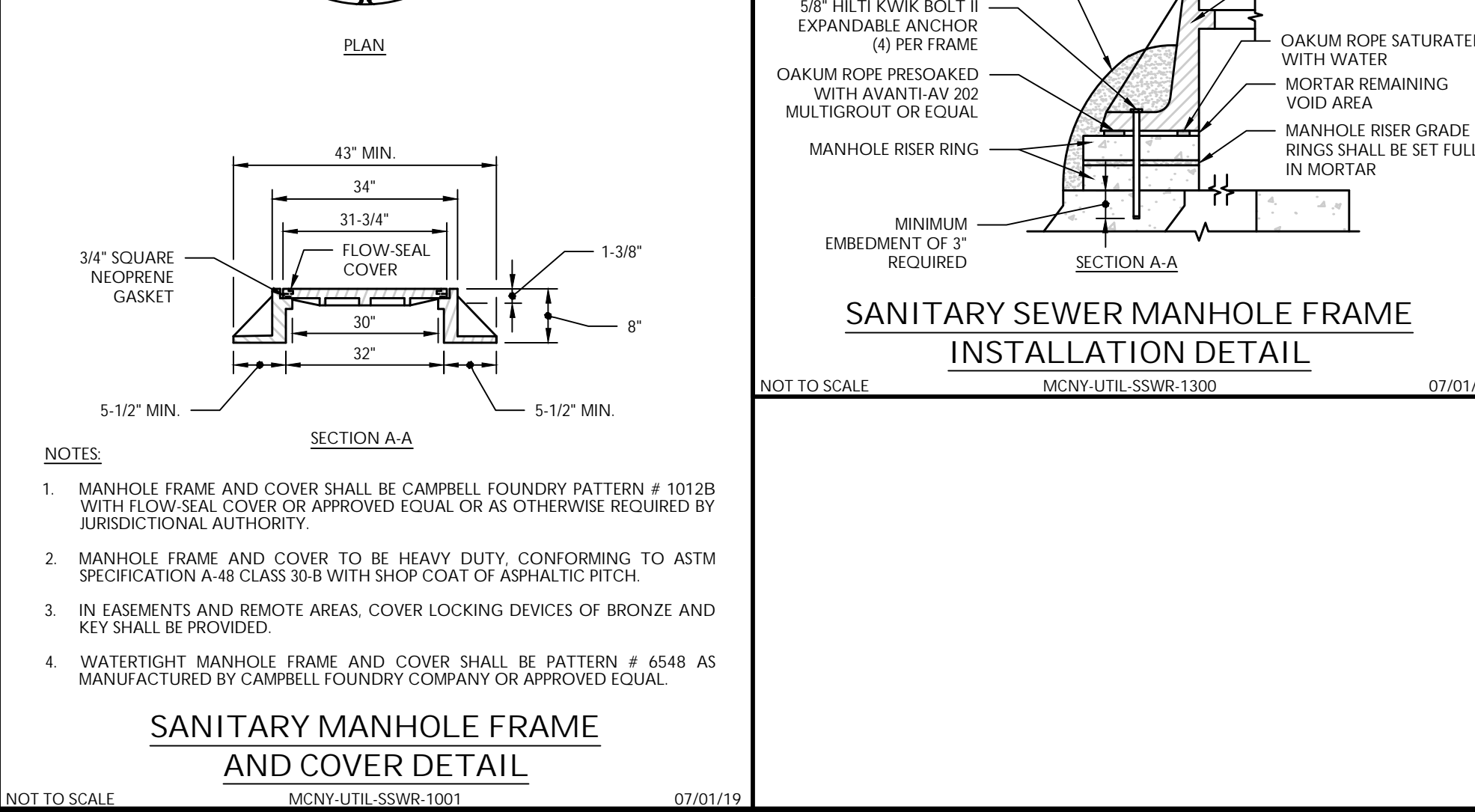
**PVC SANITARY PIPE BEDDING (GRAVITY) DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-2803 07/01/19



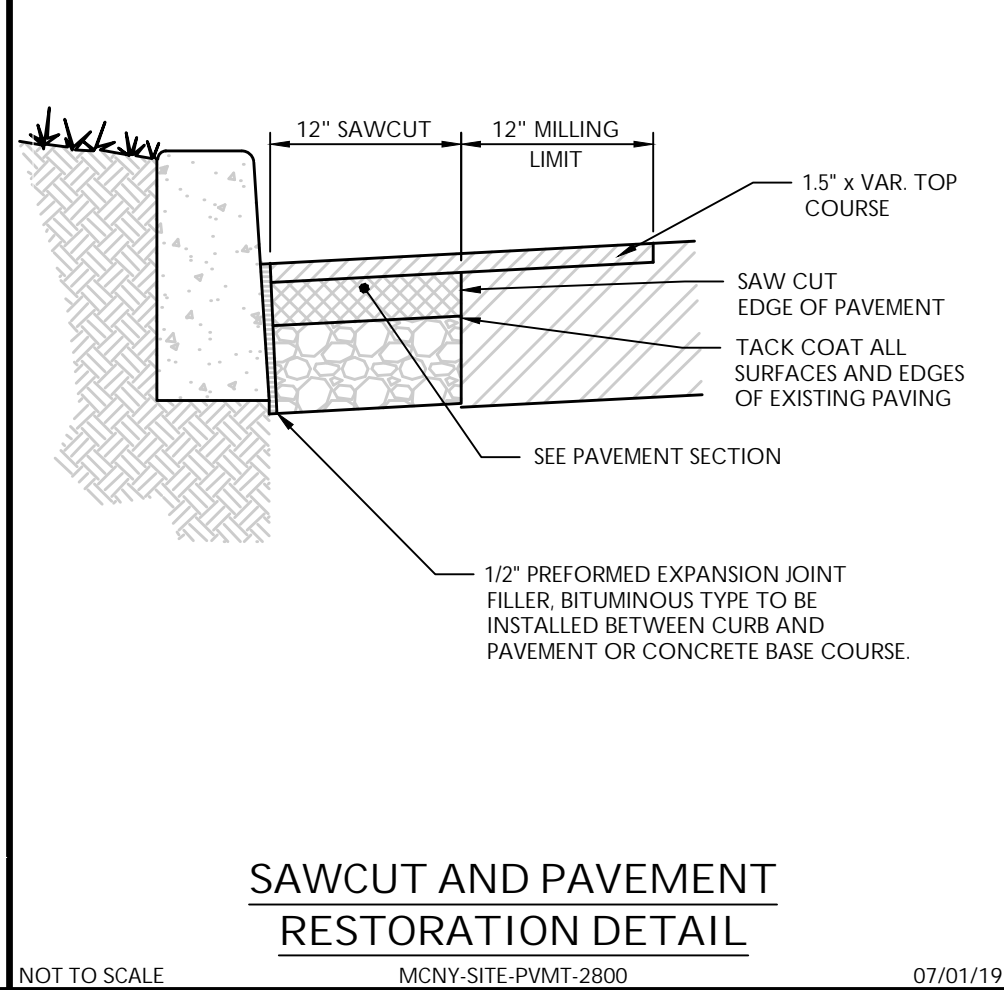
**CONNECTION TO EXISTING MANHOLE DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-2000 07/01/19



**SANITARY SEWER MANHOLE FRAME AND COVER DETAIL**

NOT TO SCALE MCNY-UTIL-SSWR-1001 07/01/19



**SAWCUT AND PAVEMENT RESTORATION DETAIL**

NOT TO SCALE MCNY-SITE-PVMT-2800 07/01/19

**Colliers Engineering & Design**  
 www.colliersengineering.com  
 Copyright © 2022 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, redrawn, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF  
 ALL STATES REQUIRE NOTIFICATION OF EXCAVATIONS, DISBURSERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
 Know what's below. Call before you dig.  
 FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DESCRIPTION
1	02/04/22	REVISED WETLAND IMPACT REDUCTION & DETAILS FOR GIES SUBMISSION
2	01/19/23	REVISED PER PLANNING BOARD COMMENTS

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cory Daniel Robinson**  
 NEW YORK LICENSED PROFESSIONAL ENGINEER  
 LICENSE NUMBER: 103788  
 COLLIER ENGINEERING & DESIGN CT, P.C.  
 N.Y. C.O.A. #: 0017609

**PRELIMINARY SITE PLANS**  
 FOR  
**DEWPOINT SOUTH**  
 SECTION 4  
 BLOCK 1  
 LOT 50.32  
 TOWN OF WAWAYANDA  
 ORANGE COUNTY  
 NEW YORK STATE

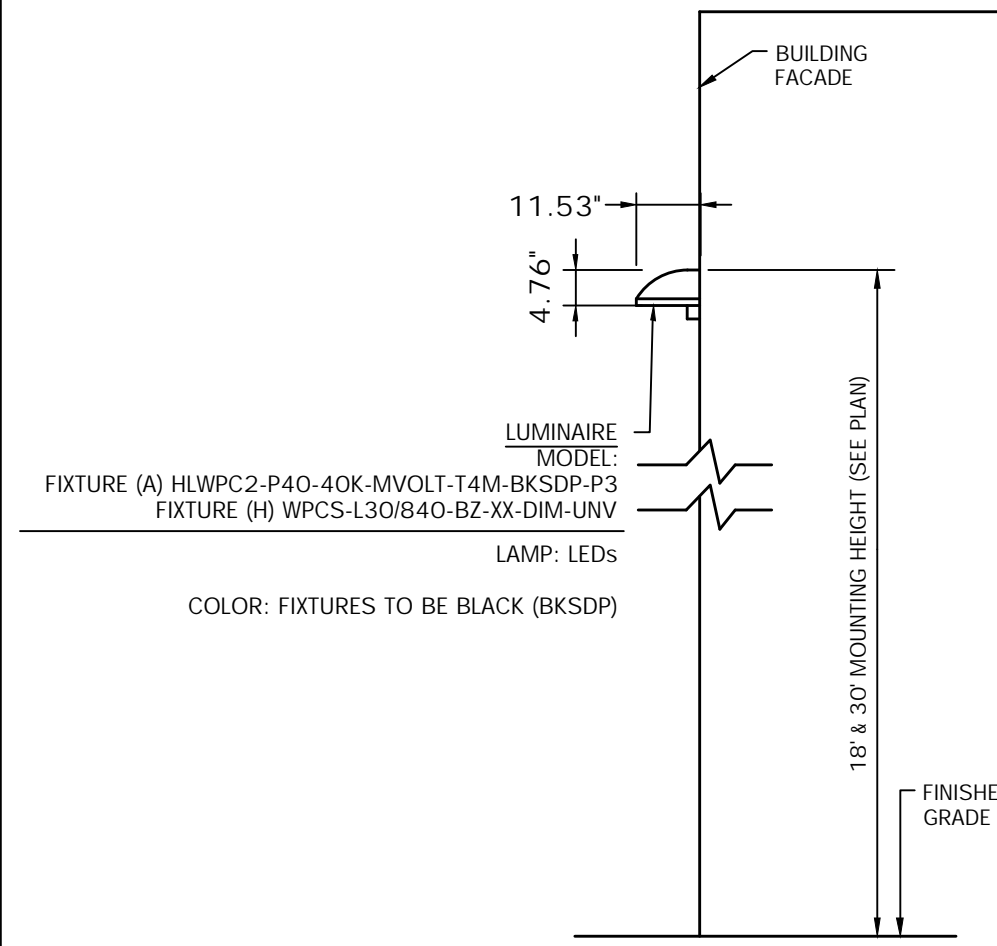
**Colliers Engineering & Design**  
 NEWBURGH  
 555 Hudson Valley Avenue  
 Suite 101  
 New Windsor, NY 12553  
 Phone: 845.564.4495  
 COLLIER ENGINEERING & DESIGN CT, P.C.  
 DOING BUSINESS AS MASER CONSULTING ENGINEERING & LAND SURVEYING

SCALE: AS SHOWN DATE: 01/10/2022 DRAWN BY: SMB CHECKED BY: CDR  
 PROJECT NUMBER: 20009912A DRAWING NAME: C-D15-50TH

SHEET TITLE: CONSTRUCTION DETAILS

SHEET NUMBER: 16 of 17

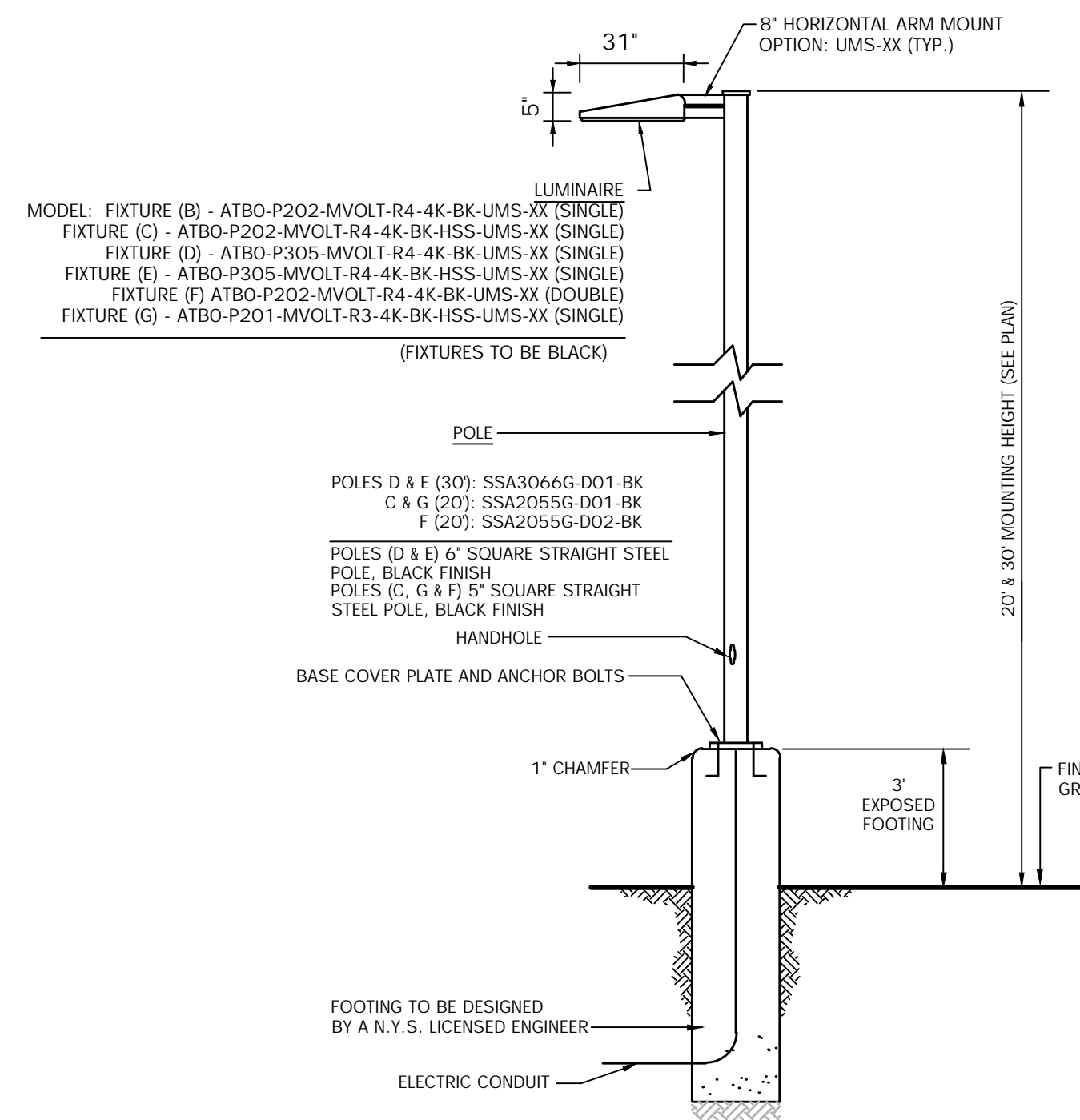




- NOTES:
- LUMINAIRES TO BE MANUFACTURED BY HOLOPHANE LIGHTING OR APPROVED EQUAL.
  - CONTRACTOR TO PROVIDE SHOP DRAWINGS OF LIGHT FIXTURES FOR REVIEW AND APPROVAL BY THE OWNER OR PROJECT LANDSCAPE ARCHITECT.
  - VOLTAGE TO BE CONFIRMED BY ELECTRICIAN CONTRACTOR.

**WALL MOUNTED FIXTURE DETAIL**

NOT TO SCALE



- NOTES:
- LUMINAIRES TO BE MANUFACTURED BY AMERICAN ELECTRIC LIGHTING AND POLES BY HOLOPHANE (MANUFACTURER TO CONFIRM POLE SIZE) OR APPROVED EQUAL.
  - CONTRACTOR TO PROVIDE SHOP DRAWINGS OF LIGHT FIXTURES FOR REVIEW AND APPROVAL BY THE OWNER OR PROJECT LANDSCAPE ARCHITECT.
  - FOOTING TO BE DESIGNED, SIGNED, AND SEALED BY A N.Y.S. LICENSED ENGINEER.
  - VOLTAGE TO BE CONFIRMED BY ELECTRICIAN CONTRACTOR.
  - PROPOSED POLES HEIGHT TO BE MODIFIED IN FIELD TO MEET DESIGN.

**POLE MOUNTED FIXTURE DETAIL**

NOT TO SCALE

- NO SOIL OR MULCH SHALL BE PLACED AGAINST ROOT COLLAR OF PLANT. MULCH SHALL NOT TOUCH THE TREE TRUNK.
- PLANTING DEPTH SHALL BE THE SAME OR HIGHER AS GROWN IN NURSERY.
- WIRE BASKETS AND NON-JUTE BURLAP MUST BE ENTIRELY REMOVED FROM THE ROOT BALL. JUTE BURLAP MUST BE REMOVED FROM THE TOP 1/3 OF THE ROOT BALL.
- DEPTH OF PLANT PIT SHALL BE INCREASED BY 12" WHEREVER POOR SOIL CONDITIONS OCCUR, WITH THE ADDITION OF LOOSE AGGREGATE.
- CONTRACTOR SHALL PARTIALLY FILL WITH WATER A REPRESENTATIVE NUMBER OF PITS IN EACH AREA OF THE PROJECT PRIOR TO PLANTING TO DETERMINE IF THERE IS ADEQUATE PERCOLATION. IF PIT DOESN'T PERCOLATE, MEASURES MUST BE TAKEN TO ASSURE PROPER DRAINAGE BEFORE PLANTING.
- PLANTING MUST BE GUARANTEED FOR TWO FULL GROWING SEASONS FROM THE TIME OF FINAL ACCEPTANCE BY THE LANDSCAPE CONSULTANT. CONTRACTOR SHALL REMOVE ALL WRAPPING AT THE END OF GUARANTEE PERIOD OR SOONER PER PROJECT LANDSCAPE ARCHITECT.
- BACKFILL MIXTURE TO BE SPECIFIED BASED UPON SOIL TEST AND CULTURAL REQUIREMENTS OF PLANT.
- PRUNE DAMAGED AND CONFLICTING BRANCHES MAINTAINING NORMAL TREE SHAPE. NEVER CUT CENTRAL TRUNK OR LEADER.

**PLANT DETAIL NOTES**

- TEMPORARY SEEDING: REFER TO SOIL EROSION AND SEDIMENT CONTROL PLANS.
- PERMANENT SEEDING SHALL CONSIST OF THE FOLLOWING MIXTURE OR APPROVED EQUAL: OPTIMUM SEEDING DATES ARE BETWEEN APRIL 1 AND MAY 31, AND AUGUST 16 AND OCTOBER 15.

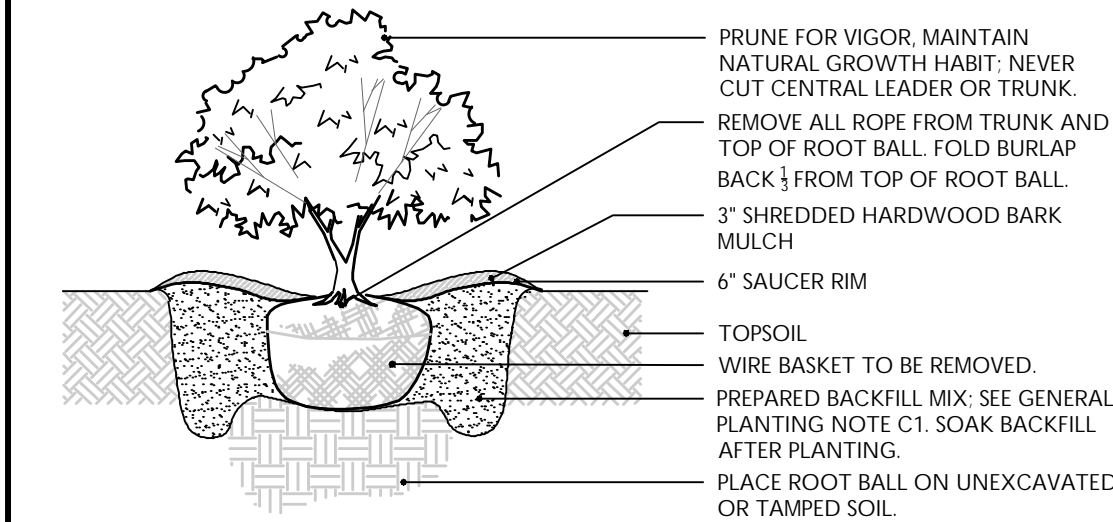
**TURF MIX (7-10 LBS / 1,000 S.F. MINIMUM)**  
 TALL FESCUE, STINGRAY (34%)  
 TALL FESCUE, RAPTOR III (33%)  
 HARD FESCUE, RIDU (33%)

**BASIN MIX (2-3 LBS / 1,000 S.F. MINIMUM)**  
 CREEPING RED FESCUE (30%)  
 TALL FESCUE (30%)  
 PERENNIAL RYE GRASS (10%)  
 BIRDSFOOT TRECLOVER (30%)

SEEDING OUTSIDE OF THE OPTIMUM DATES SHALL NOT BE CONDUCTED WITH OUT PRIOR APPROVAL.

- PERMANENT SEEDING TO BE APPLIED BY RAKING OR DRILLING INTO THE SOILS AT THE RATE GIVEN ABOVE.
- FERTILIZER FOR THE ESTABLISHMENT OF TEMPORARY AND PERMANENT VEGETATIVE COVER SHALL BE IN COMPLIANCE WITH THE LATEST NYSDEC REGULATIONS. THIS INCLUDES, BUT NOT LIMITED TO:  
 1. NO FERTILIZER SHALL BE APPLIED BETWEEN DEC. 1 AND APRIL 1 IN ANY YEAR.  
 2. SHALL NOT BE APPLIED WITHIN 20 FEET OF A WATER BODY.  
 3. ONLY LAWN FERTILIZER WITH LESS THAN 0.6% BY WEIGHT PHOSPHATE CONTENT MAY BE APPLIED. (A SOIL TEST PRIOR TO FERTILIZER APPLICATION IS RECOMMENDED.)
- IF SEASON PREVENTS THE ESTABLISHMENT OF TEMPORARY OR PERMANENT SEEDING, EXPOSED AREA TO BE STABILIZED WITH MULCH AS INDICATED IN NOTE 6.
- MULCH TO CONSIST OF SMALL GRAIN STRAW OR SALT HAY ANCHORED WITH A WOOD AND FIBER MULCH BINDER OR AN APPROVED EQUAL. MULCH WILL BE SPREAD AT RATES PER NYSDEC STANDARDS AND ANCHORED WITH A MULCH ANCHORING TOOL OR LIQUID MULCH BINDER, AND SHALL BE PROVIDED ON ALL SEEDINGS. HYDROMULCH SHALL ONLY BE USED DURING OPTIMUM GROWING SEASONS.
- AS NEEDED, WORK LIME AND FERTILIZER INTO SOIL AS NEARLY AS PRACTICAL TO A DEPTH OF 4 INCHES WITH A DISC, SPRINGTOOTH HARROW, OR OTHER SUITABLE EQUIPMENT. THE FINAL HARROWING OR DISCING OPERATION SHOULD BE ON THE GENERAL CONTOUR. CONTINUE TILLAGE UNTIL A REASONABLY UNIFORM, FINE SEEDBED IS PREPARED. ALL BUT CLAY OR SILTY SOILS AND COARSE SANDS SHOULD BE ROLLED TO FIRM THE SEEDBED WHEREVER FEASIBLE.
- REMOVE FROM THE SURFACE ALL STONES TWO INCHES OR LARGER IN ANY DIMENSION; REMOVE ALL OTHER DEBRIS SUCH AS WIRE, CABLE, TREE ROOTS, PIECES OF CONCRETE, CLODS, LUMPS, OR OTHER UNSUITABLE MATERIAL.
- INSPECT SEEDBED JUST BEFORE SEEDING. IF TRAFFIC HAS LEFT THE SOIL COMPACTED, THE AREA MUST BE RETILLED AND FIRMED AS ABOVE.

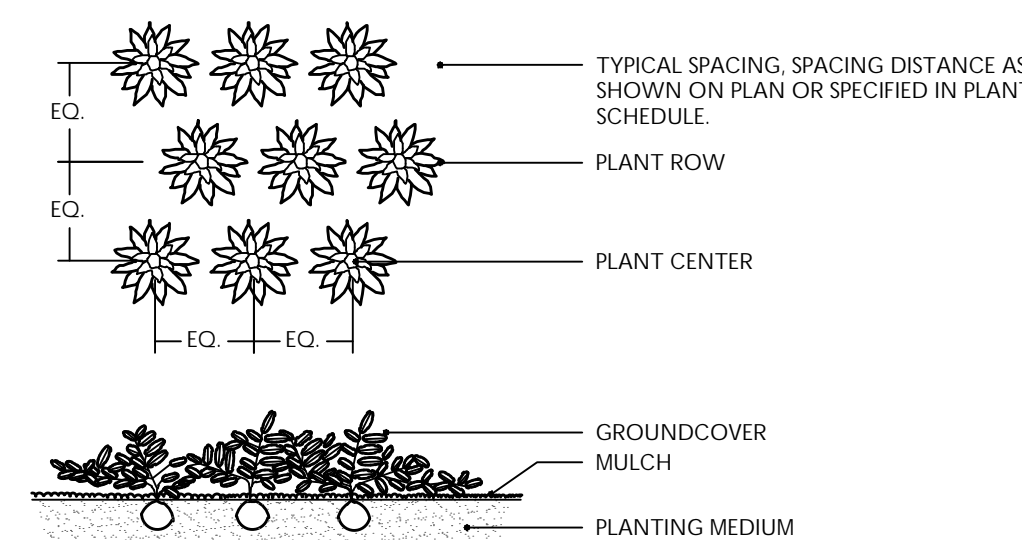
**GENERAL SEEDING NOTES**



- NOTES:
- NO SOIL OR MULCH SHALL BE PLACED AGAINST ROOT COLLAR OF PLANT.
  - PLANTING DEPTH SHALL BE THE SAME OR HIGHER AS GROWN IN NURSERY.

**SHRUB PLANTING DETAIL**

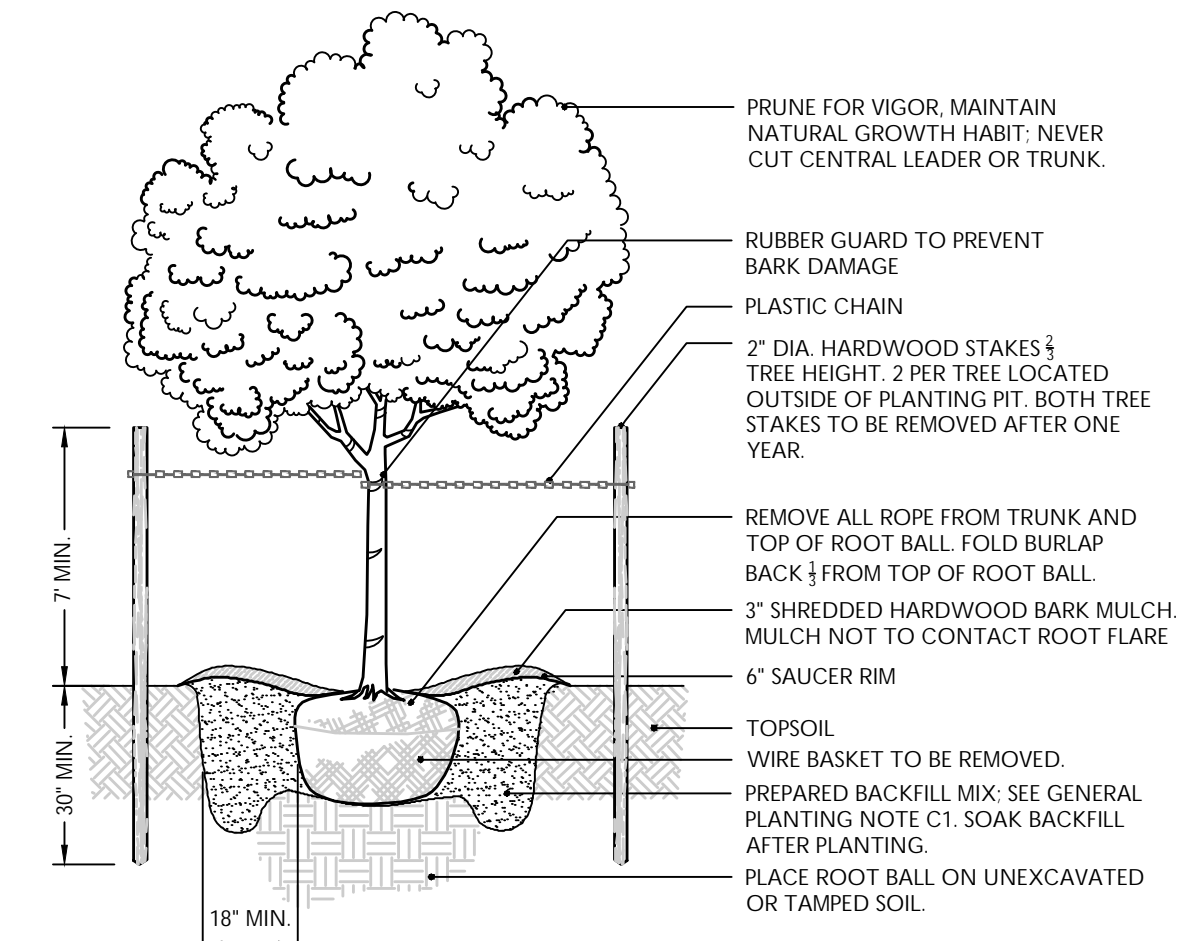
NOT TO SCALE



- NOTES:
- PLANTING DEPTH SHALL BE THE SAME OR HIGHER AS GROWN IN NURSERY.

**PERENNIAL PLANTING DETAIL**

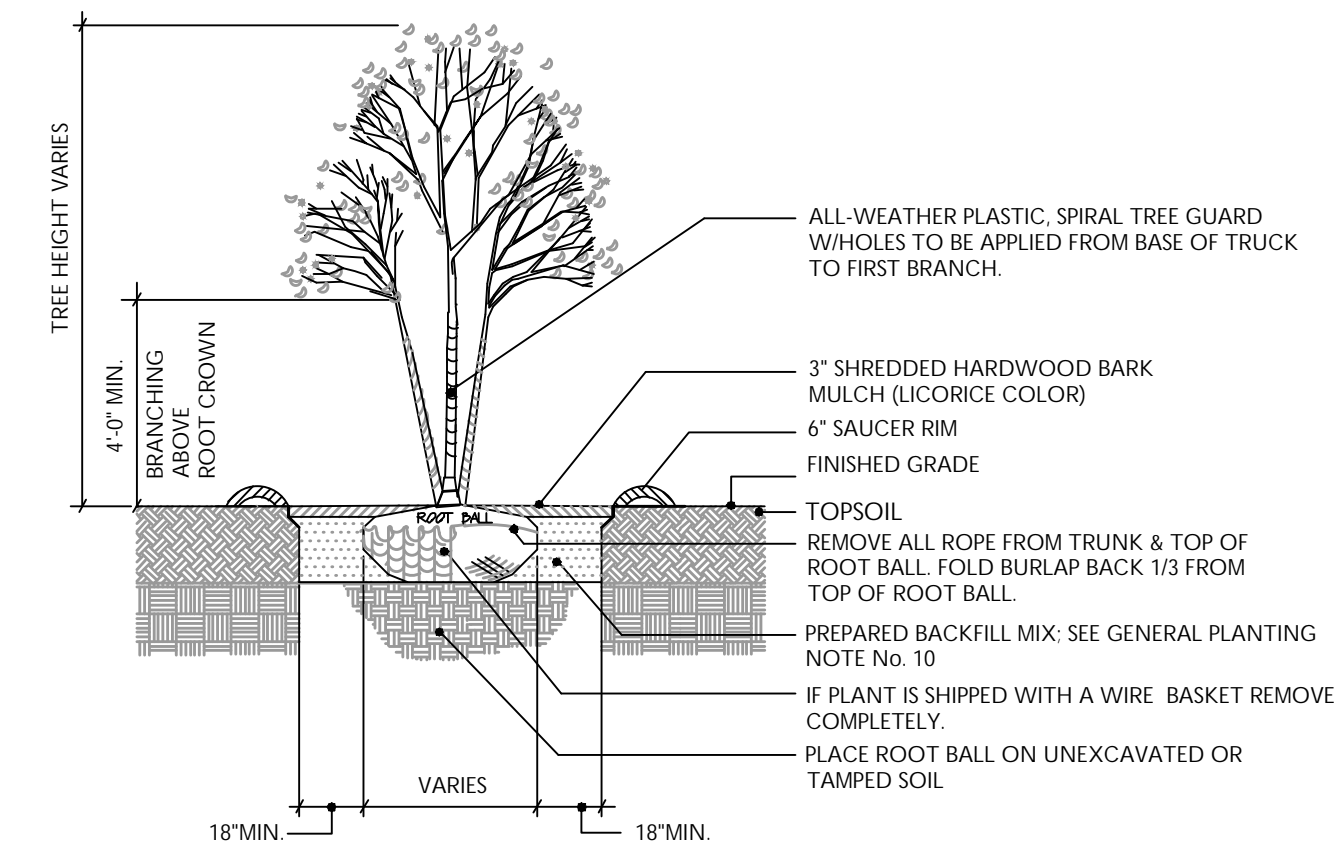
NOT TO SCALE



- NOTES:
- NO SOIL OR MULCH SHALL BE PLACED AGAINST ROOT COLLAR OF PLANT.
  - PLANTING DEPTH SHALL BE THE SAME OR HIGHER AS GROWN IN NURSERY.

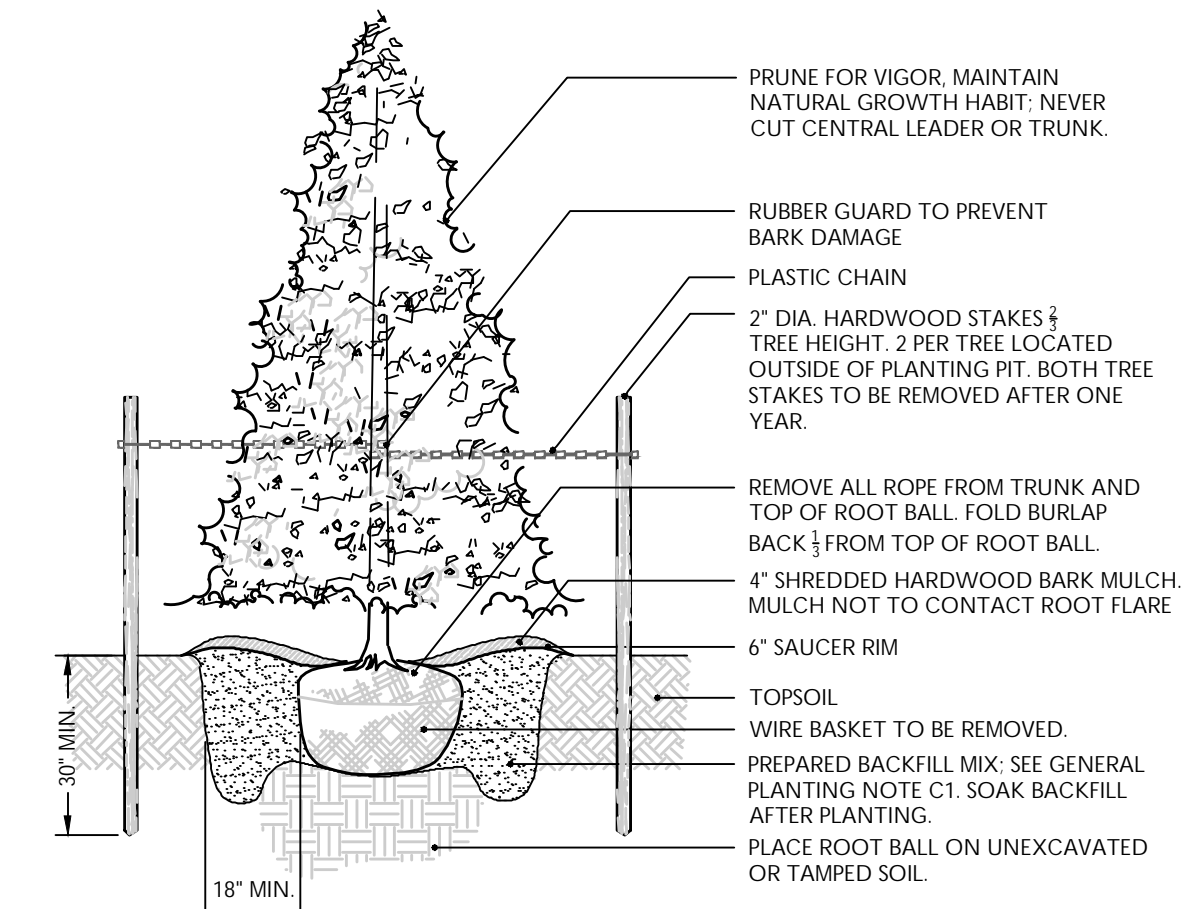
**TREE PLANTING DETAIL**

NOT TO SCALE



**MULTI-STEM TREE PLANTING DETAIL**

NOT TO SCALE



- NOTES:
- NO SOIL OR MULCH SHALL BE PLACED AGAINST ROOT COLLAR OF PLANT.
  - PLANTING DEPTH SHALL BE THE SAME OR HIGHER AS GROWN IN NURSERY.

**EVERGREEN TREE PLANTING DETAIL**

NOT TO SCALE

**TOWN OF WAWAYANDA PLANNING BOARD**

**Colliers Engineering & Design**  
 www.colliersengineering.com  
 Copyright © 2022 Colliers Engineering & Design All Rights Reserved. This drawing and all the information contained herein is authorized for use only by the party for whom the services were contracted or to whom it is certified. This drawing may not be copied, revised, redrawn, distributed or relied upon for any other purpose without the express written consent of Colliers Engineering & Design.

Doing Business as **MASER CONSULTANTS**

**811** PROTECT YOURSELF  
 ALL STATES REQUIRE NOTIFICATION OF EXCAVATORS, DESIGNERS, OR ANY PERSON PREPARING TO DISTURB THE EARTH'S SURFACE ANYWHERE IN ANY STATE.  
 Know what's below. Call before you dig.  
 FOR STATE SPECIFIC DIRECT PHONE NUMBERS VISIT: WWW.CALL811.COM

REV.	DATE	DESCRIPTION
1	02/04/22	REVISED METLAND IMPACT REDUCTION & DETAILS FOR GIS SUBMISSION.
2	01/11/23	REVISED PER PLANNING BOARD COMMENTS.

UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER IS A VIOLATION OF ARTICLE 145, SECTION 7209, SUB-DIVISION 2 OF THE NEW YORK STATE EDUCATION LAW.

**Cody D. Roberson**  
 NEW YORK LICENSED PROFESSIONAL ENGINEER  
 LICENSE NUMBER: 109788-1  
 COLLIER ENGINEERING & DESIGN CT, P.C.  
 N.Y. C.O.A.#. 0077609

**PRELIMINARY SITE PLANS FOR DEWPOINT SOUTH**

SECTION 4  
 BLOCK 1  
 LOT 50.32  
 TOWN OF WAWAYANDA  
 ORANGE COUNTY  
 NEW YORK STATE

**Colliers Engineering & Design**  
 NEWBURGH  
 555 Hudson Valley Avenue  
 Suite 101  
 New Windsor, NY 12553  
 Phone: 845.644.4495  
 COLLIER ENGINEERING & DESIGN CT, P.C.  
 DOING BUSINESS AS MASER CONSULTING ENGINEERING & LAND SURVEYING

SCALE	DATE	DRAWN BY	CHECKED BY
AS SHOWN	01/10/2022	SMB	CDR

PROJECT NUMBER: 20009912A  
 DRAWING NAME: C-DTLS-SOUTH

SHEET NUMBER: 17 of 17

## Section 7

**TOWN OF WAWAYANDA PLANNING BOARD**

**ENVIRONMENTAL ASSESSMENT FORM NARRATIVE  
DEWPOINT DEVELOPMENT LLC & GDBP 2171 LLC (“Applicant”)**

**TOWN OF WAWAYANDA, ORANGE COUNTY  
MC-1 (Mixed Commercial) zoning district**

**TAX LOT: 4-1-50.32 (the “Site”)  
February 9, 2022**

**PROPOSED ACTION**

The proposed project will consist of the construction of one warehouse/distribution facility on an existing parcel approximately 11.66 acres in size, with frontage along Dolsontown Road to the north and adjacent to NYS Route 17M to the west. The Site is proposed to host a 125,000 square foot warehouse/distribution facility with 5,000 square feet of office space located on Dolsontown Road, tax lot 4-1-50.32 (the “Project”). The Project is consistent with the Town of Wawayanda Comprehensive Plan and complies with Wawayanda’s Zoning Law.

The Project is within the Town of Wawayanda MC-1 (Mixed Commercial) zoning district. Within the MC-1 zoning district, a “Warehouse, storage and distribution facilities” use requires a special use permit subject to site plan approval by the Planning Board. Other associated site improvements proposed for the Site include 65 vehicle parking spaces and 37 truck loading docks. The Site has a proposed driveway to Dolsontown Road that will provide vehicular and truck access to the facility, as well as a gated emergency access driveway connecting to Caskey Lane.

The warehouse facility proposes water (potable & fire protection) and sanitary sewer services to service the buildings. These services will be provided service connections to the adjacent town mains within Dolsontown Road. The Project is anticipated to generate a water and sewer demand of approximately 1,875 GPD.

The Site is currently undeveloped with a mixture of woodlands and wetlands. Approximately 1,350 square feet (.03 acres) of the 2.27 acres of federally regulated wetlands identified on Site will be disturbed to accommodate the Project. The Applicant will submit a Preconstruction Notification to the Army Corps of Engineers for confirmation on jurisdiction and permission of filling.

The Project is estimated to require approximately 9 acres of site disturbance and requires the preparation of a Stormwater Pollution Prevention Plan (SWPPP). A SWPPP has been prepared in accordance with the Town and NYSDEC requirements to provide stormwater management/mitigation for water quantity and water quality and will be provided to the Planning Board with this submission as part of Appendix A.

**SEQRA COMPLIANCE AND INVOLVED AND INTERESTED AGENCIES**

The Project's potential environmental impacts must be reviewed pursuant to the State Environmental Quality Review Act and its implementing regulations in 6 NYCRR Part 617 (collectively, "SEQRA"). Pursuant to 6 NYCRR § 617.6(a)(1)(iv), "as soon as an agency receives an application for...approval of an action, it must" make a preliminary classification of the action as Type 1, Type 2 or Unlisted. This "preliminary classification will assist in determining whether a full EAF and coordinated review is necessary."

In this Project, the SEQRA "action" is the Planning Board's decision on the Applicant's applications for site plan and special use permit approvals for the Project. Because the Project entails the proposed construction of a facility with more than 100,000 square feet of gross floor area in a town having a population of 150,000 persons or less, it is properly classified as a Type 1 action pursuant to 6 NYCRR §§ 617.4(b)(6)(v). As a result, a full EAF ("FEAF") and coordinated environmental review of the Project has been conducted.

Accordingly, Applicant completed Part 1 of the FEAF as required by 6 NYCRR § 617.6(a)(2) and provided it to the Planning Board in its April 28, 2021 submission. As further required by SEQRA, Applicant identified the following other agencies that may be involved or interested in the review of the Project:

- Town of Wawayanda Town Board;
- Town of Wawayanda Building Department;
- Town of Wawayanda Highway Department;
- New Hampton Fire Company;
- Orange County Department of Planning;
- Orange County Department of Health;
- NYS Department of Environmental Conservation;
- NYS Department of Parks, Recreation and Historic Preservation;
- Army Corps of Engineers;
- New York State Department of Transportation;
- Orange County Department of Public Works

At its June 9, 2021 meeting, the Planning Board declared itself "lead agency" in a coordinated SEQRA review and circulated a Notice to Designate SEQRA Lead Agency to the identified involved and interested agencies on or about June 10, 2021. No objection was received to the Planning Board serving as lead agency.

### **EVALUATION OF POTENTIAL ENVIRONMENTAL IMPACTS**

The lead agency must consider the criteria for determining the significance of potential environmental impacts from the Project as set forth in the SEQRA regulations at 6 NYCRR § 617.7(c). To do this, the lead agency reviews all relevant information and completes Parts 2 and 3 of the FEAF to provide the basis for its SEQRA determination.

For the Project, the identification of potential impacts and assessment of potential environmental

impacts based on FEAF Part 2 is discussed below. Based on the following discussion, the Project includes the potential for at least one significant adverse environmental impact. A draft Generic Environmental Impact Statement (GEIS) was prepared to assess such potential significant adverse environmental impacts.

### **1. Impact on Land**

The Project will have minimal impacts on land. Blasting is not anticipated to be required in connection with Project construction.

Consistent with Section 5.2 "Planning for Green Infrastructure: Reduction of Impervious Cover" of the NYSDEC Stormwater Management Design Manual, the proposed site plan has been designed to include the following Green Infrastructure site planning techniques, among others: the extent of the clearing will be limited to meet the user's needs; compacted soils located in open areas without shallow utilities will be tilled in order to restore the original properties of the soil prior to seeding; roadway widths were reduced wherever possible while still maintaining the necessary access; sidewalks added where needed to adequately and safely serve the pedestrian needs of the facility; the proposed driveways have been minimized wherever possible; building footprints have been designed to meet the end user's needs.

Existing federally regulated wetland areas exist on site and will be moderately disturbed by the Project. Additionally, erosion control measures will be implemented during construction to minimize the erosion of land. Please refer to the draft GEIS for a full discussion of the Project's potential significant adverse environmental impacts to wetlands and surface water.

Based on the foregoing, the Project is not anticipated to have any significant adverse impacts on land.

### **2. Impact of Geological Features**

There are no unique landforms on the Site that will be impacted by the Project. No geological feature registered as a National Natural Landmark is present on or next to the Site. Therefore, the Project is not anticipated to have any significant adverse impact on geological features.

### **3. Impact on Surface Water**

Please refer to the draft GEIS for a full discussion of the Project's potential significant adverse environmental impacts to wetlands and surface water. Based on the findings set forth in the draft GEIS, the Project is not anticipated to have any significant adverse impact on surface water.

### **4. Impact on Groundwater**

The SWPPP provides for "good housekeeping" and material management practices to minimize the risk of spills. These practices include: keeping products in original containers unless they are not re-sealable, (retaining original labels and material safety data sheets (MSDS)), storing only enough products required to do the job, storing materials in a neat, orderly manner in their

appropriate containers (and if possible, under a roof or other enclosure and/or on non-porous blacktop), not mixing substances unless recommended by the manufacturer, using all of a product before disposing of the container, following manufacturer's recommendations for proper use and disposal of materials and daily inspections by the contractor's site superintendent to ensure proper use and disposal of materials on site.

Additionally, the contractor's Site superintendent shall serve as a spill prevention and cleanup coordinator, and the following practices, outlined in the SWPPP, shall be followed: spills, of any size, of toxic or hazardous material and/or petroleum products shall be reported to the NYSDEC and Central Hudson's Environmental Affairs division; manufacturer's recommended methods for spill cleanup shall be clearly posted and site personnel shall be made aware of the procedures and the locations of the information and cleanup supplies; materials and equipment necessary for spill cleanup shall be kept in the material storage area onsite (equipment and materials shall include but not be limited to brooms, dust pans, mops, rags, gloves, kitty litter, sand, sawdust, and plastic and metal trash containers specifically for this purpose); all spills shall be cleaned up immediately after discovery and the spill area shall be kept well ventilated and personnel shall wear appropriate protective clothing to prevent injury from contact with a hazardous substance. The spill prevention plan shall be adjusted to include measures to prevent toxic or hazardous material of spills from recurring and how to clean up the spill. A description of the spill, what caused it, and the cleanup measures shall also be included.

The proposed facility is anticipated to generate approximately 1,875 gallons per day of water and sewer usage. The facility is proposed to have water (potable & fire protection) and sanitary sewer services through connections to the existing town mains within Dolsontown Road. Please refer to the draft GEIS for a full discussion of the Project's potential significant adverse environmental impacts to groundwater.

Based on the foregoing, the Project will not create any significant adverse impacts to groundwater.

## **5. Impact on Flooding**

All storm water from the Site will be collected, managed and treated by a stormwater management system in accordance with the NYSDEC General SPDES permit for stormwater discharges and SWPPP. Furthermore, as noted on the Federal Emergency Management Administration Flood Insurance Rate Maps ("FIRM") covering the Town of Wawayanda, the Site is located outside any designated flood hazard area in an area where there is a minimal flood hazard during 100-year and 500-year storm events. There is no known flooding on the Site.

Please refer to the draft GEIS for a full discussion of the Project's potential significant adverse environmental impacts to flooding.

Based on the foregoing, the Project will not create any adverse impacts to flooding.

## **6. Impacts on Air**

The Project will not result in any significant adverse impacts on air quality. The Project does not include a State regulated air emission source or involve any activity that will have more than a minimal impact on air quality.

Several energy conservation methods will be incorporated into building construction. Energy Star approved building materials will be used that help reduce the amount of heat lost during the wintertime and cool air during the summertime. Other items such as reduced flow water fixtures that limit the amount of water flowing through the tap, thereby diminishing the amount of water used throughout the day will be used. Energy efficient light bulbs will reduce the amount of energy required for building and site light while extending the “life” of the lightbulb.

Please refer to the draft GEIS for a full discussion of the Project’s potential significant adverse environmental impacts on air associated with traffic.

Based on the foregoing, the Project will not create any significant adverse impacts to air quality.

### **7. Impact on Plants and Animals**

Please refer to the draft GEIS for a full discussion of the Project’s potential significant adverse environmental impacts on plants and animals.

Based on the findings set forth in the draft GEIS, the Project will not create any significant adverse impacts to plants and animals.

### **8. Impact on Agricultural Resources**

The Project is consistent with the Town’s Comprehensive Plan and the requirements of the MC-1 Zoning District. The Town’s Comprehensive Plan provides that “the MC mixed commercial zone is a district intended to provide a principal area for intensive nonresidential development such as office, retail, service businesses, manufacturing and industrial uses”. The Comprehensive Plan further indicates that the zone is intended to be developed with commercial enterprises and specifically excludes residential uses and observes that recently attracted uses include small contractor yards, offices, retail, large warehousing and industrial uses. The Comprehensive Plan recommends that the Town continue to allow commercial/industrial uses on a minimum 2-acre lot size. The Project is consistent with the letter and intent of the MC-1 Zone as set forth in the Town of Wawayanda Zoning Law and Comprehensive plan, as it is a permitted use on a 11.66-acre lot, far greater than the minimum lot size requirement.

Based on the foregoing, no significant adverse environmental impacts to agricultural resources are anticipated from the Project.

### **9. Impact on Aesthetic Resources**

The Project will not be visible from any officially designated federal, state, or local scenic or



aesthetic resource, nor will it impact any officially designated scenic views. The Project is located in the MC-1 zone and is consistent with the Town's Comprehensive Plan. It is consistent with existing land uses in the vicinity of the Site, with the exception of certain pre-existing nonconforming residential uses which will be screened from the Project. The Site is bounded on the south by Interstate 84. Building height is proposed to be 55 feet, 10 fewer than what is allowed by the Town's Zoning Code.

The Landscaping Plan for the site (see Appendix A) adheres to Chapter 195-24 of the Town Code, and in accordance with Section 195-24 A. has a goal of enhancing the appearance and natural beauty of the Town and protecting property values through the preservation and planting of vegetation, screening, and landscaping material. The plan includes a variety of native deciduous and evergreen trees and shrubs, as well as non-invasive ornamental species. To further break-up the building mass along the roadway, trees are proposed near the right-of-way line. The Landscaping Plan will be provided to the Planning Board with this submission.

Based on the foregoing, the Project will not result in any significant adverse impacts to aesthetic resources.

#### **10. Impact on Historic and Archeological Resources**

Please refer to the draft GEIS for a full discussion of the Project's potential significant adverse environmental impacts on historic and archaeological resources.

Based on the findings set forth in the draft GEIS, the Project will not create any significant adverse impacts on historic and archaeological resources.

#### **11. Impact on Open Space and Recreation**

The Project will not result in any loss of recreational opportunities or any reduction of an open space resource designated in a governmental open space plan. The Site is not designated open space. The Site is largely wooded and located in a zoning district intended for commercial development such as the Project. The Site is privately owned and is not used for public recreation.

Based on the foregoing, the Project will not have any significant adverse impact on open space and recreational resources.

#### **12. Impact on Critical Environmental Areas**

The Site is not located within a Critical Environmental Area. As summarized in the draft GEIS, stormwater will be managed, treated and discharged in accordance with the requirements set forth in the NYSDEC SPDES and the Project's SWPPP, which is designed to conform to applicable requirements in the NYSDEC general stormwater permit and the standards provided by the New York State Stormwater Management Design Manual (dated January 2015).

Based on the foregoing, the Project will not have any significant adverse impact on Critical Environmental Areas.

### **13. Impact on Transportation**

Please refer to the draft GEIS for a full discussion of the Project's potential significant adverse environmental impacts on traffic/transportation.

Based on the findings set forth in the draft GEIS, the Project will not create any significant adverse impacts on traffic/transportation.

### **14. Impact on Energy**

Several energy conservation methods will be incorporated into building construction. Energy Star approved building materials will be used that help reduce the amount of heat lost during the wintertime and cool air during the summertime. Other items such as reduced flow water fixtures that limit the amount of water flowing through the tap, thereby diminishing the amount of water used throughout the day will be used. Energy efficient light bulbs will reduce the amount of energy required for building and site light while extending the "life" of the lightbulb.

Based on the foregoing, the Project will not have any significant adverse impact on Energy.

### **15. Impact on Noise, Odor and Light**

#### *Noise*

The Project Site is located in the MC-1 Zoning District. As stated above, The Project is consistent with the District Intent set forth in Attachment 8 to the Town's Zoning Law, which provides that the MC District "is intended to provide the Town with a principal area for intensive nonresidential development such as office, retail, service businesses and manufacturing". Indeed, the Project is anticipated to be less intensive than a variety of other uses that are permitted by Site Plan approval or Special Use Permit, including contractor yards, motor vehicle sales and services, high traffic retail and service businesses, industrial uses, manufacturing uses and mining operations, including major mining operations.

The Project will generate noise during its construction phase. Once constructed, the Project will produce small to moderate amounts of noise, mostly due to Site generated traffic and building HVAC mechanical units.

There is typically a minimal amount of time that trucks will be idling and waiting to drop off or pick up a trailer. In the event that they are waiting for a period of more than five (5) minutes, they are required to turn off their engine in accordance with the New York State Heavy Duty Vehicle Idling Law (6 NYCRR Subpart 217-3).

Also note that a sound level measurement and analysis was completed and a February 8, 2022

memorandum summarizing the same (the “Noise Evaluation”) and will be provided to the Planning Board with this submission as part of Appendix A. The Noise Evaluation evaluated existing and projected noise levels associated with the Project at certain receptors, and found that in all instances, noise increases associated with the Project are anticipated to be less than 5dbA at all receptors. Increases of sound pressure of less than 5dB are anticipated to result in unnoticed to tolerable human reactions, pursuant to NYSDEC’s Assessing and Mitigating Noise Impacts, revised as of February 2, 2001.

Notwithstanding the foregoing, in an order to reduce future noise levels to the greatest extent reasonably possible, the Noise Evaluation recommended the following mitigation measures, which have been incorporated into Project Plans:

- The construction equipment used on-site will have to be inspected periodically to ensure that properly functioning muffler systems are used on all equipment.
- All equipment should not idle unnecessarily while on site.
- The HVAC equipment should also be positioned to face away from the adjacent residence as part of the final building design/HVAC equipment layout.
- Installation of a solid fence along the southeastern portion of the site on top of the retaining wall.  
Any onsite equipment should be equipped with alternate backup safety alarms such as “white noise” alarms, alternate radar, or infrared alarm systems.

Based on the foregoing, the Project will not have any significant adverse impacts with regard to noise.

### ***Light***

Project Site lighting will be provided for the parking lot areas surrounding the buildings and along the driveways into the Project Site. All lighting will be dark sky compliant. The exterior site lighting proposed for the Project utilizes night sky friendly fixtures which will be down directed and has been designed with fixture locations that do not present any light trespass onto neighboring properties.

The lighting will consist of energy efficient LED light fixtures. The lights will have edges that extend below the level of the fixture to reduce the potential for source glare and light spillage. The light fixtures will be mounted on poles and on the building.

Based on the foregoing, the Project will not have any significant adverse impacts with regard to light.

### ***Odor***

Regarding odor, the Project Site is not expected to produce appreciable odors. Refuse and recycling will be contained in an enclosed dumpster or compactor until pickup for disposal on a regular basis by a private carting company. In addition, the Project does not include any fixed-point source of air emissions that would cause any odor.

Based on the foregoing, the Project will not have any significant adverse impacts with regard to odor.

### **16. Impact on Human Health**

No significant impacts to human health are anticipated from the Project because all construction and operational activities will be undertaken in accordance with and in compliance with all pertinent environmental and land development regulations and related permit and approval procedures and requirements. As indicated above, water service to the facility will be provided from an existing water main line, owned and operated by the Town of Wawayanda Water Department and sanitary sewer service will be provided from an existing sewer main on, owned and operated by the Town of Wawayanda Sewer Department. As further indicated above, spill prevention and cleanup protocols are proposed to be in place.

Based on the foregoing, the Project will not have any significant adverse impacts on human health.

### **17. Consistency with Community Plans**

The Project is consistent with the Town of Wawayanda's Comprehensive Plan and complies with Wawayanda's Zoning Law that was enacted in furtherance of the Comprehensive Plan's goals.

Specifically, the Project is consistent with the requirements of the MC-1 Zoning District. The Town's Comprehensive Plan provides that "the MC mixed commercial zone is a district intended to provide a principal area for intensive nonresidential development such as office, retail, service businesses, manufacturing and industrial uses". The Comprehensive Plan further indicates that the zone is intended to be developed with commercial enterprises and specifically excludes residential uses and observes that recently attracted uses include small contractor yards, offices, retail, large warehousing and industrial uses. The Comprehensive Plan recommends that the Town continue to allow commercial/industrial uses on a minimum 2 acre lot size. The Project is consistent with the letter and intent of the MC-1 Zone as set forth in the Town of Wawayanda Zoning Law and Comprehensive plan, as it is a permitted use on a 11.66-acre lot, far greater than the minimum lot size requirement.

The Project will increase tax revenues to the Town and other taxing jurisdictions including the local school district (without generating any school age children).

For the foregoing reasons, the Project will not have a significant adverse impact on the Town of Wawayanda's community plans.

### **18. Consistency with Community Character**

The Project is a permitted use in accordance with the Town of Wawayanda Zoning Code and

located in the MC-1 zoning district. The Project is consistent with existing land uses in the vicinity of the Site, with the exception of certain pre-existing nonconforming residential uses which will be screened from the Project. The Site is bounded on the south by Interstate 84.

The Project is consistent with the District Intent set forth in Attachment 8 to the Town's Zoning Law, which provides that the MC District "is intended to provide the Town with a principal area for intensive nonresidential development such as office, retail, service businesses and manufacturing". Indeed, the Project is anticipated to be less intensive than a variety of other uses that are permitted by Site Plan approval or Special Use Permit, including contractor yards, motor vehicle sales and services, high traffic retail and service businesses, industrial uses, manufacturing uses and mining operations, including major mining operations.

In addition to the above, the Project is consistent with the surrounding community character based on the Project's design incorporating measures to limit noise and to protect adjoining properties, among other such mitigation measures discussed above and in the various reports.

Accordingly, the Project will not have a significant adverse impact on the community character of the Town of Wawayanda.